# MSPM0 Sensorless FOC Tuning



#### **ABSTRACT**

This tuning user's guide provides step-by-step guidance to set up an MSPM0 MCU and supported DRV hardware board to tune a 3-phase brushless DC motor.

#### Note

This document is in reference to the Sensorless FOC v2.04 from SDK Version **2.04.00.00** and above.

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Introduction www.ti.com

#### 1 Introduction

The MSPM0Gxxx family of 80MHz Arm® Cortex®-M0+ MCUs can commutate a 3-phase brushless DC (BLDC) motor with sensorless FOC control. The BLDC motor is driven by a three-phase brushless DC (BLDC) MOSFET gate driver or integrated MOSFET motor driver at nominal DC rails or battery-pack voltages. The driver typically integrates three current-sense amplifiers (CSAs) for sensing the three-phase currents of BLDC motors to achieve optimum FOC control.

Figure 1-1 shows a simplified schematic of an MSPM0Gxxx MCU and BLDC motor driver.

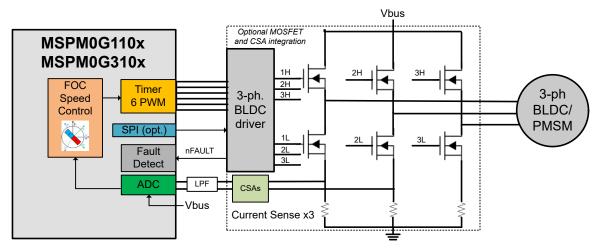


Figure 1-1. Simplified Schematic of MSPM0Gxxx + BLDC Motor Driver

This tuning guide provides the steps to tune a 3-phase BLDC motor using an MSPM0Gxxxx MCU. The tuning process is classified into four sections: **Hardware Setup, Software Setup, Basic Tuning** and **Advanced Tuning**.

- Hardware setup: Steps to set up TI-provided hardware or use a custom PCB for the tuning process.
- Software setup: Steps to set up TI-provided software for spinning and tuning a BLDC motor.
- GUI setup (optional): Steps to use a graphical user interface (GUI) for spinning & tuning a BLDC motor.
- Basic tuning: Tuning steps to successfully spin the motor in closed loop.
- · Advanced tuning: Tuning steps to conform to use-case and explore features in the device.

#### 2 Hardware Setup

The following items are required to use this tuning guide:

- LP-MSPM0G3507/LP MSPM0G3519 board
- Supported DRV83xx motor driver evaluation module (EVM)
  - BOOSTXL-DRV8323RS
  - DRV8316REVM
  - BOOSTXL-DRV8329
- Jumper wires for pin table connections
- · A computer with the MSPM0 FOC software installed
- A BLDC motor to be tuned using this process. The motor data sheet is helpful but not mandatory.
- A DC power supply rated for the motor
- Basic lab equipment such as a digital multimeter (DMM), oscilloscope, current probe, and voltage probe

Figure 2-1 shows the block diagram connections for a sensorless FOC motor system. The system can be built using:

- TI-provided hardware (LP-MSPM0G3507/LP-MSPM0G3519 and DRV83xx EVM)
- Custom PCB hardware with an onboard MSPM0Gxxx MCU and a BLDC motor driver

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The following sections describe how to configure the pins for each portion of Figure 2-1.

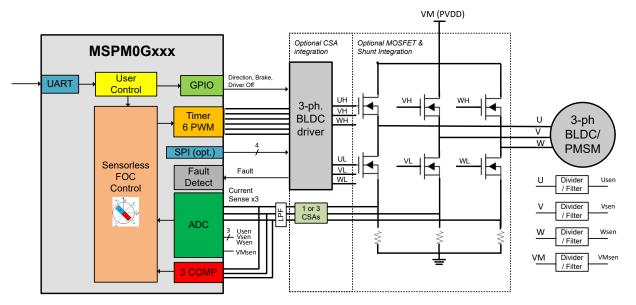


Figure 2-1. MSPM0Gxxx + BLDC Motor Driver - Sensorless FOC Block Diagram

The System Configuration tool (SysConfig) helps to configure the pins in a motor control system. The default pin configurations are provided for the EVM hardware setup to spin a motor, but pins can be remapped to other pins visually inside SysConfig. This is useful for reconfiguring different pins (such as PWM, ADC, or other control signals) on a custom PCB or for scaling to different packages across MSPM0 devices.

#### 2.1 EVM Hardware Setup

TI provides LaunchPad<sup>™</sup> development kits to evaluate MSPM0 Arm Cortex-M0+ microcontrollers and evaluation modules (EVMs) to evaluate the DRV83xx family of brushless-DC motor drivers. These evaluation boards are available on ti.com and can be used as a system evaluation platform for sensorless FOC motor control.

For supported evaluation boards, refer to Section 2.1.1.

#### Note

The provided defaults have pre-configured pins that are intended to support hardware evaluation boards. If a custom PCB is used, refer to the following *Pin Configurations* sections to assign the supported pins for the 3-phase motor driver.

### 2.1.1 EVM Hardware Support

Table 2-1 shows the supported MSPM0 LaunchPad kits and EVMs and the connection guides for 3-phase sensorless FOC motor control.

Table 2-1. Supported Hardware for Sensorless FOC Using MSPM0

MSPM0Gxxx LaunchPad™ Kit	Motor Driver Hardware	Hardware User's Guide	Current Sense Amplifiers	SPI Driver Support	Recommended Motor Voltage Range	Recommended Motor Power
LP-MSPM0G3507	BOOSTXL-	BOOSTXL-DRV8323Rx	3	Yes	6V to 60V	< 1000W
LP-MSPM0G3519	DRV8323RS	EVM User's Guide	3	3 Yes	0 10 00 0	< 1000VV
LP-MSPM0G3507	DRV8316REVM	DRV8316REVM User's	3	Yes	4.5V to 35V	< 80W
LP-MSPM0G3519	DICCOSTORECTION	Guide	3	163	4.50 to 550	< 60VV
LP-MSPM0G3507	DRV8329EVM	DRV8329AEVM User's	1	No	4.5V to 60V	<1000W
LP-MSPM0G3519	DRV6329EVIVI	Guide	Į.	INO	4.50 10 000	<1000VV
MSPM0G1507	TIDA-010250 Reference Design	TIDA-010250 Design Guide	1, 2, 3	No	265V maximum AC supply	<1000W

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#### Note

Make sure that the jumper configurations for the LaunchPad kit and EVM are correct. For more information, see the user's guides for the LaunchPad kit and EVM.

#### 2.2 Pin Configurations for PWM Outputs

The default pin configurations for PWM outputs are shown in Table 2-2. The required connections are six PWM output signals that send the commutation patterns for sensorless FOC motor control. TIMA includes features for motor control, such as complimentary PWM outputs with deadband, fault handling with <40ns response time, and repeat counters for configuring FOC loop rates.

TIMA0 is the preferred timer for motor control because it provides three complimentary pairs of PWM outputs from the same timer counter (such as TIMA0\_C1 and TIMA0\_C1N), but any TIMA0 or TIMA1 output pair can be used and cross-triggered to provide the six PWM output signals.

**Table 2-2. Pin Configurations for PWM Outputs** 

MSPM0 Pin	Function	DRV Connection	DRV Function
TIMA0_C0	TIMA0 channel 0 output pin	INHA	Phase A high side PWM input
TIMA0_C0N	TIMA0 channel 0 complimentary output pin	INLA	Phase A low side PWM input
TIMA0_C1	TIMA0 channel 1 output pin	INHB	Phase B high side PWM input
TIMA0_C1N	TIMA0 channel 1 complimentary output pin	INLB	Phase B low side PWM input
TIMA0_C2	TIMA0 channel 2 output pin	INHC	Phase C high side PWM input
TIMA0_C2N	TIMA0 channel 2 complimentary output pin	INLC	Phase C low side PWM input

#### 2.3 Pin Configurations for ADC Currents

**ADC configuration for three phase current sensing:** The default pin configurations for ADC currents for three phase current sensing are shown in Table 2-3 and Table 2-5, depending on the DRV device used. The required connections are three ADC inputs connected to the three CSA outputs from the motor driver or external CSAs.

ADC0 and ADC1 are two simultaneous-sampling 4Msps analog-to-digital converters that are used to measure phase currents and voltages. ADC0 and ADC1 measure phase currents simultaneously and bus voltage sequentially depending on the rotor angle under normal motor run conditions.

An optional low-pass RC filter can be placed in series from the CSA outputs to the ADC inputs to filter out any high-frequency noise from the switching output signals for proper ADC sampling as shown in Figure 2-2.

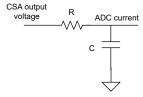


Figure 2-2. CSA Output Filter

Choose a filtering frequency  $f_c$  that it at least 10 times the PWM switching frequency ( $f_{PWM}$ ). Use Equation 1 to calculate  $f_c$  based on the RC filter design.

$$f_{c} = \frac{1}{2\pi RC} \tag{1}$$

Table 2-3. Pin Configurations for ADC Currents With Simultaneous Sampling in DRV8316 - LP\_MSPM0G3507

MSPM0 Pin	Function	DRV Connection	DRV Function
A0_3	ADC0, channel 3 input	SOA	Phase A current sense output
A0_2	ADC0, channel 2 input	SOB	Phase B current sense output
A1_2	ADC1, channel 2 input	SOB	Phase B current sense output
A1_1	ADC1, channel 1 input	SOC	Phase C current sense output

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Table 2-4. Pin Configurations for ADC Currents With Simultaneous Sampling in DRV8316 - LP MSPM0G3519

MSPM0 Pin	Function	DRV Connection	DRV Function
A1_13	ADC1, channel 13 input	SOA	Phase A current sense output
A1_14	ADC1, channel 14 input	SOB	Phase B current sense output
A0_12	ADC0, channel 12 input	SOB	Phase B current sense output
A0_2	ADC0, channel 2 input	SOC	Phase C current sense output

Table 2-5. Pin Configurations for ADC Currents Without Simultaneous Sampling in DRV8323 - LPMSPM0G3507

MSPM0 Pin	Function	DRV Connection	DRV Function
A1_2	ADC1, channel 2 input	SOA	Phase A current sense output
A0_3	ADC0, channel 2 input	SOB	Phase B current sense output
A1_3	ADC1, channel 3 input	SOC	Phase C current sense output

Table 2-6. Pin Configurations for ADC Currents Without Simultaneous Sampling in DRV8323 - LPMSPM0G3519

MSPM0 Pin	Function	DRV Connection	DRV Function
A1_13	ADC1, channel 2 input	SOA	Phase A current sense output
A1_14	ADC0, channel 2 input	SOB	Phase B current sense output
A0_4	ADC1, channel 3 input	SOC	Phase C current sense output

**ADC configuration for single shunt current sensing:** The ADC pin configurations for single shunt current sensing in DRV8329 is shown in ADC Pin Configuration for Single Shunt Current Sensing in DRV8329 - LP MSPM0G3507.

In single shunt current sensing either of ADC0/ADC1 is used to sample the same shunt current at two different instances in a single PWM cycle to estimate the three phase currents. User need to configure appropriate ADC to sample the Currest sense output from the Memory '0' index, Memory '1' Index for FOC operation. Refer to the Sensorless FOC User Guide for details on ADC cufigurations for Single shunt current sensing.

Table 2-7. ADC Pin Configuration for Single Shunt Current Sensing in DRV8329 - LP\_MSPM0G3507

MSPM0 Pin	Function	DRV Connection	DRV Function
A1_2	ADC 1, Channel 2 Input	SOX	DC bus current sense

Table 2-8. ADC Pin Configuration for Single Shunt Current Sensing in DRV8329 - LP MSPM0G3519

MSPM0 Pin	Function	DRV Connection	DRV Function
A1_14	ADC 1, Channel 14 Input	SOX	DC bus current sense

# 2.4 Pin Configurations for IPD Usage

Initial Position detection algorithm utilizes the ADC current sensing path to identify the phase current rise times to detect the rotor position. The window comparators of ADC continuously monitor the phase current against a pre-set IPD threshold current limit to create a current Pulse. A Timer is used to capture these various pulse rise times across different sectors and compared against to detect the rotor position. The Timer and ADC configurations are updated during the IPD initialization based on the Sysconfig. The algorithm configures the required WCOMP settings based on the current sense selected and Sense Amplifier configurations.

#### Note

During IPD pulse time, the rest of the algorithm interrupts are halted to continuously monitor the ADC current at very high sampling rates. The normal interrupt operation resumes once the IPD operation is complete.

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#### 2.5 Pin Configurations for ADC Voltages

The default pin configurations for ADC voltages are shown in the following tables. The required connections are four ADC inputs:

- Three ADC inputs connected to the three sensed phase voltages from the motor (VSENA, VSENB, VSENC)
- One ADC input connected to the sensed VM motor voltage (VSENVM)

The sensed voltages are realized using a resistor divider with an optional bypass filtering cap as shown in Figure 2-3. Size the resistors so any motor voltage transients do not exceed the maximum voltage of the ADC inputs. For more information on the resistor divider ratio, see Section 6.1.6.

#### Note

Phase voltage sensing is needed only if initial speed detection feature is required.

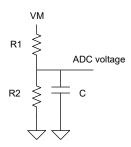


Figure 2-3. ADC Voltage Divider

### Table 2-9. Pin Configurations for ADC Phase Voltages DRV8316/DRV8329 /DRV8323- LP MSPM0G3507

MSPM0 Pin	Function	DRV Connection	DRV Function
A1_6	ADC1, channel 6 input	VSENA	Phase A sensed voltage output
A0_7	ADC0, channel 7 input	VSENB	Phase B sensed voltage output
A1_5	ADC1, channel 5 input	VSENC	Phase C sensed voltage output

#### Table 2-10. Pin Configurations for ADC Phase Voltages DRV8316/DRV8329 /DRV8323- LP MSPM0G3519

MSPM0 Pin	Function	DRV Connection	DRV Function
A0_0	ADC0, channel 0 input	VSENA	Phase A sensed voltage output
A0_1	ADC0, channel 1 input	VSENB	Phase B sensed voltage output
A0_5	ADC0, channel 5 input	VSENC	Phase C sensed voltage output

#### Table 2-11. Pin Configurations for ADC DC Bus Voltage Sensing for DRV8316/DRV8329 - LPMSPM0G3507

		<u> </u>	
MSPM0 Pin	Function	DRV Connection	DRV Function
A1_3	ADC1, channel 3 input	VSEN -Vm	DC bus voltage output

#### Table 2-12. Pin Configurations for ADC DC Bus Voltage Sensing for DRV8316/DRV8329 - LPMSPM0G3519

		<u> </u>	
MSPM0 Pin	Function	DRV Connection	DRV Function
A0_4	ADC0, channel 4 input	VSEN -Vm	DC bus voltage output

#### Table 2-13. Pin Configurations for ADC DC Bus Voltage Sensing for DRV8323 and LP\_MSPM0G3507

MSPM0 Pin	Function	DRV Connection	DRV Function
A0_2	ADC0, channel 2 input	VSEN -Vm	DC bus voltage output

#### Table 2-14. Pin Configurations for ADC DC Bus Voltage Sensing for DRV8323 and LP\_MSPM0G3519

MSPM0 Pin	Function	DRV Connection	DRV Function
A0_12	ADC0, channel 12 input	VSEN -Vm	DC bus voltage output

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#### 2.6 Pin Configurations for Faults

The default pin configurations for faults are shown in Table 2-15. Faults can be detected in hardware by the motor driver or MCU.

Typically, a motor driver drives an active-low open-drain fault pin (nFAULT) when there is a detected fault in the system. Examples are MOSFET overcurrent, gate drive, or power supply-related faults connections in the driver.

MSPM0 MCUs can detect fault inputs with dedicated hardware paths to provide low latency and response times as fast as 40ns. This is faster than using a conventional GPIO interrupt with software latency. The fault input paths can be configured for fault handling using TIMA fault handler, such as shutting off the PWMs during an overcurrent condition. Examples of TIMA inputs include an external fault pin (such as TIMA\_FLT0) and low-side overcurrent using comparators (such as COMP0\_IN0+).

**Table 2-15. Pin Configurations for Faults** 

MSPM0 Pin	Function	DRV Connection	DRV Function
TIMA0_C2	TIMA0 channel 2 input pin	nFAULT	Open-drain, active-low fault pin

# 2.7 Pin Configurations for GPIO Output Functions

Many GPIO output functions from the MSPM0 can be used for motor driver specific functions controlled by logic-level pins. Examples of motor driver functions are:

- Enable pin (ENABLE) / active-low sleep mode control (nSLEEP)
- Active high gate driver shutoff (DRVOFF)
- Active-high CSA Calibration (CAL)
- Active-high brake (BRAKE) / active-low brake (nBRAKE)
- Direction pin (DIR)

#### Note

See the motor driver data sheet and the user guide for GPIO configurable pins.

#### 2.8 Pin Configurations for SPI Communication

The default pin configurations for SPI connections are shown in Section 2.8. Some motor drivers include an optional SPI that is used for configuring control registers and reading status registers for fault diagnosis. Some examples of SPI registers are:

- · Configuring gate drive source/sink current strength
- Configuring CSA output behavior
- Running diagnostics
- · Reading fault bits when the fault pin has been detected as active low
- Clearing fault status bits once the fault condition is removed
- · Clearing watchdog timers

#### Note

If a SPI or hardware interface is used to configure system settings, see the motor driver devicespecific data sheet.

Table 2-16. Pin Configurations for SPI Connections

MSPM0 Pin	Function	DRV Connection	DRV Function
SPIx_CSy	SPI chip select (y = 0,1,2,3)	nSCS	SPI chip select
SPIx_SCK	SPI clock	SCLK	SPI clock
SPIx_POCI	SPI peripheral out controller in	SDO	SPI data out
SPIx_PICO	SPI peripheral in controller out	SDI	SPI data in

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#### Note

To determine if the SDO pin is open-drain and requires a pullup resistor, see the motor driver device-specific data sheet.

# 2.9 Pin Configurations for UART Communication

UART can be used to receive commands to configure, spin, and control the motor. The commands are sent from a host MCU or GUI and can optionally be used for advanced protocols such as LIN communication.

#### Note

Use UART instance 0 (UART0\_RX, UART0\_TX) to configure the UART interface when used along with DMA and LIN interface.

#### Note

Use UART instance 3 (UART3\_RX, UART3\_TX) to configure the UART interface for GUI communication when used along with DMA.

# Table 2-17. Pin Configurations for UART Connections

MSPM0 Pin	Function
UARTx_RX	UART receive
UARTx_TX	UART transmit

#### 2.10 External Connections for Evaluation Boards

Follow the steps below when connecting an MSPM0 LaunchPad to a DRV83xx EVM:

- 1. Connect the three motor phase terminals to the driver board (phases A, B, and C). If the motor has a center tap connection or wires for Hall-effect sensors, leave these wires unconnected.
- Make the inter-device connections from the MSPM0 LaunchPad kit to the DRV83xx EVM by mating the EVM to the LaunchPad kit or using jumper wires as shown in Figure 2-4. For hardware user's guide connection details, see Section 2.1.1.

#### **Note**

If using the GUI to communicate to the MSPM0 device using USB to backchannel UART, connect the backchannel UART connections to UART3\_TX and UART3\_RX as shown in Figure 2-5.

