

HIGH VOLTAGE SEMINAR

BEN GENEREAUX

HIGH POWER GATE DRIVERS

PCB LAYOUT GUIDELINES TO
OPTIMIZE POWER SUPPLY
PERFORMANCE

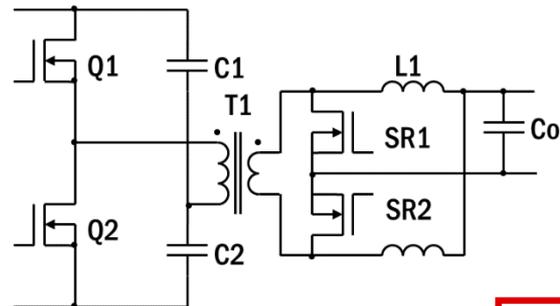


What will I get out of this session?

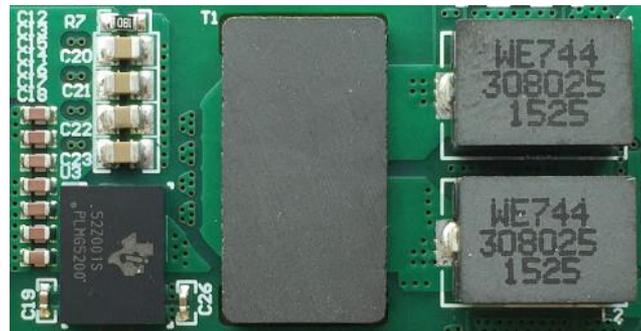
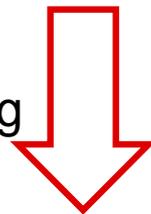
- The purpose of this session is to introduce the concepts needed to successfully layout a printed circuit board (PCB) for a switched-mode power supply (SMPS)
- This presentation is relevant to all SMPS PCB layouts, from 1 W to 10 kW
- Part numbers mentioned:
 - UCC28180
 - UCC28742
 - UCC28710
 - UCC24612
 - UCC24610
- Reference designs mentioned:
 - TIDA-00443

Why is layout important?

- The best controller in the world cannot work well if embedded in a poor layout
- PCB layout for SMPS is extremely complicated!
- Same principles govern low and high power layouts
 - The difficulty is how to apply the principles in practice
- **The PCB is often the most complex component in a design**

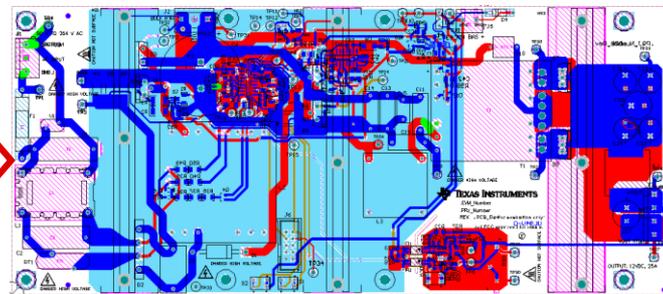
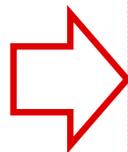
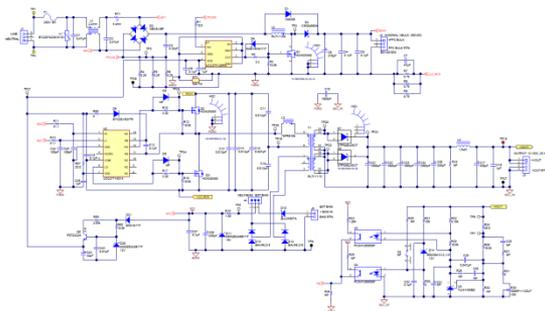


How to translate a schematic into working hardware



Agenda

- The schematic
- Parasitics
 - Resistance
 - Inductance
 - Capacitance
- EMI & safety
- Grounding & signal routing
- Thermal management
- PCB layout example
- Summary

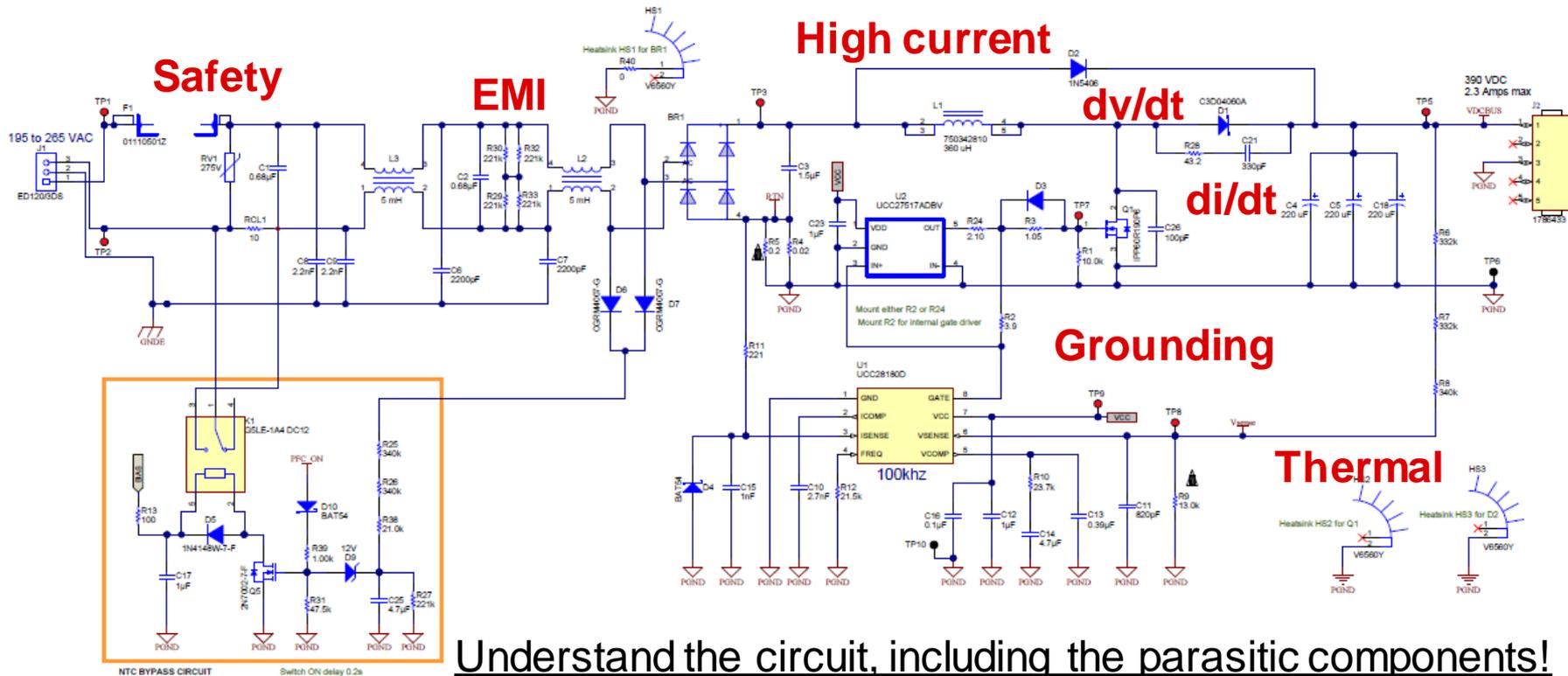


What are concerns for a power supply PCB layout?

- Safety
- EMI
- Parasitic inductance
- Parasitic capacitance
- Parasitic resistance
- Thermal performance
- High dv/dt
- High di/dt
- Grounding
- Noise

The schematic

TIDA-00443 using UCC28180 PFC controller



Understand the circuit, including the parasitic components!

Parasitic resistance

You mean copper is not a perfect conductor?

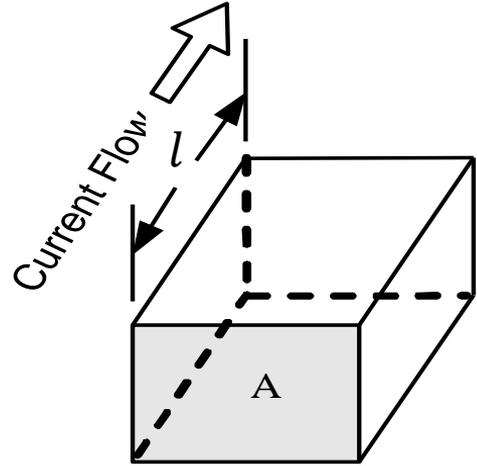
Material	mΩ-cm	mΩ-in
Copper	1.70	0.67
Gold	2.2	0.87
Lead	22.0	8.66
Silver	1.5	0.59
Silver (plated)	1.8	0.71
Tin-lead	15	5.91
Tin (plated)	11	4.33

$$\rho(\text{Cu}) = 0.67 \text{ m}\Omega\text{-in at } 25^\circ\text{C}$$

$$TCR_{Cu} \approx 4000 \text{ ppm}/^\circ\text{C} \text{ (+40\% for } 100^\circ\text{C rise)}$$

$$R = \frac{\rho \cdot l}{A}$$

$\rho = \text{resistivity}$

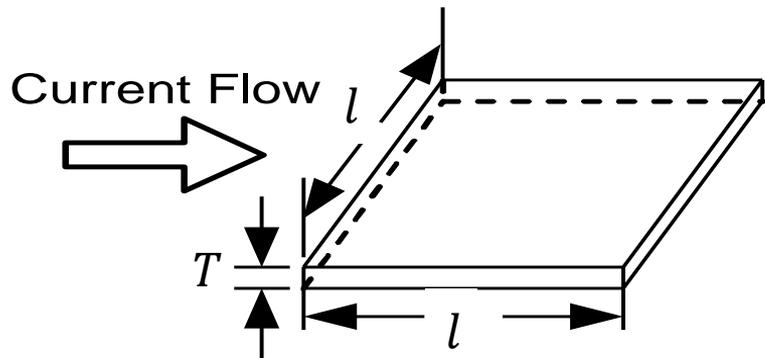


Impacts?

