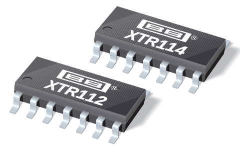


XTR112
XTR114

4-20mA CURRENT TRANSMITTERS with Sensor Excitation and Linearization

FEATURES

- LOW UNADJUSTED ERROR
- PRECISION CURRENT SOURCES
  XTR112: Two 250µA
  XTR114: Two 100µA
- RTD OR BRIDGE EXCITATION
- LINEARIZATION
- TWO OR THREE-WIRE RTD OPERATION
- LOW OFFSET DRIFT: 0.4µV/°C
- LOW OUTPUT CURRENT NOISE: 30nAp-p
- HIGH PSR: 110dB min
- HIGH CMR: 86dB min
- WIDE SUPPLY RANGE: 7.5V TO 36V
- SO-14 SOIC PACKAGE

DESCRIPTION

The XTR112 and XTR114 are monolithic 4-20mA, two-wire current transmitters. They provide complete current excitation for high impedance platinum RTD temperature sensors and bridges, instrumentation amplifier, and current output circuitry on a single integrated circuit. The XTR112 has two 250µA current sources while the XTR114 has two 100µA sources for RTD excitation.

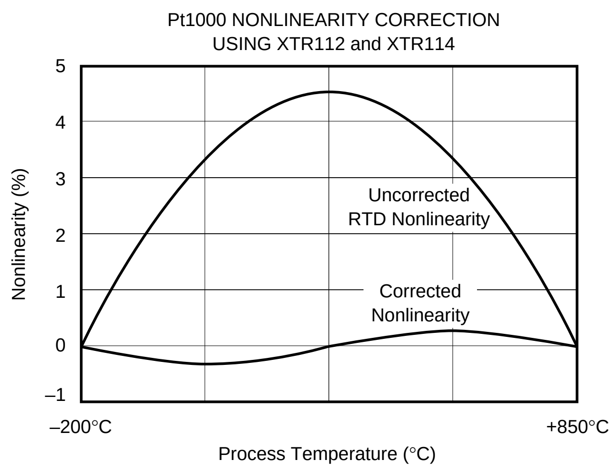
Versatile linearization circuitry provides a 2nd-order correction to the RTD, typically achieving a 40:1 improvement in linearity.

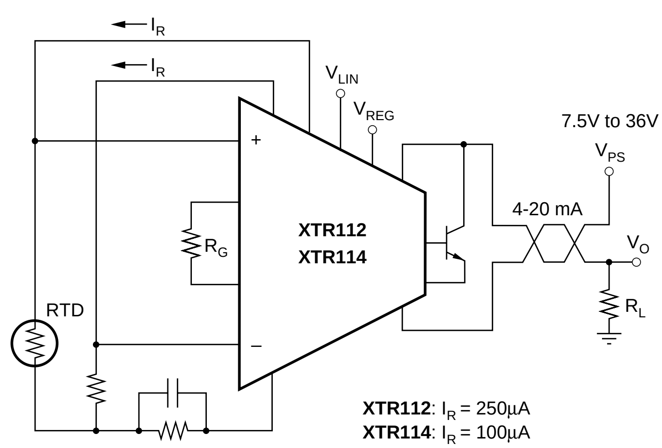
Instrumentation amplifier gain can be configured for a wide range of temperature or pressure measurements. Total unadjusted error of the complete current transmitter is low enough to permit use without adjustment in many applications. This includes zero output current drift, span drift and nonlinearity. The XTR112 and XTR114 operate on loop power supply voltages down to 7.5V.

Both are available in an SO-14 surface-mount package and are specified for the –40°C to +85°C industrial temperature range.

APPLICATIONS

- INDUSTRIAL PROCESS CONTROL
- FACTORY AUTOMATION
- SCADA REMOTE DATA ACQUISITION
- REMOTE TEMPERATURE AND PRESSURE TRANSDUCERS





