# Single-supply, high-input voltage, full-wave rectifier circuit



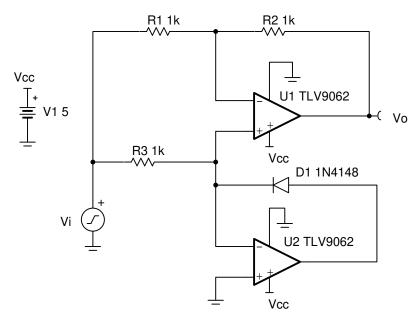
**Amplifiers** 

#### **Design Goals**

Input	Output	Frequency	Sup	pply
$V_{iMax}$	$V_{oMax}$	f <sub>Max</sub>	V <sub>cc</sub>	V <sub>ee</sub>
9Vpp	4.5Vpp	50kHz	5V	0V

#### **Design Description**

This single-supply precision full-wave rectifier is optimized for high-input voltages. When V<sub>i</sub> > 0V, D<sub>1</sub> is reverse biased and the top part of the circuit, U1, is activated resulting in a circuit with a gain of 1V/V. When Vi < 0V, D<sub>1</sub> is forward biased and the bottom part of the circuit, U2, is activated resulting in an inverting amplifier circuit with a gain of -1V/V.

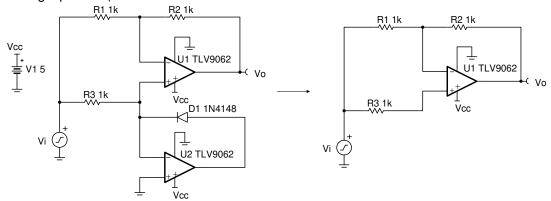


#### **Design Notes**

- 1. Observe common-mode and output swing limitations of op amps.
- 2. R<sub>3</sub> should be sized small enough that the leakage current from D<sub>1</sub> does not cause errors for positive input cycles while ensuring the op amp can drive the load.
- 3. Use a fast switching diode for D<sub>1</sub>.
- 4. Resistor tolerance determines the gain error of the circuit.
- 5. Use a negative charge pump (such as the LM7705) for output swing requirements to GND to maintain linearity for output signals near 0V. For additional information. see Single-supply, low-input voltage, full-wave rectifier circuit.
- 6. For more information on op amp linear operating region, stability, capacitive load drive, driving ADCs, and bandwidth please see the Design References section.

## **Design Steps**

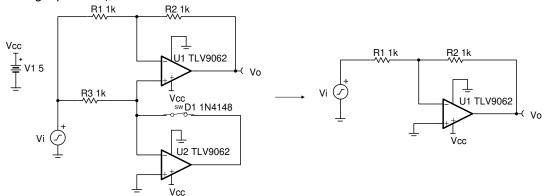
1. Circuit analysis for positive input signals. D<sub>1</sub> is reverse-biased disconnecting the output of U<sub>2</sub> from the non-inverting input of U<sub>1</sub>.



$$\frac{V_0}{V_i} = (-\frac{R_2}{R_1}) + (1 + \frac{R_2}{R_1}) = 1$$

$$V_o = V_i$$

2. Circuit analysis for negative input signals.  $D_1$  is forward biased, which connects the output of  $U_2$  to the non-inverting input of  $U_1$ , which is GND.



$$\frac{V_o}{V_i} = (-\frac{R_2}{R_1}) = -1$$

$$V_o = -V_i$$

3. Select R<sub>1</sub>, R<sub>2</sub>, and R<sub>3</sub>.

$$\frac{V_o}{V_i} = -\frac{R_2}{R_1}$$

2

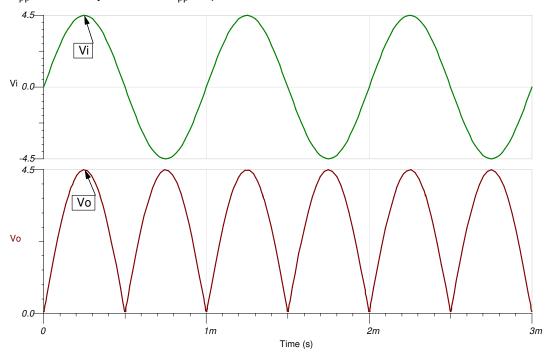
If 
$$R_2 = R_1$$
 then  $V_o = -V_i$ 

Set 
$$R_1 = R_2 = R_3 = 1k\Omega$$

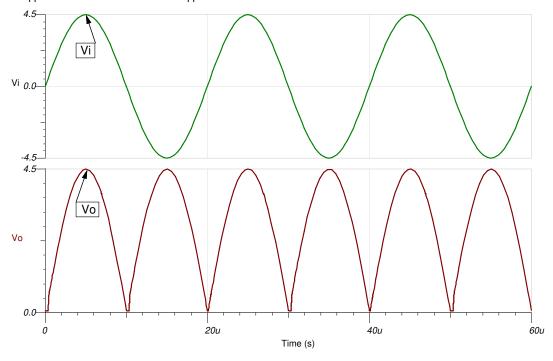
## **Design Simulations**

## **Transient Simulation Results**

A 1-kHz, 9-V  $_{pp}$  sine wave yields a 4.5-V  $_{pp}$  output sine wave.



A 50-kHz, 9-V  $_{\rm pp}$  sine wave yields a 4.5-V  $_{\rm pp}$  output sine wave.



## **Design References**

- 1. See Analog Engineer's Circuit Cookbooks for the comprehensive TI circuit library.
- 2. SPICE Simulation File SBOC529.
- 3. TI Precision Labs
- 4. See the Single-Supply Low-Input Voltage Optimized Precision Full-Wave Rectifier Reference Design.

## **Design Featured Op Amp**

TLV9062			
V <sub>ss</sub>	1.8V to 5.5V		
V <sub>inCM</sub>	Rail-to-rail		
V <sub>out</sub>	Rail-to-rail		
V <sub>os</sub>	0.30mV		
Iq	538µA		
l <sub>b</sub>	0.5pA		
UGBW	10MHz		
SR	6.5V/µs		
#Channels	1, 2, 4		
www.ti.com/product/TLV9062			

# **Design Alternate Op Amps**

	OPA322	OPA350
V <sub>ss</sub>	1.8V to 5.5V	2.7V to 5.5V
V <sub>inCM</sub>	Rail-to-rail	Rail–to–rail
V <sub>out</sub>	Rail-to-rail	Rail–to–rail
V <sub>os</sub>	2mV	0.15mV
Iq	1.9mA	5.2mA
I <sub>b</sub>	10pA	0.5pA
UGBW	20MHz	38MHz
SR	10V/μs	22V/µs
#Channels	1, 2, 4	1, 2, 4
	www.ti.com/product/OPA322	www.ti.com/product/OPA350

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