

# Test and Troubleshoot a Wireless Power Receiver

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#### ABSTRACT

Testing and troubleshooting a wireless power system sometimes is challenging and may take a lot of time. The following application note provides techniques and tricks on how to troubleshoot wireless power related issues and the correct method of testing them.

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### 1 Selecting the Right Device and Component for the Right Application

The right selection of the device, coil, PCB, and components of any application is the first and the most important step in the design cycle of a wireless power system. Any wrong selection of these parts can affect the overall performance of the whole system. For example, selecting the coil inductance value for a 5-W/5-V application affects the overall DC/DC efficiency and thermal performance of the system. Shielding material can significantly affect thermal performance of the receiver, foreign detection of the board, and coupling between the primary and secondary coils. Also, the voltage rating of the components is critical. For example, using a 10 V voltage rating on the resonant capacitors that are connected to AC pins that can go as high as 15 V is a critical mistake. This degrades the lifetime of the capacitor and causes a malfunction of the receiver.

Here are some steps that help to successfully design a wireless power receiver:

- 1. Use the Texas Instrument's evaluation board as a reference without including all the jumpers and the test points that are used for evaluation purposes only.
- 2. Do the same with the layout; follow the evaluation board as much as possible. Use the receiver layout guidelines application notes from the TI website.
- 3. Design RILIM and RTERM for the needed current limit and termination level according to the data sheet equations.
- 4. Design the status pins, as needed, such as WPG, CHG, PD\_DET and so forth. Use the appropriate datasheet for more information on the behavior of these pins.
- Design the TS pin according to the datasheet and R<sub>NTC</sub> used. Help is available using the calculation tools provided on the TI website.
- 6. Start with the default resonant caps in the EVM (Cs and Cd), then tune with the final configuration of the board and the selected coil and shielding, according to WPC.
- 7. Use the right voltage rating for the Cs, Cd, C<sub>RECT</sub>, C<sub>COMM</sub>, C<sub>BOOT</sub>, C<sub>CLAMP</sub>, and C<sub>OUT</sub>. The voltage ratings are provided in the EVM user's guide and/or the datasheet.
- 8. Use good tolerance resistors as recommended by the user guide of the corresponding evaluation board.
- Initially use the default values from the EVM as starting RFOD and ROS values. After building the board, these values need to be tuned according to WPC requirement for foreign object detection (FOD).
- 10. It is always a good idea to use two place holders in series for RFOD and ROS on the initial layout (RFOD is highly recommended). This should provide more flexibility to use non-standard values after FOD calibration is performed. Contact the TI sales office for details regarding the FOD calibration process.
- 11. The TI RX EVM user's guides generally provide a list of verified coils for that EVM. This is usually a good place to start for coil selection. For example, the bq51013BEVM-764 shows 3 coils that have been verified as functional. Note that many other coils can be used as well. For additional information, investigations can be done into different inductor wire types (single wire, bifilar, and Litz wire). The shape and physical size of the selected coil may need to be chosen based on the end-application requirements. Some applications may benefit from a coil made into a PCB these tend to be less efficient but can offer other benefits.
- 12. Always remember that metals surrounding the secondary coil can affect the coupling, efficiency, FOD and the overall performance of the system.
- 13. A layout guidelines application report (<u>SLUA710</u>) is published on the web (<u>www.ti.com/wirelesspower</u>); follow the instructions for best performance and good layout design.

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## 1.1 Troubleshooting Step by Step

Troubleshooting the RX with a known good TX, what to look for on the RX?

### 1.1.1 Steps During Start Up

STRUMENTS

- 1. Place RX on TX in WPC—analog ping from TX changes by at least 10%, signaling that a receiver is on the charging pad.
- 2. Now use digital ping to identify-digital ping is a 70-ms pulse at 175 kHz.
- 3. This powers up the RX. It sends out signal strength packet, identification packet, and configuration packet.
- 4. RX to TX communications are good—TX moves to power transfer phase.
- V<sub>RECT</sub> voltage must be between approximately 7 V to 8 V to enable 5-V internal LDO– The RX will send Control Error packets to tune TX operating point to generate approximately 8 V at Vrect. See Figure 1 for an example of start up on the bq51020 receiver.
- 5-V LDO output enabled—once V<sub>RECT</sub> has reached approximately 8 V, the LDO is enabled and voltage is applied to the load. V<sub>RECT</sub> will drop but should stay above LDO drop out of 5.1 V to 5.2 V, depending on the load and current limit.
- 7. RX then sends Control Error Packets (EPT) to tune the operating point to match load.