- Regulation
- Efficiency
- Temperature rise

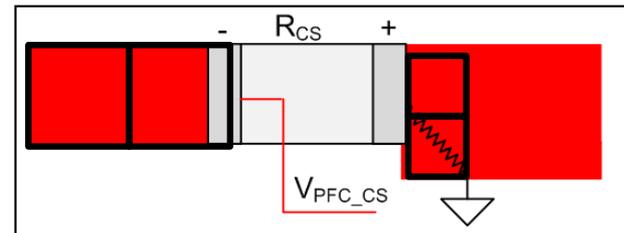
Parasitic resistance

Counting squares



$$R = \frac{\rho \cdot l}{T \cdot l} = \frac{\rho}{T}$$

Assume 1 oz. Cu

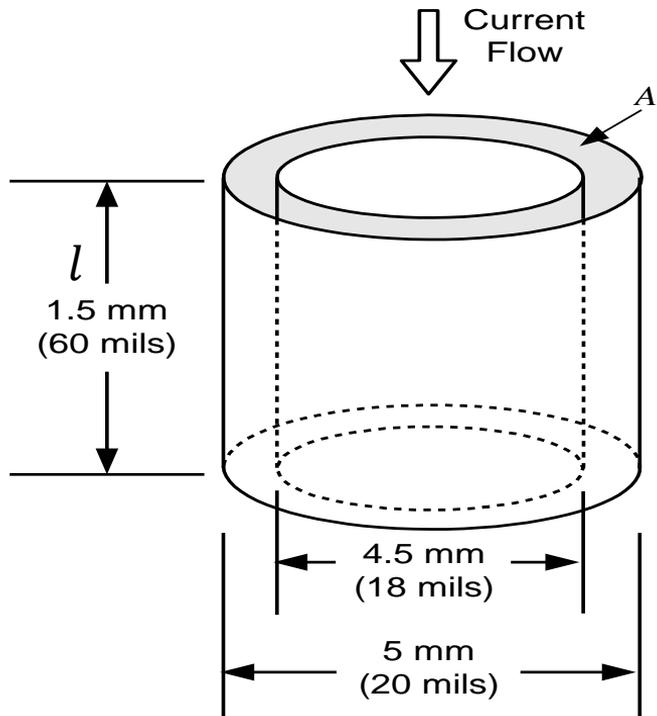


2 series squares = $\sim 1.0 \text{ m}\Omega$
2 parallel squares = $\sim 0.25 \text{ m}\Omega$

Copper Weight (Oz.)	Thickness ($\mu\text{m}/\text{mils}$)	$\text{m}\Omega$ per square (25°C)	$\text{m}\Omega$ per square (125°C)
1/2	17.5/0.7	1	1.4
1	35/1.4	0.5	0.7
2	70/2.8	0.25	0.35

Parasitic resistance

Vias have resistance too



Typical rule of thumb is 1 A to 3 A per via

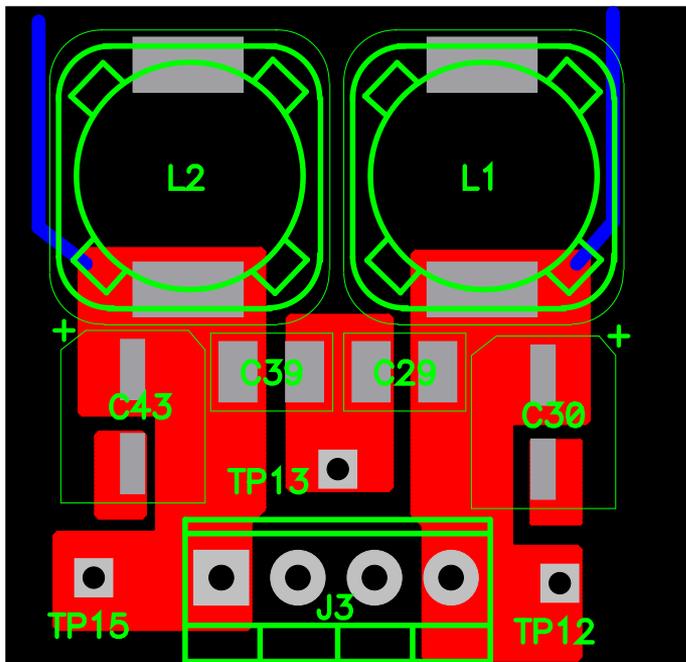
$$R = \frac{\rho \cdot l}{A}$$

$$R = \frac{\rho \cdot l}{\pi \cdot (r_o^2 - r_i^2)}$$

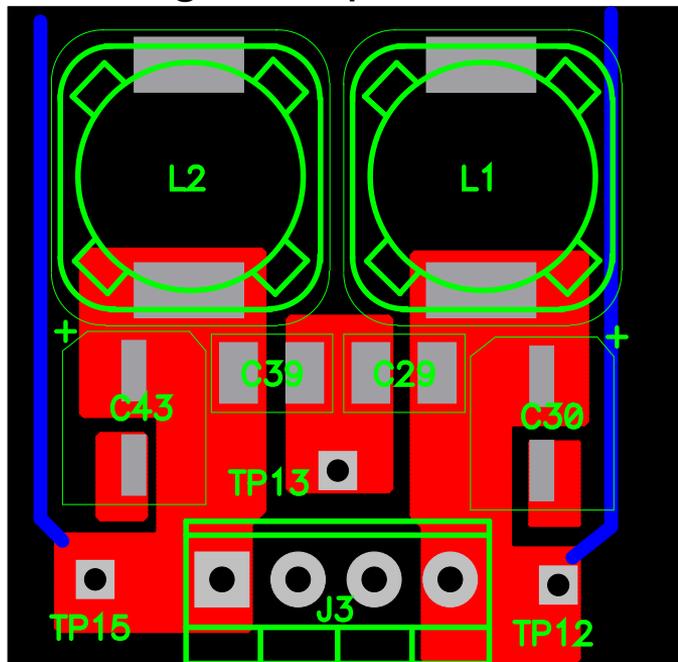
$$R = \frac{(0.67 \mu\Omega \cdot \text{in}) \cdot (0.06 \text{ in})}{\pi \cdot [(0.01 \text{ in})^2 - (0.009 \text{ in})^2]} = 0.67 \text{ m}\Omega$$

Parasitic resistance

Poor sense location



Sensing at output connector



How many $m\Omega$ between L2 and J3?

Identifying high di/dt

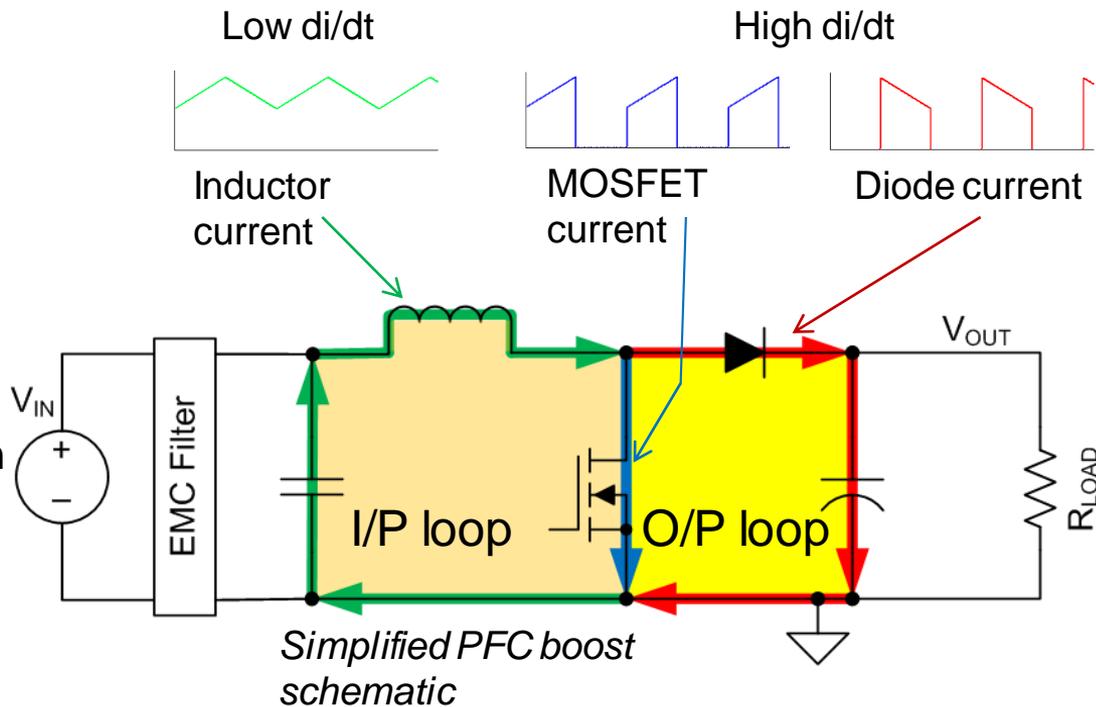
Switched current loops

I/P loop (green)