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PDS-1473A

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SBOS101

SPECIFICATIONS

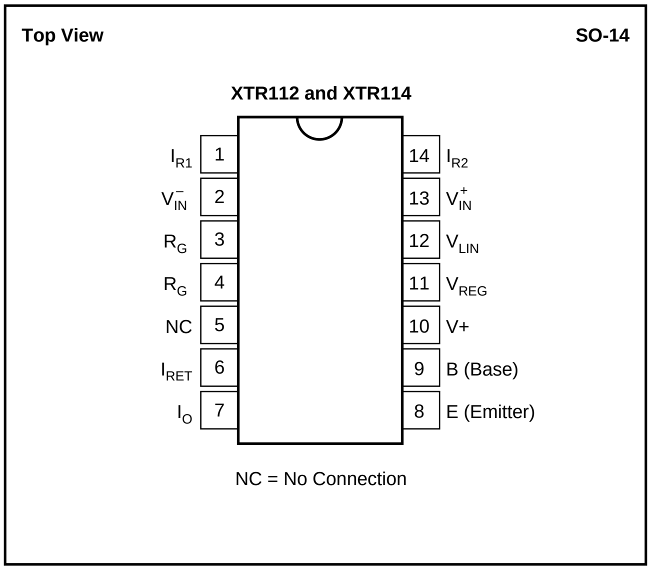
At T_A = +25°C, V+ = 24V, and TIP29C external transistor, unless otherwise noted.

PARAMETER	CONDITIONS	XTR112U XTR114U MIN	TYP	MAX	XTR112UA XTR114UA MIN	TYP	MAX	UNITS
OUTPUT								
Output Current Equation			$I_O = V_{IN} \bullet (40/R_G) + 4mA$, V_{IN} in Volts, R_G in Ω					A
Output Current, Specified Range		4		20	*		*	mA
Over-Scale Limit		24	27	30	*	*	*	mA
Under-Scale Limit: XTR112	I_{REG} = 0	0.9	1.3	1.7	*	*	*	mA
XTR114		0.6	1	1.4	*	*	*	mA
ZERO OUTPUT(1)	V_{IN} = 0V, R_G = ∞		4			*		mA
Initial Error			±5	±25		*	±50	μA
vs Temperature			±0.07	±0.5		*	±0.9	μA/°C
vs Supply Voltage, V+	V+ = 7.5V to 36V		0.04	0.2		*	*	μA/V
vs Common-Mode Voltage	V_{CM} = 1.25V to 3.5V(2)		0.02			*		μA/V
vs V_{REG} Output Current			0.3			*		μA/mA
Noise: 0.1Hz to 10Hz			0.03			*		μAp-p
SPAN								
Span Equation (transconductance)			S = 40/R_G			*		A/V
Initial Error(3)	Full Scale (V_{IN}) = 50mV		±0.05	±0.2		*	±0.4	%
vs Temperature(3)			±3	±25		*	*	ppm/°C
Nonlinearity: Ideal Input(4)	Full Scale (V_{IN}) = 50mV		0.003	0.01		*	*	%
INPUT(5)								
Offset Voltage	V_{CM} = 2V		±50	±100		*	±250	μV
vs Temperature			±0.4	±1.5		*	±3	μV/°C
vs Supply Voltage, V+	V+ = 7.5V to 36V		±0.3	±3		*	*	μV/V
vs Common-Mode Voltage, RTI (CMRR)	V_{CM} = 1.25V to 3.5V(2)		±10	±50		*	±100	μV/V
Common-Mode Input Range(2)		1.25		3.5	*		*	V
Input Bias Current			5	25		*	50	nA
vs Temperature			20			*		pA/°C
Input Offset Current			±0.2	±3		*	±10	nA
vs Temperature			5			*		pA/°C
Impedance: Differential			0.1 ∥ 1			*		GΩ ∥ pF
Common-Mode			5 ∥ 10			*		GΩ ∥ pF
Noise: 0.1Hz to 10Hz			0.6			*		μVp-p
CURRENT SOURCES	V_O = 2V(6)							
Current: XTR112			250			*		μA
XTR114			100			*		μA
Accuracy			±0.05	±0.2		*	±0.4	%
vs Temperature			±15	±35		*	±75	ppm/°C
vs Power Supply, V+	V+ = 7.5V to 36V		±10	±25		*	*	ppm/V
Matching			±0.02	±0.1		*	±0.2	%
vs Temperature			±3	±15		*	±30	ppm/°C
vs Power Supply, V+	V+ = 7.5V to 36V		1	10		*	*	ppm/V
Compliance Voltage, Positive		(V+) –3	(V+) –2.5		*	*		V
Negative(2)		0	–0.2		*	*		V
Output Impedance: XTR112			500			*		MΩ
XTR114			1.2			*		GΩ
Noise: 0.1Hz to 10Hz: XTR112			0.001			*		μAp-p
XTR114			0.0004			*		μAp-p
V_{REG}(2)			5.1			*		V
Accuracy			±0.02	±0.1		*	*	V
vs Temperature			±0.2			*		mV/°C
vs Supply Voltage, V+			1			*		mV/V
Output Current: XTR112			–1, +2.1			*		mA
XTR114			–1, +2.4			*		mA
Output Impedance			75			*		Ω
LINEARIZATION								
R_{LIN} (internal)			1			*		kΩ
Accuracy			±0.2	±0.5		*	±1	%
vs Temperature			±25	±100		*	*	ppm/°C
POWER SUPPLY								
Specified Voltage			+24			*		V
Operating Voltage Range		+7.5		+36	*		*	V
TEMPERATURE RANGE								
Specification, T_{MIN} to T_{MAX}		–40		+85	*		*	°C
Operating/Storage Range		–55		+125	*		*	°C
Thermal Resistance, θ_{JA}								
SO-14 Surface-Mount			100			*		°C/W

