## TI Designs

# Isolated RS-485 to Wi-Fi® Bridge with 24-V AC Power



#### **TI Designs**

This TI Design uses Texas Instruments SimpleLink™ Wi-Fi CC3200 Internet-on-a-chip™ Wireless MCU module to create a data bridge between an RS-485 network and a Wi-Fi network. An ISO15 transceiver provides an isolated RS-485 interface with up to 2500 V of isolation. The LM5160 Fly-Buck™ power supply provides both isolated and non-isolated 3.3-V outputs for the two portions of the circuit. The design can be powered with AC or DC power up to 30 V<sub>RMS</sub> or 48-V peak.

A version of this design with a non-isolated RS-485 interface is presented in TIDA-00485.

#### **Design Resources**

TIDA-00486	Design Folder
CC3200MOD	Product Folder
LM5160	Product Folder
TLV71333P	Product Folder
<u>ISO15</u>	Product Folder
TPD1E10B06	Product Folder



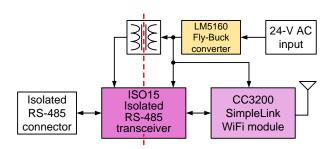
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#### **Design Features**

- Wide Input Voltage Range of 18-V to 30-V AC, 12-V to 48-V DC
- Fly-Buck Power Supply Delivers 3.3 V at 550 mA, Isolated 3.6 V at 50 mA
- Add Wi-Fi Connectivity to an RS-485 Network Quickly and Simply
- Galvanically Isolated RS-485 Interface to Improve System Safety and Reliability
- CC3200 Application Processor Provides Adaptability to Customer Communication Protocols

#### **Featured Applications**

- Building Automation
- Thermostats
- Compressors
- HVAC







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## 1 Key System Specifications

## **Table 1. Key System Specifications**

PARAMETER	SPECIFICATION	DETAILS		
	24 V nominal, AC or DC			
Input voltage	15-V to 48-V DC	See Section 7.1, Section 7.2		
	24-V AC + 25%			
Power connector	Screw terminals	See Section 4.1		
Interface	RS-485	See Section 4.4		
RS-485 connector	Screw terminals	See Section 4.4		



www.ti.com System Description

#### 2 System Description

The TIDA-00486 reference design is an Isolated RS-485 to Wi-Fi Bridge that is powered by 24-V AC nominally. The input voltage can range from 15-V to 48-V DC or  $18\text{-V}_{\text{RMS}}$  to  $30\text{-V}_{\text{RMS}}$  AC. It is intended for use with industrial and building automation systems that need to add Wi-Fi capability to an existing RS-485 network. The Isolated RS-485 to Wi-Fi Bridge can be used as a cable replacement or to add new functions to an existing network. This reference design has a half-wave rectifier, input voltage filter, and a dual 3.3-V output Fly-Buck regulator to supply the 3.3-V primary system voltage and the isolated voltage for the RS-485 interface. The isolated voltage is then regulated to 3.3 V by a low-dropout linear regulator (LDO). The system ground is suitable for use in AC systems that use a system or earth ground for one of the AC power connections.



Figure 1. Isolated RS-485 to Wi-Fi Bridge With 24-V AC Power



Block Diagram www.ti.com

## 3 Block Diagram

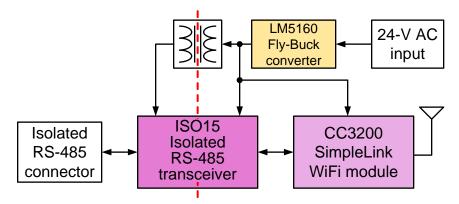


Figure 2. TIDA-00486 Block Diagram



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#### 3.1 Highlighted Products

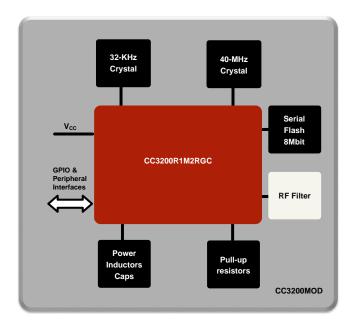
# 3.1.1 CC3200MOD SimpleLink Wi-Fi and Internet-of-Things Module Solution, a Single-Chip Wireless MCU

This device is the industry's first programmable FCC, IC, CE, and Wi-Fi Certified Wireless microcontroller (MCU) module with built-in Wi-Fi connectivity. Created for the Internet of Things (IoT), the SimpleLink CC3200MOD is a wireless MCU module that integrates an ARM® Cortex®-M4 MCU, allowing customers to develop an entire application with a single device. With on-chip Wi-Fi, Internet, and robust security protocols, no prior Wi-Fi experience is required for faster development. The CC3200MOD integrates all required system-level hardware components including clocks, SPI flash, RF switch, and passives into an LGA package for easy assembly and low-cost PCB design. The CC3200MOD is provided as a complete platform solution including software, sample applications, tools, user and programming guides, reference designs, and the TI E2E support community.

The applications MCU subsystem contains an industry-standard ARM Cortex-M4 core running at 80 MHz.

The device includes a wide variety of peripherals, including a fast parallel camera interface, I2S, SD/MMC, UART, SPI, I<sup>2</sup>C, and four-channel ADC. The CC3200 family includes flexible embedded RAM for code and data; ROM with external serial flash bootloader and peripheral drivers; and SPI flash for Wi-Fi network processor service packs, Wi-Fi certificates, and credentials.

The Wi-Fi network processor subsystem features a Wi-Fi Internet-on-a-chip and contains an additional dedicated ARM MCU that completely off-loads the applications MCU. This subsystem includes an 802.11 b/g/n radio, baseband, and MAC with a powerful crypto engine for fast, secure Internet connections with 256-bit encryption. The CC3200MOD supports station, access point, and Wi-Fi Direct™ modes. The device also supports WPA2 personal and enterprise security and WPS 2.0. The Wi-Fi Internet-on-a-chip includes embedded TCP/IP and TLS/SSL stacks, HTTP server, and multiple Internet protocols. The power-management subsystem includes integrated DC-DC converters supporting a wide range of supply voltages. This subsystem enables low-power consumption modes, such as the hibernate with RTC mode requiring less than 7 µA of current.



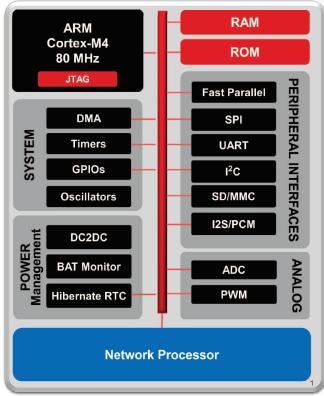


Figure 3. CC3200MOD Functional Block Diagram

Figure 4. CC3200 Hardware Overview



Block Diagram www.ti.com

#### 3.1.2 LM5160 Wide Input 65-V, 1.5-A Synchronous Step-Down DC-DC Converter

The LM5160 family is a 65-V, 1.5-A synchronous step-down converter with integrated high-side and step-down converter with integrated high-side and scheme requires no loop compensation and supports high step-down ratios with fast transient response. An internal feedback amplifier maintains ±1% output voltage regulation over the entire operating temperature range. The on-time varies inversely with input voltage resulting in nearly constant switching frequency. Peak and valley current limit circuits protect against overload conditions. The undervoltage lockout (EN/UVLO) circuit provides independently adjustable input undervoltage threshold and hysteresis. The LM5160 is programmed through the FPWM pin to operate in programmed through the FPWM pin to operate in full load or to automatically switch to discontinuous conduction mode (DCM) at light load for higher efficiency. Forced CCM operation supports multiple output and isolated Fly-Buck applications using a coupled inductor.

The LM5160A shares the same features and pin configuration as the LM5160. An external bias supply can be connected to the VCC pin of the LM5160A in either Buck or Fly-Buck applications. This additional capability can improve efficiency at high input voltages.

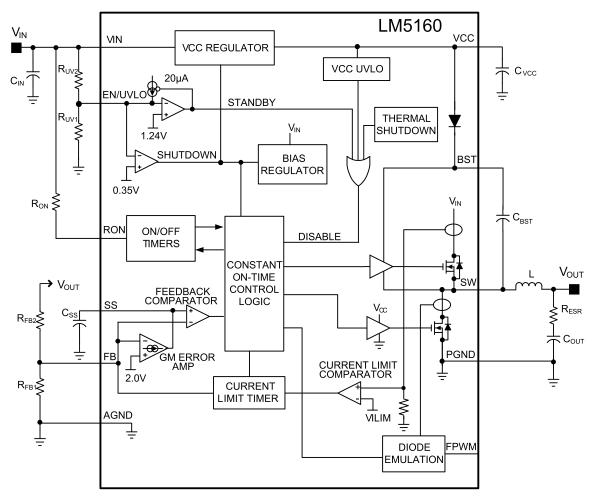


Figure 5. LM5160 Functional Block Diagram



www.ti.com Block Diagram

#### 3.1.3 TLV71333P 150-mA, Low-Dropout Regulator with Foldback Current Limit for Portable Devices

The TLV713 series of low-dropout (LDO) linear regulators are low quiescent current LDOs with excellent line and load transient performance and are designed for power-sensitive applications. These devices provide a typical accuracy of 1%.

The TLV713 series of devices is designed to be stable without an output capacitor. The removal of the output capacitor allows for a very small solution size. However, the TLV713 series is also stable with any output capacitor if an output capacitor is used.

The TLV713 also provides inrush current control during device power up and enabling. The TLV713 limits the input current to the defined current limit to avoid large currents from flowing from the input power source. This functionality is especially important in battery-operated devices.

The TLV713 series is available in standard DQN and DBV packages. The TLV713P provides an active pulldown circuit to quickly discharge output loads.