- di/dt rates much lower
- Stray inductance is less critical
- C_{IN} provides local low impedance source

O/P loop (blue/red)

- Inductor current alternates between MOSFET and diode paths
- Pulsating currents
- Stray inductance will cause voltage spikes



Identifying high di/dt

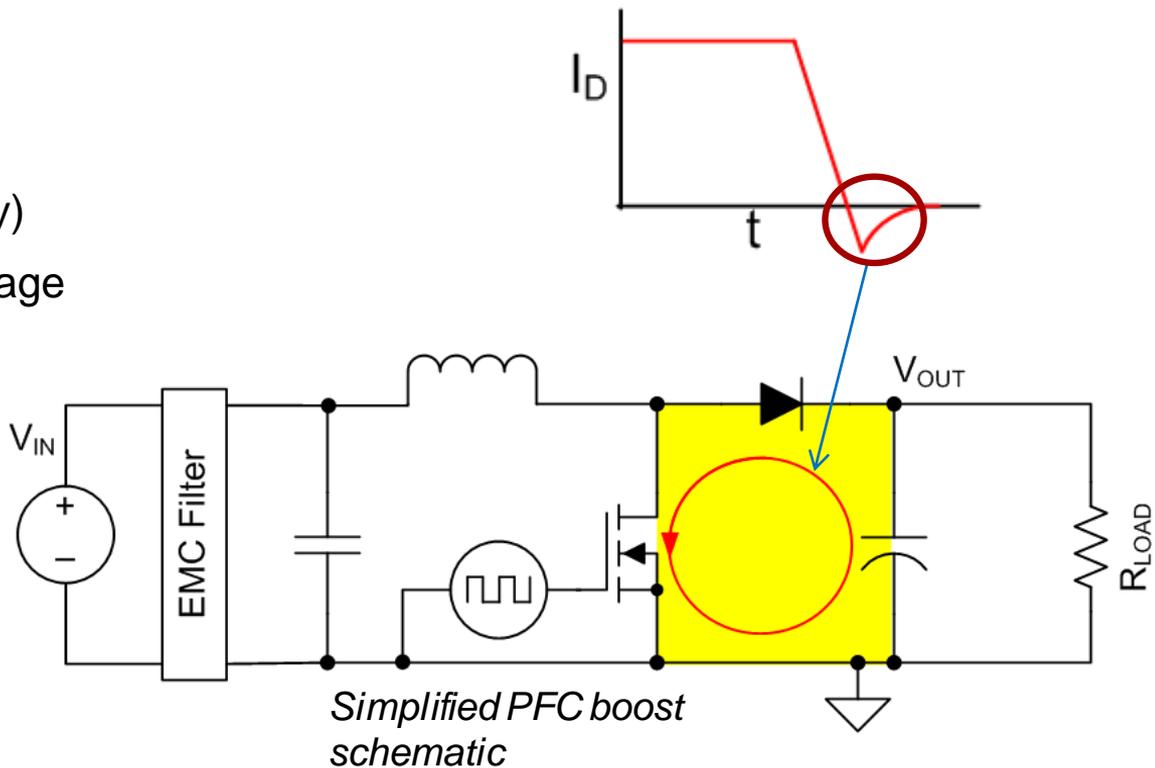
Reverse recovery

Occurs when:

- MOSFET turns ON during CCM operation (nearly every topology)
- Stray inductance will cause voltage spikes

Mitigation:

- Minimize loop inductance
- Use low Q_{RR} rectifiers –
 - SiC for high V_{OUT}
 - Schottky or ultra-fast diodes
 - Sync rectifiers with low Q_{RR}



Identifying high di/dt

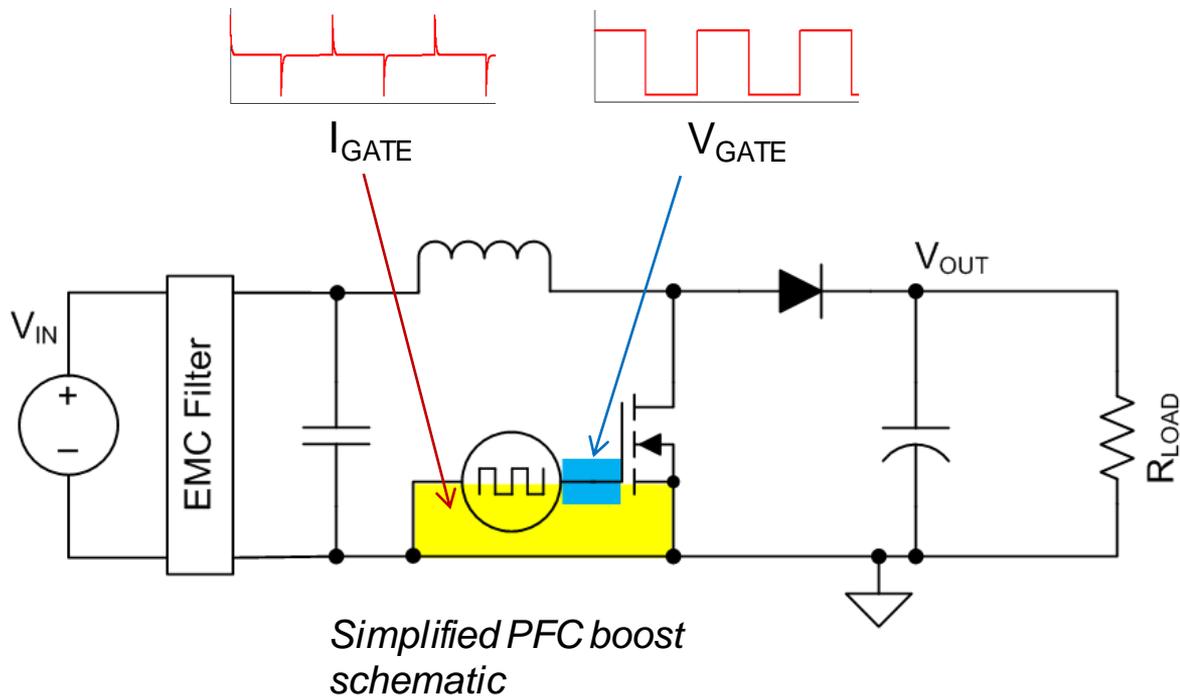
Gate drives

High di/dt in loop (yellow)

- Stray inductance:
 - Limits drive current
 - Can cause ringing
- Minimize loop inductance

High dv/dt on gate (blue)

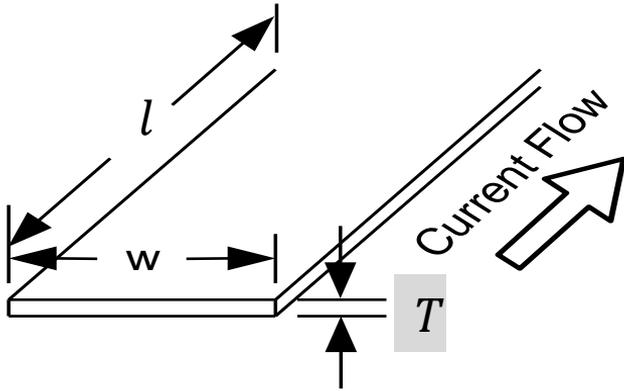
- Can couple to noise-sensitive nodes
- Minimize capacitance



Parasitic inductance

Self inductance of PWB traces

- Due to the natural logarithmic relationship, large changes in conductor width have minimal impact on inductance



$$L = 2 \cdot l \cdot \left(\ln \left(\frac{l}{T + W} \right) + \frac{1}{2} \right) \text{ nH/cm}$$