* Specification same as XTR112U, XTR114U.

NOTES: (1) Describes accuracy of the 4mA low-scale offset current. Does not include input amplifier effects. Can be trimmed to zero. (2) Voltage measured with respect to I_{RET} pin. (3) Does not include initial error or TCR of gain-setting resistor, R_G. (4) Increasing the full-scale input range improves nonlinearity. (5) Does not include Zero Output initial error. (6) Current source output voltage with respect to I_{RET} pin.

PIN CONFIGURATION



ABSOLUTE MAXIMUM RATINGS(1)

Power Supply, V+ (referenced to I_O pin)	40V
Input Voltage, V_{IN}^+, V_{IN}^- (referenced to I_O pin)	0V to V+
Storage Temperature Range	–55°C to +125°C
Lead Temperature (soldering, 10s)	+300°C
Output Current Limit	Continuous
Junction Temperature	+165°C

NOTE: (1) Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability.

ELECTROSTATIC DISCHARGE SENSITIVITY

This integrated circuit can be damaged by ESD. Burr-Brown recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

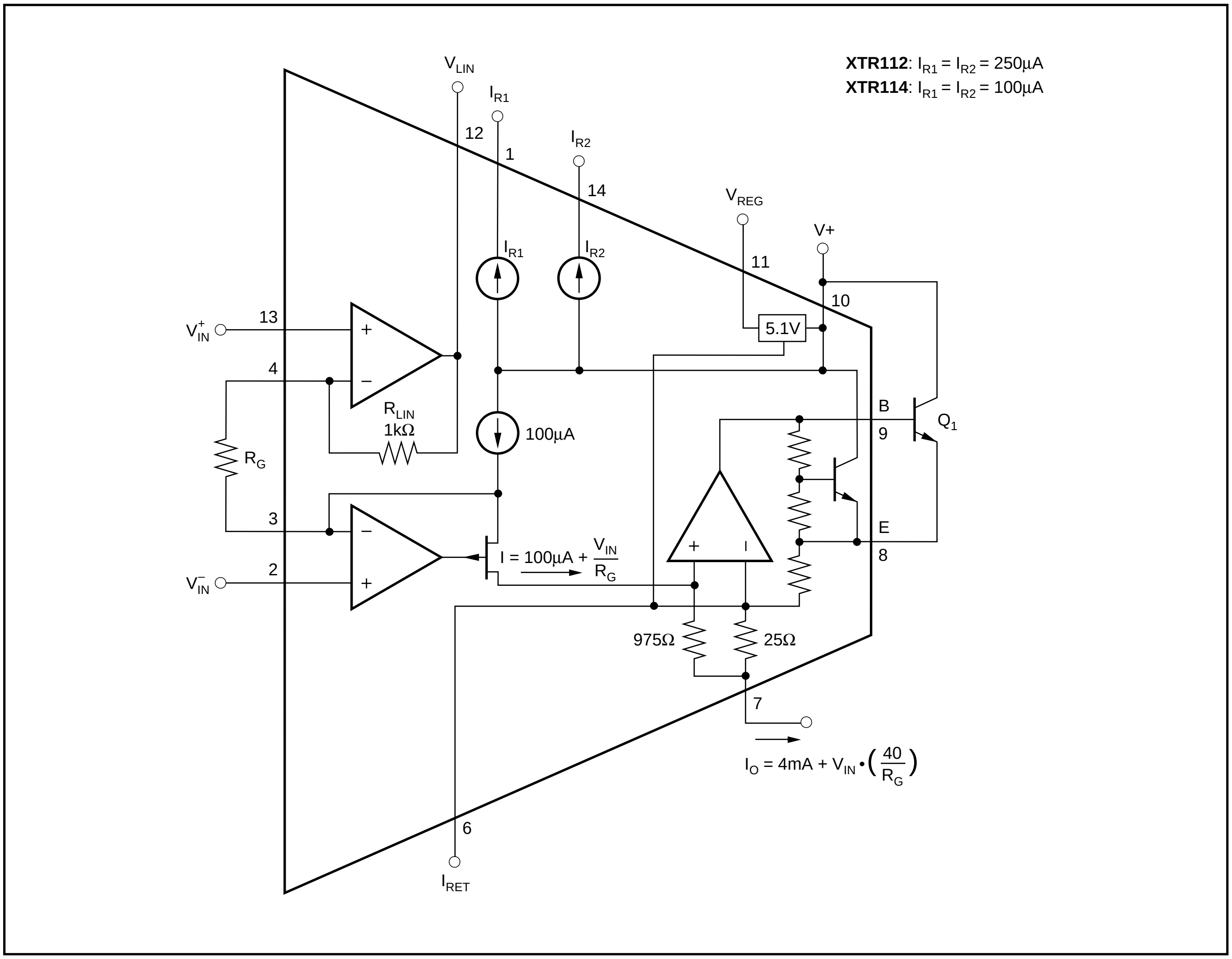
ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