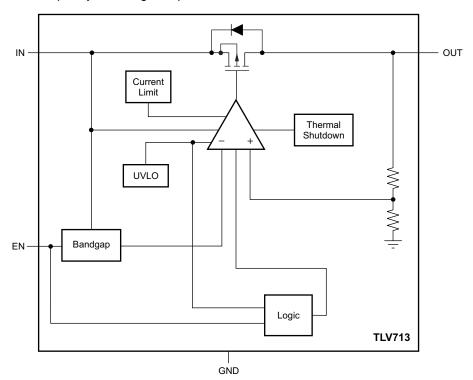


Figure 6. TLV71333P Functional Block Diagram



Block Diagram www.ti.com

#### 3.1.4 ISO15 Isolated 3.3-V Half-Duplex RS-485 Transceiver

The ISO15 is an isolated half-duplex differential line transceiver. The ISO15M and has an extended ambient temperature rating of –55°C to 125°C while the ISO15 is specified over –40°C to 85°C.

This device is ideal for long transmission lines because the ground loop is broken to allow for a much larger common-mode voltage range. The symmetrical barrier of the device is tested to provide isolation of  $4000~V_{PK}$  per VDE and  $2500~V_{RMS}$  per UL and CSA between the bus-line transceiver and the logic-level interface.

Any cabled I/O can be subjected to electrical noise transients from various sources. These noise transients can cause damage to the transceiver and nearby sensitive circuitry if they are of sufficient magnitude and duration. These isolated devices can significantly increase protection and reduce the risk of damage to expensive control circuits.

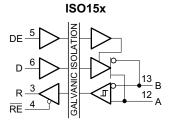


Figure 7. ISO15 Simplified Schematic Diagram

#### 3.1.5 TPD1E10B06 Single Channel ESD in 0402 Package With 10-pF Capacitance and 6-V Breakdown

The TPD1E10B06 device is a single-channel electrostatic discharge (ESD) transient voltage suppression (TVS) diode in a small 0402 package. This TVS protection product offers ±30-kV contact ESD, ±30-kV IEC air-gap protection, and has an ESD clamp circuit with a back-to-back TVS diode for bipolar or bidirectional signal support. The 12-pF line capacitance of this ESD protection diode is suitable for a wide range of applications supporting data rates up to 400 Mbps. The 0402 package is an industry standard and is convenient for component placement in space-saving applications.

Typical applications of this ESD protection product are circuit protection for audio lines (microphone, earphone, and speaker phone), SD interfacing, keypad or other buttons, VBUS pin and ID pin of USB ports, and general-purpose I/O ports. This ESD clamp is good for the protection of the end equipment like ebooks, tablets, remote controllers, wearables, set-top boxes, and electronic point of sale equipment.

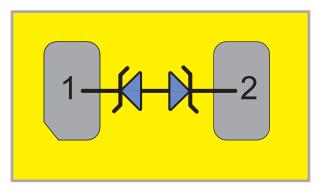


Figure 8. TPD1E10B06 Device Configuration



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#### 4 System Design Theory

The TIDA-00486 reference design has two primary circuit functions: converting a 24-V AC or DC input into two 3.3-V DC supplies, one galvanically isolated and one non-isolated, and converting RS-485 traffic to Wi-Fi traffic.

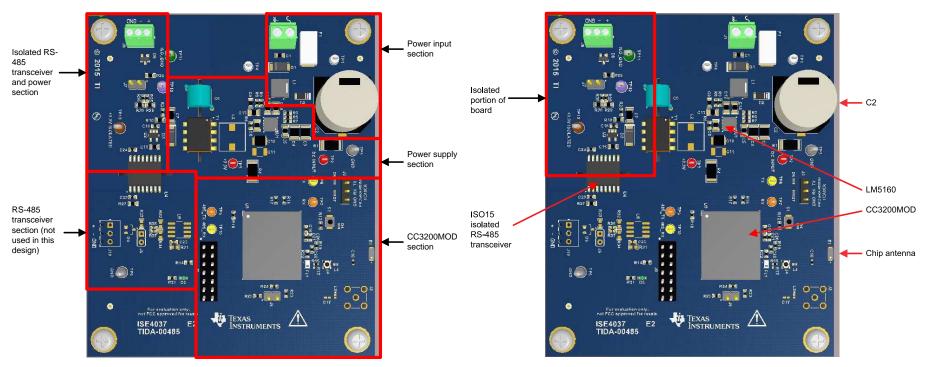


Figure 9. RS-485 to Wi-Fi Bridge Board Partitioning

Figure 10. RS-485 to Wi-Fi Bridge Board Features



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#### 4.1 Power Input

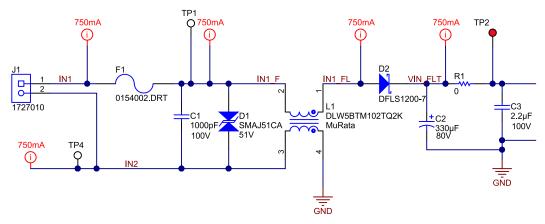


Figure 11. Power Input Schematic

D2 is a rectifier to convert the AC input to DC for use by the step-down regulator. D1 is a transient absorber with a 51-V break-down voltage, which limits the input voltage range to 51 V. C1 and L1 form an input filter to reduce conducted RF both into and out of the system. L1 is a common-mode choke. C1 is included to further reduce high frequency signal content. C2 is a 330- $\mu$ F, 80-V aluminum electrolytic capacitor provided to maintain the DC voltage between the AC voltage peaks. The value of the capacitor was determined by estimating the voltage input to the regulator when the input voltage is at its minimum or 18 V<sub>RMS</sub> (peak voltage = 25.45 V) while the load is the estimated maximum of 600 mA at 3.3 V with an estimated power supply efficiency of 60%. Figure 12 shows the rectified input voltage as well as the estimated voltage on C2 when the load is at its maximum.

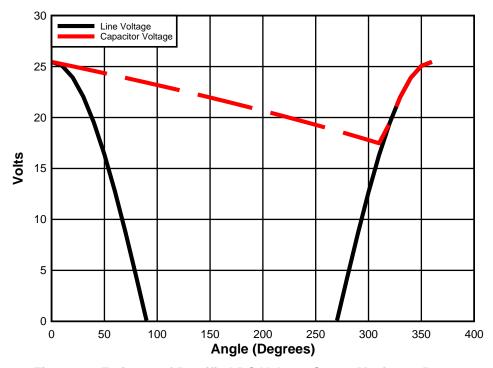


Figure 12. Estimate of Rectified DC Voltage Sag at Maximum Power

This value of C2 insures that the input voltage to the LM5160 power supply is above 15 V even when the input voltage is at its lowest rated value. The graph above was calculated for a 60-Hz power input.



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#### 4.2 3.3-V Power Supply

The 3.3-V power supply is provided by the LM5160. The LM5160 was chosen for this design due to its flexibility. The design of the Isolated RS-485 to Wi-Fi Bridge is actually two designs, one with a galvanically isolated RS-485 interface and one without isolation. TI Design TIDA-00485 is the non-isolated version and TIDA-00486 is the isolated version. The power supply design is easily convertible between the two designs by simply swapping L2 for T1.

The CC3200MOD has its maximum current load of 450 mA when the input voltage is 3.3 V. This occurs during CC3200 calibration at power on. The maximum load during data transmission is typically less than 300 mA. To insure there is enough power supply capacity for the RS-485 transceiver and the application processor, the design load current was chosen to be 600 mA.

The design procedure for the LM5160 uses the LM5160 Fly-Buck Quick Start Calculator spreadsheet linked on the LM5160 product page. There are spreadsheets to design either a buck converter or a Fly-Buck converter. Both were used for the design of this circuit board. This document will only present the LM5160 Fly-Buck version of the design.

Design parameters used in the LM5160 Fly-Buck design spreadsheet are as shown in Table 2.

Table 2. Power Supply Design Spreadsheet Input Parameters

Desired seize en control trolle se	2.2	\/
Desired primary output voltage	3.3	V
Desired secondary output voltage	3.7	V
D, isolated rectifier diode V <sub>F</sub>	0.3	V
Selected turns ratio N	0.83	
Minimum input voltage	14	V
Nominal input voltage	24	V
Maximum input voltage	45	V
Secondary load current	0.05	Α
Primary load current	0.55	Α
Desired Vin, rising threshold	10	V
Desired Vin hysteresis	2.5	V
Select the value of RUV2	127	kΩ
Select the value of RUV1	18.2	kΩ
Select the value of RFB1	3	kΩ
Select the value of RFB2	1.96	kΩ
Desired nominal switching frequency	300	kHz
Select the value of RON2	110	kΩ
Select the value for L	47	μΗ
Desired soft start time	15	ms
Select the value for CSS	0.082	μF



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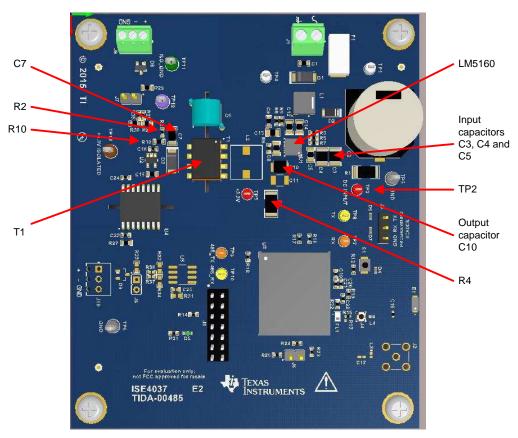


Figure 13. Power Supply Major Components



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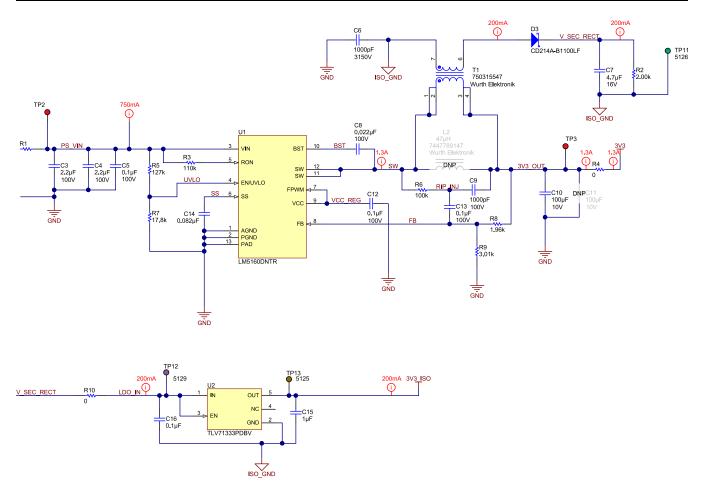


Figure 14. Power Supply Schematic

The output ripple configuration was chosen as type 3 for this design since type 3 is required for a Fly-Buck regulator. The spreadsheet gives values for the various capacitors around the LM5160 such as the boost capacitor C8; the VCC capacitor C12; the soft-start capacitor C14; the values of the ripple components R6, C9, and C13; the input capacitors C3 and C4; and output capacitors C10 and C11. C10 has been set to 100  $\mu$ F to comply with the design requirements for the CC3200MOD, which asks for two 100- $\mu$ F capacitors. C11 is left unpopulated in case the second 100  $\mu$ F is needed. R1 and R4 are provided to allow easy current measurements for power supply efficiency measurements. T1 is a custom-wound transformer provided by Würth Electronik for this design, part number 750315547. The primary minimum inductance is 42  $\mu$ H with a saturation current of 1.1 A. The turns ratio is 1.2:1, which is the inverse of the 0.83 used in the power supply design spreadsheet. L2 is grayed out in the schematic since it is not populated in this design.