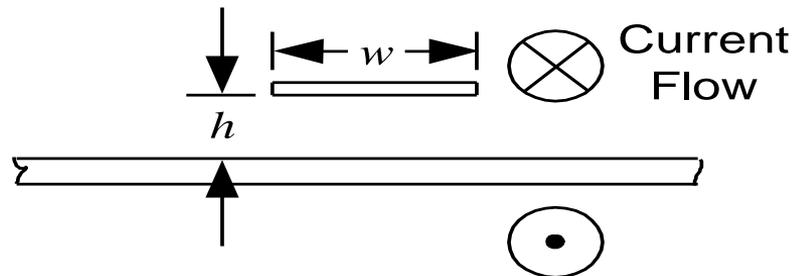
$$L = 5 \cdot l \cdot \left(\ln \left(\frac{l}{T + W} \right) + \frac{1}{2} \right) \text{ nH/in}$$

W (mm/in)	T(mm/in)	Inductance (nH/cm or nH/in)
0.25/0.01	0.07/0.0028	10/24
2.5/0.1	0.07/0.0028	6/14
12.5/0.5	0.07/0.0028	2/6

Parasitic inductance

PWB traces over ground planes

- Substantial inductance reduction
- Inductance inversely proportional to width



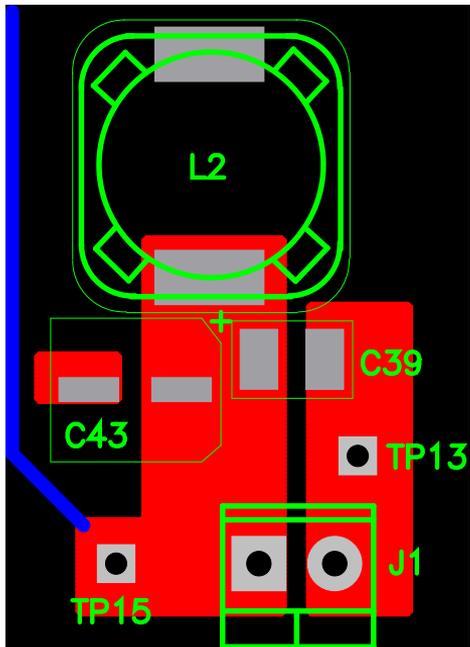
$$L = \frac{2 \cdot h \cdot l}{w} \text{ nH/cm}$$

$$L = \frac{5 \cdot h \cdot l}{w} \text{ nH/in}$$

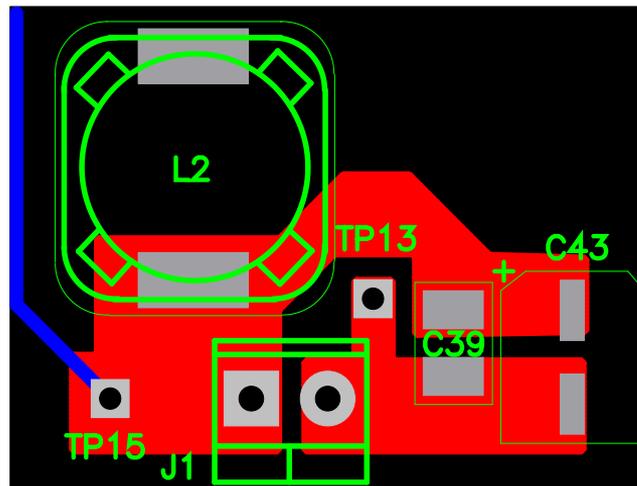
Metric			English		
h (cm)	w (cm)	Inductance (nH/cm)	h (in)	w (in)	Inductance (nH/in)
0.25	2.5	0.2	0.01	0.1	0.5
1.5	2.5	1.2	0.06	0.1	3.0

Parasitic inductance

Low series inductance



High series inductance



How much inductance in series with C39? (total length ~ 2 cm)

Identifying high dv/dt

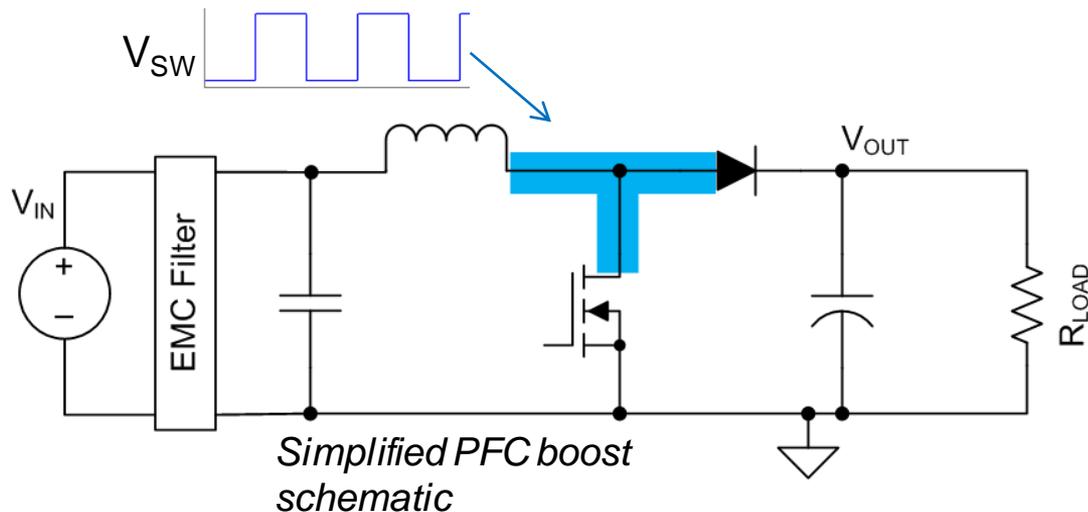
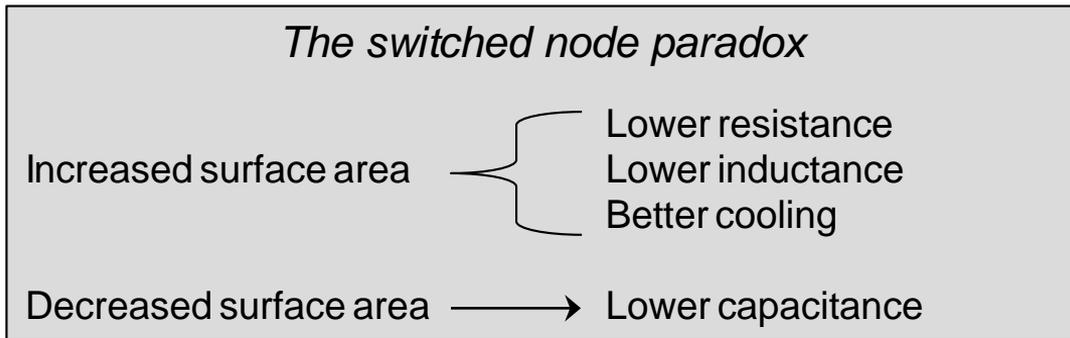
Switched nodes

High dv/dt at switched node (blue):

- Switched between 0V and V_{OUT}
- Stray capacitance can cause:
 - EMI problems
 - Noise injected to internal circuits
 - Reduced efficiency

Mitigation:

- Minimize V_{SW} surface area
- Keep sensitive etch and components away from V_{SW}
- Ground the heatsink!

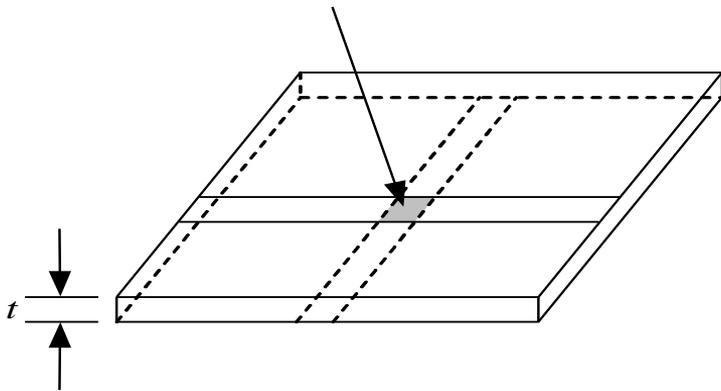


Parasitic capacitance

Sample capacitance calculation

Consider two 10 mil traces crossing with 10 mil PWB thickness

$$A = 0.00025 \text{ m} \times 0.00025 \text{ m}$$



Note: 10 mils = 0.00025 m

$$C = \frac{\epsilon_r \cdot \epsilon_0 \cdot A}{t}$$

$$C = \frac{5 \cdot (8.85 \times 10^{-12} \text{ F/m}) \cdot (0.25 \text{ mm})^2}{2.5 \text{ mm}}$$