PACKAGE/ORDERING INFORMATION

PRODUCT	CURRENT SOURCES	PACKAGE	PACKAGE DRAWING NUMBER(1)	SPECIFIED TEMPERATURE RANGE	ORDERING NUMBER(2)	TRANSPORT MEDIA
XTR112U	2 x 250µA	SO-14 Surface Mount	235	–40°C to +85°C	XTR112U	Rails
"	"	"	"	"	XTR112U/2K5	Tape and Reel
XTR112UA	2 x 250µA	SO-14 Surface Mount	235	–40°C to +85°C	XTR112UA	Rails
"	"	"	"	"	XTR112UA/2K5	Tape and Reel
XTR114U	2 x 100µA	SO-14 Surface Mount	235	–40°C to +85°C	XTR114U	Rails
"	"	"	"	"	XTR114U/2K5	Tape and Reel
XTR114UA	2 x 100µA	SO-14 Surface Mount	235	–40°C to +85°C	XTR114UA	Rails
"	"	"	"	"	XTR114UA/2K5	Tape and Reel

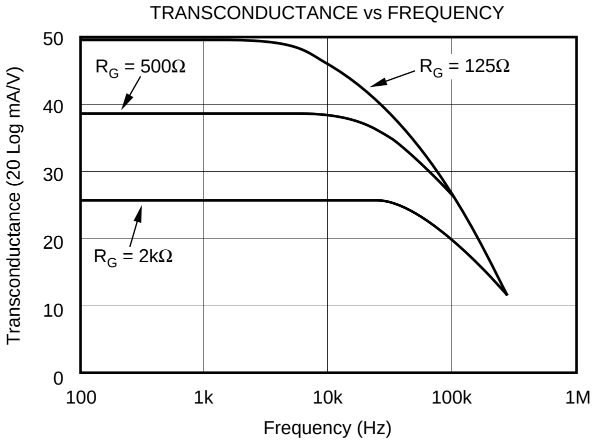
NOTES: (1) For detailed drawing and dimension table, please see end of data sheet, or Appendix C of Burr-Brown IC Data Book. (2) Models with a slash (/) are available only in Tape and Reel in the quantities indicated (e.g., /2K5 indicates 2500 devices per reel). Ordering 2500 pieces of "XTR112UA/2K5" will get a single 2500-piece Tape and Reel. For detailed Tape and Reel mechanical information, refer to Appendix B of Burr-Brown IC Data Book.