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In order to maintain the galvanic isolation for the RS-485 interface, the power for the transceiver must be isolated as well so that the ground potential can be matched safely to the RS-485 network. The isolated power is provided by a secondary on T1. This voltage needs to be high enough to insure that the voltage is above the dropout voltage of the LDO. As shown in Table 2, the design target for the rectified output was set to 3.7 V. Diode D3 is the rectifier for the secondary, and C7 provides filtering. Resistor R2 forms a resistive load to insure that the output of the isolated supply remains low. If it were not there, the filter capacitor C7 would charge up to the peak input voltage times the turns ratio, or about 51 V. The LDO is provided to insure the supply voltage for the RS-485 transceiver remains within the operating voltage range of 3.15 V to 3.6 V of the ISO15 transceiver. A TI TLV71333P LDO was chosen for this application since the total load is estimated to be no more than 50 mA and the dropout voltage is less than 75 mV for a 3.3-V output. C16 provides the input bypass capacitor for the LDO and C15 is the output capacitor. R10 is provided in order to make current measurements in the isolated power supply. C6 is a 3150-V capacitor that provides a path for high-frequency noise that is coupled between the two ground domains to be shorted back to its source while insuring that no DC or low frequency AC current flows between the grounds.



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#### 4.3 CC3200MOD

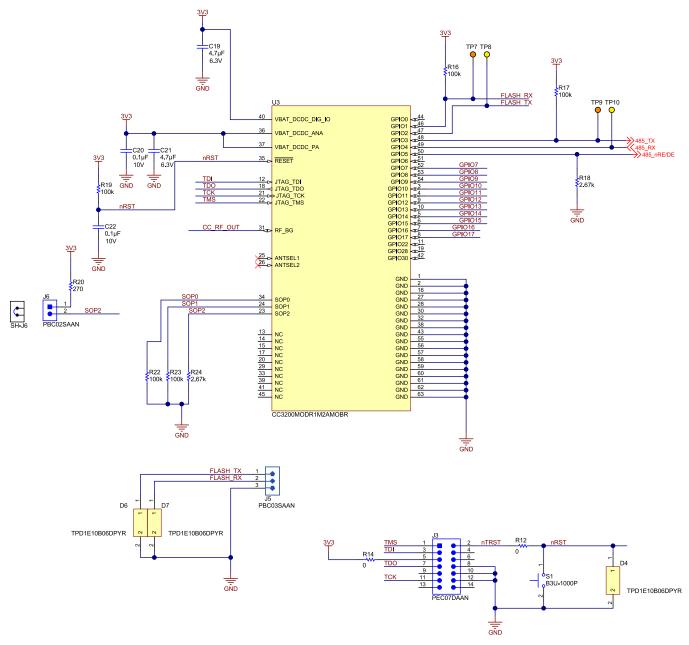


Figure 15. CC3200MOD Schematic

The CC3200MOD is an easy-to-use module that contains the serial memory and crystals required for a CC3200-based system. The only external components are the necessary bypass capacitors and pull-down resistors. One UART interface is used for system programming and another is used for RS-485 communication.



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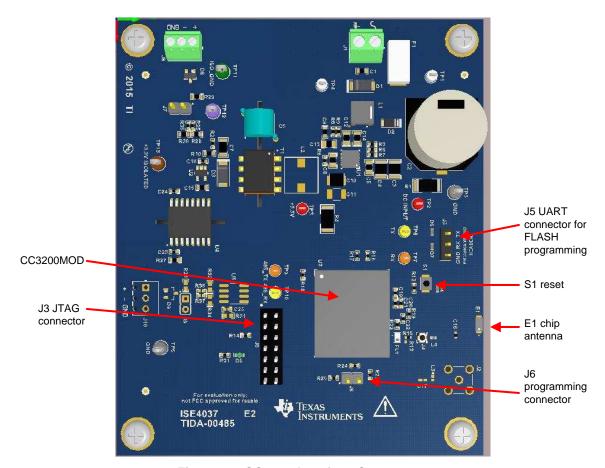


Figure 16. CC3200 Interface Connectors

There are several connectors provided for test and expansion. J6 is provided for FLASH programming. J6 is shorted for programming operations and is left open during normal operation. J3 is a JTAG connector for system debugging. It follows the TI 14-pin JTAG format. Connector J5 is a three-pin header that connects to the UART0 pins of the CC3200MOD to allow FLASH reprogramming with the CCS UNIFLASH tool and a USB-to-UART converter. RESET button S1 provides a manual reset capability. Diodes D4 through D7 provide ESD protection for the UART connection and the reset.



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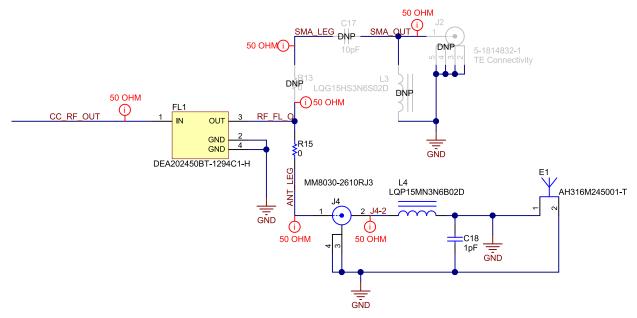


Figure 17. Antenna Section Schematic

The RF antenna output section has two antenna options. The PCB is populated with the parts for the onboard chip antenna E1. Connector J4 is an RF test connector. J2 is an SMA connector for use with an external antenna. Components associated with the J2 path are not populated. To use the SMA connector, R15 should be removed and components R13, C17 and L3 installed. Actual values for C17 and L3 should be chosen based on the signal matching requirements of the antenna to be connected to J2.

#### 4.4 RS-485 Interface

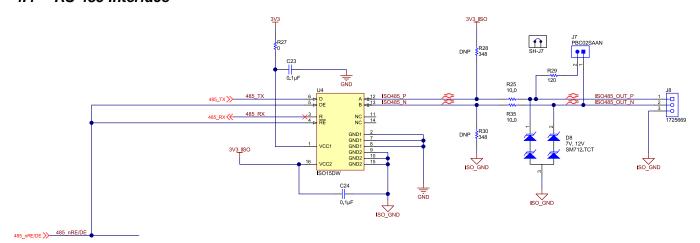


Figure 18. Isolated RS-485 Transceiver

The RS-485 transceiver is a TI ISO15. This part was chosen because both the digital interface and the isolated RS-485 interface operate with 3.3-V power supplies and its RS-485 connections are internally isolated from the digital interface. J8 is a screw-terminal connector with the RS-485 + and – connections and system ground. D8, R25, and R35 provide additional transient protection for the transceiver. J7 is a jumper that can be used to disconnect the 120- $\Omega$  termination resistor R29 for use in systems that already have network termination resistors. R28 and R30 provide voltage references for the + and – connections.



#### 5 Getting Started: Firmware

In order for the Isolated RS-485 to Wi-Fi Bridge reference design to work CC3200MOD software must be able to control the RS-485 driver enable control line, receive data from the RS-485 transceiver, and transmit that data using a socket to another end node connected in the same network. The software must also be able to receive data from the socket and write the data to the RS-485 transceiver. For this application, the serial-Wi-Fi application from CC3200 SDK was modified. Note that SDK version 1.1.0 for CC3200 silicon revision R1 was used as the code base.

#### 5.1 Application Overview

The firmware relies heavily on the serial-Wi-Fi application, which showcases the capability of the CC3200MOD to provide easy, self-contained terminal access over a UART interface connected to a RS-485 transceiver. The application provides a driver-less solution and allows operation based on ASCII character set interpretation. Leveraging the complete network stack integration of the CC3200, it allows secure, robust end-to-end communication.

#### 5.2 Application Features

The following features are provided in the application:

- Support to connect to an Enterprise or Personal network using OPEN, WEP, or WPA authentication.
- Automatic network discovery of an available peer using mDNS.
- Once a network is configured, the CC3200MOD can auto connect to the AP on every boot.
- Ability to use optional secure sockets.

#### 5.3 Operating Modes

The application operates in three modes:

- 1. Terminal/Interpreter mode
  - Interpreter mode behaves as pure point-to-point cable replacement. This is the most common use in which a serial cable formerly used to carry information is replaced by SimpleLink devices on both ends of the line. This mode can also be used to extend an existing line farther without additional serial communication cable being installed.
- 2. Local control mode
  - This allows issuing commands to the locally connected device. These commands encompass a close set of options to control the SimpleLink device. The mode is entered using a predefined escape sequence (//<).
- 3. Remote control mode
  - This allows issuing commands to the remotely connected device. These commands encompass the same set of options to control the remote SimpleLink as the local device. The mode is entered using a predefined escape sequence (//>).



#### 5.4 **Application Modifications**

In order for the serial-Wi-Fi application to run on the Isolated RS-485 to Wi-Fi Bridge reference design, the following sections describe the modifications required.

#### 5.4.1 **Pinmux**

The following pin configurations are used in the Isolated RS-485 to Wi-Fi Bridge reference design. The files Pinmux.c and pinmux.h from the original version of Serial-Wi-Fi need to be updated to agree with Table 3.