- 3. Connect a micro-USB cable from the MSPM0 LaunchPad kit to the PC.
  - a. Remove GND and 3V3 isolation jumpers on the bridge if desired to isolate the PC from the motor system. If this step is done, 3V3 must be provided externally or from the DRV83xx EVM board, if available.
- 4. Supply a voltage compliant with the Power Supply Voltage (VM) range. For the recommended voltage range, see the board-specific user's guide or DRV-specific data sheet.

www.ti.com Hardware Setup

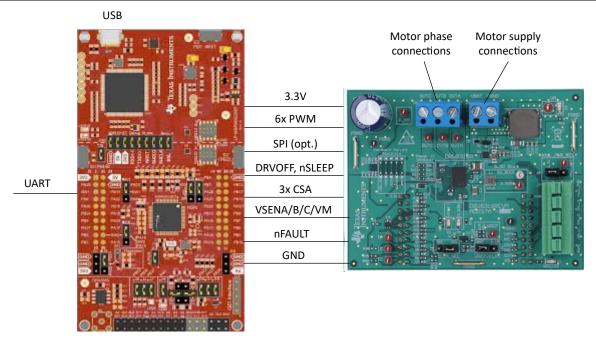


Figure 2-4. MSPM0 LaunchPad Kit and DRV83xx EVM External Configuration

Hardware Setup www

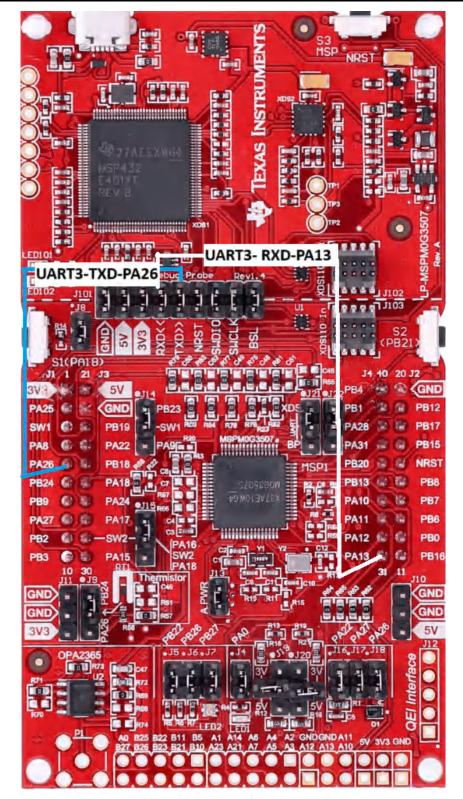


Figure 2-5. LP-MSPM0G3507 Backchannel Connection to UART3

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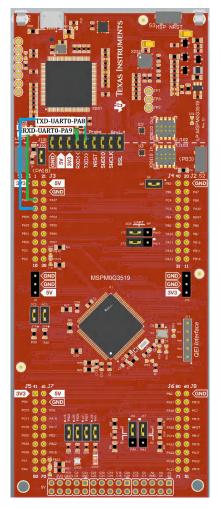


Figure 2-6. LP-MSPM0G3519 Backchannel Connection to UART0

#### Note

If a different UARTn port is used to connect the serial pins, configure appropriate UART instance pins in the SYSCONFIG file of the CCS project.

Software Setup Www.ti.com

## 3 Software Setup

Sensorless FOC software examples for MSPM0 MCUs are provided inside MSPM0-SDK and is available for evaluation with Code Composer Studio™ (CCS) IDE.

Table 3-1 shows the software and documentation supported for Sensorless FOC control in TI Resource Explorer.

**Table 3-1. Software Support for FOC Control** 

Sensorless FOC User's Guide <sup>(1)</sup>	Code Examples	GUI
Sensorless FOC User's Guide	Sensorless FOC Examples	MSPM0G Sensorless FOC GUI

<sup>(1)</sup> Includes library overview, software setup, hardware setup, and more.

# 4 GUI Setup

The user can optionally use the MSPM0 Sensorless FOC GUI as a host to send commands to the MSPM0 MCU at the target to control the motor using serial to UART interface as described in UART COMMUNICATION USER GUIDE.

The GUI contains a USB-to-UART codec that can send UART commands as a host to the MSPM0 LaunchPad kit. The application software includes a configurable UART register map and data format that translates the UART data into simplified motor control commands.

**Table 4-1. GUI Connection Types** 

Connection	Interface	Hardware Connections
GUI to target MSPM0 MCU	UART	UART3_TX, UART3_RX

To launch the GUI, go to the MSPM0 Sensorless FOC GUI. page.

#### 4.1 Serial Port Configuration

Configure the serial port based on the connected port to the PC and configure the Baud rate as 115200.



Figure 4-1. Option to Select Serial Port Configuration

ww.ti.com GUI Setup

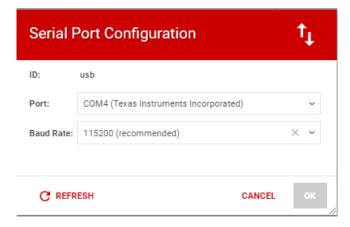


Figure 4-2. Serial Port Settings

## 4.2 GUI Home Page

Below is the GUI home page from which user can navigate to various windows for specific configurations.

# 4.3 System Configurations

User can set the basic configurations of Motor and EVM system parameters from the system configuration page.

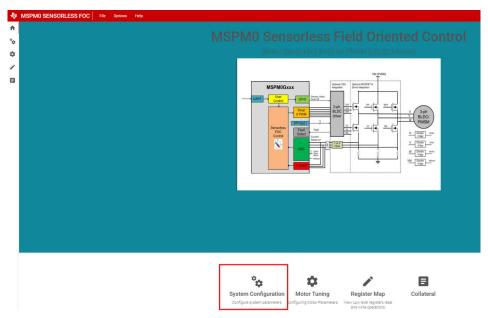


Figure 4-3. Option to Select System Configurations

GUI Setup www.ti.com

## 4.4 Register Map

Register Map page contains the configurations for all the available Motor Tuning parameters that can be configured before starting the Motor. Register map page also contains the Status variables, which can be continuously monitored.

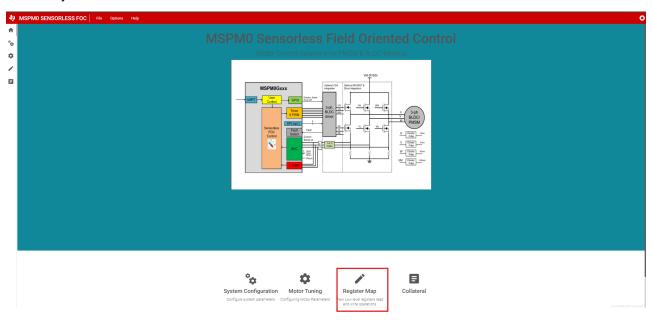


Figure 4-4. Option to Select Register Configurations

# 4.5 Motor Tuning Page

User can set the speed command and monitor the motor status and fault variables from this window.

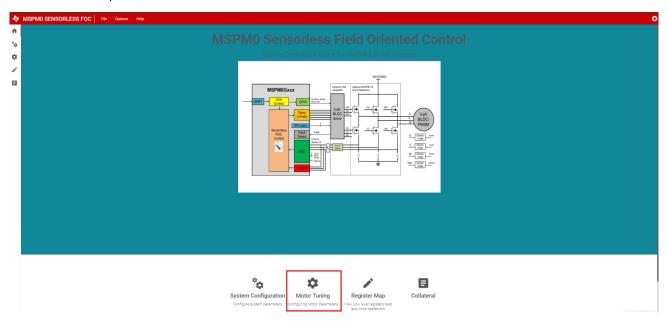


Figure 4-5. Option to Select Motor Tuning Configurations

www.ti.com GUI Setup

#### 4.6 Collateral Page

This page holds the links to various user guides to set up the software and migrate to different platforms.

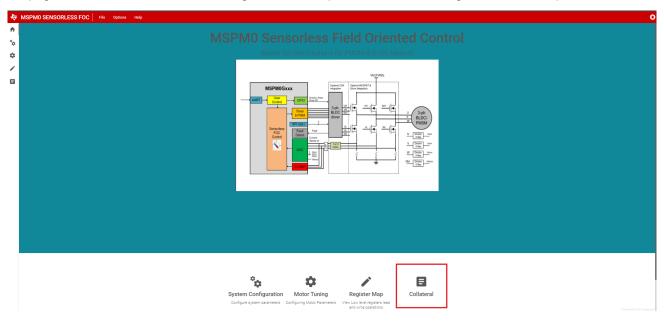


Figure 4-6. Option to select Collateral page

## 4.7 Loading and Saving register Configurations

Once the desired tuning for a given motor is completed, the tuning configurations can be saved for future reference. In the top menu, click on the File  $\rightarrow$  Save Register option as detailed below to save the configurations to downloads.

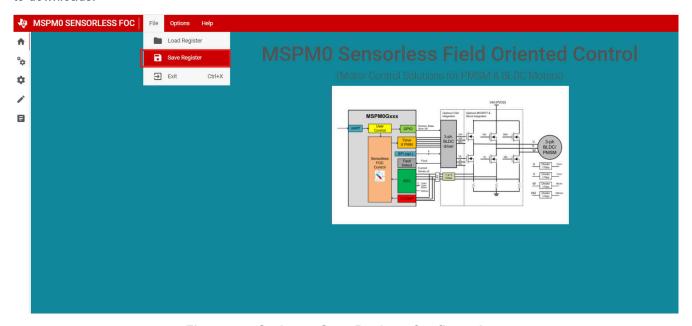


Figure 4-7. Option to Save Register Configurations

Similarly, to load the tuned configurations which are saved previously, click in the menu options File  $\rightarrow$  load Register to populate the configurations into the register space.



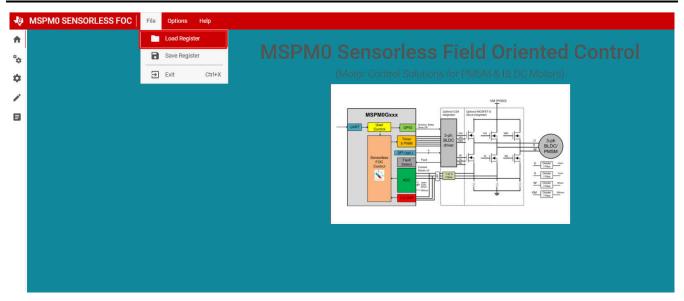


Figure 4-8. Option to Load Register Configurations

# **5 Register Map**

Register map contains set of three register structures for Setting the Motor Control Tuning Parameters, Monitoring the Motor Status variables and Setting the Real time Control parameters using User Input registers, User Status registers and User Control Registers, respectively.

Real time control of the FOC registers can be performed in three ways.

1. Import the structures into the expression window of CCS during the code debug as shown in Figure 5-1.



Figure 5-1. Expressions for Input, Control and Status Registers in CCS Debug Mode

- 2. Read/Write the parameters over UART as described in UART\_COMUNICATION\_USER\_GUIDE
- 3. Control and monitor the variables using Motor Control FOC GUI.

The following sections describe registers and the variables associated with these structures.

www.ti.com Register Map

## 5.1 Register Map Page in GUI

The above register variables can also be configured using GUI. Figure 5-2 details all the available user configurable registers available in the Sensorless FOC application. After connecting the GUI with the controller, click *Read all* option in the register page to reflect the default programmed parameters.

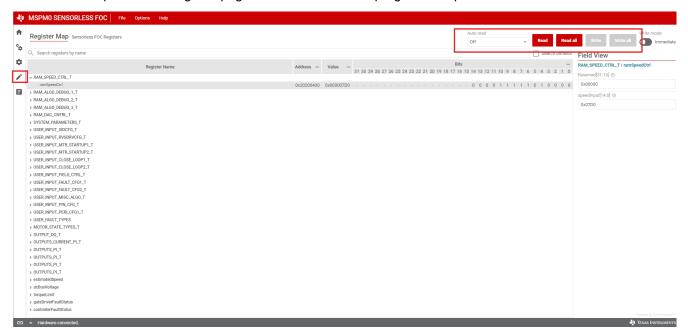


Figure 5-2. Register Map Page in GUI

### 5.2 User Control Registers (Base Address = 0x20200400h)

User Control Registers are set of user configurable parameters to control the Motor in real time.

These set of registers can be modified in the application code using pointer variable **pUserCtrlRegs**. Below are the set of user Control registers as imported in CSS expression window.

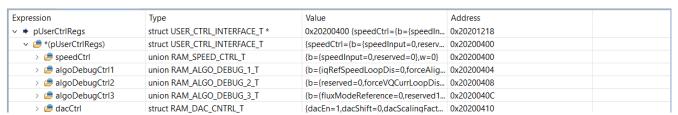


Figure 5-3. User Control Registers in CCS Debug Mode

Table 5-1. User Control Registers

Offset	Acronym	Register Name	Section
0h	SPEED_CTRL	Speed Control Register	Section 5.2.1
4h	ALGO_DEBUG_CTRL1	Algorithm Debug Control 1 register	Section 5.2.2
8h	ALGO_DEBUG_CTRL2	Algorithm Debug Control 2 register	Section 5.2.3
Ch	ALGO_DEBUG_CTRL3	Algorithm Debug Control 3 register	Section 5.2.4
10h	DAC_CTRL	DAC Configuration and Control register	Section 5.2.5



Complex bit access types are encoded to fit into small table cells as shown in Table 5-2.

Table 5-2. Register Configuration Access Type Codes

Access Type	Code	Description		
Read Type				
R	R	Read		
Write Type	Write Type			
W	W	Write		
Reset or Default Value				
-n		Value after reset or the default value		

# 5.2.1 Speed Control Register (Offset = 0h) [Reset = 00000000h]

Table 5-3 shows the register to control Motor Speed.

Table 5-3. SPEED\_CTRL Register Field Descriptions

Bit	Field	Туре	Reset	Description
31 - 15	RESERVED	R	0h	Reserved
14-0	SPEED_CTRL	W		Target Motor Speed/Torque value % of speed or Torque command × 32768

# 5.2.2 Algo Debug Control 1 Register (Offset = 4h) [Reset = 00000000h]

Table 5-4 shows the register to control Algorithm debug functions.

Table 5-4. Algorithm Debug Control 1 Register Field Descriptions

Bit	Field	Туре	Reset	Description
31	CLEAR_FAULT	W	0b	Bit to clear set controller and Gate Driver Faults. Bit is automatically reset.  1h = Clear Fault Command
30-22	FORCED_ALIGN_ANGLE	W	000000 000b	9-bit value (in °) used during forced align state ( FORCE_ALIGN_EN = 1) Angle applied (°) = FORCED_ALIGN_ANGLE % 360°
21-16	RESERVED	R	0h	
15	CLOSED_LOOP_DIS	W	0b	Use to disable closed loop  0h = Enable closed loop  1h = Disable closed loop, motor commutation in open loop
14	FORCE_ALIGN_EN	W	0b	Force align state enable  0h = Disable force align state, device comes out of align state if  MTR_STARTUP is selected as ALIGN or DOUBLE ALIGN  1h = Enable force align state, device stays in align state if  MTR_STARTUP is selected as ALIGN or DOUBLE ALIGN
13	FORCE_SLOW_FIRST_C YCLE_EN	W	0b	Force slow first cycle enable  0h = Disable force slow first cycle state, device comes out of slow first cycle state if MTR_STARTUP is selected as SLOW FIRST CYCLE  1h = Enable force slow first cycle state, device stays in slow first cycle state if MTR_STARTUP is selected as SLOW FIRST CYCLE
12	FORCE_IPD_EN	W	0b	Force IPD enable 0h = Disable Force IPD state, device comes out of IPD state if MTR_STARTUP is selected as IPD 1h = Enable Force IPD state, device stays in IPD state if MTR_STARTUP is selected as IPD

www.ti.com Register Map

**Table 5-4. Algorithm Debug Control 1 Register Field Descriptions (continued)** 

Bit	Field	Туре	Reset	Description
11	FORCE_ISD_EN	W	0b	Force ISD enable  0h = Disable Force ISD state, device comes out of ISD state if ISD_EN is set  1h = Enable Force ISD state, device stays in ISD state if ISD_EN is set
10	FORCE_ALIGN_ANGLE_SRC_SEL	W	0b	Force align angle state source select  0h = Force Align Angle defined by ALIGN_ANGLE  1h = Force Align Angle defined by FORCED_ALIGN_ANGLE
9-0	Reserved	R	0b	Reserved

# 5.2.3 Algo Debug Control 2 Register (Offset = 8h) [Reset = 00000000h]

Table 5-5 shows the register to control Algorithm Debug functions.

Table 5-5. Algorithm Debug Control 2 Register Field Descriptions

	Table 5-5. Algorithm Debug Control 2 Register Field Descriptions						
Bit	Field	Type	Reset	Description			
31 - 30	RESERVED	R	0h	Reserved			
29	UPDATE_SYS_PARAMET ERS	W	1h	Dynamically updates System parameters every 200mS like PI gains of Speed/Torque loops to tune for required performance 0b = Dynamic System updates Disabled 1b = Dynamic System updates Enabled			
28	UPDATE_CONFIGS	R	0b	This bit gives user the status of configuration updates. This bit is reset every 200mS when the tuning configurations are updated by algorithm and motor is not spinning. To gaurantee that User configurations are reflected in algorithm, user can set this bit after required tuning configurations are made and wait for this status bit to reset before giving the speed command.			
27	STATUS_UPDATE_ENAB LE	W	0b	This bit enables the continuous update of user Status variables in real time.			
26	CURRENT_LOOP_DIS	W	0b	Use to control the FORCE_VD_CURRENT_LOOP_DIS and FORCE_VQ_CURRENT_LOOP_DIS. If CURRENT_LOOP_DIS = 1b, current loop and speed loop are disabled 0h = Enable Current Loop  1h = Disable Current Loop			
25-16	FORCE_VD_CURRENT_ LOOP_DIS	W-IQ(9)	Oh	Sets Vd_ref in IQ(9) PU when current loop and speed loop are disabled If CURRENT_LOOP_DIS = 1b, then Vd is controlled using FORCE_VD_CURRENT_LOOP_DIS Vd_ref = (FORCE_VD_CURRENT_LOOP_DIS / 500) if FORCE_VD_CURRENT_LOOP_DIS < 500 - (FORCE_VD_CURRENT_LOOP_DIS - 512) / 500 if FORCE_VD_CURRENT_LOOP_DIS > 512 Valid values: 0 to 500 and 512 to 1000			
15-6	FORCE_VQ_CURRENT_ LOOP_DIS	W-IQ(9)	0h	Sets Vq_ref in IQ(9) PU when current loop speed loop are disabled If CURRENT_LOOP_DIS = 1b, then Vq is controlled using FORCE_VQ_CURRENT_LOOP_DIS Vq_ref = (FORCE_VQ_CURRENT_LOOP_DIS / 500) if FORCE_VQ_CURRENT_LOOP_DIS < 500 - (FORCE_VQ_CURRENT_LOOP_DIS - 512) / 500 if FORCE_VQ_CURRENT_LOOP_DIS > 512 Valid values: 0 to 500 and 512 to 1000			
5-0	RESERVED	R	0h	Reserved			

## 5.2.4 Algo Debug Control 3 Register (Offset = Ch) [Reset = 00000000h]

Table 5-6 shows the register to control Algorithm Debug 3 functions.

## Table 5-6. Algorithm Debug Control 3 Register Field Descriptions

Bit	Field	Type	Reset	Description
31-10	RESERVED	R	0h	
9-0	FLUX_MODE_REF	W-IQ(9)	0h	Sets Id_ref in IQ(9) PU when flux of the motor along D-axis is to be controlled Positive Id Control: (FLUX_MODE_REF/ 511) , if FLUX_MODE_REF < 512 Negative Id Control: -(FLUX_MODE_REF - 512) / 511 if FLUX_MODE_REF > 512 Valid values are 0 to 511 and 512 to 1000

# 5.2.5 DAC Configuration Register (Offset = 10h) [Reset = 00000000h]

DAC control registers defines configurations for monitoring the Real Time Algorithm and Hardware Register data on scope using the 12 bit DAC available on MSPM0G. for a detailed example on how to monitor an algorithm variable using DAC, see Section 8.4.