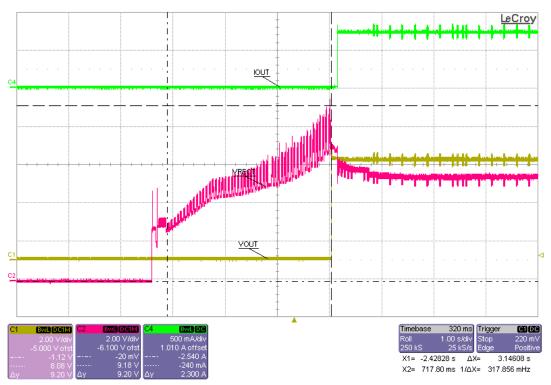


Figure 1. Good Start-Up Sequence Using the bq51020

- 8. In a PMA system, the startup sequence is different from WPC.
- 9. The rectification voltage comes up immediately after the digital pings from the PMA Type 1 transmitter.
- 10. Next is the stabilization period, then RXID message, with the Guard Time following after.
- 11. The Guard Time is used to give some time to the PMA Type 1 TX to calculate CRC and validate the received RXID.
- 12. The required start up time for PMA Type 1 TX should be less than 1 second. It should be measured from the first digital ping to the time  $V_{OUT}$  opens up.



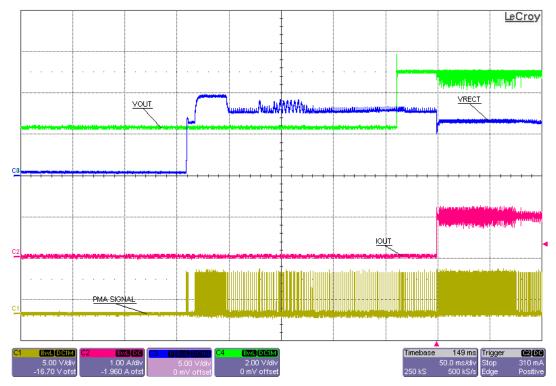


Figure 2. Good Start Up Sequence in PMA

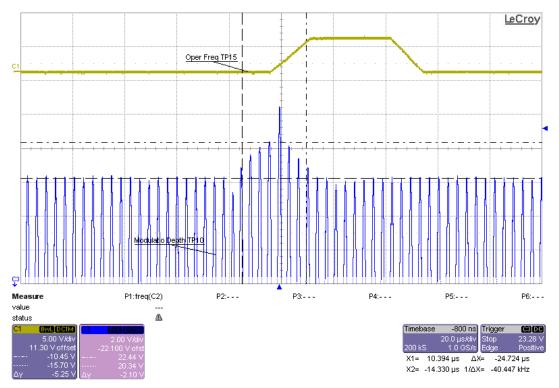
#### 1.1.2 Troubleshooting After Start Up

- Ripple on the output voltage:
  - Increase the output and/or the RECT cap, this helps absorb some ripples.
  - Reduce the output trace length; this reduces picking up noise, voltage drops, and parasitic inductance issues.
  - Input cap of the upstream charger, make sure they are designed properly—the cap value, the voltage rating of the cap, and layout (distance from the pin of the IC) need to be designed properly.
  - Sometimes the ripple at the output voltage is caused by the communication current limit feature of the receiver IC. If this feature is enabled, it limits the current to a certain level during communication. Thus, the output voltage drops to VIN-DPM of the charger. If this behavior is not desired, disable the communication limit feature of the receiver. The communication current limit is useful for noisy load systems and helps robust communication.
- Bad load transients
  - Make sure to have a VIN-DPM of the battery charger
  - Use LPRB in the bq51221 to help better load transients
  - Increase the output cap, as possible (as necessary and possible)
  - Check the coil inductor and see if designed properly—coil manufacturers should be able to advise for proper coil value for the needed application. For example, dual mode (PMA and WPC) application requires less coil inductance than a WPC-only system. Higher output voltage requires higher inductance too.

TEXAS INSTRUMENTS

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- Modulation depth
  - If a modulation depth does not meet the requirement for PMA and/or WPC, increase the communication cap values. If the communication pocket in WPC-only system is too high, reduce the COMM caps. 22 nF to 100 nF is the recommended range.
  - Check if the voltage rating on the caps is as recommended by the datasheet or the user's guide of the part (mostly, at least 25 V is required).
  - Make sure the COMM caps are placed as close to the IC as possible and not corrupted by noisy traces.
  - A good PMA modulation depth plot is shown in Figure 3.



### Figure 3. Modulation Depth in PMA System

- Triggering overvoltage protection (OVP) of the RX during start up or during load transients
  - The coil inductor is too high and causes the rectifier voltage to overshoot to 15 V during startup or during load transients
  - Reduce the inductor for better transient response for this case
  - Reducing the coupling also helps
- OVP on the upstream charger is triggered
  - Increase the OVP level of the charger
  - If possible, reduce the  $V_{\text{OUT}}$  level of the receiver
  - Increase the output caps of the receiver and/or the input cap of the charger



- Saturation and weak coil issues
  - To confirm that the coil is saturating, measure the transmitter operating frequency. If the frequency is near the minimum of operating frequency range, then the RX coil is saturating or weak. Usually, under this condition the coil is not able to deliver full load power.
  - To fix this, the shielding needs to be improved to increase the mutual inductance of the system
  - Increase the inductance of the coil
  - Change the shape and the size of the coil, including reducing the Z distance between the RX and TX coils
- Soldering issues
  - We have seen this before, some customer issues are happening due to bad soldering of some components in the board.
  - Try to use different boards when debugging to avoid this issue
  - Use common sense and eye inspection, if possible, to avoid this situation; otherwise hours of debugging will be spent for a simple bad connection of the component on the board.