PIN **FUNCTION DESCRIPTION** UART0\_TX (mode 3) **UART** flashing 55 57 UART0\_RX (mode 3) **UART** flashing 58 UART1\_TX (mode 6) RS-485 UART1\_RX (mode 6) 59 RS-485 GPIO (mode 0) RS-485 driver enable control line 60

Table 3. UART Pin Assignments for the CC3200

Note that the pin numbers correspond to the raw CC3200 part and not the pins assigned to these functions on the CC3200MOD.

#### **Application UART Peripheral** 5.4.2

The serial-Wi-Fi application uses UART0 peripheral by default. Since the RS-485 transceiver is connected to UART1, the application needs to be modified to use UART1. In serial wifi.h and uart if.h, change CONSOLE from UARTA0 to UARTA1.

#### 5.4.3 **Secure Sockets**

The serial-Wi-Fi application can be configured for secure or non-secure sockets. For non-secure sockets, comment out "#define SECURE SOCKETS" inside serial wifi.h.

#### 5.4.4 **RS-485 Driver Enable Control Line**

By default, the RS-485 driver enable control line is low, which means that the RS-485 receiver is enabled and the driver is disabled. To send data onto the RS-485 network, the driver needs to be enabled (by setting the driver enable control line high) prior to transmitting UART packets.

The following sequence needs to occur when a UART transmit API is called:

- 1. Set RS-485 driver enable control line high to enable driver GPIO\_IF\_Set(RS485\_CNTRL, ControlPort, ControlPin, 1);
- 2. Transmit the UART data MAP\_UARTCharPut(CONSOLE, c);
- 3. Wait until all UART data has been transmitted while(MAP\_UARTBusy(CONSOLE));
- 4. Set RS-485 driver enable control line low to disable driver and enable receiver GPIO\_IF\_Set(RS485\_CNTRL, ControlPort, ControlPin, 0);

#### **Disable Receiver Echo** 5.4.5

By default, the serial-Wi-Fi application echoes all data that is received on the UART peripheral. Due to the nature of the RS-485 bus, it is recommended to disable the echo feature to eliminate the possibility of bus contention when CC3200 is echoing the received data and the host is transmitting the next data.

The echo functionality occurs in the GETChar function in uart\_config.c. Remove all MAP\_UARTCharPut API calls inside the function.



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#### 6 Getting Started

The following assumes that the user has installed the CC3200 SDK, Code Composer Studio (CCS), and UniFlash to program the FLASH device on the TIDA-00485 PCB. It is recommended that the user be familiar with CC3200 Project 0 from the CC3200 wiki site. This will insure that Code Composer is set up correctly, the CCS UniFlash utility is installed, and the drivers (simplelink, ti\_rtos\_config, driverlib, oslib) have been built. The drivers must be built before the procedure in Section 6.2 can be run. If application debugging capability is needed, a TI TMDSEMU100V2U-14T JTAG Emulator can be connected to J3 on the PCB.

#### 6.1 Hardware Setup

In order to test the Isolated RS-485 to Wi-Fi Bridge reference design, two systems running the modified serial-Wi-Fi application must be used. Each board must have a terminal program such as Tera Term running on a host computer. Use two host computers with the terminal program running on each if two computers are available, one for each RS-485 to Wi-Fi node. However, a single host running two terminal windows can be used.

To power the board, connect a power supply to the power connector J1. The power supply can be any AC supply between 18  $V_{RMS}$  and 30  $V_{RMS}$  or a DC supply between 15 and 48 V. The power supply should have at least a 1-A capacity.

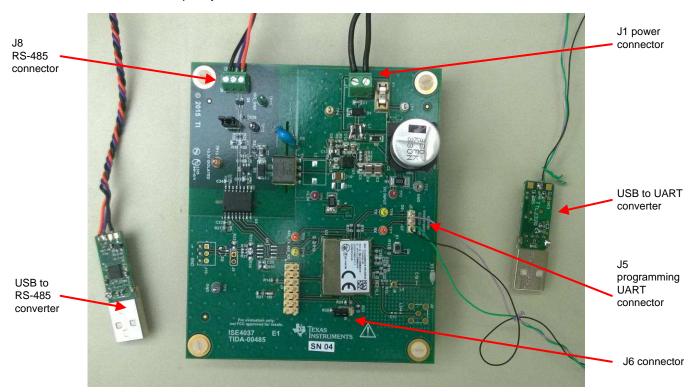


Figure 19. Power, UART, and RS-485 Connections

To monitor the RS-485 traffic, connect the J8 signals to the appropriate signals on a USB-to-RS-485 adapter. Connect the USB-to-RS-485 USB connector to the host. The dedicated UART J5 connection is the programming connection for the Isolated RS-485 to Wi-Fi Bridge PCB. Connect these signals to a USB-to-UART adapter and connect it to the host as well. Make sure that the jumper is installed on J6 before applying power to the PCB.



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#### 6.2 Software Setup

For testing purposes, the modified serial-Wi-Fi application will be used. For simplicity, the application will use non-secure sockets for the communication. The following steps describe the procedure to configure the application for non-secure sockets, build the binary, flash onto the Isolated RS-485 to Wi-Fi Bridge PCB, configure, and test.

For more information about the serial-Wi-Fi application and the use of secure sockets for communication, see the CC32xx Serial Wi-Fi documentation that is provided in the CC3200 SDK.

#### 6.2.1 Configure the Application

- 1. Open CCS and import serial wifi example application from CC3200 SDK.
- 2. Configure the application as described in Section 5.4.
- 3. Build the project:
  - (a) Go to Project → Build Project.
  - (b) If using default settings, this should generate the file, serial\_wifi.bin.
- 4. Flash binary:
  - (a) Enable programming mode (pulling SOP2 high) by placing jumper on J6.
  - (b) Connect USB-to-UART converter and adapter cable from the Isolated RS-485 to Wi-Fi Bridge PCB to host computer.
  - (c) Power on Isolated RS-485 to Wi-Fi Bridge PCB.
  - (d) Look in Device Manager and note the Isolated RS-485 to Wi-Fi Bridge PCB's COM port.
  - (e) Open CCS UniFlash program.
  - (f) Click File → New Configuration:
    - Connection: CC3x Serial (UART) Interface
    - Board or Device: SimpleLink Wi-Fi CC3100/CC3200
  - (g) Change COM Port to match the COM port found from Device Manager.
  - (h) If first time booting the hardware, perform a Service Pack Update:
    - (i) Click "Service Pack Update".
    - (ii) Find the CC3200 Service Pack binary.
  - (i) Flash the serial-Wi-Fi application:
    - (i) Click on "/sys/mcuimg.bin".
    - (ii) Change URL to point to serial wifi.bin file generated from Step 3.
    - (iii) Make sure only the Update box is checked.
    - (iv) Go to Operation → Program.
  - (j) Power off Isolated RS-485 to Wi-Fi Bridge PCB.
  - (k) Change back to run mode (pulling SOP2 low) by removing jumper from J6.
- 5. Repeat Steps 1 through 4 on the second Isolated RS-485 to Wi-Fi Bridge PCB.



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#### 6.2.2 Run the Application

1. Open a terminal with the following settings:

Port: COM port from Device Manager

Baud Rate: 115200

Data: 8 bitParity: NoneStop: 1 bit

Flow control: None

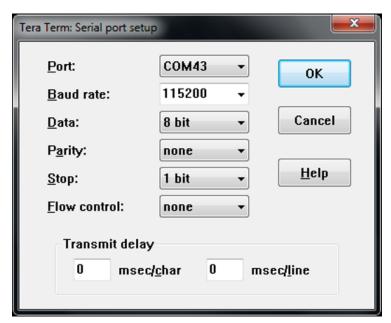


Figure 20. Tera Term Port Setup

- 2. Enable local echo mode.
  - If using Tera Term, go to Setup → Terminal and check "Local echo".

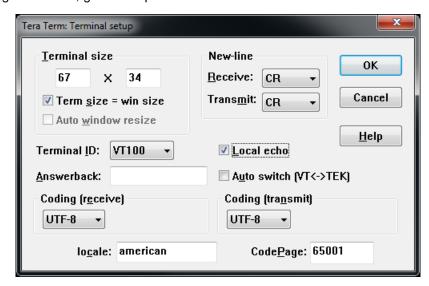


Figure 21. Setting Tera Term for Local Echo



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- 3. Start the serial-Wi-Fi application:
  - (a) Power on the Isolated RS-485 to Wi-Fi Bridge PCB.
  - (b) The terminal should show "CC3200 SERIAL WiFi Application".
  - (c) If not, go back to the Step 4: Flash binary from Section 6.2.1 and try flashing application again.
- 4. Connect to Access Point (AP):
  - (a) Upon reset, the device will connect to the stored AP using the AUTO connect policy. If device connects to AP, go to <a href="Step 5">Step 5</a>: Configure mDNS. If the device does not connect to an AP in six seconds, the application will prompt the user to connect to a known AP using the local control mode.

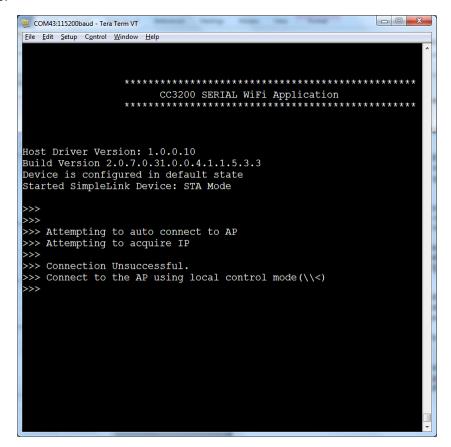


Figure 22. Terminal Information With No AP

(b) Enter local control mode (\\<).