**Table 5-7. DAC Configuration Registers** 

Variables	Туре	Reset	Description
DAC_EN	Unsigned Short (RW)	0h	0h = Disable DAC 1h = Enable DAC
DAC_SHIFT	short (RW)	Oh	+ve value specifies the number of left bit shifts before loading the value to 12bit DAC registerve value specifies the number of right bit shifts before loading the value to 12bit DAC register.  DAC Shift is used for monitoring unsigned integer values and Registers
DAC_SCALING_FACTOR	int(RW)	0x00000000h	Non zero scaling factor is used for numbers represented in IQ format to be monitored in DAC. To monitor the Global IQ(27) format variables DAC scaling factor of _IQ(1.0) is used.  To represent other IQx format variables, set DAC scaling factor to IQx/IQGlobal.
DACOUT_ADDRESS	unsigned int(RW)	0x00000000h	Defines the 32bit aligned address of 32 bit variable that is to be monitored through DAC.

www.ti.com Register Map

## 5.3 User Input Registers (Base Address = 0x20200000h)

User input registers are set of configurable registers to tune the motor performance in real time for various motor control features and save them in flash

Below are the set of Input Registers that can be imported in the CCS expression window using structure pointer *pUserInputRegs* .

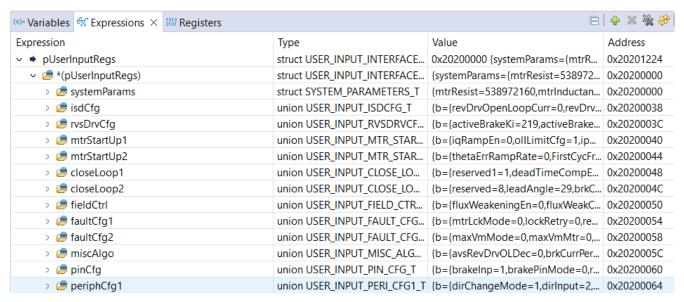


Figure 5-4. User Input Registers in CCS Debug Mode

#### Table 5-8. User Input Registers

Offset	Acronym	Register Name	Section
0h	SYSTEM_PARAMETERS	System Parameters	Section 5.3.1
38h	ISD_CFG	Initial Speed Detection Configuration	Section 5.3.2
3Ch	RVS_DRV_CONFIG	Reverse Drive Configuration	Section 5.3.3
40h	MOTOR_STARTUP1	Motor Startup 1 Configuration	Section 5.3.4
44h	MOTOR_STARTUP2	Motor Startup 2 Configuration	Section 5.3.5
48h	CLOSELOOP1	Close Loop1 Configuration	Section 5.3.6
4Ch	CLOSELOOP2	Close Loop2 Configuration	Section 5.3.7
50h	FLIED_CTRL	Flux Control Configuration	Section 5.3.8
54h	FAULT_CONFIG1	Fault Configuration 1	Section 5.3.9
58h	FAULT_CONFIG2	Fault Configuration 2	Section 5.3.10
5Ch	MISC_ALGO_CONFIG	Miscellaneous Algorithm Configuration	Section 5.3.11
60h	PIN_CONFIGURATION	Pin Configuration	Section 5.3.12
64h	PERI_CONFIG	Peripheral Configuration	Section 5.3.13

Complex bit access types are encoded to fit into small table cells as below.

Table 5-9. Register Configuration Access Type Codes

Access Type	Code	Description		
Read Type				
R	R	Read		
Write Type				
W	W	Write		
Reset or Default Value				

# Table 5-9. Register Configuration Access Type Codes (continued)

Access Type	Code	Description
-n		Value after reset or the default value

# 5.3.1 SYSTEM\_PARAMETERS (Offset = 0h)

Set of basic system configuration parameters essential for motor control system functionality.

# Table 5-10. Motor Resistance Configuration Registers (Offset = 0h)

Bit	Field	Type	Reset	Description
31-0	MTR_RESISTANCE	R/W	0000h	Motor Resistance in milliohms

## **Table 5-11. Motor Inductance Configuration (Offset = 4h)**

Bit	Field	Туре	Reset	Description
31-0	MTR_INDUCTANCE	R/W	0000h	Motor Inductance in microhenry. For Salient pole motors (Lq + Ld)/2

# **Table 5-12. Motor Saliency Configuration (Offset = 8h)**

Bit	Field	Туре	Reset	Description
31-0	MTR_SALIENCY	R/W	0.0(Float)	Saliency of Motor (Lq-Ld)/(Lq+Ld) in float.

#### **Table 5-13. Motor BEMF Constant Configuration (Offset = Ch)**

Bit	Field	Type	Reset	Description
31-0	MTR_BEMF_CONSTANT	R/W	0000h	Motor BEMF constant in mV/Hz × 10.

#### Table 5-14. Base Voltage Configuration (Offset = 10h)

Bit	Field	Туре	Reset	Description
31-0	VOLTAGE_BASE	R/W	0.0(Float)	Base voltage of the board calculatedas the maximum measurable voltage detailed in Equation 7 MAX_DC_VOLTAGE/sqrt(3)

### Table 5-15. Base Current Configuration (Offset = 14h)

Bit	Field	Туре	Reset	Description
31-0	CURRENT_BASE	R/W	0.0(Float)	Base current of the board calculated based on the CSA gain in as (1.65V - ADC OffsetVoltage/ CSA Gain in volts/amp) in amps.  1.65V is the reference mid point voltage of the ADC for bidirectional current sensing.  0.4125 is the offset Voltage in DRV8329  If the CSA gain is in V/V , multiply with current sense resistor value in ohms to compute CSA gain in volts/amp

#### Table 5-16. Motor Max Speed Configuration (Offset = 18h)

Bit	Field	Type	Reset	Description
31-0	MOTOR_MAX_SPEED	R/W	0.0(Float)	Rated motor speed in Hz from the data sheet

# Table 5-17. Motor Max Power Configuration (Offset = 1Ch)

Bit	Field	Type	Reset	Description
31-0	MOTOR_MAX_POWER	R/W	0.0(Float)	Rated motor power in Hz from the data sheet

#### Table 5-18. Speed Loop Proportional Gain (Offset = 20h)

Bit	Field	Туре	Reset	Description
31-0	SPEED_POWER_LOOP_ KP	R/W	0.0(Float)	Proportional gain for the closed loop speed control /Power Loop Control in float

www.ti.com Register Map

Table 5-19. Speed Loop Integral Gain (Offset = 24h)

Bit	Field	Туре	Reset	Description
31-0	SPEED_POWER_LOOP_ KI	R/W	0.0(Float)	Integral gain for the closed loop speed control /Power Loop Control in float

# Table 5-20. Torque Loop Proportional Gain (Offset = 28h)

Bit	Field	Туре	Reset	Description
31-0	CURR_LOOP_KP	R/W	0.0(Float)	Proportional gain for the closed loop torque control in float

# Table 5-21. Torque Loop Integral Gain (Offset = 2Ch)

Bit	Field	Type	Reset	Description
31-0	CURR_LOOP_KI	R/W	0.0(Float)	Integral gain for the closed loop torque control in float

#### **Table 5-22. Flux Weakening Controller Proportional Gain (Offset = 30h)**

			•	• ,
Bit	Field	Туре	Reset	Description
31-0	FLUX_WEAK_KI	R/W	0.0(Float)	Proportional gain for the Flux weakening control in float

# Table 5-23. Flux Weakening Controller Integral Gain (Offset = 34h)

Bit	Field	Туре	Reset	Description
31-0	FLUX_WEAK_KP	R/W	0.0(Float)	Integral gain for the Flux weakening control in float

# 5.3.2 ISD\_CONFIG Register (Offset = 38h) [Reset = 00000000h]

Table 5-24 shows the register to configure Initial Speed Detection.

# Table 5-24. ISD\_CONFIG Register

Bit	Field	Туре	Reset	Description
31-30	BEMF_RESYNC_THRES HOLD	R/W	00b	Minimum ratio of estimated BEMF with respect to actual BEMF for ISD resynchronization  0h = 0.75  1h = 0.80  2h = 0.85  3h = 0.90
29	ISD_EN	R/W	0b	ISD Enable 0h = Disable 1h = Enable
28	BRAKE_EN	R/W	0b	Brake enable 0h = Disable 1h = Enable
27	HIZ_EN	R/W	0b	Hi-Z enable 0h = Disable 1h = Enable
26	RVS_DR_EN	R/W	0b	Reverse drive enable 0h = Disable 1h = Enable
25	RESYNC_EN	R/W	0b	Resynchronization Enable 0h = Disable 1h = Enable



# Table 5-24. ISD\_CONFIG Register (continued)

Bit	1			Description
<b>Bit</b> 24-21	Field  FW_DRV_RESYN_THR	Type R/W	Reset Oh	Description  Minimum Speed threshold to resynchronize to close loop (% of MAX_SPEED)  0h = 5%  1h = 10%  2h = 15%  3h = 20%  4h = 25%  5h = 30%  6h = 35%  7h = 40%  8h = 45%  9h = 50%  Ah = 55%  Bh = 60%  Ch = 70%
20	BRK_CONFIG	R/W	0b	Dh = 80% Eh = 90% Fh = 100%  Brake configuration 0h = Brake time is used to come out of brake state 1h = Brake current threshold is used to come out of brake state
16-19	BRK_TIME	R/W	Ob	Brake time 0h = 10ms 1h = 50ms 2h = 100ms 3h = 200ms 4h = 300ms 5h = 400ms 6h = 500ms 7h = 750ms 8h = 1s 9h = 2s Ah = 3s Bh = 4s Ch = 5s Dh = 7.5s Eh = 10s Fh = 15s

Register Map

# Table 5-24. ISD\_CONFIG Register (continued)

Bit	Field	Type	Reset	Description
15-12	HIZ_TIME	R/W	0b	
15-12	III   IIII   III   III	FK/VV	OD	Hi-Z time
				0h = 10ms
				1h = 50ms
				2h = 100ms
				3h = 200ms
				4h = 300ms
				5h = 400ms
				6h = 500ms
				7h = 750ms
				8h = 1s
				9h = 2s
				Ah = 3s
				Bh = 4s
				Ch = 5s
				Dh = 7.5s
				Eh = 10s
				Fh = 15s
11-9	STAT_DETECT_THR	R/W	000b	BEMF threshold to detect if motor is stationary
				0h = 50mV
				1h = 75mV
				2h = 100mV
				3h = 250mV
				4h = 500mV
				5h = 750mV
				6h = 1000mV
				7h = 1500mV
8-5	REV_DRV_HANDOFF_T	R/W	0h	Speed threshold used to transition to open loop during reverse
	HR			deceleration (% of MAX_SPEED)
				0h = 2.5%
				1h = 5%
				2h = 7.5%
				3h = 10%
				4h = 12.5%
				5h = 15%
				6h = 20%
				7h = 25%
				8h = 30%
				9h = 40%
				Ah = 50%
				Bh = 60%
				Ch = 70%
				Dh = 80%
				Eh = 90%
				Fh = 100%



# Table 5-24. ISD\_CONFIG Register (continued)

D:4				Description
Bit	Field	Туре	Reset	Description
4-0	REV_DRV_OPEN_LOOP	R/W	00000b	Open loop current limit during speed reversal in % of CURRENT_BASE
	CURRENT			0h = 7.5%
				1h = 8.0%
				2h = 8.5%
				3h = 9.0%
				4h = 9.5%
				5h = 10%
				6h = 11%
				7h = 12%
				8h = 13%
				9h = 14%
				Ah = 15%
				Bh = 16%
				Ch = 17%
				Dh = 18%
				Eh = 20%
				Fh = 22.5%
				10h = 25%
				11h = 27.5%
				12h = 30%
				13h = 35%
				14h = 40%
				15h = 45%
				16h = 50%
				17h = 55%
				18h = 60%
				19h = 70%
				1Ah = 75%
				1Bh = 80%
				1Ch = 85%
				1Dh = 90%
				1Eh = 95%
				1Fh = 100%

www.ti.com Register Map

# 5.3.3 RVS\_DRV\_CONFIG Register (Offset = 3Ch) [Reset = 00000000h]

Table 5-25 shows the register to configure Reverse Drive.

# Table 5-25. RVS\_DRV\_CONFIG Register

	Field		Reset	Description
	RESERVED	<b>Type</b> R	0h	Reserved
	REV_DRV_CONFIG	R/W	0b	Chooses between forward and reverse drive setting for reverse drive 0h = Open loop current, A1, A2 based on forward drive 1h = Open loop current, A1, A2 based on reverse drive
	REV_DRV_OPEN_LOOP _ACCEL_A1	R/W	Oh	Reverse Drive Open loop acceleration coefficient A1 during reverse drive  0h = 0.01Hz/s 1h = 0.05Hz/s 2h = 1Hz/s 3h = 2.5Hz/s 4h = 5Hz/s 5h = 10Hz/s 6h = 25Hz/s 7h = 50Hz/s 8h = 75Hz/s 9h = 100Hz/s Ah = 250Hz/s Bh = 500Hz/s Ch = 750Hz/s Dh = 1000Hz/s Eh = 5000Hz/s Fh = 10000Hz/s
	REV_DRV_OPEN_LOOP _ACCEL_A2	R/W	Oh	Reverse Drive Open loop acceleration coefficient A2 during reverse drive  0h = 0.0Hz/s2  1h = 0.05Hz/s2  2h = 1Hz/s2  3h = 2.5Hz/s2  4h = 5Hz/s2  5h = 10Hz/s2  6h = 25Hz/s2  7h = 50Hz/s2  8h = 75Hz/s2  9h = 100Hz/s2  Ah = 250Hz/s2  Bh = 500Hz/s2  Ch = 750Hz/s2  Dh = 1000Hz/s2  Eh = 5000Hz/s2  Fh = 10000Hz/s2
19-0 I	RESREVED	R	0h	Reserved



# 5.3.4 MOTOR\_STARTUP1 Register (Offset = 40h) [Reset = 00000000h]

Table 5-26 shows the register to configure motor startup settings1.

# Table 5-26. MOTOR\_STARTUP1 Register Field Descriptions

Bit	Field			Pagarintian
		Туре	Reset	Description
31-30	MTR_STARTUP_OPTION	R/W	00b	Motor start-up method  0h = Align  1h = Double align  2h = IPD  3h = Slow first cycle
29-26	ALIGN_SLOW_RAMP_RA TE	R/W	Oh	Align, slow first cycle and open loop current ramp rate  0h = 0.1A/s  1h = 1A/s  2h = 5A/s  3h = 10A/s  4h = 15A/s  5h = 25A/s  6h = 50A/s  7h = 100A/s  8h = 150A/s  9h = 200A/s  Ah = 250A/s  Bh = 500A/s  Ch = 1000A/s  Eh = 5000A/s  Fh = No Limit A/s
25-22	ALIGN_TIME	R/W	Oh	Align time 0h = 10ms 1h = 50ms 2h = 100ms 3h = 200ms 4h = 300ms 5h = 400ms 6h = 500ms 7h = 750ms 8h = 1s 9h = 1.5s Ah = 2s Bh = 3s Ch = 4s Dh = 5s Eh = 7.5s Fh = 10s

Register Map

Table 5-26. MOTOR\_STARTUP1 Register Field Descriptions (continued)

Bit	Field	Type	Reset	Description (continued)
21-17	ALIGN_OR_SLOW_CUR	R/W	00h	Current limit during Align/Slow First Cycle in % of CURRENT_BASE
2117	RENT_ILIMIT		0011	0h = 7.5%
				1h = 8.0%
				2h = 8.5%
				3h = 9.0%
				4h = 9.5%
				5h = 10%
				6h = 11%
				7h = 12%
				8h = 13%
				9h = 14%
				Ah = 15%
				Bh = 16%
				Ch = 17%
				Dh = 18%
				Eh = 20%
				Fh = 22.5%
				10h = 25%
				11h = 27.5%
				12h = 30%
				13h = 35%
				14h = 40%
				15h = 45%
				16h = 50%
				17h = 55%
				18h = 60%
				19h = 70%
				1Ah = 75%
				1Bh = 80%
				1Ch = 85%
				1Dh = 90%
				1Eh = 95% 1Fh = 100%
16-14	IPD_CLK_FREQ	R/W	000b	IPD clock frequency
				0h = 50Hz
				1h = 100Hz 2h = 250Hz
				3h = 500Hz
				4h = 1000Hz
				5h = 2000Hz
				6h = 5000Hz
				7h = 10000Hz
13-7	IPD_CURR_THR	R/W	0h	7 bit value for IPD current limit × CURRENT_BASE / 2 <sup>7</sup>
6	RESERVED	R/W	0h	Reserved
5-4	IPD_ADV_ANGLE	R/W	00b	IPD advance angle
J <del>-4</del>	II D_VDA_VINGEE	12/14	UUD	Oh = 0°
				1h = 30°
				2h = 60°
				3h = 90°
		1		



Table 5-26. MOTOR\_STARTUP1 Register Field Descriptions (continued)

	14516 0-20. 1410	TOIL OIA	1101 11108	jister i leid Descriptions (continued)
Bit	Field	Type	Reset	Description
3-2	IPD_REPEAT	R/W	00b	Number of times IPD is executed
				0h = 1 time
				1h = average of 2 times
				2h = average of 3 times
				3h = average of 4 times
1	OL_ILIMIT_CONFIG	R/W	0b	Open loop current limit configuration
				0h = Open loop current limit defined by OL_ILIMIT
				1h = Open loop current limit defined by ILIMIT
0	IQ_RAMP_EN	R/W	0b	Iq ramp down before transition to close loop
				0h = Disable Iq ramp down
				1h = Enable Iq ramp down

# 5.3.5 MOTOR\_STARTUP2 Register (Offset = 44h) [Reset = 00000000h]

Table 5-27 shows the register to configure motor startup settings2.