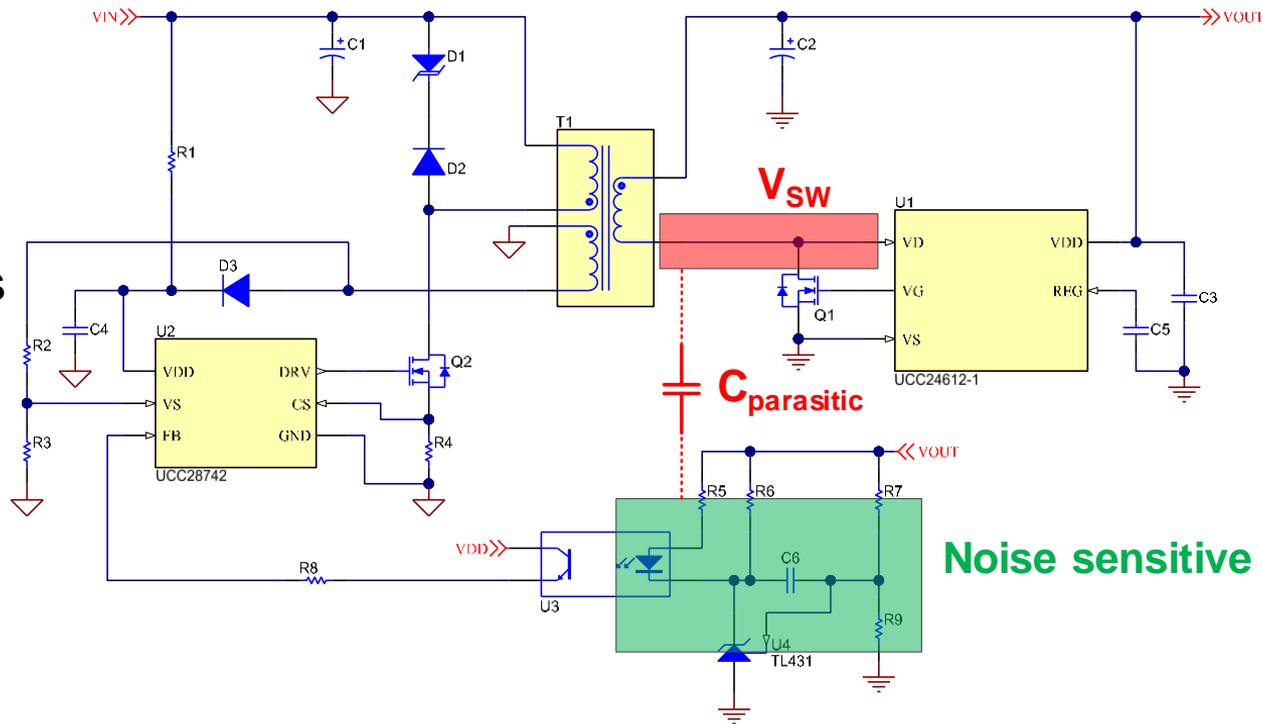
$$C = 0.01 \text{ pF}$$

Not much capacitance but consider the area of all components connected to the feedback network

Parasitic capacitance

Chaos created by noise injection

Ten $0.05 \times 0.02 \text{ in}^2$ pads can increase parasitic capacitance to 2 pF

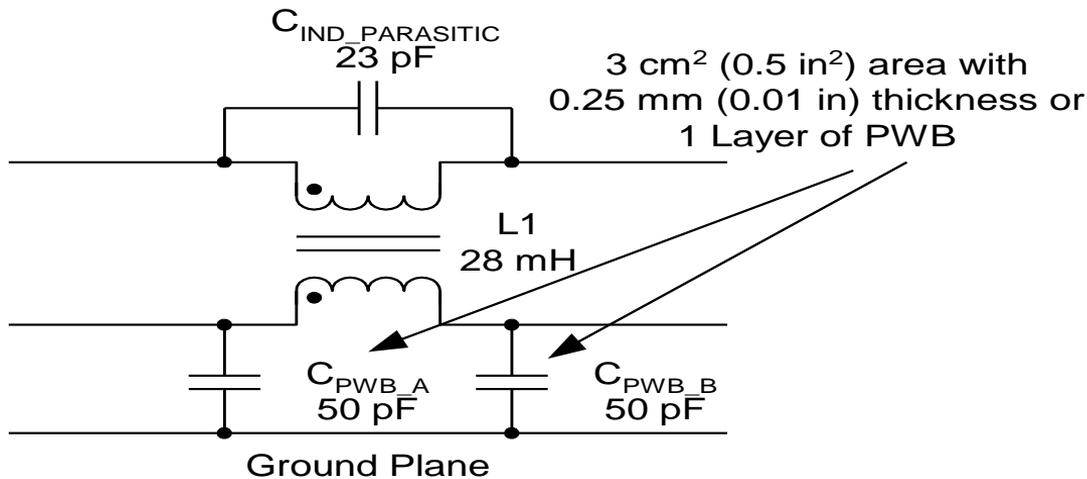
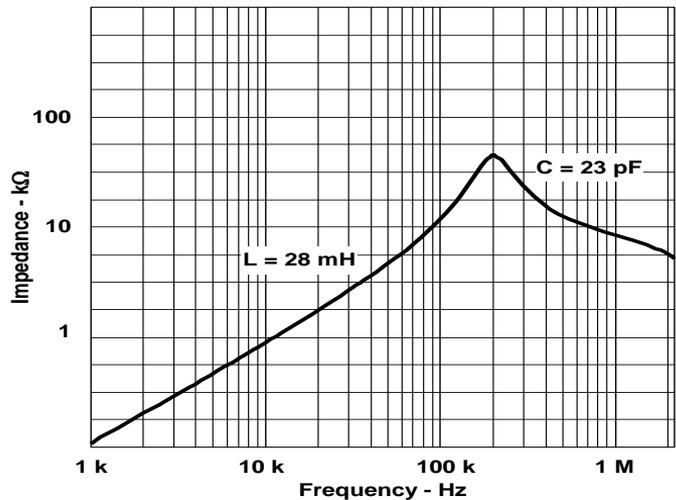


Noise sensitive

Parasitic capacitance

At high frequency inductors turn into capacitors

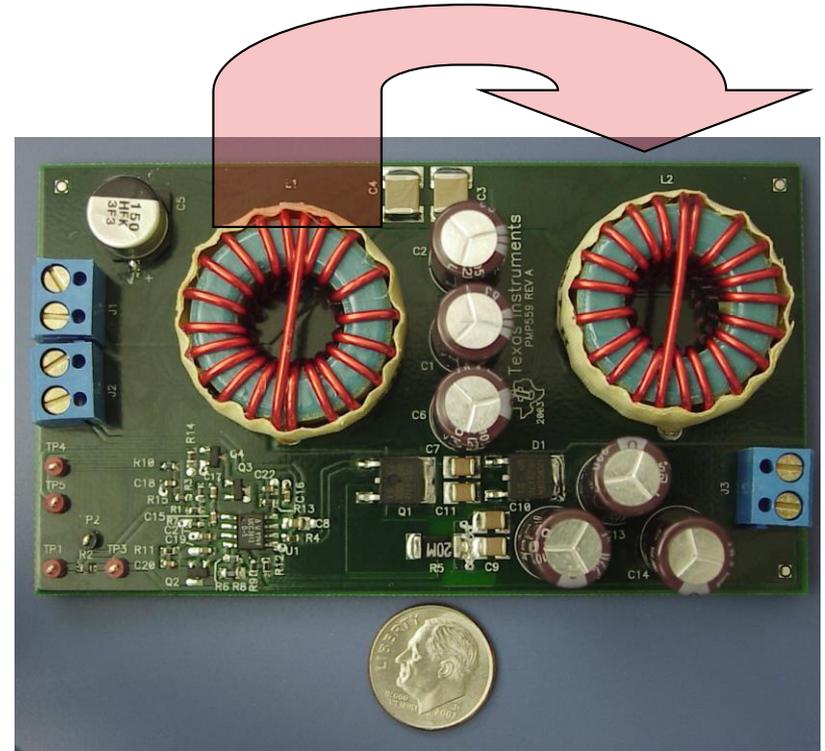
Don't route planes under common mode inductors!