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(c) Use the following command to connect to an AP:

Format: wlan\_connect [SSID] [Type] [Sec] [User] [Key]

SSID: Name of AP Type: 0-Personal, 1-ENT Sec: 0-OPEN, 1-WEP, 2-WPA

User: Username, only needed if using ENT

Key: Password for WEP and WPA

Example:

"TI\_AP" SSID with no security wlan\_connect TI\_AP 0 0

"TI\_AP" SSID with WPA security and password "TI\_password" wlan\_connect TI\_AP 0 2 TI\_password

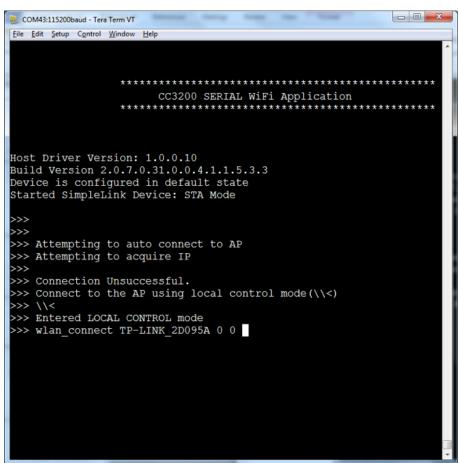


Figure 23. Setting Up the Access Point SSID



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(d) Once completed, the application will show that it was able to connect to the AP and an IP address has been acquired.

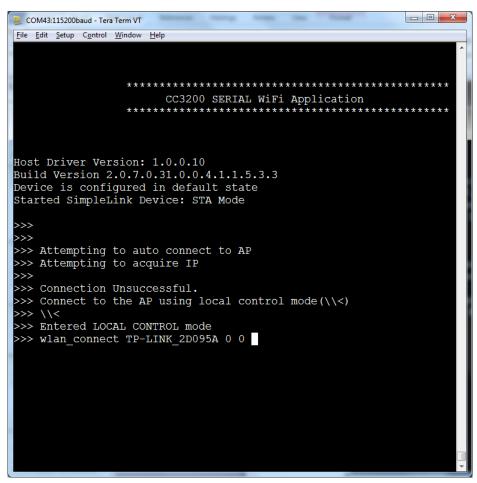


Figure 24. Terminal Window Screenshot Showing Isolated RS-485 to Wi-Fi Bridge Console

- 5. Configure mDNS:
  - (a) This step only needs to be done the first time after performing a serial erase.
  - (b) One node must be configured as mDNS server. Use local control mode to program.
  - (c) Enter local control mode (\\<).
  - (d) Configure for client or server: mDNS 0 <0-server, 1-client>



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6. Repeat Steps 1 through 5 for the second Isolated RS-485 to Wi-Fi Bridge PCB.

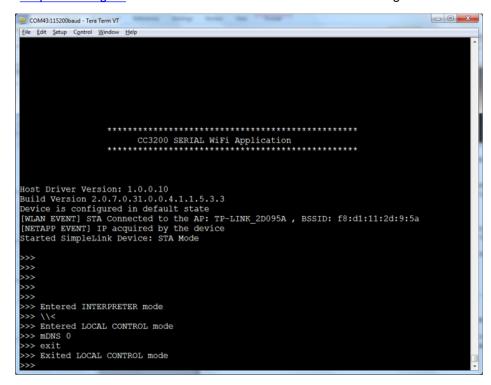


Figure 25. Setting DNS as Server

Devices should now be in interpreter mode. If a device is still in control mode, type "exit" to resume interpreter mode.

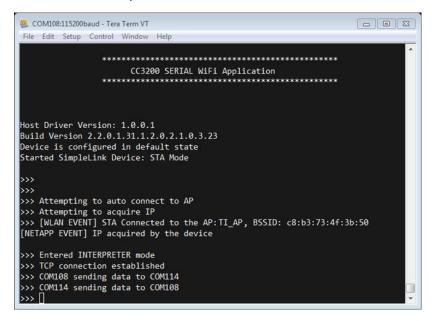


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#### 6.3 Communication Test

Note that the communication test can use any CC3200 hardware running the serial-Wi-Fi application. This has been tested with combinations of CC3200 LaunchPads, TIDA-0375 UART to Wi-Fi Bridge hardware, TIDA-00485 RS-485 to Wi-Fi Bridge hardware, and TIDA-00486 Isolated RS-485 to Wi-Fi Bridge hardware.

- 1. Power off both nodes.
- 2. Power on the client node first, followed by the server node. This insures that the TCP connection gets made.
- 3. Both nodes should connect to the same AP and acquire an IP address.
- 4. Verify that "TCP connection established" appears on both nodes.
- 5. Type on the server terminal and press <Enter> to see the same characters on the client.
- 6. Type on the client terminal and press <Enter> to see the same characters on the server.



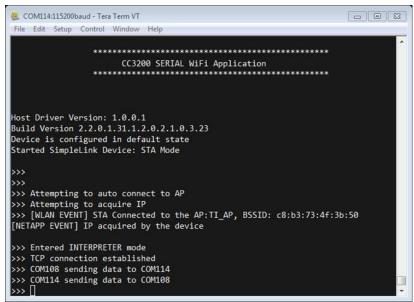


Figure 26. Terminal Window Screenshots Showing Both Consoles



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## 7 Testing

## 7.1 Power Supply DC Testing

### 7.1.1 Efficiency Testing With Static Loads

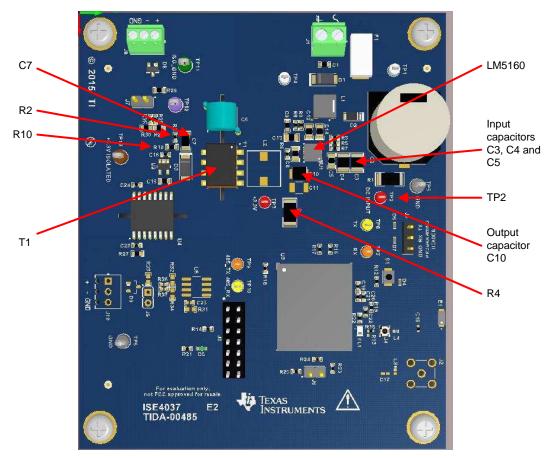


Figure 27. Power Supply Major Components



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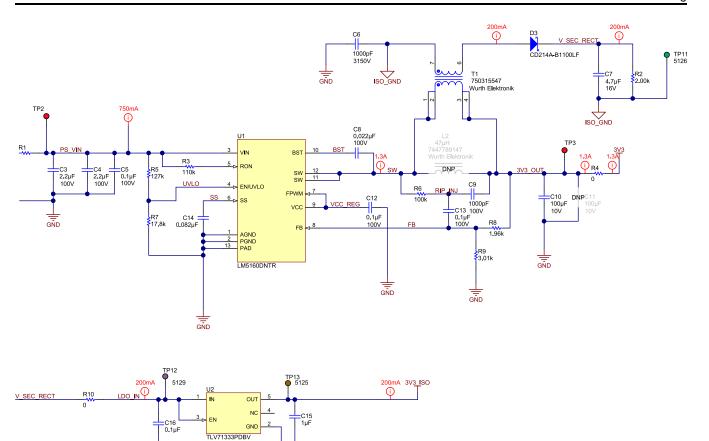


Figure 28. Power Supply Schematic

ISO\_GND

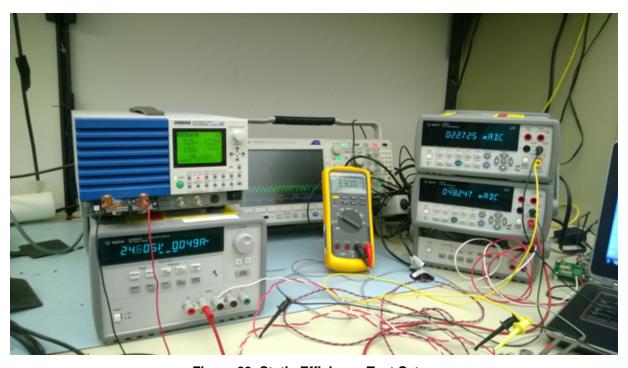


Figure 29. Static Efficiency Test Setup



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The purpose of this test is to determine the power supply operating efficiency without the variations imposed by the varying nature of the load that the CC3200 presents. For this test, the test equipment used included an Agilent 34410A DMM, a Fluke model 87-V DMM, an Agilent E3634A Power Supply, and a Kikusui PLZ334WL active load.

In order to test the power supply efficiency, DC input voltage was used to simplify testing. The input power was connected to power connector J1. Input current was measured with a DMM connected in series with the input power. Input voltage for the regulator was measured at TP2 with a DMM to insure the input rectifier and filter losses were not added to the efficiency calculation. Voltages throughout the input voltage range were applied. To measure the output power, resistors R4 and R10 were removed so that the output power for the two supply sections was determined only by the static loads. An active load was connected to the non-isolated, or primary, 3.3 V supply at TP3. The output voltage was measured across C10. The output current for the non-isolated supply was the active load setting. The isolated, or secondary, 3.6-V supply was tested with resistive loads connected in parallel with R2. The secondary output voltage was measured across C7. The secondary output current was calculated by measuring the current into the added load with a DMM and adding this current to the current calculated by dividing the output voltage by the value of R2. R2 was 1,998  $\Omega$  on this board. Load resistors were selected to get secondary currents of approximately 25 mA and 50 mA. Table 4 shows the combinations of loads were used to test the power supply:

Table 4. Loads for the Static DC Efficiency Test

TEST NUMBER	POWER SUPPLY LOAD					
1E31 NOWIBER	NON-ISOLATED 3.3 V (mA)	ISOLATED 3.6 V (mA)				
Test 1	0	25				
Test 2	0	50				
Test 3	250	25				
Test 4	250	50				
Test 5	550	50				



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Test 5 corresponds to the maximum design target for this power supply. The resulting efficiencies are in Table 5:

### **Table 5. Static Power Supply Efficiency**

TEST NUMBER	INPUT VOLTAGE (V)	INPUT CURRENT (mA)	INPUT POWER (mW)	PRIMARY OUTPUT VOLTAGE (V)	PRIMARY OUTPUT CURRENT (mA)	PRIMARY OUTPUT POWER (mW)	SECONDARY OUTPUT VOLTAGE (V)	SECONDARY OUTPUT CURRENT (mA)	SECONDARY OUTPUT POWER (mW)	TOTAL OUTPUT POWER (mW)	EFFICIENCY
	12.07	14.59	176.10	3.300	0	0	3.555	24.19	85.995	85.995	48.83%
	18.08	12.37	223.65	3.301	0	0	3.567	24.25	86.500	86.500	38.68%
	24.08	11.46	275.96	3.301	0	0	3.576	24.33	87.004	87.004	31.53%
Test 1	30.08	11.07	332.99	3.301	0	0	3.584	24.37	87.342	87.342	26.23%
	36.09	10.93	394.46	3.301	0	0	3.591	24.42	87.692	87.692	22.23%
	40.09	10.94	438.58	3.301	0	0	3.596	24.47	87.994	87.994	20.06%
	48.09	11.11	534.28	3.302	0	0	3.605	24.51	88.359	88.359	16.54%
	12.04	22.17	266.93	3.301	0	0	3.497	47.44	165.898	165.898	62.15%
	18.06	17.47	315.51	3.301	0	0	3.514	47.67	167.512	167.512	53.09%
	24.08	15.30	368.42	3.301	0	0	3.523	47.79	168.364	168.364	45.70%
Test 2	30.07	14.16	425.79	3.301	0	0	3.531	47.91	169.170	169.170	39.73%
	36.07	13.51	487.31	3.301	0	0	3.539	48.00	169.872	169.872	34.86%
	40.08	13.27	531.86	3.301	0	0	3.543	48.06	170.277	170.277	32.02%
	48.08	13.05	627.44	3.302	0	0	3.551	48.16	171.016	171.016	27.26%
	11.87	88.90	1055.24	3.301	250	825.25	3.633	24.71	89.771	915.021	86.71%
	17.93	62.11	1113.63	3.301	250	825.25	3.636	24.73	89.918	915.168	82.18%
	23.96	48.89	1171.40	3.301	250	825.25	3.633	24.70	89.735	914.985	78.11%
Test 3	29.98	41.39	1240.87	3.301	250	825.25	3.641	24.76	90.151	915.401	73.77%
	36.00	36.45	1312.20	3.301	250	825.25	3.648	24.81	90.507	915.757	69.79%
	40.01	34.01	1360.74	3.301	250	825.25	3.646	24.81	90.457	915.707	67.29%
	48.02	30.42	1460.77	3.302	250	825.50	3.644	24.78	90.298	915.798	62.69%
	11.86	97.07	1151.25	3.301	250	825.25	3.577	48.52	173.556	998.806	86.76%
	17.91	67.59	1210.54	3.301	250	825.25	3.588	48.67	174.628	999.878	82.60%
	23.95	53.06	1270.79	3.301	250	825.25	3.588	48.67	174.628	999.878	78.68%
Test 4	29.97	44.64	1337.86	3.301	250	825.25	3.594	48.75	175.208	1000.458	74.78%
	35.99	39.22	1411.53	3.301	250	825.25	3.602	48.86	175.994	1001.244	70.93%
	40.00	36.50	1460.00	3.301	250	825.25	3.602	48.86	175.994	1001.244	68.58%
	48.02	32.52	1561.61	3.302	250	825.50	3.601	48.84	175.873	1001.373	64.12%
	11.74	191.62	2249.62	3.300	550	1815.00	3.660	49.65	181.719	1996.719	88.76%
	17.81	130.30	2320.64	3.301	550	1815.55	3.679	49.91	183.619	1999.169	86.15%
	23.85	100.61	2399.55	3.301	550	1815.55	3.687	50.02	184.424	1999.974	83.35%
Test 5	29.88	83.01	2480.34	3.301	550	1815.55	3.687	50.01	184.387	1999.937	80.63%
	35.91	71.58	2570.44	3.301	550	1815.55	3.686	50.00	184.300	1999.850	77.80%
	39.92	66.08	2637.91	3.301	550	1815.55	3.685	49.99	184.213	1999.763	75.81%
	47.95	57.83	2772.95	3.301	550	1815.55	3.687	50.02	184.424	1999.974	72.12%



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In Table 5, the efficiency is calculated by taking the sum of the output power calculations and dividing this by the input power calculation:

Efficiency = 
$$\left[ \frac{\left( V_{PRIMARY} \times I_{PRIMARY} \right) + \left( V_{SECONARY} \times I_{SECONDARY} \right)}{\left( V_{IN} \times I_{IN} \right)} \right] \times 100\%$$
 (1)

In all of the tests, efficiency is higher at lower input voltages. Tests 1 and 2 are very light loads and are only on the secondary and yield low efficiencies. The efficiency improves greatly as the loads are increased in Tests 3, 4, and 5. The results are graphed in Figure 30.

# Power Supply Efficiency As a Function of Output Power and Input Voltage

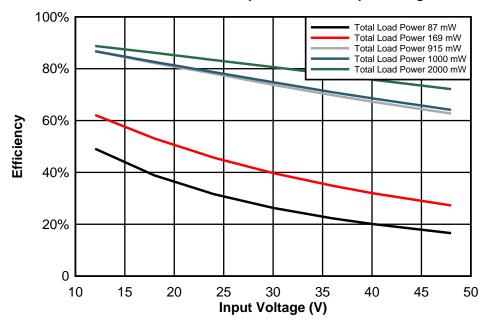


Figure 30. Power Supply Efficiency as a Function of Output Power and Input Voltage



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#### 7.1.2 Power Supply DC Testing During System Operation

The purpose of this test is to show how the DC power supply operates when the system load is connected and to characterize the load itself. For this test, the test equipment used included Agilent 34401A and 34410A DMMs and a Chroma model 62006P-100-25 Programmable DC Power Supply. Input current was measured through the power leads connected to J1. Input voltage was measured at TP2. Primary output voltage was measured at TP3. The output current was measured by removing R4 and connecting a DMM set to measure current in R4's place. Secondary output power was measured by measuring the output voltage across C7. The output current was measured by removing R10 and connecting a DMM across its pads to measure the current into U2, the TLV71333 LDO. Since R2 adds to this load, the additional current was calculated by dividing the measured secondary output voltage by the value of R2, which is 1,998  $\Omega$ .

All tests were performed at 23°C.

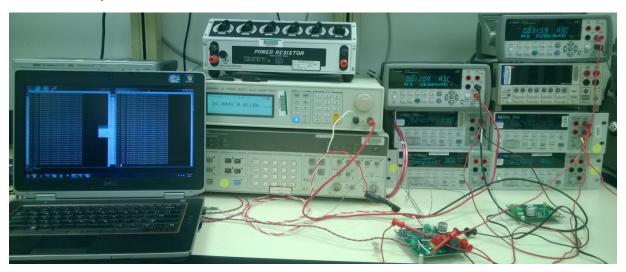


Figure 31. Efficiency Test Setup

The RS-485 data was monitored using a Tera Term terminal for each board. Two boards were programmed with the RS-485 serial-Wi-Fi software: one as DNS master and one as DNS slave. One unit was used for power measurements. Power was measured when there was no RS-485 data being sent and when there was continuous RS-485 data sent into the unit under test. With no data, the power consumption is lowest since the Wi-Fi transmissions are just beacons to maintain the connection to the AP and no data packets are sent. With continuous RS-485 data, data packets are constantly being sent with a baud rate of 115.2 kbaud, and the average current used by the system increases compared to the no data case since the Wi-Fi link is being used more often. No other cases were measured since the results will fall between these two extremes. Power was measured at different voltages from 12-V to 48-V DC.



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Data for these two data transmission cases are shown in Table 6 and Table 7. Efficiency was calculated in the same manner as in Section 7.1.1.

Table 6. Operating Power Efficiency, No RS-485 Data

INPUT VOLTAGE (V)	INPUT CURRENT (mA)	INPUT POWER (mW)	PRIMARY OUTPUT VOLTAGE (V)	PRIMARY OUTPUT CURRENT (mA)	PRIMARY OUTPUT POWER (mW)	SECONDARY OUTPUT VOLTAGE (V)	TOTAL SECONDARY OUTPUT CURRENT (mA)	SECONDARY OUTPUT POWER (mW)	EFFICIENCY
12.04	22.6	272.10	3.300	39.4	130.02	3.604	14.366	51.774	66.81%
15.05	19.4	291.97	3.300	37.8	124.74	3.609	14.368	51.855	60.48%
18.06	18.1	326.89	3.300	39.5	130.35	3.612	14.370	51.903	55.75%
21.06	16.7	351.70	3.300	37.8	124.74	3.613	14.380	51.955	50.24%
24.07	15.8	380.31	3.301	38.0	125.44	3.608	14.368	51.838	46.61%
27.07	15.5	419.59	3.301	39.5	130.39	3.617	14.382	52.020	43.47%
30.07	15.0	451.05	3.301	39.7	131.05	3.615	14.381	51.988	40.58%
35.08	13.6	477.09	3.301	38.3	126.43	3.626	14.387	52.166	37.43%
40.08	13.3	533.06	3.301	39.2	129.40	3.628	14.388	52.198	34.07%
45.08	13.2	595.06	3.301	39.7	131.05	3.634	14.391	52.296	30.81%
48.08	13.1	629.85	3.301	39.3	129.73	3.646	14.397	52.490	28.93%

Table 7. Operating Power Efficiency, RS-485 Data Sent Continuously at 115.2 kbaud

INPUT VOLTAGE (V)	INPUT CURRENT (mA)	INPUT POWER (mW)	PRIMARY OUTPUT VOLTAGE (V)	PRIMARY OUTPUT CURRENT (mA)	PRIMARY OUTPUT POWER (mW)	SECONDARY OUTPUT VOLTAGE (V)	TOTAL SECONDARY OUTPUT CURRENT (mA)	SECONDARY OUTPUT POWER (mW)	EFFICIENCY
12.02	28.3	340.17	3.300	58.3	192.39	3.604	14.466	52.134	71.88%
15.04	23.7	356.45	3.300	56.8	187.44	3.610	14.469	52.232	67.24%
18.04	21.3	384.25	3.300	56.9	187.77	3.613	14.470	52.281	62.47%
21.05	19.6	412.58	3.301	56.0	184.86	3.614	14.471	52.297	57.48%
24.05	18.8	452.14	3.301	58.8	194.10	3.610	14.459	52.196	54.47%
27.06	17.6	476.26	3.301	56.7	187.17	3.617	14.462	52.310	50.28%
30.06	16.9	508.01	3.301	57.3	189.15	3.615	14.471	52.313	47.53%
35.07	15.5	543.59	3.301	57.8	190.80	3.627	14.487	52.545	44.77%
40.07	14.7	589.03	3.301	53.0	174.95	3.628	14.488	52.561	38.63%
45.08	14.4	649.15	3.301	53.8	177.59	3.640	14.494	52.757	35.48%
48.08	14.2	682.74	3.301	54.7	180.56	3.646	14.497	52.855	34.19%



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Comparing the efficiencies calculated in Table 6 and Table 7 shows that the power supply efficiency is higher for the high power continuously transmitting case. The average load current, and therefore the average power, is very low, even though the load current can be quite high during data transmissions. Figure 32 shows an oscilloscope trace of the primary 3.3-V supply load current and the output ripple over a period of four seconds. This shows the short duration current peaks. It also shows the overall voltage ripple and noise of 86 mV peak-to-peak.