Table 5-27. MOTOR\_STARTUP2 Register Field Descriptions

31-27 OL_ILIMIT R/W Oh Open loop current limit in % of CURRENT_BASE Oh = 7.5% 1h = 8.0% 2h = 8.5% 3h = 9.0% 4h = 9.5% 5h = 10% 6h = 11% 7h = 12% 8h = 13% 9h = 14% Ah = 15% Bh = 16% Ch = 17% Dh = 18% Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 18h = 80% 1Ch = 85% 1Dh = 90% 1Fh = 100% 1Fh = 1	Bit	Field	Туре	Reset	Description
1h = 8.0% 2h = 8.5% 3h = 9.0% 4h = 9.5% 5h = 10% 6n = 11% 7h = 12% 8h = 13% 9h = 14% Ah = 15% Bh = 16% Ch = 17% Dh = 18% Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 18h = 80% 19h = 70% 18h = 80% 16h = 85% 16h = 95%	31-27	OL_ILIMIT	R/W	0h	
2h = 8.5% 3h = 9.0% 4h = 9.5% 5h = 10% 6h = 11% 7h = 12% 8h = 13% 9h = 14% Ah = 15% Bh = 16% Ch = 17% Dh = 18% Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 18h = 80% 1Ah = 75% 18h = 80% 1Ch = 85%					
3h = 9.0% 4h = 9.5% 5h = 10% 6h = 11% 7h = 12% 8h = 13% 9h = 14% Ah = 15% Bh = 16% Ch = 17% Dh = 18% Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 18h = 80% 1Ch = 85% 1Dh = 90% 1Eh = 90%					
4h = 9.5% 5h = 10% 6h = 11% 7h = 12% 8h = 13% 9h = 14% Ah = 15% Bh = 16% Ch = 17% Dh = 18% Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					2h = 8.5%
5h = 10% 6h = 11% 7h = 12% 8h = 13% 9h = 14% Ah = 15% Bh = 16% Ch = 17% Dh = 18% Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					3h = 9.0%
6h = 11% 7h = 12% 8h = 13% 9h = 14% Ah = 15% Bh = 16% Ch = 17% Dh = 18% Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					4h = 9.5%
7h = 12% 8h = 13% 9h = 14% Ah = 15% Bh = 16% Ch = 17% Dh = 18% Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					5h = 10%
8h = 13% 9h = 14% Ah = 15% Bh = 16% Ch = 17% Dh = 18% Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					6h = 11%
9h = 14% Ah = 15% Bh = 16% Ch = 17% Dh = 18% Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					7h = 12%
Ah = 15% Bh = 16% Ch = 17% Dh = 18% Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					8h = 13%
Bh = 16% Ch = 17% Dh = 18% Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					9h = 14%
Ch = 17% Dh = 18% Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					Ah = 15%
Dh = 18% Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					Bh = 16%
Eh = 20% Fh = 22.5% 10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					Ch = 17%
Fh = 22.5%  10h = 25%  11h = 27.5%  12h = 30%  13h = 35%  14h = 40%  15h = 45%  16h = 50%  17h = 55%  18h = 60%  19h = 70%  1Ah = 75%  1Bh = 80%  1Ch = 85%  1Dh = 90%  1Eh = 95%					Dh = 18%
10h = 25% 11h = 27.5% 12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					Eh = 20%
11h = 27.5%  12h = 30%  13h = 35%  14h = 40%  15h = 45%  16h = 50%  17h = 55%  18h = 60%  19h = 70%  1Ah = 75%  1Bh = 80%  1Ch = 85%  1Dh = 90%  1Eh = 95%					Fh = 22.5%
12h = 30% 13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					10h = 25%
13h = 35% 14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					11h = 27.5%
14h = 40% 15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					12h = 30%
15h = 45% 16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					13h = 35%
16h = 50% 17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					14h = 40%
17h = 55% 18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					15h = 45%
18h = 60% 19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					16h = 50%
19h = 70% 1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					17h = 55%
1Ah = 75% 1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					18h = 60%
1Bh = 80% 1Ch = 85% 1Dh = 90% 1Eh = 95%					19h = 70%
1Ch = 85% 1Dh = 90% 1Eh = 95%					1Ah = 75%
1Dh = 90% 1Eh = 95%					1Bh = 80%
1Eh = 95%					1Ch = 85%
					1Dh = 90%
1Fh = 100%					1Eh = 95%
					1Fh = 100%

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Table 5-27. MOTOR\_STARTUP2 Register Field Descriptions (continued)

Bit	Field	Type	Reset	Description (continued)
26-23	OL_ACC_A1	R/W	Oh	Open loop acceleration coefficient A1  0h = 0.01Hz/s  1h = 0.05Hz/s  2h = 1Hz/s  3h = 2.5Hz/s  4h = 5Hz/s  5h = 10Hz/s  6h = 25Hz/s  7h = 50Hz/s  8h = 75Hz/s  9h = 100Hz/s  Ah = 250Hz/s  Ch = 750Hz/s  Dh = 1000Hz/s  Eh = 5000Hz/s  Fh = 10000Hz/s
22-19	OL_ACC_A2	R/W	Oh	Open loop acceleration coefficient A2  0h = 0.0Hz/s2  1h = 0.05Hz/s2  2h = 1Hz/s2  3h = 2.5Hz/s2  4h = 5Hz/s2  5h = 10Hz/s2  6h = 25Hz/s2  7h = 50Hz/s2  8h = 75Hz/s2  9h = 100Hz/s2  Ah = 250Hz/s2  Bh = 500Hz/s2  Ch = 750Hz/s2  Dh = 1000Hz/s2  Eh = 5000Hz/s2  Fh = 10000Hz/s2
18	AUTO_HANDOFF_EN	R/W	0h	Auto handoff enable 0h = Disable Auto Handoff (and use OPN_CL_HANDOFF_THR) 1h = Enable Auto Handoff



# Table 5-27. MOTOR\_STARTUP2 Register Field Descriptions (continued)

17-13 OPN_CL_HANDOFF_TH R/W Oh Open to close loop handoff threshold (% of MAX_SPEED) On = 1% 1h = 2% 2h = 3% 3h = 4% 4h = 5% 5h = 6% 6h = 7% 7h = 8% 8h = 9% 9h = 10% Ah = 11% Bh = 12% Ch = 13% Dh = 14% Eh = 15% Fh = 16% 10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 1Ah = 37.5% 1Bh = 42.5% 1Dh = 45% 1Eh = 47.5% 1Fh = 50% 18h = 47.5% 1Fh = 47	Bit	Field	Type	Reset	Description (continued)
1h = 2% 2h = 3% 3h = 4% 4h = 5% 5h = 6% 6h = 7% 7h = 8% 8h = 9% 9h = 10% Ah = 11% Bh = 12% Ch = 13% Dh = 14% Eh = 15% Fh = 16% 10h = 17% 11h = 18% 12h = 199% 13h = 20% 14h = 22.5% 15h = 25% 16h = 25.5% 17h = 30% 18h = 32.5% 19h = 35% 18h = 37.5% 18h = 40% 1Ch = 42.5% 1Dh = 42.5%	17-13	OPN_CL_HANDOFF_TH	R/W	0h	Open to close loop handoff threshold (% of MAX_SPEED)
2h = 3% 3h = 4% 4h = 5% 5h = 6% 6h = 7% 7h = 8% 8h = 9% 9h = 10% Ah = 11% Bh = 12% Ch = 13% Dh = 14% Eh = 15% Fh = 16% 10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 18h = 37.5% 18h = 40% 1Ch = 42.5% 1Dh = 42.5% 1Dh = 45% 1Dh = 45% 1Dh = 45% 1Eh = 47.5%		R			0h = 1%
3h = 4% 4h = 5% 5h = 6% 6h = 7% 7h = 8% 8h = 9% 9h = 10% Ah = 11% Bh = 12% Ch = 13% Dh = 14% Eh = 15% Fh = 16% 10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 15h = 25.5% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 18h = 37.5% 18h = 40% 1Ch = 42.5% 1Dh = 45% 1Dh = 45% 1Dh = 45% 1Eh = 47.5%					1h = 2%
4h = 5% 5h = 6% 6h = 7% 7h = 8% 8h = 9% 9h = 10% Ah = 11% Bh = 12% Ch = 13% Dh = 14% Eh = 15% Fh = 16% 10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 5h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 18h = 35.5% 18h = 37.5% 18h = 37.5% 18h = 40.5% 10h = 45% 11h = 45%					2h = 3%
5h = 6% 6h = 7% 7h = 8% 8h = 9% 9h = 10% Ah = 11% Bh = 12% Ch = 13% Dh = 14% Eh = 15% Fh = 16% 10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 45% 1Dh = 45% 1Dh = 45% 1Dh = 45% 1Eh = 47.5%					3h = 4%
6h = 7% 7h = 8% 8h = 9% 9h = 10% Ah = 11% Bh = 12% Ch = 13% Dh = 14% Eh = 15% Fh = 16% Fh = 16% 10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					4h = 5%
7h = 8% 8h = 9% 9h = 10% Ah = 111% Bh = 12% Ch = 13% Dh = 14% Eh = 15% Fh = 16% 10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 19h = 35% 11h = 40% 11ch = 42.5% 11h = 45% 11ch = 45% 11ch = 45% 11ch = 47.5%					5h = 6%
8h = 9% 9h = 10% Ah = 11% Bh = 12% Ch = 13% Dh = 14% Eh = 15% Fh = 16% 10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Dh = 45% 1Eh = 47.5%					6h = 7%
9h = 10% Ah = 11% Bh = 12% Ch = 13% Dh = 14% Eh = 15% Fh = 16% 10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					7h = 8%
Ah = 11% Bh = 12% Ch = 13% Dh = 14% Eh = 15% Fh = 16% 10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					8h = 9%
Bh = 12% Ch = 13% Dh = 14% Eh = 15% Fh = 16% 10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Dh = 45% 1Eh = 47.5%					9h = 10%
Ch = 13% Dh = 14% Eh = 15% Fh = 16% 10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					Ah = 11%
Dh = 14% Eh = 15% Fh = 16% 10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					Bh = 12%
Eh = 15% Fh = 16% 10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					Ch = 13%
Fh = 16%  10h = 17%  11h = 18%  12h = 19%  13h = 20%  14h = 22.5%  15h = 25%  16h = 27.5%  17h = 30%  18h = 32.5%  19h = 35%  1Ah = 37.5%  1Bh = 40%  1Ch = 42.5%  1Dh = 45%  1Eh = 47.5%					Dh = 14%
10h = 17% 11h = 18% 12h = 19% 13h = 20% 14h = 22.5% 15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					Eh = 15%
11h = 18%  12h = 19%  13h = 20%  14h = 22.5%  15h = 25%  16h = 27.5%  17h = 30%  18h = 32.5%  19h = 35%  1Ah = 37.5%  1Bh = 40%  1Ch = 42.5%  1Dh = 45%  1Eh = 47.5%					Fh = 16%
12h = 19%  13h = 20%  14h = 22.5%  15h = 25%  16h = 27.5%  17h = 30%  18h = 32.5%  19h = 35%  1Ah = 37.5%  1Bh = 40%  1Ch = 42.5%  1Dh = 45%  1Eh = 47.5%					10h = 17%
13h = 20%  14h = 22.5%  15h = 25%  16h = 27.5%  17h = 30%  18h = 32.5%  19h = 35%  1Ah = 37.5%  1Bh = 40%  1Ch = 42.5%  1Dh = 45%  1Eh = 47.5%					11h = 18%
14h = 22.5% 15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					12h = 19%
15h = 25% 16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					13h = 20%
16h = 27.5% 17h = 30% 18h = 32.5% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					14h = 22.5%
17h = 30% 18h = 32.5% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					15h = 25%
17h = 30% 18h = 32.5% 19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					16h = 27.5%
19h = 35% 1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					
1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					18h = 32.5%
1Ah = 37.5% 1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					19h = 35%
1Bh = 40% 1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					
1Ch = 42.5% 1Dh = 45% 1Eh = 47.5%					
1Dh = 45% 1Eh = 47.5%					
1Eh = 47.5%					
					1Fh = 50%

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Table 5-27. MOTOR\_STARTUP2 Register Field Descriptions (continued)

12-8 ALIGN_ANGLE  R/W  Oh  Align angle Oh = 0" 1h = 10" 2h = 20" 3h = 30" 4h = 45" 5h = 60" 6h = 70" 7h = 80" 8h = 90" 9h = 110" Ah = 120" Bh = 135" Ch = 150" Dh = 160" Eh = 170" Fh = 180" 10h = 190" 11h = 210" 12h = 225" 13h = 240" 14h = 250" 15h = 260" 16h = 270" 17h = 280" 18h = 90" 19h = 315" 1Ah = 330" 19h = 315" 1Ah = 330" 11h = 340" 10h = 180" 10h = 180" 17h = 280" 18h = 30" 18h = 30" 18h = 340" 10h = 350" 10h = N/A 1Fh = N/A 1Fh = N/A 1Fh = N/A  7-4  SLOW_FIRST_CYC_FRE Q  On = 1% Frequency of first cycle in close loop startup (% of MAX_SPEED On = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%	Bit	Field	_		Description (continued)
0 m = 0° 1 h = 10° 2 h = 20° 3 h = 30° 4 h = 45° 5 h = 60° 6 h = 70° 7 h = 80° 8 h = 90° 9 h = 110° Ah = 120° Bh = 135° Ch = 150° Dh = 160° Eh = 170° Fh = 180° 10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 770° 17h = 280° 18h = 900° 19h = 315° 1Ah = 330° 18h = 900° 19h = 315° 1Ah = 330° 16h = 340° 10h = 10h N/A 1Fh = N					
1h = 10° 2h = 20° 3h = 30° 4h = 45° 5h = 60° 6h = 70° 7h = 80° 8h = 90° 9h = 110° Ah = 120° Bh = 135° Ch = 150° Dh = 160° Eh = 170° Fh = 180° 10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 18h = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%	12-8	ALIGN_ANGLE	R/W	Un Un	
2h = 20° 3h = 30° 4h = 45° 5h = 60° 6h = 70° 7h = 80° 8h = 90° 9h = 110° Ah = 120° Bh = 135° Ch = 150° Dh = 160° Eh = 770° Fh = 180° 10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 18h = 340° 10h = 350° 10h = N/A 1Eh = 1% 1E = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 100% 6h = 12.5%					
3h = 30° 4h = 45° 5h = 60° 6h = 70° 7h = 80° 8h = 90° 9h = 110° Ah = 120° Bh = 135° Ch = 150° Dh = 160° Eh = 170° Fh = 180° 10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 18h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					
## 45° \$5 = 60° 66 = 70° 7 h = 80° 8h = 90° 9h = 110° Ah = 120° Bh = 135° Ch = 150° Dh = 160° Eh = 170° Fh = 180° 10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 330° 18h = 330° 18h = 340° 1Ch = 350° 1Dh = NIA 1Eh = NIA 1Eh = NIA 1Fh = NIA  7-4 SLOW_FIRST_CYC_FRE Q   ## 7-8  ## 7-5% 5h = 10% 6h = 12.5%					
Sh = 60°   6h = 70°   7h = 80°   8h = 90°   9h = 110°   Ah = 120°   Bh = 135°   Ch = 150°   Dh = 160°   Eh = 170°   Fh = 180°   10h = 190°   11h = 210°   12h = 225°   13h = 240°   14h = 250°   15h = 260°   16h = 270°   17h = 280°   18h = 290°   19h = 315°   1Ah = 330°   1Bh = 340°   1Ch = 350°   1Dh = N/A   1Eh = N/A   1Fh = N/A   1Fh = N/A   Frequency of first cycle in close loop startup (% of MAX_SPEED Oh = 1%					
6h = 70° 7h = 80° 8h = 90° 9h = 110° Ah = 120° Bh = 135° Ch = 150° Dh = 160° Eh = 170° Fr = 180° 10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED Oh = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					
7h = 80° 8h = 90° 9h = 110° Ah = 120° Bh = 135° Ch = 150° Dh = 160° Eh = 170° Fh = 180° 10h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Fh = N					
Sh = 90°   9h = 110°   Ah = 120°   Bh = 135°   Ch = 150°   Dh = 160°   Eh = 170°   Fh = 180°   10h = 190°   11h = 210°   12h = 225°   13h = 240°   14h = 250°   15h = 260°   16h = 270°   17h = 280°   18h = 290°   19h = 315°   1Ah = 330°   1Bh = 340°   1Ch = 350°   1Dh = N/A   1Eh = N/A   1Fh					6h = 70°
9h = 110° Ah = 120° Bh = 135° Ch = 150° Dh = 160° Eh = 170° Fh = 180° 10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh					7h = 80°
Ah = 120° Bh = 135° Ch = 150° Dh = 160° Eh = 170° Fh = 180° 10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					8h = 90°
Bh = 135° Ch = 150° Dh = 160° Eh = 170° Fh = 180° 10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED Oh = 1% Oh					9h = 110°
Bh = 135° Ch = 150° Dh = 160° Eh = 170° Fh = 180° 10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED Oh = 1% Oh					Ah = 120°
Ch = 150° Dh = 160° Eh = 170° Fh = 180° 10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh					
Dh = 160° Eh = 170° Fh = 180° 10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					
Eh = 170° Fh = 180° 10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					
Fh = 180° 10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A 1Fh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh  Frequency of first cycle in close loop startup (% of MAX_SPEED Oh = 1% Oh =					
10h = 190° 11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 390° 19h = 315° 14h = 330° 18h = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh					
11h = 210° 12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED Oh = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					
12h = 225° 13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 290° 18h = 340° 12h = 330° 18h = 340° 16h = N/A 15h =					
13h = 240° 14h = 250° 15h = 260° 16h = 270° 17h = 280° 18h = 390° 19h = 315° 1Ah = 330° 18h = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED Oh = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					
7-4 SLOW_FIRST_CYC_FRE Q  The substitute of the					
15h = 260° 16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED Oh = 1% Oh					
16h = 270° 17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED Oh = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					
17h = 280° 18h = 290° 19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					
18h = 290°   19h = 315°   1Ah = 330°   1Bh = 340°   1Ch = 350°   1Dh = N/A   1Eh = N/A   1Fh = N/A					
19h = 315° 1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  8/W  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED Oh = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					
1Ah = 330° 1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					18h = 290°
1Bh = 340° 1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED Oh = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					19h = 315°
1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED Oh = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					1Ah = 330°
1Ch = 350° 1Dh = N/A 1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED Oh = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					1Bh = 340°
1Dh = N/A 1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED 0h = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					
1Eh = N/A 1Fh = N/A  7-4 SLOW_FIRST_CYC_FRE Q  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED 0h = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					
7-4 SLOW_FIRST_CYC_FRE Q  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED 0h = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					
7-4 SLOW_FIRST_CYC_FRE Q  Oh Frequency of first cycle in close loop startup (% of MAX_SPEED 0h = 1% 1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					
Q					
1h = 2% 2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%	7-4		R/W	0h	
2h = 3% 3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%		Q			
3h = 5% 4h = 7.5% 5h = 10% 6h = 12.5%					
4h = 7.5% 5h = 10% 6h = 12.5%					
5h = 10% 6h = 12.5%					
6h = 12.5%					4h = 7.5%
					5h = 10%
76 - 450/					6h = 12.5%
					7h = 15%
8h = 17.5%					8h = 17.5%
9h = 20%					9h = 20%
Ah = 25%					
Bh = 30%					
Ch = 35%					
Dh = 40%					
Eh = 45%					
Fh = 50%					
	3		R/W	0h	First cycle frequency in open loop for align, double align and IPD
Startup options		EL			
0h = Defined by SLOW_FIRST_CYC_FREQ					
1h = 0Hz					1n = UHZ



Table 5-27. MOTOR\_STARTUP2 Register Field Descriptions (continued)

	Tuble o El . III o	TOIL_CIAL	1101 Z 110	gister i leia Bescriptions (continuea)
Bit	Field	Туре	Reset	Description
2-0	THETA_ERROR_RAMP_	R/W	0h	Ramp rate for reducing difference between estimated theta and open
	RATE			loop theta
				0h = 0.01 deg/ms
				1h = 0.05 deg/ms
				2h = 0.1 deg/ms
				3h = 0.15 deg/ms
				4h = 0.2 deg/ms
				5h = 0.5 deg/ms
				6h = 1 deg/ms
				7h = 2 deg/ms

# 5.3.6 CLOSED\_LOOP1 Register (Offset = 48h) [Reset = 00000000h]

Table 5-28 shows the register to configure close loop settings1.