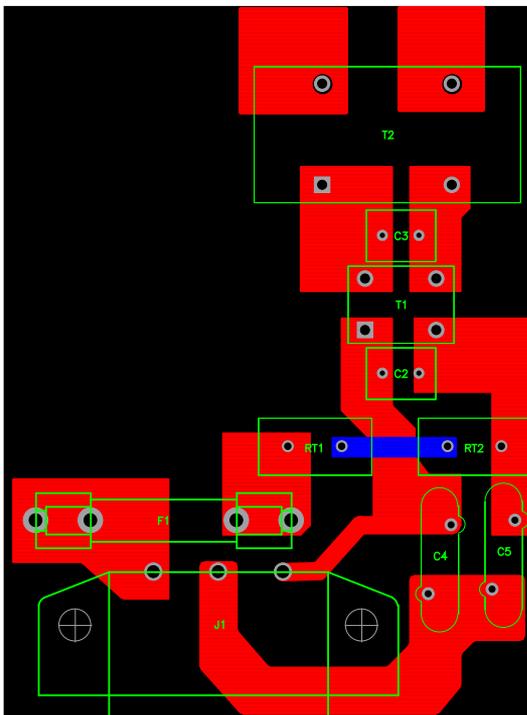
EMI considerations

Magnetic coupling

- External fields couple between inductors
- Can cause EMI issues
- Consider alternate orientation of second inductor to minimize coupling
- Use core shapes that provide better shielding



EMI considerations



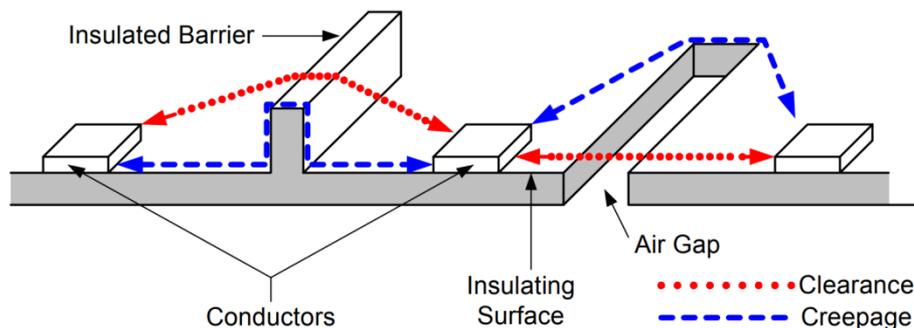
Input filter layout

- Place components away from noise sources
- Common mode inductor T2 input pins do not cross output pins
- No GND plane under EMI filter
- Wide, short etch used to minimize losses
- Wide spacing between etches meets high-voltage requirements and minimizes coupling capacitance

Safety

Separate hazardous voltages from user accessible points

- Consult your safety expert!
- Create a very clear channel between primary and secondary
- Spacing depends on:
 - Type of insulation
 - Pollution degree
 - AC mains voltage
 - Working voltage
- Types of insulation:
 - Functional
 - Basic/supplementary
 - Reinforced



Working Voltage		AC Mains < 150 V (Transient to 1500 V) Pollution levels 1 and 2			AC Mains < 300 V (Transient to 2500 V) (Pollution levels 1 and 2)		
Peak dc V	rms V	F	B/S	R	F	B/S	R
71	50	0.4	1.0	2.0	1.0	2.0	4.0
210	150	0.5	1.0	2.0	1.4	2.0	4.0
420	300	1.5	2.0	4.0	1.5	2.0	4.0
840	600	3.0	3.2	6.4	3.0	3.2	6.4

Partial Clearance Dimensions (mm) from UL60950-1, Section 2.10.3, Table 2H

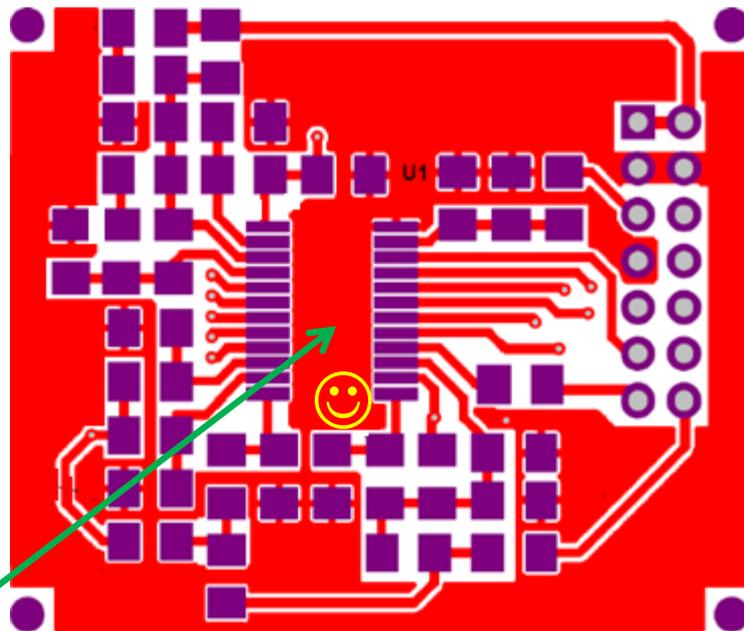
Ground planes

Ground planes provide:

- Low resistance return paths
- Low inductance return paths
- Lateral heat spreading across board

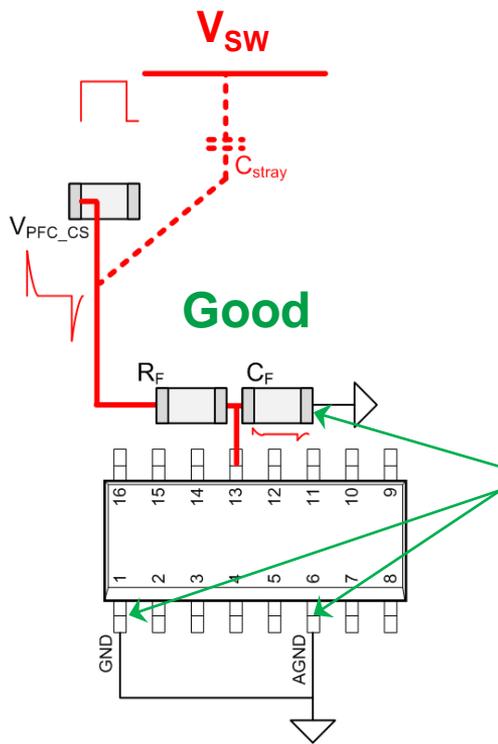
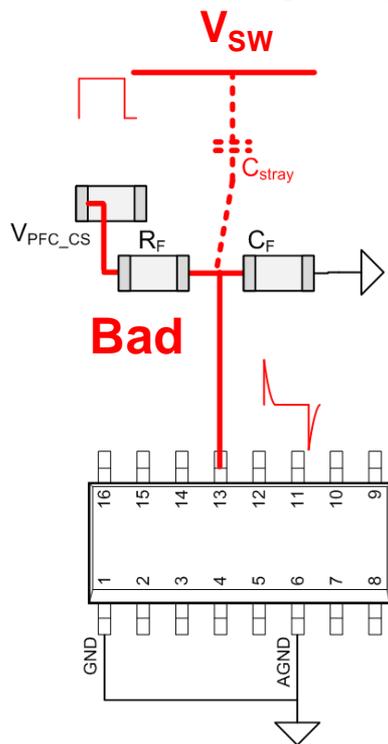
General ground plane tips:

- Consider flooding empty areas with ground
- Avoid putting slots in GND planes
- Use jumpers on single layer boards to improve GND planes
- Place as much GND under the IC as possible



Signal routing/placement

Avoid coupling noise to sensitive nodes



- Maximize the separation
 - Move the source, reduce C_{stray}
- Place capacitors and resistors near pins
- Place GND vias near caps, resistors, and IC
- Minimize the unfiltered track length

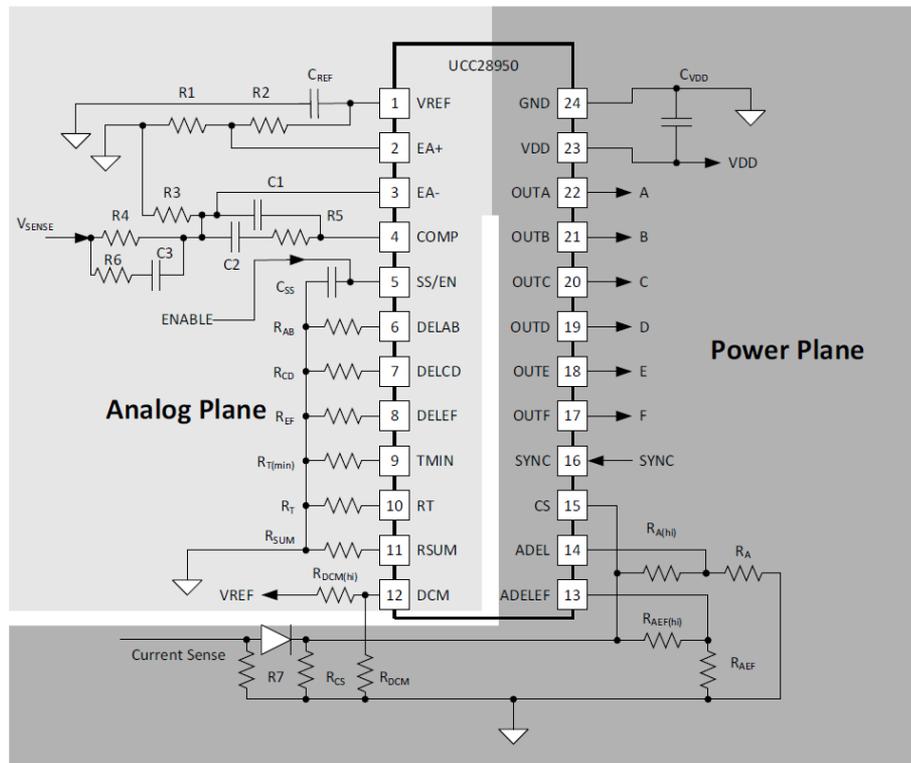
Signal routing/placement

Data sheets normally contain PCB layout guidelines

10.1 Layout Guidelines

In order to increase the reliability and robustness of the design, TI recommends the following layout guidelines.