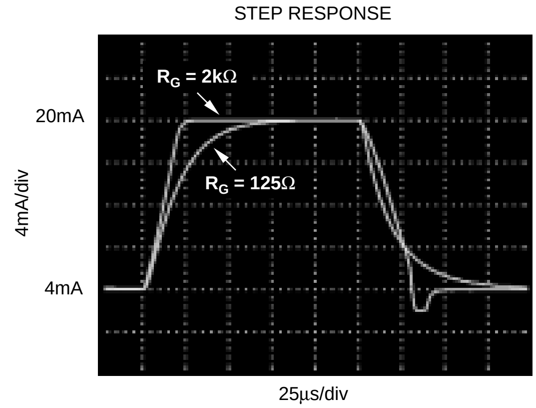
FUNCTIONAL BLOCK DIAGRAM

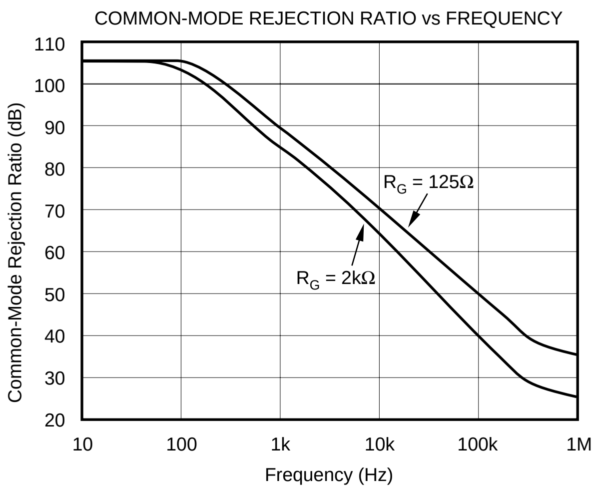


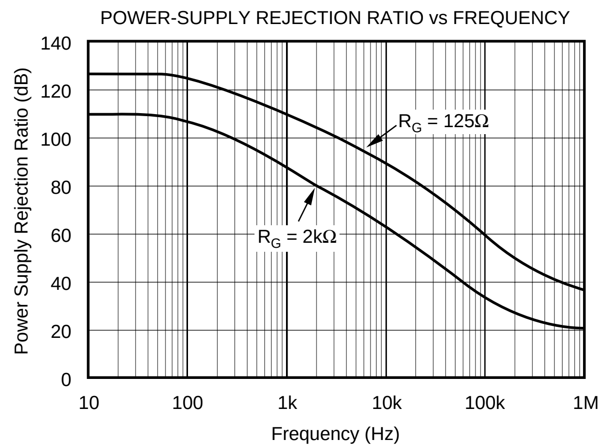
TYPICAL PERFORMANCE CURVES

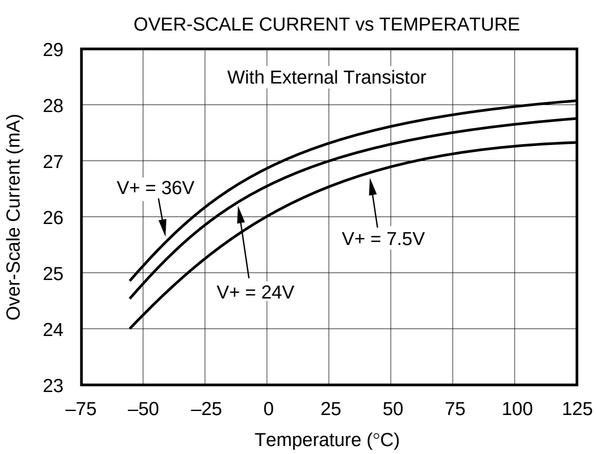
At T_A = +25°C, and V+ = 24V, unless otherwise noted.