Table 5-28. CLOSED\_LOOP1 Register Field Descriptions

Bit	Field	Type	Reset	Description
31-30	RESERVED	R/W	0h	Reserved
29-28	CONTROL_MODE	R/W	Oh	FOC Closed loop Mode of operation  0h = Closed Loop Speed Control  1h = Closed Loop Power Control  2h = Closed Loop Torque Control  3h = Voltage Control mode.
27	HIGH_FREQ_FOC_EN	R/W	0b	Enable /Disable High FOC Sampling rate. Higher the Sampling rate, lower the CPU bandwidth available for other tasks.  0h = High Frequency FOC Enable.(Max FOC Frequency 16Khz)  1h = High Frequency FOC Disable(Max FOC Frequency 8Khz)

Register Map

## Table 5-28. CLOSED\_LOOP1 Register Field Descriptions (continued)

Bit	Field			Ster Field Descriptions (continued)
		Туре	Reset	Description
26-22	ILIMIT	R/W	0h	Current limit in Closed loop Torque Mode and Closed loop Speed control in % of CURRENT_BASE
				0h = 7.5%
				1h = 8.0%
				2h = 8.5%
				3h = 9.0%
				4h = 9.5%
				5h = 10%
				6h = 11%
				7h = 12%
				8h = 13%
				9h = 14%
				Ah = 15%
				Bh = 16%
				Ch = 17%
				Dh = 18%
				Eh = 20%
				Fh = 22.5%
				10h = 25%
				11h = 27.5%
				12h = 30%
				13h = 35%
				14h = 40%
				15h = 45%
				16h = 50%
				17h = 55%
				18h = 60%
				19h = 70%
				1Ah = 75%
				1Bh = 80%
				1Ch = 85%
				1Dh = 90%
				1Eh = 95%
				1Fh = 100%
04.00	MTD CTOD	DAA	001-	
21-20	MTR_STOP	R/W	00b	Motor stop method 0h = Hi-z
				1h = Active spin down
				2h = Braking
				3h = Reserved
19	OVERMODULATION_	R/W	0b	Overmodulation enable
	ENABLE			0h = Disable Over Modulation
				1h = Enable Over Modulation



Register Map www.ti.com

## Table 5-28. CLOSED\_LOOP1 Register Field Descriptions (continued)

Bit	Field	Type	Reset	Description (Continued)
18-14	CL_ACC	R/W	0h	Closed loop acceleration
				0h = 0.5Hz/s
				1h = 1Hz/s
				2h = 2.5Hz/s
				3h = 5Hz/s
				4h = 7.5Hz/s
				5h = 10Hz/s
				6h = 20Hz/s
				7h = 40Hz/s
				8h = 60Hz/s
				9h = 80Hz/s
				Ah = 100Hz/s
				Bh = 200Hz/s
				Ch = 300Hz/s
				Dh = 400Hz/s
				Eh = 500Hz/s
				Fh = 600Hz/s
				10h = 700Hz/s
				11h = 800Hz/s
				12h = 900Hz/s
				13h = 1000Hz/s
				14h = 2000Hz/s
				15h = 4000Hz/s
				16h = 6000Hz/s
				17h = 8000Hz/s
				18h = 10000Hz/s
				19h = 20000Hz/s
				1Ah = 30000Hz/s
				1Bh = 40000Hz/s
				1Ch = 50000Hz/s
				1Dh = 60000Hz/s
				1Eh = 70000Hz/s
				1Fh = No limit
13	CL_DEC_CONFIG	R/W	0h	Closed loop deceleration configuration
				0h = Closed loop deceleration defined by CL_DEC
				1h = Closed loop deceleration defined by CL_ACC

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## Table 5-28. CLOSED\_LOOP1 Register Field Descriptions (continued)

Bit	Field		Reset	Description
		Туре		
12-8	CL_DEC	R/W	0h	Closed loop deceleration. This register is used only if AVS is disabled
				and CL_DEC_CONFIG is set to '0' 0h = 0.5Hz/s
				1h = 1Hz/s
				2h = 2.5Hz/s
				3h = 5Hz/s
				4h = 7.5Hz/s
				5h = 10Hz/s
				6h = 20Hz/s
				7h = 40Hz/s
				8h = 60Hz/s
				9h = 80Hz/s
				Ah = 100Hz/s
				Bh = 200Hz/s
				Ch = 300Hz/s
				Dh = 400Hz/s
				Eh = 500Hz/s
				Fh = 600Hz/s
				10h = 700Hz/s
				11h = 800Hz/s
				12h = 900Hz/s
				13h = 1000Hz/s
				14h = 2000Hz/s
				15h = 4000Hz/s
				16h = 6000Hz/s
				17h = 8000Hz/s
				18h = 10000Hz/s
				19h = 20000Hz/s
				1Ah = 30000Hz/s
				1Bh = 40000Hz/s
				1Ch = 50000Hz/s
				1Dh = 60000Hz/s
				1Eh = 70000Hz/s
				1Fh = No limit
7-8	PWM_FREQ_OUT	R/W	0h	Output PWM switching frequency
				0h = 5kHz
				1h = 10kHz
				2h = 16kHz
				3h = 20kHz
				4h = 25kHz
				5h = 32kHz
				6h = 40kHz
				7h = 48kHz
				8h = 50kHz
				9h = 64kHz
				Ah = 80kHz
				Bh = N/A
				Ch = N/A
				Dh = N/A
				Eh = N/A
				Fh = N/A
14	PWM_MODE	R/W	0b	PWM modulation
				0h = Continuous Space Vector Modulation
				1h = Discontinuous Space Vector Modulation
	1			



Register Map www.ti.com

Table 5-28. CLOSED\_LOOP1 Register Field Descriptions (continued)

Bit	Field	Туре	Reset	Description
3	AVS_EN	R/W	0b	AVS enable
				0h = Disable
				1h = Enable
2	DEADTIME_COMP_EN	R/W	0b	Dead-time compensation enable
				0h = Disable
				1h = Enable
1	SPEED_LOOP_DIS	R/W	0b	Speed loop disable
				0h = Enable
				1h = Disable

# 5.3.7 CLOSED\_LOOP2 Register (Offset = 4Ch) [Reset = 00000000h]

Table 5-29 shows the register to configure close loop settings2.

Table 5-29. CLOSED\_LOOP2 Register Field Descriptions

Bit	Field	Туре	Reset	Description
31-28	ACT_SPIN_THR	R/W	0h	Speed threshold for active spin down (% of MAX_SPEED)
				0h = 100%
				1h = 90%
				2h = 80%
				3h = 70%
				4h = 60%
				5h = 50%
				6h = 45%
				7h = 40%
				8h = 35%
				9h = 30%
				Ah = 25%
				Bh = 20%
				Ch = 15%
				Dh = 10%
				Eh = 5%
				Fh = 2.5%
27-24.	BRAKE_SPEED_THRES HOLD	R/W	0h	Speed threshold for BRAKE pin and motor stop options (Low Side Braking or align braking) (% of MAX_SPEED)  0h = 100%
				1h = 90%
				2h = 80%
				3h = 70%
				4h = 60%
				5h = 50%
				6h = 45%
				7h = 40%
				8h = 35%
				9h = 30%
				Ah = 25%
				Bh = 20%
				Ch = 15%
				Dh = 10%
				Eh = 5%
				Fh = 2.5%
				111 - 2.070

www.ti.com Register Map

## Table 5-29. CLOSED\_LOOP2 Register Field Descriptions (continued)

Bit	Field	Type	Reset	Description
23-19	BRK_CURR_THR	R/W	0h	Brake current limit in % of CURRENT_BASE
				Oh = 7.5%
				1h = 8.0%
				2h = 8.5%
				3h = 9.0%
				4h = 9.5%
				5h = 10%
				6h = 11%
				7h = 12%
				8h = 13%
				9h = 14%
				Ah = 15%
				Bh = 16%
				Ch = 17%
				Dh = 18%
				Eh = 20%
				Fh = 22.5%
				10h = 25%
				11h = 27.5%
				12h = 30%
				13h = 35%
				14h = 40%
				15h = 45%
				16h = 50%
				17h = 55%
				18h = 60%
				19h = 70%
				1Ah = 75%
				1Bh = 80%
				1Ch = 85%
				1Dh = 90%
				1Eh = 95%
				1Fh = 100%
18-14	LEAD_ANGLE	R/W	0h	Lead Angle in degrees applied in Voltage Control Mode
				0 - 15 = 1 * Bit Value
				15 - 31 = 2 *( Bit Value -15) + 15
13-0	RESERVED	R/W	0h	Reserved
			I	

Register Map www.ti.com

## 5.3.8 FIELD\_CTRL Register (Offset = 50h) [Reset = 00000000h]

Table 5-30 shows the register to configure Flux Control settings.

## Table 5-30. FIELD\_CTRL Register Bit Descriptions

Bit	Field	Type	Reset	Description
31-7	Reserved	R	0h	Reserved
6	MTPA_EN	R/W	0b	Enable/Disable Maximum Torque Per Ampere Control (MTPA) 0h = Disable MTPA 1h = Enable MTPA
5-4	FLUX_WEAK_REF	R/W	00b	Modulation Index Reference to be tracked in Flux Weakening mode 0h = 70% 1h = 80% 2h = 90% 3h = 95%
3-1	FLUX_WEAK_CURR_RA TIO	R/W	000Ь	Max value of Flux Weakening Current Reference as % of ILIMIT  0h = Only Circular Limit in Place  1h = 80%  2h = 70%  3h = 60%  4h = 50%  5h = 40%  6h = 30%  7h = 20%
0	FLUX_WEAK_EN	R/W	0b	Enable/Disable Flux Weakening Control (MTPA)  0h = Disable Flux Weakening  1h = Enable Flux Weakening

## 5.3.9 FAULT\_CONFIG1 Register (Offset = 54h) [Reset = 00000000h]

Table 5-31 shows the register to configure fault settings1.

## Table 5-31. FAULT\_CONFIG1 Register Field Descriptions

Bit	Field	Type	Reset	Description
31-6	RESERVED	R/W	0h	Reserved
5-2	LCK_RETRY	R/W	0h	Lock detection retry time
				0h = 100ms
				1h = 500ms
				2h = 1s
				3h = 2s
				4h = 3s
				5h = 4s
				6h = 5s
				7h = 6s
				8h = 7s
				9h = 8s
				Ah = 9s
				Bh = 10s
				Ch = 11s
				Dh = 12s
				Eh = 13s
				Fh = 14s

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## Table 5-31. FAULT\_CONFIG1 Register Field Descriptions (continued)

		_		, , , , , , , , , , , , , , , , , , , ,
Bit	Field	Туре	Reset	Description
1-0	MTR_LCK_MODE	R/W	00b	Motor Lock Mode
				0h = Motor lock detection causes latched fault; nFAULT active;
				1h = Fault automatically cleared after LCK_RETRY time.
				2h = Motor lock in report only mode.
				3h = Motor lock detection is disabled

# 5.3.10 FAULT\_CONFIG2 Register (Offset = 58h) [Reset = 00000000h]

Table 5-32 shows the register to configure fault settings2.

## Table 5-32. FAULT\_CONFIG2 Register Field Descriptions

			_CONFIG2 Register Fleid Descriptions	
Bit	Field	Type	Reset	Description
31-27	RESERVED	R/W	0h	Reserved
26	LOCK1_EN	R/W	0b	Lock 1 : Abnormal speed enable  0h = Disable  1h = Enable
25	LOCK2_EN	R/W	0b	Lock 2 : Abnormal BEMF enable  0h = Disable  1h = Enable
24	LOCK3_EN	R/W	0b	Lock 3 : No motor enable 0h = Disable 1h = Enable
23-21	LOCK_ABN_SPEED	R/W	000Ь	Abnormal speed lock threshold (% of MAX_SPEED) 0h = 130% 1h = 140% 2h = 150% 3h = 160% 4h = 170% 5h = 180% 6h = 190% 7h = 200%
20-18	ABNORMAL_BEMF_THR	R/W	000Ь	Abnormal BEMF lock threshold (% of expected BEMF)  0h = 40%  1h = 45%  2h = 50%  3h = 55%  4h = 60%  5h = 65%  6h = 67.5%  7h = 70%



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## Table 5-32. FAULT\_CONFIG2 Register Field Descriptions (continued)

Bit	Field	Type	Reset	Description (Continued)
17-13	NO_MTR_THR	R/W	00000b	No Motor current limit in % of CURRENT_BASE  0h = 7.5%
				1h = 8.0%
				2h = 8.5%
				3h = 9.0%
				4h = 9.5%
				5h = 10%
				6h = 11%
				7h = 12%
				8h = 13%
				9h = 14%
				Ah = 15%
				Bh = 16%
				Ch = 17%
				Dh = 18%
				Eh = 20%
				Fh = 22.5%
				10h = 25%
				11h = 27.5%
				12h = 30%
				13h = 35%
				14h = 40%
				15h = 45%
				16h = 50%
				17h = 55%
				18h = 60%
				19h = 70%
				1Ah = 75%
				1Bh = 80%
				1Ch = 85%
				1Dh = 90%
				1Eh = 95%
				1Fh = 100%
12-8	RESERVED	R/W	0h	Reserved.
7-5	MIN_VM_MOTOR	R/W	000b	Minimum voltage for running motor in % of BASE_VOLTAGE
			0002	0h = No Limit
				1h = 5%
				2h = 10%
				3h = 12%
				4h = 15%
				5h = 18%
				6h = 20%
				7h = 25%
4	MIN_VM_MODE	R/W	0b	Undervoltage fault mode
	t_v.iii_iii3bE	1 3, 4 4		0h = Latch on Undervoltage
				1h = Automatic clear if voltage in bounds
	1			

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Table 5-32. FAULT\_CONFIG2 Register Field Descriptions (continued)

Bit	Field	Туре	Reset	Description
3-1	MAX_VM_MOTOR	R/W	000b	Maximum voltage for running motor in % of BASE_VOLTAGE
				0h = 60%
				1h = 65%
				2h = 70%
				3h = 75%
				4h = 80%
				5h = 85%
				6h = 90%
				7h = Max Voltage
0	MAX_VM_MODE	R/W	0b	Overvoltage fault mode
				0h = Latch on Overvoltage
				1h = Automatic clear if voltage in bounds

## 5.3.11 MISC\_ALGO Register (Offset = 5Ch) [Reset = 00000000h]

Table 5-33 shows the register to multiple miscellaneous Algorithm Configuration.

Table 5-33. MISC ALGO Register Field Descriptions

Table 5-33. MISC_ALGO Register Field Descriptions				
Bit	Field	Type	Reset	Description
31-22	RESERVED	R/W	0h	Reserved
21-20	IPD_MAX_OVERFLOW	R/W	00b	Maximum Number of Timer Overflows before hitting the IPD Time Out Fault with 16 bit Timer running at 80Mhz 0b = 5 Overflows (4mS) 1b = 10 Overflows (8mS) 10b = 20 Overflows (16mS) 11b = 40 Overflows (32mS)
19-16	CL_SLOW_ACC	R/W	Oh	Close loop acceleration when estimator is not yet fully aligned  0h = 0.1Hz/s  1h = 1Hz/s  2h = 2Hz/s  3h = 3Hz/s  4h = 5Hz/s  5h = 10Hz/s  6h = 20Hz/s  7h = 30Hz/s  8h = 40Hz/s  9h = 50Hz/s  Ah = 100Hz/s  Bh = 200Hz/s  Ch = 500Hz/s  Dh = 750Hz/s  Eh = 1000Hz/s  Fh = 2000Hz/s
15	RESERVED	R	0b	Reserved
14	FAST_ISD_EN	R/W	0b	Fast initial speed detection enable 0h = Disable Fast ISD 1h = Enable Fast ISD
13-12	ISD_STOP_TIME	R/W	00b	Persistence time for declaring motor has stopped 0h = 1ms 1h = 5ms 2h = 50ms 3h = 100ms



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Table 5-33. MISC\_ALGO Register Field Descriptions (continued)

D:4	Table 5-33. MISC_ALGO Register Field Descriptions (continued)						
Bit	Field	Type	Reset	Description			
11-10	ISD_RUN_TIME	R/W	00b	Persistence time for declaring motor is running 0h = 1ms 1h = 5ms 2h = 50ms 3h = 100ms			
9-8	ISD_TIMEOUT	R/W	00b	Timeout in case ISD is unable to reliably detect speed or direction 0h = 500ms 1h = 750ms 2h = 1000ms 3h = 2000ms			
7-5	AUTO_HANDOFF_MIN_B EMF	R/W	000Ь	Minimum BEMF for handoff  0h = 0mV  1h = 50mV  2h = 100mV  3h = 250mV  4h = 500mV  5h = 1000mV  6h = 1250mV  7h = 1500mV			
4-3	BRAKE_CURRENT_PER SIST	R/W	00b	Persistence time for current below threshold during brake 0h = 50ms 1h = 100ms 2h = 250ms 3h = 500ms			
2-0	REV_DRV_OPEN_LOOP _DEC	R/W	000b	% of open loop acceleration to be applied during open loop deceleration in reverse drive  0h = 50%  1h = 60%  2h = 70%  3h = 80%  4h = 90%  5h = 100%  6h = 125%  7h = 150%			

# 5.3.12 PIN\_CONFIG Register (Offset = 60h) [Reset = 00000000h]

Table 5-34 shows the register to configure hardware pins.

## Table 5-34. PIN\_CONFIG Register Field Descriptions

Bit	Field	Туре	Reset	Description
31-20	RESERVED	R/W	0h	Reserved
19	VDC_FILT_DIS	R/W	0b	Vdc Filter Disable 0h = Enabled 1h = Disabled
18-3	RESERVED	R/W	0h	Reserved
2	BRAKE_PIN_MODE	R/W	0b	Brake pin mode 0h = Low side Brake 1h = Align Brake

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Table 5-34. PIN\_CONFIG Register Field Descriptions (continued)

Bit	Field	Type	Reset	Description
1-0	BRAKE_INPUT	R/W	00b	Brake pin override
				0h = Hardware Pin BRAKE
				1h = Override pin and brake / align according to BRAKE_PIN_MODE
				2h = Override pin and do not brake / align
				3h = Hardware Pin BRAKE

# 5.3.13 PERI\_CONFIG Register (Offset = 64h) [Reset = 00000000h]

Table 5-35 shows the register to peripheral.

Table 5-35. PERI\_CONFIG1 Register Field Descriptions

Bit	Field	Type	Reset	Description Descriptions
31-15	RESERVED	R	0h	Reserved
14-9	MCU_DEAD_TIME	R/W	0h	Dead time applied between the High Side and Low side switches = 50ns × MCU_DEAD_TIME
8-4	BUS_CURRENT_LIMIT_E	R/W	00000b	Bus Current Limit in % of CURRENT_BASE  0h = 7.5%  1h = 8.0%  2h = 8.5%  3h = 9.0%  4h = 9.5%  5h = 10%  6h = 11%  7h = 12%  8h = 13%  9h = 14%  Ah = 15%  Bh = 16%  Ch = 17%  Dh = 18%  Eh = 20%  Fh = 22.5%  10h = 25%  11h = 27.5%  12h = 30%  13h = 35%  14h = 40%  15h = 45%  16h = 50%  17h = 55%  18h = 60%  19h = 70%  1Ah = 75%  1Bh = 80%  1Ch = 85%  1Dh = 90%  Eh = 95%  IFh = 100%  Bus current limit enable
	NABLE			0h = Disable 1h = Enable



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Table 5-35. PERI\_CONFIG1 Register Field Descriptions (continued)

Bit	Field	Туре	Reset	Description
2-1	DIR_INPUT	R/W	00b	DIR pin override 0h = Hardware Pin DIR 1h = Override DIR pin with clockwise rotation OUTA-OUTB-OUTC 2h = Override DIR pin with counter clockwise rotation OUTA-OUTC-OUTB 3h = Hardware Pin DIR
0	DIR_CHANGE_MODE	R/W	0b	Response to change of DIR pin status  0h = Follow motor stop options and ISD routine on detecting DIR change  1h = Change the direction through Reverse Drive while continuously driving the motor

## 5.4 User Status Registers (Base Address = 0x20200430h)

User Status Registers are set of consolidated variables available for user to read the Motor status and analyze the control performance.

Below are the set of Status Registers that can be imported in the CCS expression window using structure pointer *pUserStatusRegs*.

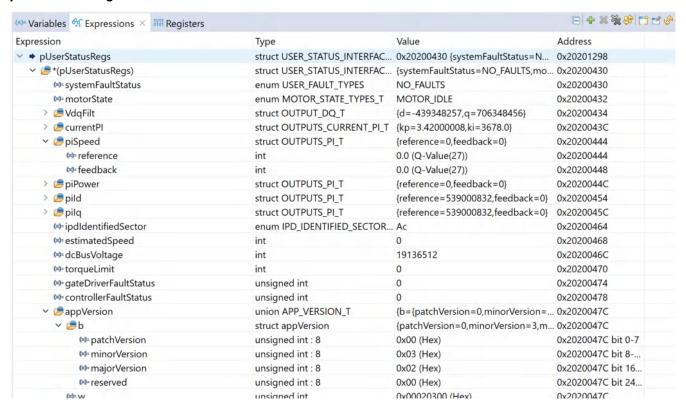


Figure 5-5. User Status Registers in CCS Debug Mode

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Table 5-36 lists the definitions of variables available for monitoring.