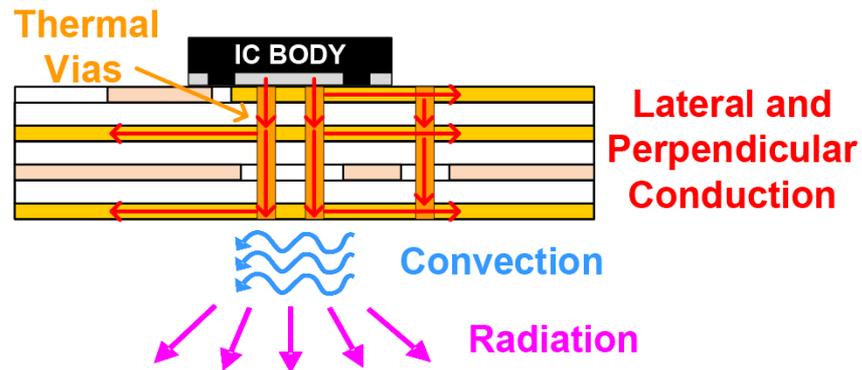
- VREF pin. Decouple this pin to GND with a good quality ceramic capacitor. A 1- μ F, X7R, 25V capacitor is recommended. Keep VREF PCB tracks as far away as possible from sources of switching noise.
- EA+ pin. This is the non-inverting input to the error amplifier. It is a high impedance pin and is susceptible to noise pickup. Keep tracks from this pin as short as possible.
- EA- pin. This is the inverting input to the error amplifier. It is a high impedance pin and is susceptible to noise pickup. Keep tracks from this pin as short as possible.
- COMP pin. The error amplifier compensation network is normally connected to this pin. Keep tracks from this pin as short as possible.
- SS/EN pin. Keep tracks from this pin as short as possible. If the Enable signal is coming from a remote source then avoid running it close to any source of high dv/dt (MOSFET Drain connections for example) and add a simple RC filter at the SS/EN pin.
- DELAB, DELCD, DELEF, TMIN, RT, R_{SUM} , DCM, ADELEF and ADEL pins. The components connected to these pins are used to set important operating parameters. Keep these components close to the IC and provide short, low impedance return connections to the GND pin.
- CS pin. This connection is arguably the most important single connection in the entire PSU system. Avoid running the CS signal traces near to sources of high dv/dt . Provide a simple RC filter as close to the pin as possible to help filter out leading edge noise spikes which will occur at the beginning of each switching cycle.
- SYNC pin. This pin is essentially a digital I/O port. If it is unused, then it may be left open circuit or tied to ground via a 1-k Ω resistor. If Synchronisation is used, then route the incoming Synchronisation signal as far away from noise sensitive input pins as possible.
- OUTA, OUTB, OUTC, OUTD, OUTE and OUTF pins. These are the gate drive output pins and will have a high dv/dt rate associated with their rising and falling edges. Keep the tracks from these outputs as far away from noise sensitive input pins as possible. Ensure that the return currents from these outputs do not cause voltage changes in the analog ground connections to noise sensitive input pins. Follow the layout recommendation for Analog and Power ground Planes in [Figure 45](#).
- VDD pin. This pin must be decoupled to GND using ceramic capacitors as detailed in the 'Power Supply Recommendations' section. Keep this capacitor as close to the VDD and GND pins as possible.
- GND pin. This pin provides the ground reference to the controller. Use a Ground Plane to minimize the impedance of the ground connection and to reduce noise pickup.



Thermal management

PCB cooling strategy

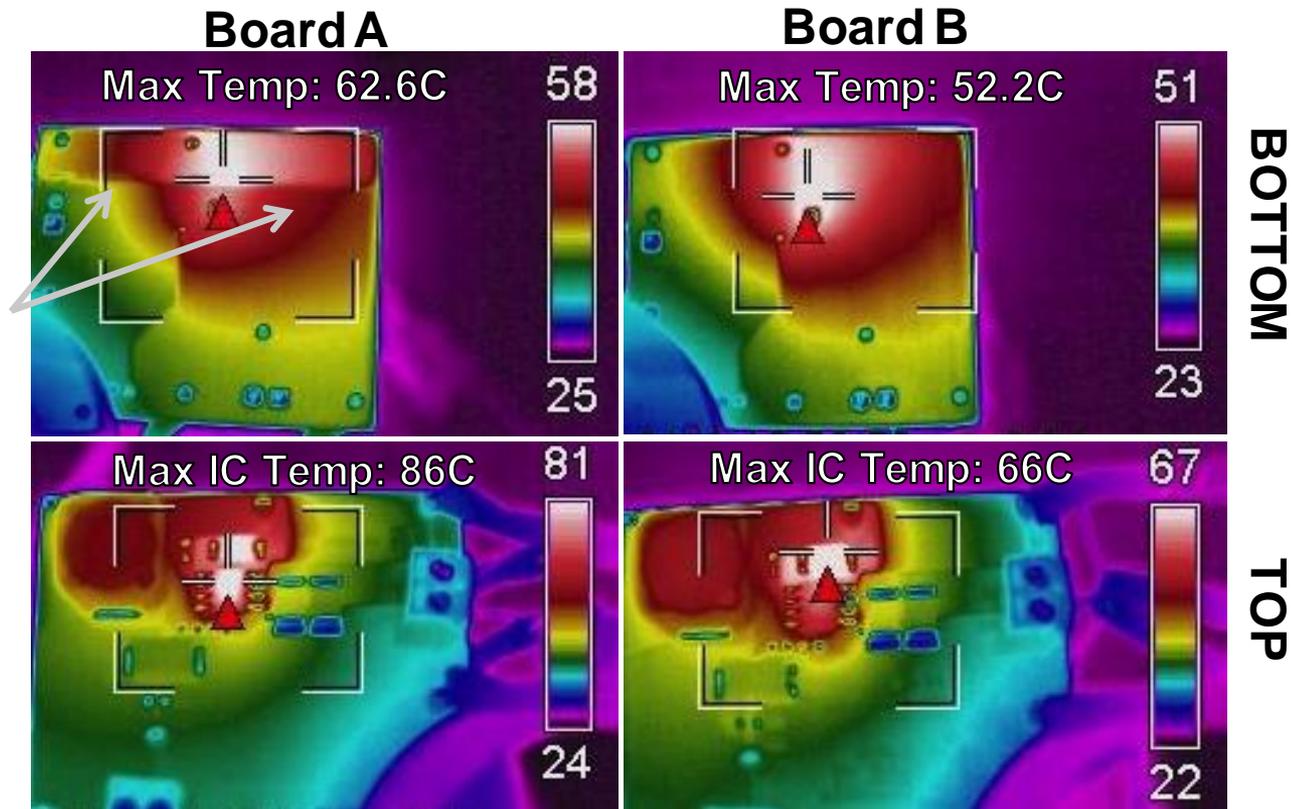
- Have **solid ground planes** to better spread heat across the layer
 - **Avoid breaks in planes** as they substantially degrade lateral heat flow
 - Use **thermal vias** to spread heat to other layers
 - **Thermal pads** help to get the heat out of the IC into the PCB
 - Use both sides of the board to cool
- Maximize the thermal paths with partial pours wherever practical
 - DO NOT use switched node for cooling



Thermal management

Why is Board A hotter than Board B?

- Traces on the bottom layer **prevent heat from spreading** effectively
- **Removing horizontal trace** for a more solid bottom layer reduces IC temp on board B
- Hottest component on B is the catch diode



PCB layout example

Gather information and place large components

Useful information:

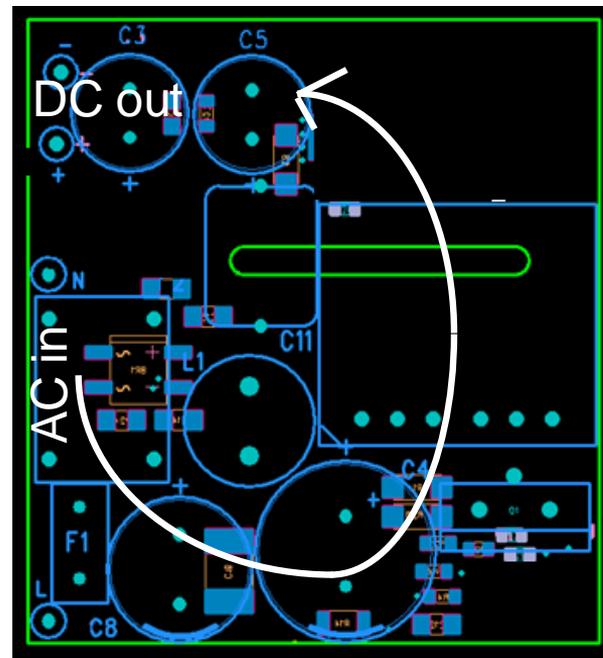
- PCB size and (layers, layer spacing, material)
- Position of inlet and outlet connections
- Mechanical restraints (keep outs and height restrictions)
- Manufacturing process constraints
- Know the creepage and clearance requirements