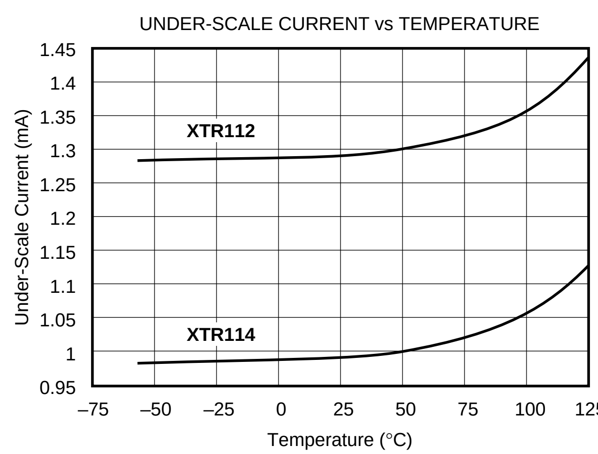






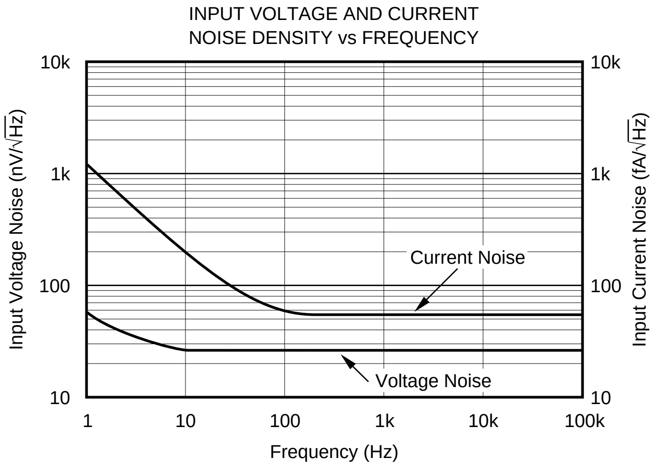


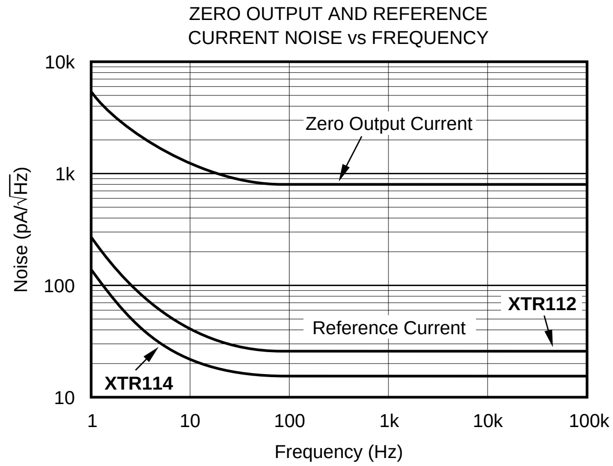


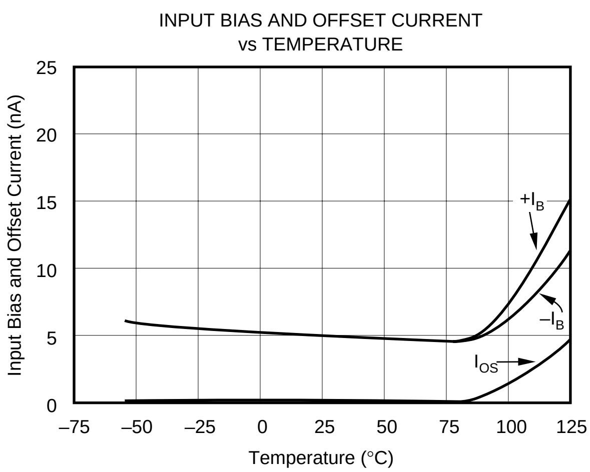


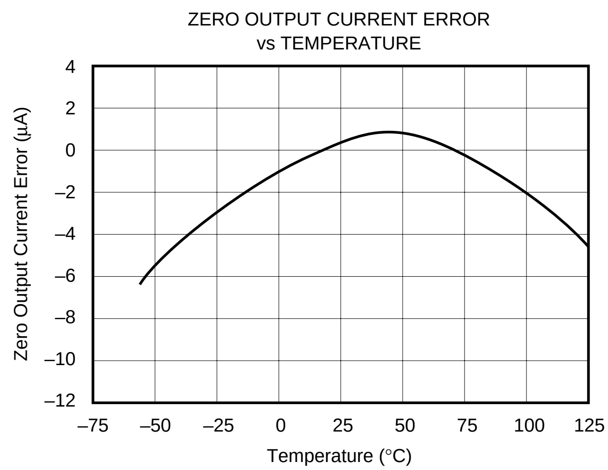
TYPICAL PERFORMANCE CURVES (CONT)

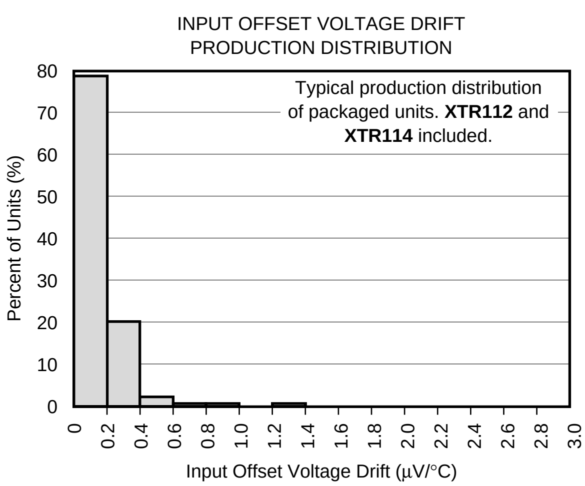
At T_A = +25°C, and V+ = 24V, unless otherwise noted.