## 2 Efficiency Check

Compare the efficiency number with the datasheet and the data provided in the user guide. There are two types of efficiency commonly measured in wireless power systems:

- 1. DC/DC efficiency checks for the whole system (from the DC input of the TX to the DC output of the RX)
- 2. AC/DC efficiency checks only the receiver side (AC input of the secondary coil to DC output of the RX)
  - Efficiency =  $P_{OUT} / P_{IN} = \{I \times V(DC)\} / \{I_AC \times V_AC \times cos(\phi)\}$

## 2.1 How to Measure AC/DC Efficiency

- $P_{OUT} = V_{OUT} \times I_{OUT}$
- Both V<sub>OUT</sub> and I<sub>OUT</sub> are DC, easy to measure
- A multimeter can be used to measure both

## Output Current and Out Voltage Measurements



Figure 4. Pout Measurement

Efficiency Check



- $P_{IN} = V_{IN}(AC) \times I_{OUT}(AC)$ 
  - Measure  $I_{\mbox{\scriptsize IN}}$  using current probe in the coil connector
  - Measure  $V_{IN}$  using voltage probe, the GND of the probe to AC1 and positive of the probe to AC2
  - Use a low-noise current probe as shown in Figure 5

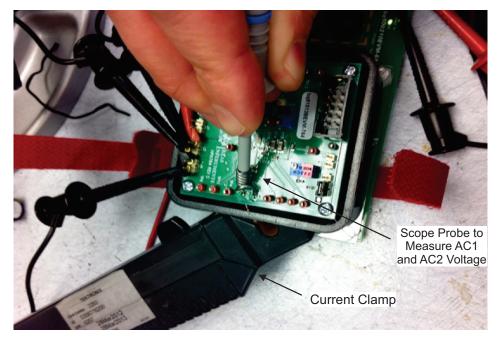


Figure 5. AC Input Power Measurements

- Calculate the product between the two measurements using the scope itself. There is a math function in the scope, using the product of the two channels.
- Calculate the mean between the resulted data after the product on the scope
- Next, read the measurements directly from the scope
- Perform the efficiency calculation for different loads
- Other methods can be used to do the AC/DC efficiency



### 3 Thermal Issues

One of the main reasons for thermal issues on the board is bad layout. Make sure that power balls of the IC are connected to as much copper as possible in the WCSP package. Use power ground for power dissipation to spread out the heat on a bigger copper surface.

Thermal Issues

Here are some other concerns when doing layout of a custom receiver PCB:

- AC1 and AC2 trace resistance and width, losses on the trace will decrease thermal performance
- OUT trace resistance
- Good GND connection for thermal dissipation
- COMM, CLAMP, BOOT capacitors connections
- Use QFN package, if possible.
- Copper weight (> 2 oz)
- Number of layers, higher is better for thermal dissipation and flexibility

In addition to layout, a proper shielding of friendly objects is needed. Friendly objects are the metal objects inside belonging to the end product. For example, in a smart phone there is battery frame, USB connector, camera, and so forth. These objects are made of metal and are located close enough to the coil, they can absorb the magnetic flux. Any friendly metals closer to the flux field will absorb some of the transmitted energy from the primary side. The energy is then transferred into heat and heats up the board over time.

## 4 Foreign Object Detection (FOD) Check

Foreign objects are any metal objects outside and not belonging to the end product such as car keys, coins, and any other metals. These metals are close enough to the magnetic flux, they can absorb the energy transmitted by the primary coil, therefore they heat up. As part of WPC1.1 requirements, foreign object temperature is limited and must be controlled. One of the methods to limit temperature rise of foreign objects is to monitor and control the power losses from the transmitter to the receiver to foreign objects during power transfer. This feature is called foreign object detection (FOD). If triggered, it may cause abnormal behavior.

The following steps can be used to troubleshoot:

- 1. If a WPC 1.1 transmitter is used and the receiver is not tuned for FOD yet. Disable FOD on TX before testing.
- 2. The following symptoms indicate FOD:  $V_{OUT}$  should be fluctuating and starts providing nearly 5 W, then drops to no output and will retry.
- 3. FOD calibration should be performed on the final configuration.
- 4. If FOD calibration is performed on RX, any changes on the RX board will affect the calibration and has to be done again.

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