Understand the circuit:

- High current paths
- High di/dt paths
- High dv/dt nodes
- Hot parts

Imagine a general 'flow'

- Trunk packing algorithm



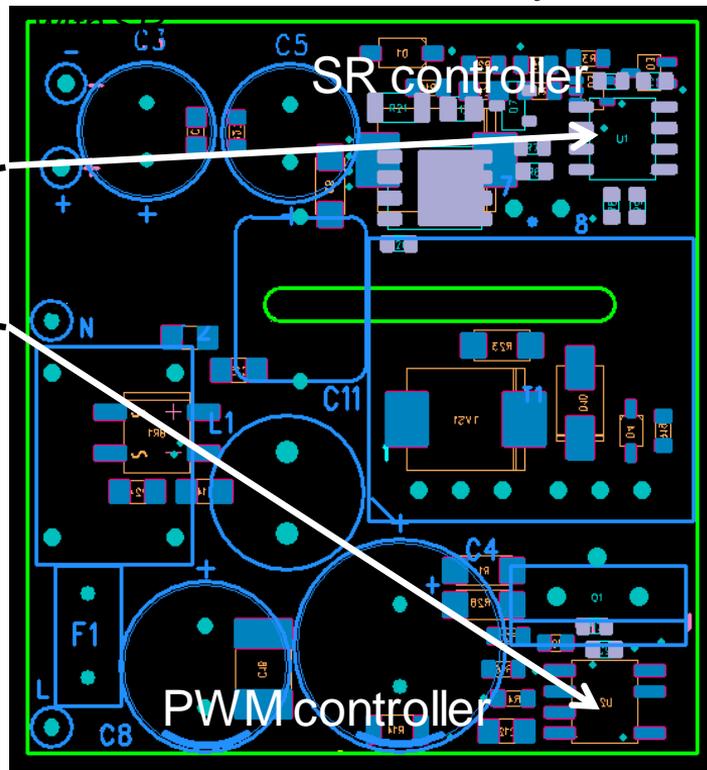
UCC28710/UCC24610 PSR flyback with SR

PCB layout example

Place remaining components

- Place the large parts in the power path first
- Reserve a 'quiet' location for the controller
 - NOT under transformer or node with high dv/dt
 - Place its associated parts nearby
- Reserve an area for the input filter
 - Keep filter input away from output
 - Rotate, reposition, reassign pins, repeat

UCC28710/UCC24610 PSR flyback



PCB layout example

Route power and signal etch

Two layers:

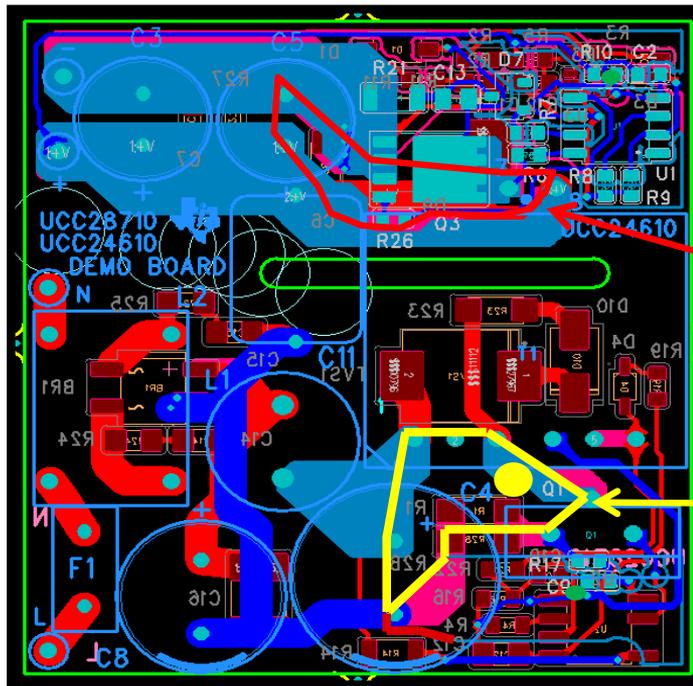
- Bottom layer (red)
- Top layer (blue)

Route power path first

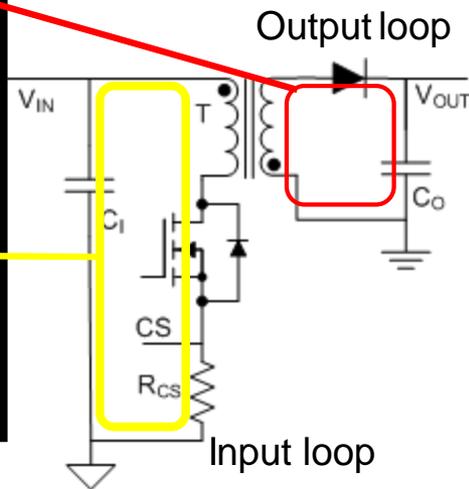
- Use wide etch and polygon pours
- Minimize high di/dt loop area
- Minimize high dv/dt surface area

Route signal etch last

- Keep away from high dv/dt nodes
- Keep noise sensitive etch short
- Shorten return paths



UCC28710/UCC24610 PSR flyback with SR



PCB layout example

Pour ground planes

Flood empty areas:

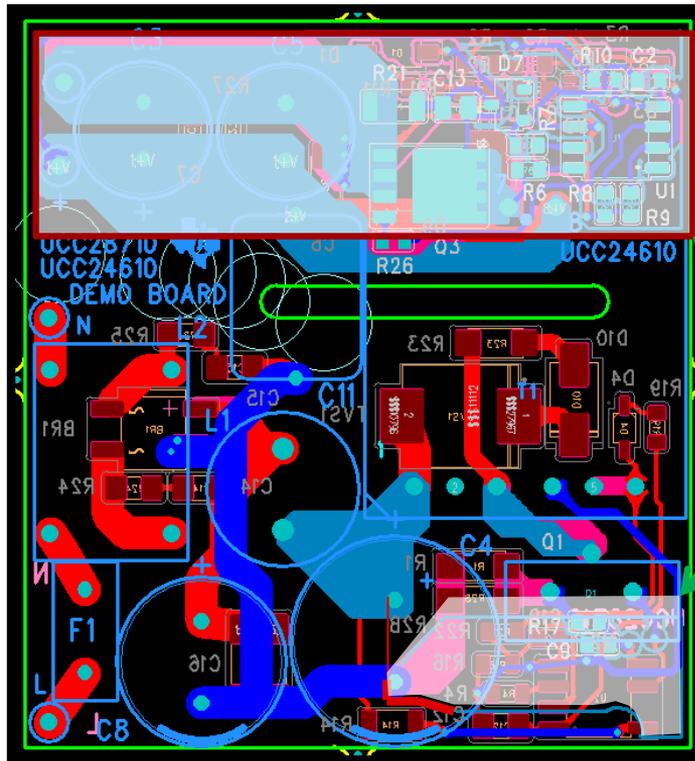
- Primary GND
- Secondary GND

Use vias to connect to GND planes

- Near caps/resistors
- Near GND pins of ICs

Check for blocked GND connections

- Move parts/etch as necessary
- Be mindful of parasitic resistance and inductance



Flood highlighted areas with GND

UCC28710/UCC24610 PSR flyback with SR

Summary: keys to a successful SMPS layout

- Understand your circuit: **high current and di/dt paths, high dv/dt nodes**
- Understand how **parasitic resistance, inductance, and capacitance** are manifested
- Understand how layout can significantly affect **EMI**
- Understand the **safety requirements** for your product
- Understand **how heat is transferred** through the PCB
- Follow a logical procedure:
 - Place large parts, place small parts, power routing, signal routing, pour planes
- Have someone review your layout!

Summary: references

- ***Constructing Your Power Supply - Layout Considerations***; R. Kollman; 2004 TI Power Supply Design Seminar; www.ti.com/seclit/ml/slup230/slup230.pdf
- ***Safety Considerations in Power Supply Design***; B. Mammano and L. Bahra; 2004 TI Power Supply Design Seminar; www.ti.com/seclit/ml/slup227/slup227.pdf
- ***Common Mistakes in DC/DC Converters and How to Fix Them***; P. Shenoy and A. Fagnani; 2018 TI Power Supply Design Seminar; www.ti.com/seclit/ml/slup384/slup384.pdf
- ***Grounding in Mixed-Signal Systems Demystified, Part 1 & Part 2***; S. Pithadia and S. More; 1Q 2013, TI Analog Applications Journal; www.ti.com/lit/an/slyt499/slyt499.pdf; www.ti.com/lit/an/slyt512/slyt512.pdf
- ***Why Should You Count Squares***; Brigitte; 2016 TI Power House Blog; http://e2e.ti.com/blogs_/b/powerhouse/archive/2016/10/03/why-should-i-count-squares

Thank you

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