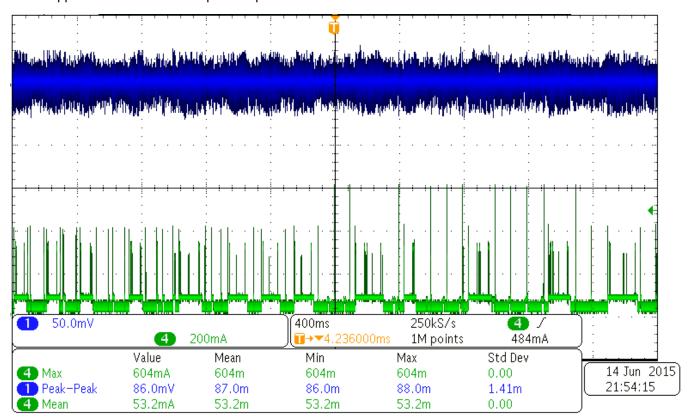


Figure 32. Load Current, No Data transmission (Green); 3.3-V Supply Ripple (Blue)



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The oscilloscope trace shows many short, high current pulses. The peak load current is 604 mA, while the average current is only 53.2 mA. Figure 33 shows a close up view of a 612-mA current peak. It is only about 100 µs long.

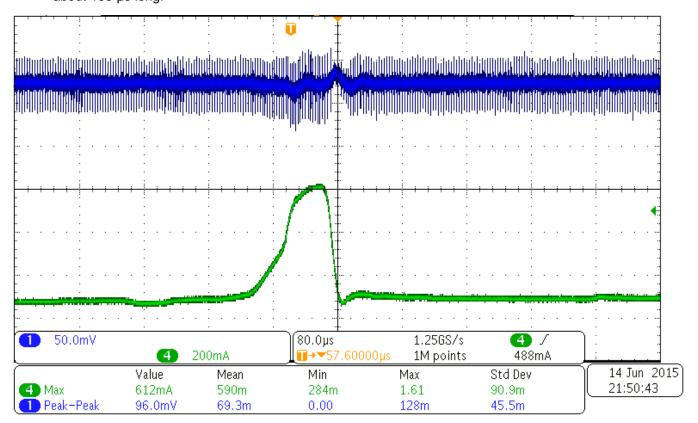


Figure 33. Close View of One Current Peak

The isolated 3.3-V supply from U2, the TLV71333 LDO, measures 3.298 V for all input voltage conditions. When RS-485 communication is idle, the current into the LDO is 12.56 mA. When RS-485 communication is running continuously at 115.2 kbaud, the current into the LDO is 12.65 mA. Most of this current flows into the ISO15 transceiver since the TLV71333 has a quiescent current of 50  $\mu$ A.



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### 7.2 Power Supply AC Testing

The Isolated RS-485 to Wi-Fi Bridge was tested with a Kikusui PCR500M AC Power Supply. The minimum AC voltage that the system worked at was 7.7-V AC, 60 Hz. Lowering the voltage to 7.7-V AC leads to the processor resetting. The system would not start up again unless the input voltage was 8.3-V AC.

The voltage on the filter capacitor C2 was measured with an oscilloscope to compare the results to the ripple voltage expected from Section 4.1. The assumption when choosing C2 was that the load would be drawing its maximum current for an entire 60-Hz cycle. Figure 32 in Section 7.1.2 shows that the high current condition in the load occurs for short periods and is not continuous. Because of this, the voltage ripple at C2 is much lower than calculated. The ripple voltage for an input voltage of 18-V AC on C2 is shown in Figure 34.

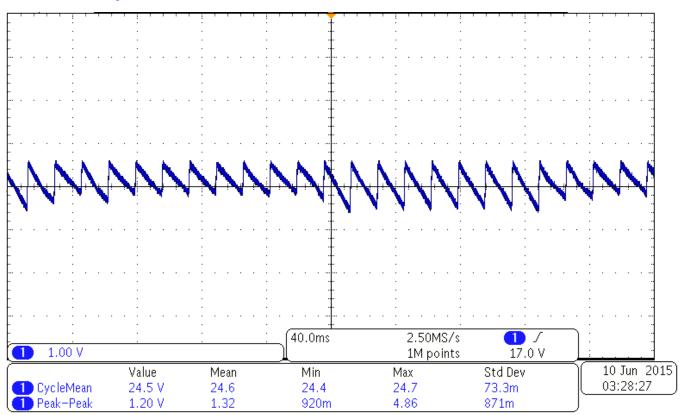


Figure 34. Ripple Voltage at C2 for an 18-V AC Input

For the measurement in Figure 34, the system was transmitting constantly as it was for the efficiency measurement, ensuring a maximum ripple. The peak-to-peak voltage ripple is only 1.2 V in this case, much less than the expected 8 V.



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For a 50-Hz input, the voltage ripple on C2 is higher (see Figure 35). 40.0ms 2.50MS/s **1** 1.00 V 17.0 V 1M points Std Dev 10 Jun 2015 Value Mean Min Max 03:30:33 CycleMean 24.4 V 24.6 24.3 24.7 98.2m

Figure 35. Ripple Voltage at C2 for an 18-V AC Input

4.86

832m

The ripple is higher in this case, 1.48 V peak-to-peak, due to the lower input voltage frequency.

920m

🚹 Peak-Peak

1.48 V

1.33



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#### 7.3 CC3200 Performance

#### 7.3.1 Data Throughput

The data in this section was provided by the CC3100 and CC3200 design team. It is included here to show the Wi-Fi data throughput performance.

The following two graphs show data throughput measurements with the hardware set up as both an AP and a Station. The data was not taken on the hardware described in this document. It was taken with a CC3100-based system that includes the CC3100 BoosterPack. The CC3100 and CC3200 have the same network processor subsystems, so their performance will be the same. The antenna on the PCB for the Isolated RS-485 to Wi-Fi Bridge is the same antenna used in the CC3100 BoosterPack, and great care has been taken to ensure the Isolated RS-485 to Wi-Fi Bridge RF output circuit matches the CC3100 BoosterPack, including the trace width, the thickness of the PCB dielectric between the RF output traces and the ground plane, and the overall board thickness.

The CC3100 system was tested in a chamber using a Cisco AP 1252 router and a Cisco-Linksys AE1000 router. The test measures throughput versus path loss (range) where the AP or Station is placed in a chamber. Range is simulated by using an attenuator to reduce the module output power.

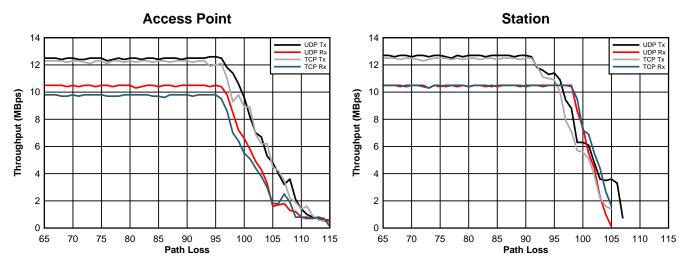


Figure 36. Data Throughput versus Path Loss (CC3100 AP)

Figure 37. Data Throughput versus Path Loss (CC3100 Station)

The Isolated RS-485 to Wi-Fi Bridge is limited in its throughput by the CC3200 UART module. The UART module has a maximum bit rate of 3 Mbits per second.



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### 7.3.2 In-Office Range Test

For these tests, the UART in the Isolated RS-485 to Wi-Fi Bridge was tested at 115.2 bits per second.

In order to see how the Isolated RS-485 to Wi-Fi Bridge can perform in an office environment, tests were run with the hardware set up as described in Section 6.2. Using a TP-Link model TL-WR740N router at the AP, one of the systems was moved away from the router and communication was re-checked. In one test, communication was still possible with one system at a distance of 83.3 meters from the AP. There were no obstructions between the system and the AP, though the RF line-of-sight was down a narrow corridor with walls and cubicles lining the corridor. Another test had the system 25.4 meters form the AP, but the RF signal had to penetrate four walls and several rows of cubicles to get from the AP to the system.

This test is not meant to be a definitive performance test. Actual user performance depends upon many factors, such as the model of the AP used, the amount of RF interference in the environment in which the hardware is installed, the location of the hardware in relation to walls or metal objects, and other factors unique to each installation.



www.ti.com Other Applications

### 8 Other Applications

The software used to test the Isolated RS-485 to Wi-Fi Bridge with 24-V AC Power acts as a cable bridge between two disconnected sections of a network. The Isolated RS-485 to Wi-Fi Bridge was also tested with a UART to Wi-Fi Bridge that was designed for TI Design TIDA-00375 and they interoperate seamlessly.

There are many other uses for this hardware that were not developed for this project. This hardware can be used as an AP and could serve a web page with information about the RS-485 network. This could be accessed by a technician using a smart phone, a tablet, or a laptop computer. Another use is to have the hardware set up as a station connected to an external AP that is connected to the internet. In this way, the Isolated RS-485 to Wi-Fi Bridge would provide data to a cloud server that can be remotely accessed or used for data analysis.