## Table 5-36. User Status Registers

		User Status Regis	
Variables	Туре	Reset Value	Description
SYSTEM_FAULT_STATUS	USER_FAULT_TYPES	NO_FAULT	Defines the status of motor faults.  MOTOR_STALL: Indicates motor lock faults - abnormal BEMF, no motor, abnormal speed  VOLTAGE_OUT_OF_BOUNDS:Indicates undervoltage or overvoltage.  LOAD_STALL:Indicates IPD fault.  HARDWARE_OVER_CURRENT:Indicates DC bus current limit fault  HV_DIE: Indicates gate driver fault if applicable.
MOTOR_STATE	MOTOR_STATE_TYPE	MOTOR_IDLE	Defines the state of Current Motor Running Status  MOTOR_IDLE: Motor Idle State  MOTOR_ISD: Motor in Initial Speed Detection state  MOTOR_TRISTATE: Motor in Tristate or Hi-Z mode.  MOTOR_BRAKE_ON_START: Motor Brake during Start up.  MOTOR_IPD: Motor in Initial position  Detection  MOTOR_SLOW_FIRST_CYCLE: Motor in Slow First Cycle Startup Method.  MOTOR_ALIGN: Motor in Align Start State  MOTOR_OPEN_LOOP: Motor in openloop ramp up state.  MOTOR_CLOSE_LOOP_UNALIGNED:  Motor in Closed loop run State with Angle unaligned  MOTOR_CLOSE_LOOP_ALIGNED: Motor in closed loop run state aligned angle.  MOTOR_SOFT_STOP: Motor in Stop state  MOTOR_BRAKE_ON_STOP Motor in Brake stop state  MOTOR_FAULT Motor in Motor Fault State
V_DQ_FILT	IQ GLOBAL 27	IQ27(0)	Indicates the filtered Vd and Vq applied to the motor. Output of current PI controllers.
I_DQ_PI	IQ GLOBAL 27	IQ27(0)	Indicates the Kp and Ki values of current PI controllers.
PI_SPEED PI_POWER	IQ GLOBAL 27	IQ27(0)	Indicates the reference and feedback values of speed PI controller set by FOC algorithm in PU.  Indicates the reference and feedback values of Power PI controller set by FOC algorithm in
			PU.
PI_ID	IQ GLOBAL 27	IQ27(0)	Indicates the reference and feedback values of direct current PI controller set by FOC algorithm in PU.
PI_IQ	IQ GLOBAL 27	IQ27(0)	Indicates the reference and feedback values of quadrature current PI controller set by FOC algorithm in PU.
IPD_IDENTIFIED_SECTOR	COMMUTATION_STATE	0b	Indicates the IPD identified nearest rotor state.
ESTIMATED_SPEED	IQ GLOBAL 27	IQ27(0)	Indicates the motor speed in PU estimated by the FOC observer algorithm.

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Table 5-36. User Status Registers (continued)

Variables	Туре	Reset Value	Description
DC_BUS_VOLTAGE	IQ GLOBAL 27	IQ27(0)	Indicates the DC bus voltage value in PU
TORQUE_LIMIT	IQ GLOBAL 27	IQ27(0)	Indicates the quadrature current controller saturation limit set by FOC. This value is based on the limit set in ClosedLoop1 configuration.
GATE_DRIVER_FAULT_STATUS	Unsigned Int	0x00000000h	Defines the Index of Gate Driver Specific faults as defined in gateDriverLib.
CONTROLLER_FAULT_STATUS	Unsigned Int	0x00000000h	Defines the Index of FOC Control Algorithm Specific Faults as defined in main.h.
APP_VERSION	Unsigned hex	0x00000000h	Defines the Version number of Application Firmware

## 6 Basic Tuning

The goal of this section is to help spin user motors successfully in closed loop with minimal configurations. This section provides standardized mandatory steps to tune parameters for successful Motor spin-up in closed loop. "Closed loop" is defined as sensorless closed loop Field-oriented control where the motor spins at the commanded Speed/Torque reference.

## 6.1 System Configuration Parameters

The system configuration defines the primary parameters associated with the motor control system to start the motor spinning in closed loop torque/speed control modes.

Below are the set of System parameters that are to be specified for accurate sensorless FOC operation. These variables can be added in the expression window using the pUserInputRegs.

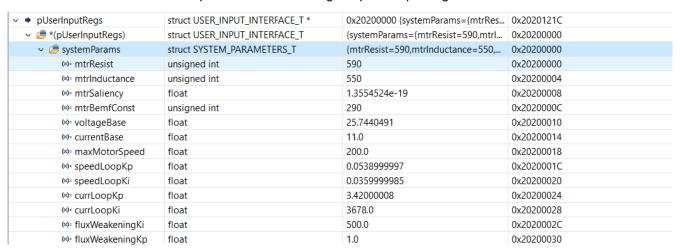


Figure 6-1. System Configurations Registers in CCS Debug Mode

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## 6.1.1 Configuring System Parameters From GUI

Configure the system parameters using the **System Configuration** page in the GUI as shown in Figure 6-2. If the parameters are already programmed in the firmware for a given system, the GUI page displays the default programmed values upon pressing READ ALL REGS. These parameters to be updated accordingly from the below steps.

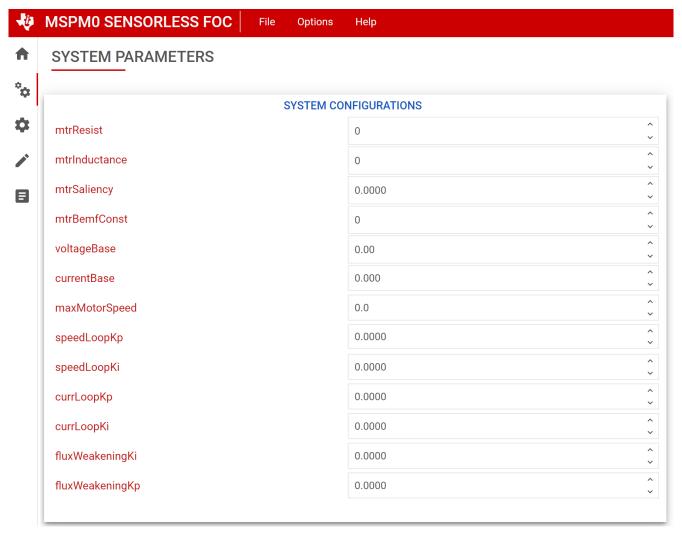


Figure 6-2. GUI System Parameter Configuration

## 6.1.2 Motor Resistance in Milliohms ( $m\Omega$ )

Using the motor data sheet, the user can input the motor phase resistance in milliohms ( $m\Omega$ ) using the *mtrResist* parameter in the **System Configuration** page. If the motor does not have a data sheet, then measure the phase-to-phase resistance across any two phases using a digital multimeter and calculate the phase resistance by dividing the phase-to-phase resistance by 2 as shown in Resistance Measurement

Phase resistance = Measured Phase to Phase Resistance 
$$\times$$
 (0.5) (2)



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The motor phase resistance refers to the equivalent phase to center tap resistance, R<sub>PH</sub>, as shown in Figure 6-3. This measurement is valid for both star wound and delta wound motors.

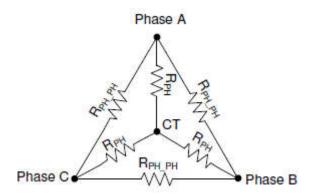


Figure 6-3. Resistance Measurement

## 6.1.3 Motor Inductance in Microhenries (µH)

From the motor data sheet, input the motor phase inductance in microhenry (µH) using the *mtrInductance* parameter in the **System Configuration** page. To know the motor inductance, measure the phase-to-phase inductance at 1kHz across any two phases using an LCR meter. Calculate the phase inductance by dividing the phase to phase inductance by 2 as shown in Figure 6-4.

Phase Inductance = Measured Phase to Phase Inductance  $\times$  (0.5) (3)

Motor phase inductance refers to the inductance from the phase output to the center tap, L<sub>PH</sub>, as shown in Figure 6-4. For motors with different phase to phase inductances(Salient pole motors), measure all three phase to phase inductances and calculate the average and use this value as the phase to phase inductance. This measurement is valid for both star wound and delta wound motors.

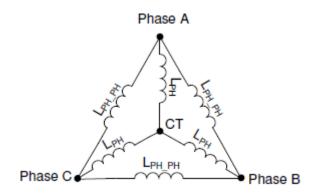


Figure 6-4. Inductance Measurement

## 6.1.4 Saliency of IPMSM Motor

Saliency of an IPMSM motor is a measure of variation in Inductance between the quadrature axis and direct rotor axis. For FOC algorithm this value is to be given as (Lq - Ld) / (Ld + Lq) in float variable.

The simplest method to deduce the Ld and Lq values is by measuring the inductance across any two phases and vary the rotor position slowly for one full rotation. The maximum measured inductance value can be noted as Lq, and the minimum measured inductance value can be noted as Ld.

## 6.1.5 Motor BEMF Constant

Using the motor's data sheet, the user can input the motor's BEMF constant Ke in mV/Hz and program mtrBEMFConst in the **System Configuration** Page as Ke  $\times$  10.

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Equation 4 and Equation 5 can be used to convert Ke in mV/rpm, mV\*sec/rad and torque constant Kt to Ke in mV/Hz.

$$BEMF Constant \left[ \frac{mV}{Hz} \right] = \frac{Ke \left[ \frac{mV}{RPM} \right] * 60}{\# \ pole \ pairs}$$
(4)

$$BEMF Constant \left[ \frac{mV}{Hz} \right] = \frac{Kt \left[ \frac{mN \cdot m}{A} \right]^* 2\pi}{\# pole \ pairs}$$
 (5)

If the motor does not have a data sheet, measure the voltage across any two phases of the motor using an oscilloscope by manually spinning the motor. A sinusoidal or trapezoidal voltage appears on the oscilloscope. Measure the peak voltage Ep in milli-volts and time period Tp in seconds. Calculate BEMF constant Ke as shown in Equation 6.

Bemf Constant Ke = Ep \* Tp / 
$$\sqrt{3}$$
 (6)

## 6.1.6 Base Voltage (V)

Base voltage represents the maximum measurable bus voltage and phase voltages in the motor control system. Input the system base voltage (in volts) in the *voltageBase* parameter of the **System Configuration** page in GUI. The user can compute the system base voltage based on the Voltage scaling resistor divider bridge values R1 and R2 and the Full Scale ADC voltage (FSV) of 3.3V as shown in Equation 7. For hardware configuration of the voltage divider scaling ratio, see Figure 2-3.

$$Base_{Voltage} = \frac{ADC \text{ Full Scale Value}}{Voltage \text{ Divider Scaling Ratio}} = \frac{3.3V}{R1}$$

$$\frac{R1}{R1 + R2}$$
(7)

For example, in a system with resistor divider scaling ratio of 1/20 from DC supply voltage to ADC input, the base voltage or maximum measurable system voltage by the ADC is 3.3V / (1/20) = 66V.

#### 6.1.7 Base Current (A)

Base current represents the maximum measurable motor phase current in the motor control system. The user inputs the system base current (in Amps) in the *currentBase* parameter of the **System Configuration** page in GUI. The user can compute the system base current based on the current sense amplifier gain (CSAGAIN) in volts/amp and the full-scale ADC voltage (FSV) of 3.3V and Zero Current Offset voltage from the CSA as shown in below equation

Base Current = 
$$\frac{3.3v - ADC\_Offset\_volts}{CSA\_GAIN\left(\frac{V}{A}\right)}$$
 (8)

In case of bidirectional current sensing the zero-current offset is often selected as 1.65V, half of ADC Full Scale Voltage 3.3v.

In case of Unidirectional Current Sensing, 80-90% of ADC Full Scale Voltage is typically used for +ve Current Sensing. In general, Unidirectional current sensing is used in single shunt DC Bus current sensing architecture.

If the system uses a current sense resistor (R<sub>SENSE</sub>) with CSAGAIN units mentioned in volts/volt (V/V), the CSA gain in volts/amp can be computed using below equation .

$$CSA GAIN\left(\frac{\text{volts}}{\text{Amp}}\right) = R_{\text{sense}} \times CSA GAIN\left(\frac{\text{volts}}{\text{volts}}\right)$$
(9)

For example, in a system with CSAGAIN = 0.15V/A and ADC Offset Voltage of 1.65v, the base current or maximum measurable system current by the ADC is (3.3v - 1.65v)/(0.15V/A) = 11A.

In system with Rsense of 10milli Ohms, CSA gain of 10V/V, ADC Offset Voltage of 0.4125v, the base current is derived as (3.3-0.4125)/(10m \* 10) = 28.875A

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#### Note

In some driver devices, CSAGAIN can be set as a register over I2C or SPI or by hardware using a resistor value. For how to configure the driver CSAGAIN setting, see the device-specific driver data sheet.

## 6.1.8 Maximum Motor Electrical Speed (Hz)

Using the motor's data sheet, the user can input the maximum motor electrical speed in Hz using the *maxMotorSpeed* parameter in the **System Configuration** Page. If this data is not available, the user can input the number of pole pairs and motor mechanical speed in RPM. The user can convert the motor mechanical speed in RPM to motor electrical speed in Hz using Equation 10.

$$f_{Electrical} = \frac{n_{PolePairs} \cdot \omega_{Mechanical}}{60}$$
 (10)

#### Where:

- $\omega$  Mechanical is the mechanical speed in units revolutions per minute (RPM)
- f Electrical is the electrical speed in units of hertz (Hz)
- · n PolePairs is the number of motor pole pairs

#### Note

To determine the number of motor poles without a motor data sheet:

- 1. Use a lab power supply and make sure the current limit is set to less than the motor rated current. Do not turn on the supply.
- 2. Connect V+ of the supply to phase A and V- of the supply to phase B of the motor. Any 2 of the 3 phases can be chosen at random if the phases not labeled.
- 3. Turn on supply, The rotor settles at one position by injecting current.
- 4. Manually rotate the rotor until rotor snaps to another settle position. Rotor settle down at various positions around one mechanical cycle.
- 5. Count the number of settle-down positions for one fully mechanical cycle, which is the number of pole pairs. Multiplying by two calculates the number of poles.

Be careful of gearing systems within a motor. The gearing ratio determines how many rotor revolutions correlate to the shaft mechanical revolution.

### 6.1.9 Maximum Motor Power(W)

User need to input the Maximum Power Rating of the motor when Closed loop Power Control is required. To determine the Maximum Rated Power of the motor, see the Motor data sheet and compute the product of Rated Motor Voltage in Volts and Rated Motor Current in Amps and feed the value to MOTOR\_MAX\_POWER in the System parameters.

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## 6.2 Control Configurations for Basic Motor Spinning

After configuring the system parameters in the GUI, the user can go to the **Register Map** page and configure the Register Map Tuning parameters as shown in Figure 6-5. By default, the firmware has the recommended settings, which can be read into the GUI by pressing the "READ ALL REG" button.

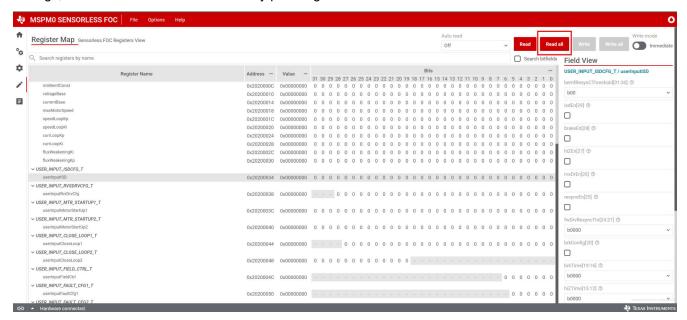


Figure 6-5. Register Map GUI Page

### 6.2.1 Basic Motor Startup

Sensorless FOC relies on the position detection estimated from BEMF to accurately drive the motor. At startup, since the motor can be at standstill or the motor can be spinning with unknown speeds, the rotor position is unknown.

The FOC algorithm has various startup algorithms to reliably start the motor and ramp the motor with sufficient speeds or estimate the position of an already spinning motor before switching to the estimator for continuous rotor position tracking. The following sections describe the basic configuration needed to start and ramp the motor from standstill until open-loop spin up. If any motor faults are observed during basic open-loop spin up, see Section 6.3.

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#### 6.2.1.1 Disable ISD

Initial Speed Detection (ISD) is a feature to enter the motor automatically when the motor is already spinning. This is also called Headwind/Tailwind startup, or Catch-on-the-fly startup. For basic spinning for motor, the ISD feature is disabled by default by setting *isdEn* = 0 on the **Register Map** page. For basic motor tuning, the motor is expected to be at standstill before giving the speed command. To tune the motor for ISD, refer to Section 7.

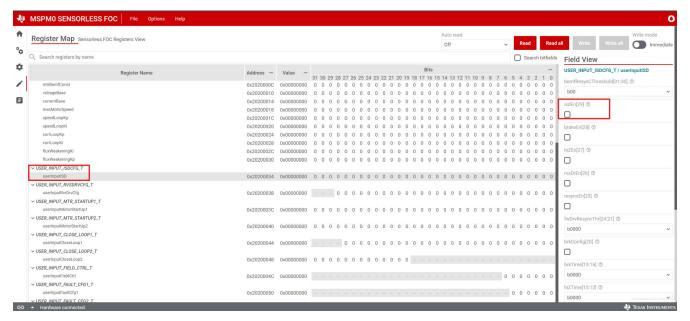


Figure 6-6. Disabling ISD in GUI

### 6.2.1.2 Motor Start Option - Align

When the motor is ramping up from standstill, the Motor Align startup algorithm forces the rotor to align to a fixed ALIGN\_ANGLE with a defined current limit acting as a torque reference for a predefined ALIGN\_TIME. By default, the motor startup option is set as Align (*mtrStartUpOption* = 0b) in the MTR\_STARTUP of MOTOR\_STARTUP1 configuration. For basic spinning, use the default parameters which works for most of the motors.

If the motor fails to align for the given load setup, increase the *alignOrSlowCurrentLimit* parameter on the **Register Map** page. For fine tuning the Motor Align configuration, see Section 7.

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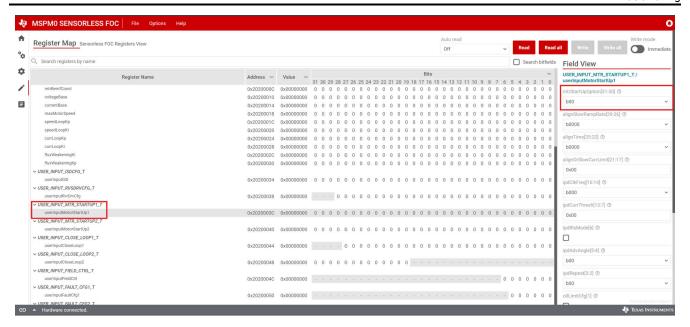


Figure 6-7. Motor Startup in GUI

### 6.2.1.3 Motor Open Loop Ramp

To estimate the rotor position accurately, the motor needs to build sufficient BEMF before switching to closed loop. During startup, the FOC algorithm accelerates the motor with a second order open loop ramp profile to increase the speed until sufficient BEMF is built. By default, for basic spin up of motor, the open loop ramp up parameters are configured with a linear first order configuration with sluggish acceleration, which works for most of the motors. Disable switching to closed loop control to verify the appropriate functionality of open loop, using closedloopDis = 1b in ALGO\_DEBUG\_CTRL on the **Motor Tuning** page. To further optimize the startup time, see Section 7 to fine tune the startup performance.

Depending on the load of the motor, tune the OL\_ILIMIT to the lowest possible value for smooth handoff once the closed loop is enabled ( *closedloopDis* = 0b).