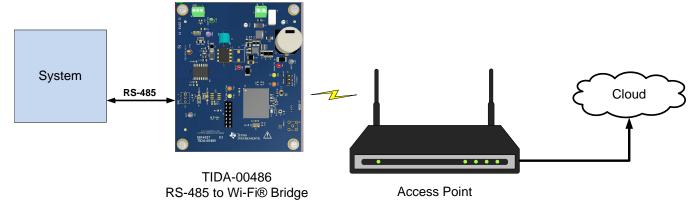


Figure 38. RS-485 to Cloud System



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# 9 Design Files

### 9.1 Schematics

To download the schematics, see the design files at TIDA-00486.

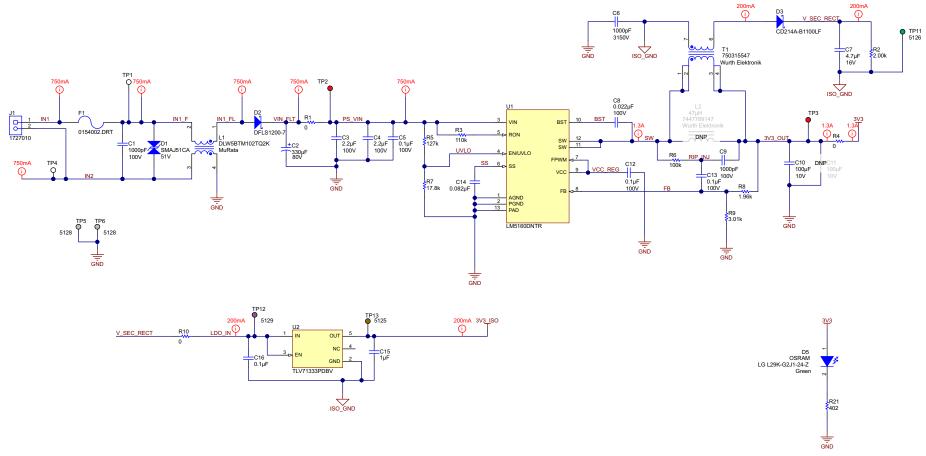


Figure 39. Power Supply Schematic



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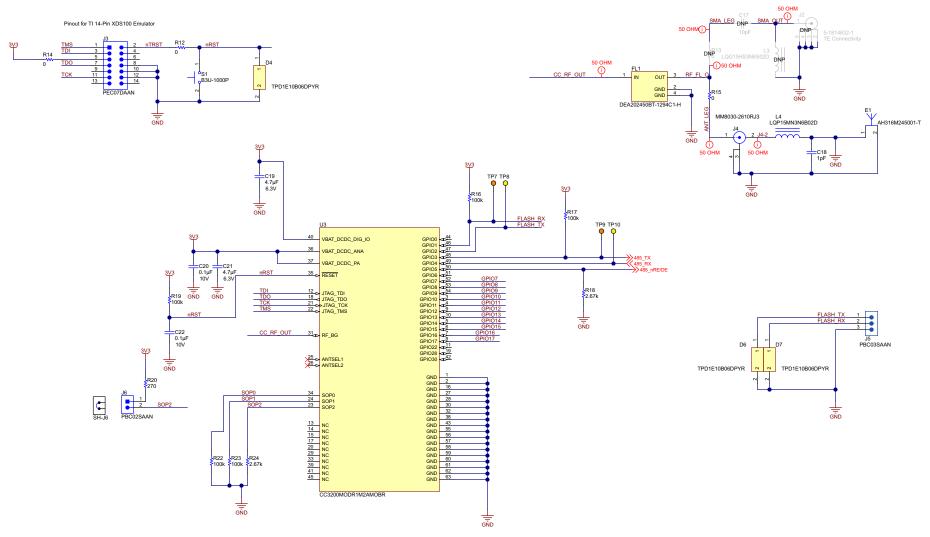


Figure 40. CC3200MOD Schematic



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#### ISOLATED TRANSCEIVER

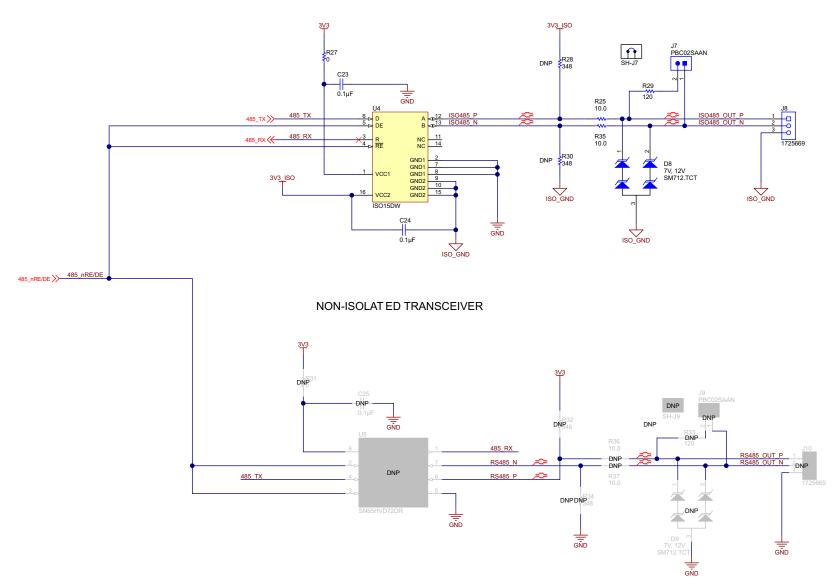


Figure 41. Interface Schematic



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### 9.2 Bill of Materials

To download the bill of materials (BOM), see the design files at TIDA-00486.

### 9.3 PCB Layout Recommendations

The layout of this PCB was done by carefully following the recommended guidelines for the LM5160, the CC3200MOD, and for the Taiyo Yuden AH316M245001-T chip antenna. The power nets from J1 through to the 3V3 net are made as wide as practical. For the CC3200MOD, follow the *Hardware Design Review Process and PCB Layout Design Guidelines* found on the SimpleLink™ Wi-Fi® CC31xx/CC32xx Main Page for best results.

### 9.3.1 Layer Plots

To download the layer plots, see the design files at TIDA-00486.

### 9.4 Altium Project

To download the Altium project files, see the design files at TIDA-00486.

### 9.5 Gerber Files

To download the Gerber files, see the design files at TIDA-00486.

# 9.6 Assembly Drawings

To download the assembly drawings, see the design files at TIDA-00486.



Software Files www.ti.com

#### 10 Software Files

To download the software files, see the design files at TIDA-00486.

#### 11 References

- 1. Texas Instruments, CC3200MOD SimpleLink™ Wi-Fi® and Internet-of-Things Module Solution, a Single-Chip Wireless MCU, CC3200MOD Datasheet (SWRS166)
- 2. Texas Instruments, SimpleLink™ Wi-Fi® CC31xx/CC32xx Main Page (link)
- 3. Texas Instruments, SimpleLink Wi-Fi CC3100 BoosterPack (http://www.ti.com/tool/cc3100boost)
- 4. Texas Instruments, *Wide Input 65-V, 1.5-A Synchronous Buck / Fly-Buck™ Converter*, LM5160 Datasheet (SNVSA03)
- 5. Texas Instruments, *LM5160 Buck Regulator Quick Start Calculator* (http://www.ti.com/tool/lm5160dntbk-calc)
- 6. Texas Instruments, *TLV713 Capacitor-Free, 150-mA, Low-Dropout Regulator with Foldback Current Limit for Portable Devices*, TPL71333P Datasheet (SBVS195)
- 7. Texas Instruments, 3.3V-Supply RS-485 with IEC ESD Protection, SN65HVD72 Datasheet(SLLSE11)
- 8. Texas Instruments, *TPD1E10B06 Single Channel ESD in 0402 Package*, TPD1E10B06 Datasheet (SLLSEB1)

### 12 Terminology

**AP**— Access Point. This is the radio to which Wi-Fi devices attach. This can be a router or a CC3200.

**DMM**— Digital Multimeter

# 13 Acknowledgments

The authors would like to thank Ben Gilboa, Moshe Leibo, and all of the members of the CC3100/CC3200 SimpleLink team for their support for this project and especially for the throughput data.

#### 14 About the Author

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www.ti.com Revision C History

# **Revision C History**

Changes from B Revision (September 2015) to C Revision	Page
Changed from USB-to-RS-485 to USB-to-UART	21
NOTE: Page numbers for previous revisions may differ from page numbers in the current version.	
Revision B History	
Changes from A Revision (July 2015) to B Revision	Page
• Changed Equation 1 from "(V <sub>PRIMARY</sub> × I <sub>PRIMARY</sub> ) × (V <sub>SECONDARY</sub> × I <sub>SECONDARY</sub> )" to "(V <sub>PRIMARY</sub> × I <sub>PRIMARY</sub> ) + (V <sub>SECONDARY</sub> )" to "(V <sub>PRIMARY</sub> × I <sub>PRIMARY</sub> ) + (V <sub>SECONDARY</sub> )" to "(V <sub>PRIMARY</sub> × I <sub>PRIMARY</sub> ) + (V <sub>SECONDARY</sub> )" to "(V <sub>PRIMARY</sub> × I <sub>PRIMARY</sub> ) + (V <sub>SECONDARY</sub> )" to "(V <sub>PRIMARY</sub> × I <sub>PRIMARY</sub> ) + (V <sub>SECONDARY</sub> )" to "(V <sub>PRIMARY</sub> × I <sub>PRIMARY</sub> ) + (V <sub>SECONDARY</sub> )" to "(V <sub>PRIMARY</sub> × I <sub>PRIMARY</sub> ) + (V <sub>SECONDARY</sub> )" to "(V <sub>PRIMARY</sub> × I <sub>PRIMARY</sub> ) + (V <sub>SECONDARY</sub> )" to "(V <sub>PRIMARY</sub> × I <sub>PRIMARY</sub> ) + (V <sub>SECONDARY</sub> )" to "(V <sub>PRIMARY</sub> × I <sub>PRIMARY</sub> ) + (V <sub>SECONDARY</sub> )" to "(V <sub>SECONDARY</sub> )"	x I <sub>SECONDARY</sub> )" 32
NOTE: Page numbers for previous revisions may differ from page numbers in the current version.	
Revision A History	
Changes from Original (June 2015) to A Revision	Page
Changed from preview page	1
NOTE: Page numbers for previous revisions may differ from page numbers in the current version.	

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