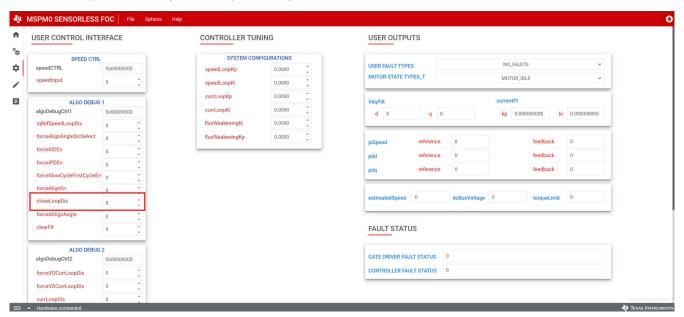


Figure 6-8. Setting Closed Loop Disable in GUI

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#### 6.2.1.4 Motor Open Loop Debug

If motor fails to spin in open loop continuously or if motor current oscillates without spinning the motor, the user can fine tune the open loop configurations in the RAM ALGO DEBUG 2 parameters.

To verify the signal path or check the motor parameters accuracy, the user can disable the current loop by setting the *currLoopDis* bit and setting the *forceVQCurrLoopDis* and *forceVDCurrLoopDis* on the **Register Map** page.

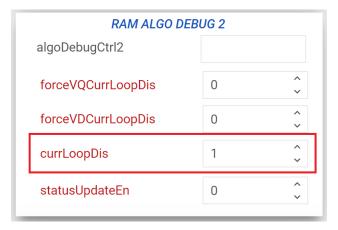


Figure 6-9. Disabling Current Loop in GUI

Adjust Vd and Vq values to spin the motor. Once the motor is spinning at a constant speed, observe the Id and Ig outputs in the User Outputs section of the **Motor Tuning** page to check the stability of the current loop.

## 6.2.2 Controller Configuration for spinning the Motor in Closed Loop

After tuning the open loop with the motor spinning continuously in the open loop state, the user can switch to closed loop by clearing *closedloopDis* = 0b in ALGO\_DEBUG\_CTRL on the **Motor Tuning** page. Follow the below steps to achieve closed loop speed control.

## 6.2.2.1 PI Controller Tuning for Closed Loop Speed Control

#### 6.2.2.1.1 Current Controller Tuning

The FOC Algorithm uses two current PI controllers: one each for Id and Iq to control flux and torque separately. Kp and Ki coefficients are the same for both PI controllers and are configured through *currLoopKp* and *currLoopKi* in the **Motor Tuning** page.

For the basic tuning, configure *currLoopKp* and *currLoopKi* parameters as "0" in Controller Tuning tab so that these values are auto-computed based on the motor parameters and reflected in the User Outputs section of the **Motor Tuning** page in the GUI as highlighted in below figure. These values can be further updated for fine tuning the performance and controlling the dynamics of the system. Typically the default generated Kp and Ki values can be further scaled down 3 to 10 times to meet the desired overdamped response.

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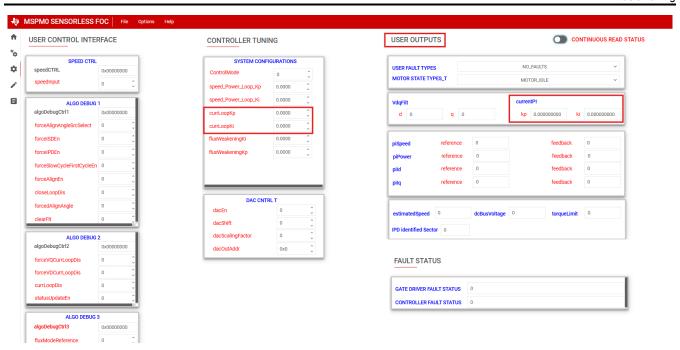


Figure 6-10. PI Loop Tuning in GUI Motor Tuning page

### 6.2.2.1.2 Speed Controller Tuning

The FOC Algorithm uses an integrated speed control loop /Power Control Loop that helps maintain a constant speed/ Constant power over varying operating conditions. The Kp and Ki coefficients are configured through <code>speedLoopKp</code> and <code>speedLoopKi</code> in the "System Configurations" section on the <code>Motor Tuning</code> page. The output of the speed loop / power Loop is used to generate the current reference for torque control. The output of the speed loop /power Loop is limited by configuring <code>iLIMIT</code> in the closedLoop1 configuration in the Register Map page of GUI. When output of the speed loop / Power Loop saturates, the integrator is disabled to prevent integral wind-up.

To tune the Kp and Ki values for speed loop:

- 1. Configure the motor to spin continuously in open loop by setting *closedloopDis* to 1b. Disable the automatic handoff by setting *autoHandOffEn* to *0b*.
- 2. Set the closed loop hand off threshold to around 50% of maximum speed using olClHandOffThr.
- 3. Set the *iqRampEn* bit to 1b in the userInputMotorStartUp1 register.
- 4. The current reference gradually decreases and settles down to the lowest possible lqref to run at the given threshold speed.
- 5. Speed loop Kp [SPD\_LOOP\_KP] is calculated using this equation: SpeedLoop  $K_p$  = Current Reference at olClHandOffThr in Amps / olClHandOffThr in Hz
- 6. Speed loop Ki [SPD\_LOOP\_KI] is calculated using this equation: Speed Loop  $K_i$  = Speed Loop  $K_p \times 0.1$
- 7. Enable closed loop by clearing the closedloopDis to (0b) in the configuration in the **Register Map** page of the GUI.

#### Note

The tuning of speed loop Kp and Ki is experimental. If the above recommendation does not work, manually tune speed loop Kp and Ki until the desired results are achieved.



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Table 6-1 shows general guidelines to change controller gains.

Table 6-1. Steady State and Transient Response Trends With Increase in PI Loop Gain Coefficients

Parameter	Rise Time	Overshoot	Settling Time	Stead State Error	Stability
Кр	Decreases	Increases	Small Change	Decreases	Degrades
Ki	Decreases	Increases	Increases	Eliminates	Degrades

### 6.2.2.2 Testing for Successful Startup Into Closed Loop

## 1. Apply a nonzero speed command.

Change the "Speed Input Command" to a nonzero value. When the speed command is issued, the device starts to commutate and the motor spins at a speed that is proportional to Speed Command × MAXIMUM MOTOR SPEED / 32767.

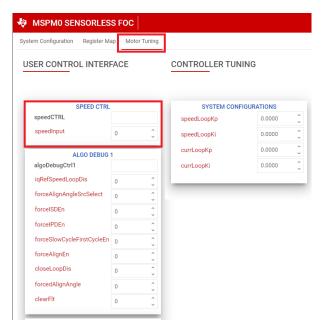


Figure 6-11. Setting Speed Input From GUI

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## 2. Check if motor spins in closed loop at commanded speed.

Enable the "Continuous Read status" toggle button towards the bottom right corner of the GUI and monitor the Fault Status register. If no faults is triggered, move to the Section 7.

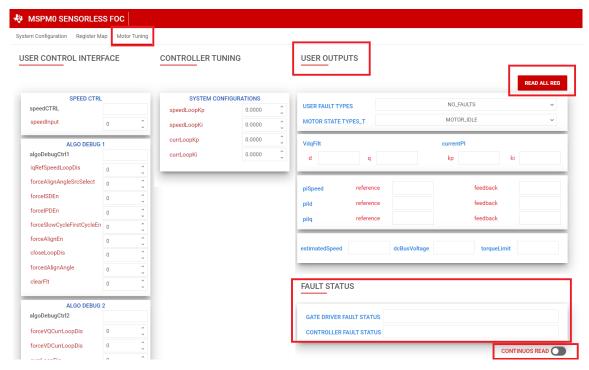


Figure 6-12. Reading Fault Status From GUI

- 3. If any fault is triggered, tune the configuration for fault handling using these steps:
  - a. Set zero speed command by setting the Speed Input command to 0.
  - b. Clear the fault status registers by setting the clear fault bit (*ClearFlt*) bit in the ALGO DEBUG CTRL1 register.
  - c. Check Section 6.3 for steps to debug faults.

## 6.3 Fault Handling

The following sections describe faults that can be triggered based on the default register configuration.

## 6.3.1 Abnormal BEMF Fault [ABN\_BEMF]

This fault is triggered when the estimated BEMF voltage drops below the programmed Abnormal BEMF threshold percentage [ABNNORMAL\_BEMF\_THR]. For example, if the estimated or measured Ke is 5mV/Hz and the programmed Abnormal BEMF threshold is 40%, this fault is triggered when the estimated Ke drops below 2mV/Hz. This fault can also be triggered when the programmed Ke is inaccurate.

There are two cases for Abnormal BEMF threshold:

Case 1: Estimated BEMF voltage drops when the motor speed drops. Motor speed can drop due to load dynamics (sudden change in load). For applications with load dynamics, the speed is expected to drop and recover back. Because the speed drops, the BEMF voltage also drop and can trigger this fault. For such applications, the recommended value of 10% is to be set for the Abnormal BEMF threshold to avoid triggering this fault.

**Case 2**: This fault can be triggered if the programmed Ke is inaccurate. Follow steps recommended in section MOTOR\_BEMF\_CONSTANT to obtain accurate Ke.



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## 6.3.2 Monitoring Power Supply Voltage Fluctuations for Voltage Out of Bound Faults

In applications where the power supply fluctuates, user needs to specify the minimum and maximum power supply voltage range. During an undervoltage condition, the motor operates in overmodulation region to achieve the target speed leading to current distortion, inefficiency or noise. During an overvoltage condition, the MOSFETs and motor are stressed with continued operation in high voltage.

**Tuning Under Voltage Limit 1**: Keep decreasing the supply voltage until there is a drop in the speed. Measure the bus voltage at which the speed drops and set MIN\_VM\_MOTOR to that value. Range of minimum bus voltage that can be configured is between 0 to 25% of Maximum BASE\_VOLTAGE.

**Tuning Over Voltage Limit**: Keep increasing the bus voltage to a point where the motor phase voltage reaches the maximum rated voltage of the motor. MAX\_VM\_MOTOR is the bus voltage at which motor phase voltage reaches the maximum rated voltage of the motor. Range of maximum bus voltage that can be configured is between 60% to Maximum BASE\_VOLTAGE.

### Note

The FOC Algorithm provides an undervoltage recovery mode [MIN\_VM\_MODE] and an overvoltage recovery mode [MAX\_VM\_MODE]. Undervoltage recovery mode can be configured to either automatically clear Undervoltage fault [MTR\_UNDER\_VOLTAGE] or latch on Undervoltage fault. Overvoltage recovery mode can be configured to either automatically clear Overvoltage fault [MTR\_OVER\_VOLTAGE] or latch on Overvoltage fault.

## 6.3.3 No Motor Fault [NO MTR]

This fault is triggered when the phase current is below the No motor lock threshold % of base current.

- 1. Make sure the motor phases are connected to the terminals as shown in the Hardware User Guide.
- 2. If the fault persists, decrease the No-Motor lock current threshold [NO MTR THR].

## 7 Advanced Tuning

This section helps you spin motors successfully in closed loop with minimal configurations. This section provides standardized mandatory steps to tune parameters for successful motor spin-up in closed loop. Closed loop is defined as the sensorless closed loop where motor spins at the commanded speed and torque reference.

## 7.1 Control Configurations Tuning

## 7.1.1 Control Mode of Operation

FOC Application can be controlled in below four modes using the variable CONTROL\_MODE in CLOSED\_LOOP1 Register. The reference input for Speed/Power/Torque/Voltage is configured through the SPEED\_CTRL register.

#### 7.1.1.1 Closed Loop Speed Control Mode

This mode can be selected by setting the CONTROL\_MODE in CLOSED\_LOOP1 Register as 0h. In speed control mode, the speed of the motor (Electrical Hz) is controlled using a closed loop PI control according to the input reference set as SPEED\_CTRL value in Speed Control Register (P.U value in IQ15 format). The P.U speed is computed as the ACTUAL\_MOTOR\_SPEED / MOTOR\_MAX\_SPEED value configured in SYSTEM\_PARAMETERS.

Example: For MOTOR\_MAX\_SPEED set to 100Hz, Setting reference Input in SPEED\_CTRL to 0x3FFFh (0.5 P.U in IQ15) sets the Motor Speed to 50Hz.

## 7.1.1.2 Closed Loop Power Control Mode

This mode can be selected by setting the CONTROL\_MODE in CLOSED\_LOOP1 Register as 1h. In power control mode, the input electrical Power of the motor (Watts) is controlled using a closed loop PI control according to the input reference set as SPEED\_CTRL value in Speed Control Register (P.U value in IQ15 format). The P.U power is computed as the ACTUAL\_MOTOR\_POWER / MOTOR\_MAX\_POWER value configured in SYSTEM\_PARAMETERS.

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Example: For MOTOR\_MAX\_POWER set to 100Watts, Setting reference Input in SPEED\_CTRL to 0x3FFFh (0.5 P.U in IQ15) operates the Motor at a constant power of 50W.

## 7.1.1.3 Closed Loop Torque Control Mode

This mode can be selected by setting the CONTROL\_MODE in CLOSED\_LOOP1 Register as 2h. In Torque control mode, the Torque Component current Iq of the motor (in Amps) is controlled using a closed loop PI control according to the input reference set as SPEED\_CTRL value in Speed Control Register (P.U value in IQ15 format). The P.U Torque Component of Current is computed as the TORQUE\_CURRENT\_COMPONENT / CURRENT\_BASE value configured in SYSTEM\_PARAMETERS.

Example: For CURRENT\_BASE set to 10 Amps, Setting reference Input in SPEED\_CTRL to 0x3FFFh (0.5 P.U in IQ15) operates the Motor at a constant Iq current of 5A (Appropriate load to be connected to the motor).

## 7.1.1.4 Voltage Control Mode

This mode can be selected by setting the CONTROL\_MODE in CLOSED\_LOOP1 Register as 3h. In Voltage control mode, the modulation index of the motor is controlled according to the input reference set as SPEED\_CTRL value in Speed Control Register (P.U value in IQ15 format).

Example: Setting reference Input in SPEED\_CTRL to 0x3FFFh (0.5 P.U in IQ15) operates the Motor with a constant modulation Index of 0.5.

Lead Angle Control : In Voltage control mode , Lead Angle can be adjusted to derive the best efficiency from the motor for a given speed. LEAD\_ANGLE configuration in CLOSED\_LOOP2 register can be used to set the Lead Angle.

For a given LeadAngle θ, Appled Voltages Vq and Vd are defined as

 $Vq = MODULATION_INDEX * Cos\theta$ 

 $Vd = MODULATION INDEX * Sin\theta$ 

Figure 7-1 can be used to set the above Control modes through GUI.

## CONTROLLER TUNING

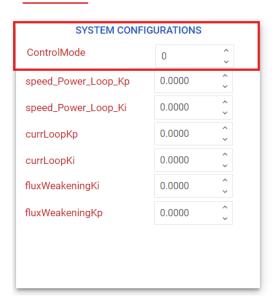


Figure 7-1. Control Mode Configuration



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## 7.1.2 Initial Speed Detection of the Motor for Reliable Motor Resynchronization

The Initial Speed Detection (ISD) function is used to identify the initial condition of the motor. It is important to know the initial condition of the motor for reliable resynchronization. Motor resynchronization failures can occur when the device attempts to start the motor while the motor is coasting or spinning in the direction opposite to the intended direction of spin. Motors can coast in applications that require frequent motor starts and stops, if the motor is being forced externally, or if there is a power interruption. Motors can spin in the direction opposite to the intended direction of spin if motor phase wires are connected to OUTA, OUTB, and OUTC in wrong sequence or when the wrong direction command is issued. Motors with higher inertia coast for a longer period of time. Enable ISD in applications that require frequent motor starts and stops, and use higher inertia motors.

For example, ceiling fan motors have higher inertia due to the fan blades and can coast for a long time before stopping.

- 1. Enable ISD [ISD\_EN].
- 2. Enable Motor ISD Resynchronize [RESYNC\_EN].

**Note** 

If the motor fails to start:

- 1. Increase the Motor Stationary BEMF Threshold [STAT DETECT THR].
- 2. Increase the Motor Stationary Persistence Time [ISD STOP TIME].
- 3. Increase the Motor Run Persistence Time [ISD\_RUN\_TIME].
- 4. Increase the minimum speed threshold to resynchronize to closed loop.

## 7.1.3 Unidirectional Motor Drive Detecting Backward Spin

For applications that require spinning the motor in a specific direction, it is important to know if the motor is coasting or spinning in the direction opposite to the intended direction of spin. The MSPM0 FOC Algorithm reverse drive function acts to reverse decelerate the motor through zero speed and to accelerate after changing direction until it transitions into closed loop as shown in Figure 7-2.

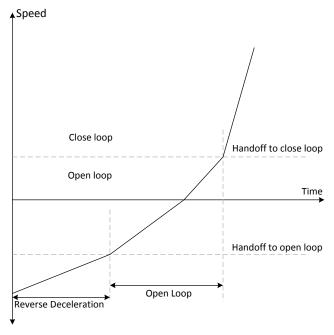


Figure 7-2. Reverse Drive Function

The MSPM0 FOC algorithm provides an option to apply brakes and stop the motor while the motor is coasting or spinning in reverse direction and then accelerate into closed loop after changing the direction.

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In applications such as ceiling fans and pumps, it is required to spin the motor in a specific direction for desired results. For such applications, follow these recommendations:

- 1. Enable ISD [ISD\_EN].
- 2. Enable Motor ISD Reverse drive [RVS DR EN].
- 3. Enable reverse resynchronization [RESYNC\_EN].

#### Note

Follow these recommendations if the motor fails to resynchronize in reverse direction:

- 1. Increase the reverse deceleration speed threshold to transition to open loop
- 2. Enable Open loop reverse drive configuration [REV\_DRV\_CONFIG]
- 3. Increase the Reverse Drive Open Loop Current Reference [REV DRV OPEN LOOP CURRENT]
- 4. Decrease open loop acceleration coefficient A1 and A2 during reverse drive

## 7.1.4 Preventing Back Spin of Rotor During Startup

For applications where a reverse spin is not acceptable, the Initial Position Detection algorithm (IPD) function is an alternative way to start up the motor. With the proper IPD setting, the motor startup can be faster than using align. While this function is suitable for motors with high inertia, such as heavy blades (for example: a ceiling or appliance fan), it is not suitable for motors with low inertia, such as small blades (for example: a computer fan), because the current injection can cause the motor to shake, resulting in the IPD not being accurate.

In applications where the acoustic noise ("chirp") generated by IPD is not acceptable during startup, select "Slow first cycle" as the startup method.

### 7.1.4.1 Option 1: IPD

- 1. If IPD is chosen as startup method, select IPD in the Motor startup option [MTR\_STARTUP] in "USER INPUT MTR STARTUP1 T configuration of REGISTER MAP" tab in the GUI.
- 2. Select the IPD Current threshold [IPD\_CURR\_THR]. IPD current threshold is selected based on the inductance saturation point of the motor. A higher current has better chance to accurately detect the initial position. However, higher current can result in rotor movement, vibration, and noise. Start with 50% of the rated current of the motor. If the motor startup is unsuccessful, increase the threshold until the motor starts successfully. Do not set the IPD current threshold higher than the rated current of the motor.
- 3. Select IPD clock value [IPD\_CLK\_FREQ]. IPD clock defines how fast the IPD pulses are applied. Motors with higher time constants and higher current thresholds need longer time to decay the current before next IPD pulse is excited. So, set the clock at a slower time as starting value and increase till the IPD TIME OUT fault is not triggered. A slower clock makes the IPD noise softer but lasts longer, so set the clock such that IPD fault is not triggered and Noise is reasonably acceptable.

## Note

The device triggers the IPD timeout fault IPD\_FAULT\_CLOCK\_TIMEOUT for motors with very high time constant, or if the motor is not connected. If this fault is triggered, make sure that the motor is connected to the device. If the fault still persists, decrease the IPD Clock frequency [IPD\_CLK\_FREQ].

4. Select IPD Advance Angle [IPD\_ADV\_ANGLE]. Start with 90° for maximum startup torque. If there is sudden jerk observed during startup, reduce the angle to 60° or 30° for a smoother startup.



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### 7.1.4.2 Option 2: Slow First Cycle

Follow these steps if the slow first cycle is chosen as the startup method:

1. Select Slow first cycle in the Motor startup option [MTR\_STARTUP] in "Control Configuration – Motor Startup Stationary" tab in the GUI.

- 2. Select align or slow first cycle current reference [ALIGN\_OR\_SLOW\_CURRENT\_ILIMIT]. Lower current reference can lose synchronization of motor. Higher current can lead to sustained oscillations for high inertia motors, or sudden jerky motion for low inertia motors. It is recommended to start with 50% of the rated current of the motor. In applications where the startup torque is high, the motor might lose synchronization. In such applications, increase the current reference. In applications where sustained oscillations or sudden jerks are observed, decrease the current reference.
- 3. Select align or slow first cycle current ramp rate [ALIGN\_SLOW\_RAMP\_RATE]. Current reference is ramped to avoid reverse rotation of the motor. Lower current ramp rate can lose synchronization of motor. A higher current ramp rate can lead to sustained oscillations for high inertia motors, or sudden jerking motion for low inertia motors. Start with setting the ramp time to 0.5 seconds to ramp to rated current of the motor. In applications where the startup torque is high, the motor can lose synchronization. In such applications, increase the current ramp rate. In applications where sustained oscillations or sudden jerks are observed, decrease the current ramp rate.
- 4. Select the frequency of the first cycle [SLOW\_FIRST\_CYC\_FREQ]. Lower frequency can give a jerky motion at startup. Higher frequency might not be able to synchronize the motor. Start with 20% of the maximum speed of the motor. In applications where the startup torque is high, the motor can lose synchronization. In such applications, decrease the frequency. In applications where jerky motions are observed, increase the frequency.

## 7.1.5 Gradual and Smooth Start up Motion

For applications that require slow and gradual startup with lower speed overshoots during handoff, follow the steps below:

- 1. Decrease Open loop acceleration coefficient A1 [OL\_ACC\_A1] and Open loop acceleration coefficient A2 [OL\_ACC\_A2].
- 2. Enable Iq ramp down after transition to closed loop [IQ\_RAMP\_EN].

If there is speed overshoots, decrease ramp rate for reducing difference between estimated theta and open loop theta [THETA ERROR RAMP RATE].

### 7.1.6 Faster Startup Timing

Startup time is the time taken for the motor to reach the target speed from zero speed. For applications that require quick startup time, we recommend choosing either Initial Position Detection (IPD) or Slow first cycle as the startup method.

#### 7.1.6.1 Option 1: Initial Position Detection (IPD)

- 1. Select IPD [MTR STARTUP] as the motor startup method.
- 2. Increase IPD current threshold [IPD CURR THR] to rated current of the motor.
- 3. Increase IPD clock value [IPD\_CLK\_FREQ] to higher frequency up to a value where the device does not trigger IPD frequency fault. Check Section 7.1.4 (Step 3) for more details.
- 4. Select IPD repeating times [IPD\_REPEAT] to 1 time.
- 5. Select Open loop current limit [OL\_ILIMIT] to be the same as Current limit for Torque PI Loop [ILIMIT].

#### Note

Configuring current Limits to a value higher than motor stall current overheats or damages the motor.

- 6. Increase Open loop acceleration coefficient A1 [OL\_ACC\_A1] and Open loop acceleration coefficient A2 [OL\_ACC\_A2].
- 7. Select Minimum BEMF for handoff [AUTO HANDOFF MIN BEMF] to 0mV.
  - If the device triggers Abnormal BEMF [ABN\_BEMF] fault, then recommended to increase the [AUTO HANDOFF MIN BEMF].
- 8. Keep increasing ramp rate for reducing difference between estimated theta and open loop theta to 2deg/ms.

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9. Increase Closed loop acceleration rate [CL ACC].

### 7.1.6.2 Option 2: Slow First Cycle

- 1. Select Slow first cycle as the motor startup method in [MTR STARTUP].
- 2. Select Align or slow first cycle current limit [ALIGN\_OR\_SLOW\_CURRENT\_ILIMIT] to be the same as Current limit for Torque PI loop [ILIMIT].
- 3. Keep increasing Align or slow first cycle current ramp rate [ALIGN\_SLOW\_RAMP\_RATE] until the open loop current reaches 100% of the rated current of the motor.
- 4. Follow Step 5 to Step 9 in Option 1.

## 7.1.7 Stopping Motor Quickly

For applications that require stopping the motor quickly, configure Motor stop options [MTR\_STOP] to either Low side braking:

- 1. Configure motor-stop options [MTR\_STOP] to low-side braking.
- 2. Select speed threshold for BRAKE pin and motor STOP options. Setting speed threshold to higher speed can result in FETs carrying large current. Setting speed threshold to lower speed results in increase in the stop time of the motor. Recommended to start with 50% of the maximum speed. If the motor phase current exceeds the FET maximum current rating, then decrease the threshold. If the stop time is too high, then recommended to increase the threshold without hitting the maximum current limit.

## 7.1.8 Flux Weakening: Operating Motor at Speeds Higher than Rated Speed

The FOC algorithm provides control for adjusting the rotor flux by changing the flux current component ld. Reducing the rotor flux enables motor to enter the field weakening zone through which motor speed can go beyond rated speed.

### Note

During flux weakening operation, the motor cannot deliver the rated torque. The torque limit Iq is automatically adjusted based on the circular motor current limit defined by  $I_{LIMIT} = Id^2 + Iq^2$ .

Steps to enable the flux weakening:

- 1. Set the FLUX WEAK EN bit in FieldCtrl register as 1b.
- 2. Adjust FLUX\_WEAK\_CURR\_RATIO to limit the maximum flux component of current to torque component current ratio. This value limits the flux component current Id and maintain the torque component current Iq based on the circular limit ILIMIT as Id<sup>2</sup> + Iq<sup>2</sup>.
- 3. Maximum modulation index beyond which the field weakening is enabled can be tuned using FLUX\_WEAKE\_REF configuration. This register field values sets the square of modulation index value above which the Id is regulated to weaken the flux.

## Note

Entering field weakening is not efficient below rated speeds. Field weakening is recommended to be activated only when the modulation index limit is reached and no longer be able to meet the desired speed requirement with the sine modulation.

## 7.1.9 Maximum Torque Per Ampere: Improve Efficiency of IPMSM Motors

The FOC algorithm enables users to achieve maximum efficiency for motors with saliency (IPM motors). User can configure the saliency of the motor as nonzero value as detailed in saliency parameter description.

Users can enable this feature by configuring the MTPA EN in the Section 5.3.8.

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## 7.1.10 Preventing Supply Voltage Overshoot During Motor Stop.

For applications that require preventing supply voltage overshoots during motor stop, select active spin down as Motor stop options. Active spin down can be used as a motor stop option in applications where fast stop is not required but some amount of inductive energy going back to power supply is acceptable.

- 1. Configure Motor stop options [MTR\_STOP] to Active spin down.
- Configure active spin down speed threshold [ACT\_SPIN\_THR]. It is recommended to set the
  ACT\_SPIN\_THR to 50% of the maximum speed. If there is voltage overshoot seen on the power supply,
  decrease the ACT\_SPIN\_THR till the voltage overshoot reaches acceptable limit.

## 7.1.11 Protecting the Power Supply

Protecting the power supply from drawing higher current or potential voltage overshoots is important in battery operated applications or applications that do not have an internal overcurrent or overvoltage protection built into the power supply.

- When the load on the motor increases, the device draws higher current from the power supply. To limit
  the current drawn from the power supply, enable bus current limit [BUS\_CURRENT\_LIMIT\_ENABLE] and
  configure the bus current limit [BUS\_CURRENT\_LIMIT] to protect the power supply from drawing higher
  current.
  - For example, limiting the current drawn from power supplies such as batteries is required because the battery life depends on the charge and discharge cycles. Enabling the bus current limit limits the power supply current by limiting the speed of the motor.
- 2. When a command is issued for the motor to decelerate, based on the deceleration rate, energy from the motor can be pumped back to the power supply, increasing the supply voltage to levels that are possibly unsafe for electronics. Enable the antivoltage surge [AVS] to protect the power supply from voltage overshoots that override any deceleration limit set by any other register and automatically apply a safe deceleration rate.

Figure 7-3 shows overshoot in power supply voltage when AVS is disabled. Motor decelerates from 100% duty cycle to 10% duty cycle at a deceleration rate of 70000Hz/s. Figure 7-4 shows no overshoot in power supply voltage when AVS is enabled.

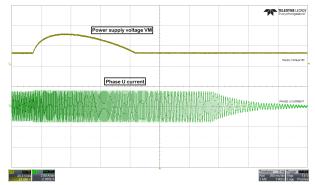


Figure 7-3. Power Supply Voltage and Phase Current Waveform When AVS is Disabled

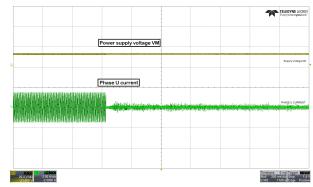


Figure 7-4. Power Supply Voltage and Phase Current Waveform When AVS is Enabled

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#### 7.1.12 FOC Bandwidth Selection

The FOC algorithm is periodically executed in the interrupt routine to update the rotor angle to extract the maximum efficiency from the motor. This FOC rate can be configured by user based on the application bandwidth requirements.

HIGH\_FREQ\_FOC\_EN bit configuration in the Section 5.3.6 can be set to 0b to get the maximum FOC execution rate of 16kHz. Setting this bit to 1b reduces the maximum FOC execution rate by 2.

#### Note

FOC routine can only be executed at a multiple of PWM frequency, Hence, the maximum achievable FOC rate of 16kHz is applicable for PWM frequencies with multiple of 16 (for example, 16kHz, 32kHz, 48kHz). For PWM frequencies of 20KHz, 40kHz, and so on, the maximum FOC rate is limited to 10kHz (20KHz/2, 40KHz/4, and so on).

## 8 Hardware Configurations

## 8.1 Direction Configuration

The FOC algorithm lets you set the direction of the motor using a register-based direction configuration:

### Register-based direction configuration

The direction of motor spin can be set based on register setting as shows below:

- DIR\_INPUT 01b: apply phase sequence OUT A → OUT B →OUT C.
- DIR\_INPUT 10b: apply phase sequence OUT A → OUT C → OUT B.

## 8.2 Brake Configuration

FOC Algorithm enables user to brake the motor under various scenarios. Brake state can be configured to either low side braking (Low-Side Braking) or align brake (Align Braking) through BRAKE\_PIN\_MODE. FOC Algorithm decreases output speed to value defined by BRAKE\_SPEED\_THRESHOLD before entering brake state. As long as BRAKE is driven 'High', motor stays in brake state. Brake functionality can be achieved the following way:

## · Register based Brake configuration.

User can configure the BRAKE\_INPUT in PIN\_CONFIG register to apply the brakes using register settings as below.

- BRAKE INPUT 1b: Override pin and brake / align according to BRAKE PIN MODE
- BRAKE\_INPUT 10b: Override pin and do not brake / align

## 8.3 Main.h Definitions

## 8.3.1 Sense Amplifier Configuration

Sense amplifier configuration defines the direction of CSA output. Decreasing CSA Output for a Positive current coming out of phase indicates the Sense Amplifier is inverting. Increasing CSA output for a Positive current indicates Non Inverting Current sense amplifier.

For Inverting amplifier configuration, #define \_INVERT\_ISEN has to be included in the main.h.

For Non Inverting amplifier configuration, #define \_NONINVERT\_ISEN has to be included in the main.h file

## 8.3.2 Driver Propagation Delay

Driver propagation delay defines the Time delay in ns between the Input PWM logic edge fed to the gate driver and actual Gate Driver output. This delay impacts the Current Sense sampling instance on the actual gate driver output and has to be fed to the algorithm for accurate Current Sensing.

This value in ns has to be defined using #define DRIVER\_PROPAGATION\_DELAY\_nS macro in the main,h file.

#### 8.3.3 Driver Min On Time

Driver Min on time defines the combined rise time and settling time of the current sense amplified output. This value has to be captured independently for a full scale change in voltage across the current shunt. For accurate current sense reading, the current sense amplifier output to be settled before the current signal is captured.

This CSA Settling + Rise time is to be set using #define DRIVER\_MIN\_ON\_TIME\_nS macro in the main,h file.

## 8.3.4 Current Shunt Configuration Selection

The SDK FOC example can be configured for various shunt configuration options such as Single Shunt, Dual Shunt and Three Shunt. Based on the HW design the appropriate shunt configuration has to be selected for proper operation of algorithm.

FOC Application supports simultaneously sampling the two phases at a given instance to optimize the current sampling time. By default in all shunt configurations, both the ADC instances are used to utilize the simultaneous sampling feature. User needed to route at least one current sense onto each of the two ADC instance channels and appropriate shunt configuration has to be defined in the main.h configuration as below.

### 8.3.4.1 Three Shunt Configurations

**#define CURRENT\_THREE\_SHUNT\_AB\_C**: Select this configuration if A and B phases are sensed through ADC0 and C phase is sensed through ADC1.

**#define** \_\_CURRENT\_THREE\_SHUNT\_A\_BC : Select this configuration if A phase is sensed through ADC0 and B, C phases are sensed through ADC1.

User can also route one of the Phases say 'B' to both the ADC 0 and 1 instance and the other two phases to two different ADC instances. For example say 'phase A' is routed to ADC0 and Phase 'C' is routed to ADC1, Phase B is routed to both ADC0 and ADC1 instances, In this example, algorithm can dynamically switch to the two samples which gives the best current sampling time based on the given sector.

In this three shunt configuration, application supports shifting the current sensing estimation dynamically to the two phases for maximizing the modulation index. As in a balanced three phase Motor, any one of the phase current can be estimated with the other two phase currents as  $i_a$ = -( $i_b$  +  $i_c$ ). Based on the operational sector the two phases with lowest modulation index are selected for current measurement and third phase with highest modulation index is estimated using the other two phase currents. This method helps in extending the modulation index to higher limits with continuous SVM operation.

To select this configuration user can include **#define \_\_CURRENT\_THREE\_SHUNT\_DYNAMIC** macro in the main.h file. Along with this user need to enable the dynamic shunt selection by setting the macro **#define DYNAMIC\_CURRENT\_SHUNT\_CONFIG\_EN** to **TRUE**.

## 8.3.4.2 Dual Shunt Configuration

**#define** \_\_CURRENT\_TWO\_SHUNT\_A\_B : Select this configuration if only two shunt sense across phase A and B are available current sampling where A is channeled to ADC 0 and B to ADC1.

**#define** \_\_CURRENT\_TWO\_SHUNT\_B\_C : Select this configuration if only two shunt sense across phase B and C are available current sampling where B is channeled to ADC 0 and C to ADC1.

**#define** \_\_CURRENT\_TWO\_SHUNT\_C\_A: Select this configuration if only two shunt sense across phase A and B are available current sampling and A is channeled to ADC 0 and C to ADC1.

#### Note

If user has a different combination of phases routed to the ADC 0 and 1 instances than the default connections in SDK. Appropriate changes can be done in following file: projectroot/modules/hal/gateDriverInterface/source/<driverSpecific> focHalInterface.c

### 8.3.4.3 Single Shunt Configuration

If a single shunt is used in the HW for current sensing, below definitions are to be included for proper motor operation.

#define \_\_CURRENT\_SINGLE\_SHUNT macro to be included in the main.h file.



## 8.3.5 CSA Offset Scaling Factor Selection

FOC application converts the sampled currents through ADC into PU system based on the maximum current that can be sensed through the ADC. This depends on the CSA offset introduced from the amplifier. Typically for bipolar current sense measurement, full scale value of ADC 3.3V / 2 = 1.65V is given as offset. For applications where the current sensing is always unipolar, offset values are set less than 0.5V to use the maximum full scale ADC output for +ve current measurement and small margin is left for -ve current measurement.

FOC application requires this scaling to be specified for appropriate functionality. As the ADC 12-bit value is converted to PU value, if the offset is set as 0 : Then the scaling factor to be set as IQ(1).

If the CSA offset in HW is set as 1.65V (3.3V / 2) for bipolar current sense measurement the scaling factor to be set as \_IQ(2).

For any arbitrary offset values, the scaling values to be specified as

\_IQ(3.3v/(3.3v - CSA\_OFFSET in volts)). This value to be added as macro definition in the *projectroot/modules/hal/gateDriverInterface/source/<driverSpecific>\_focHalInterface.c.* 

For example : Refer to example project DRV8329 - where #define DRV8329\_CURRENT\_SF\_IQ is specified as \_IQ(1.42857142) for a CSA offset of 0.4125V.

## 8.4 Real Time Variable Tracking

32-bit algorithm variables can be output in real time from the MCU through the DAC. DAC output is enabled by setting DAC\_EN = 1. The DAC in MSPM0 is 12 bit, thus a scaling needs to be applied before output. User has two ways to scale the variable before output.

## For variables in global IQ format(IQ27):

In the above equation setting the DAC\_SCALING\_FACTOR to 1 enables user to represent a data of IQ(1.0) to IQ(-1.0) in between 0V and 3.3V. To represent the data exceeding the value 1.0 use higher DAC\_SCALING\_FACTOR.

For Example: To represent a data from -2.0 to +2.0, set the DAC SCALING FACTOR to 0.5.

#### For variables in other IQ format:

For output of any other IQ, user can left shift or right shift the variable to bring the data in a 12-bit range before output. This mode is selected by setting DAC\_SCALING\_FACTOR to 0.

If variable value is less than a 12-bit value, set DAC\_SCALE to positive, the DAC output follows as shown in Equation 12:

If variable value is greater than a 12-bit value, set DAC\_SCALE to negative, the DAC output follows as shown in Equation 13:

$$DAC\_OUTPUT\_VOLTAGE = (VARIABLE\_VALUE >> DAC\_SCALE) \times 3.3V$$
(13)

#### Note

Settings DAC\_EN = 1 feeds the variable output to the DAC registers, but user needs to enable the DAC peripheral in TI SysConfig for the DAC peripheral to function. Also make sure the DAC output pin is not loaded by any other peripheral.

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Table 8-1. Address Table for DAC Monitoring

Variable	Address
A phase current	0x20200608
B phase current	0x2020060C
C phase current	0x20200610
A phase current raw ADC value	0x20200614
B phase current raw ADC value	0x20200618
C phase current raw ADC value	0x2020061C
A phase voltage	0x20200678
B phase voltage	0x2020067C
C phase voltage	0x20200680
A phase voltage raw ADC value	0x20200684
B phase voltage raw ADC value	0x20200688
C phase voltage raw ADC value	0x2020068C
D axis current	0x20200750
Q axis current	0x20200754
D axis voltage	0x20200758
Q axis voltage	0x2020075C
D axis Filtered BEMF	0x20200BD4
Q axis Filtered BEMF	0x20200BD8
Estimated motor velocity filtered	0x20200BF4
Estimated rotor angle	0x20200BFC
Power Feedback	0x20200930
SVM output duty A phase	0x20200720
SVM output duty B phase	0x20200724
SVM output duty C phase	0x20200728

# **9 Revision History**

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Revision B (November 2024) to Revision C (March 2025)	Page
Updated support for MSPM0G3519 devices throughout document	1
Added support for MSPM0G3519 devices in Section 2.4	7
Added support for MSPM0G3519 devices in Section 2.5	8
Added support for MSPM0G3519 devices in Section 2.10	10
Updated offset address for Table 5-22 and Table 5-23,	<mark>24</mark>
• Updated Table 5-26 by removing IPD_RLS_MODE. By default IPD operates in Hi-Z Mode	
Updated PWM Frequency Table Values in Closed Loop 1 register in Table 5-28	
Updated image for Figure 5-5	48
Added IPD IDENTIFIED SECTOR for Table 5-36	
Added FOC supports maximum of 16KHz FOC frequency in Section 7.1.12	

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