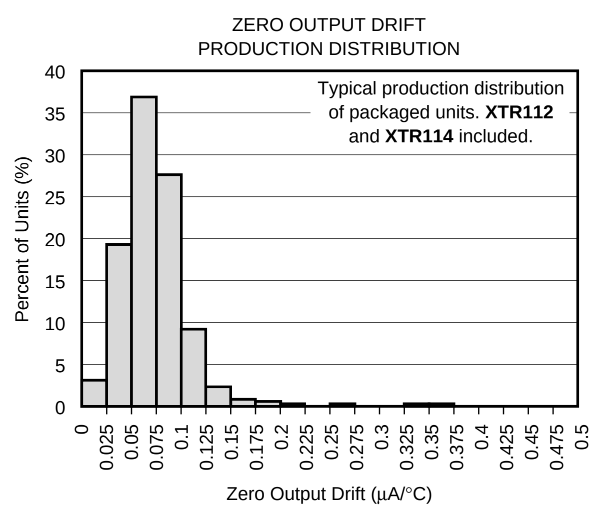






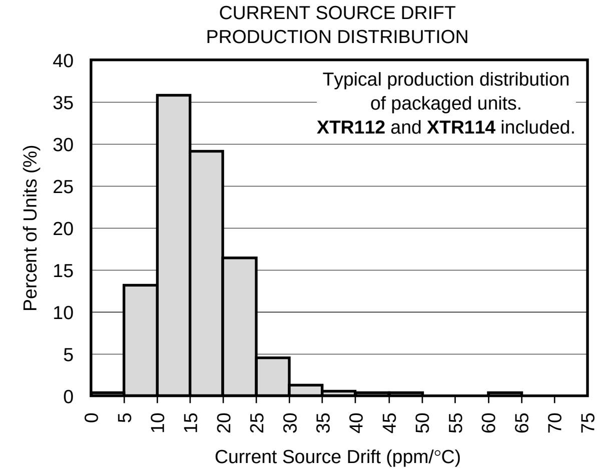


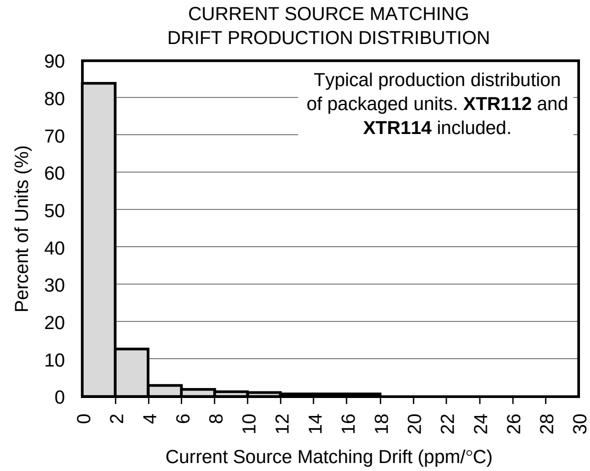


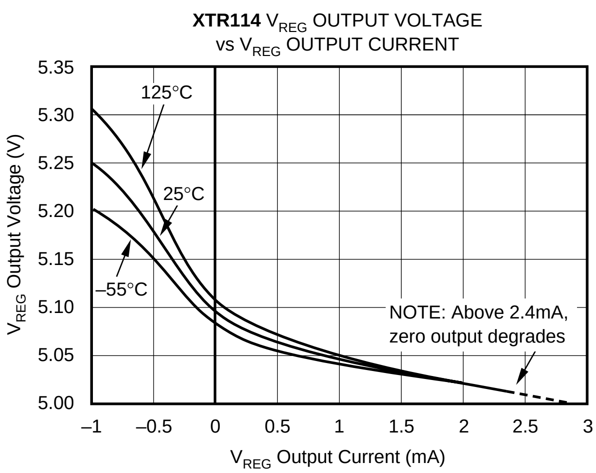


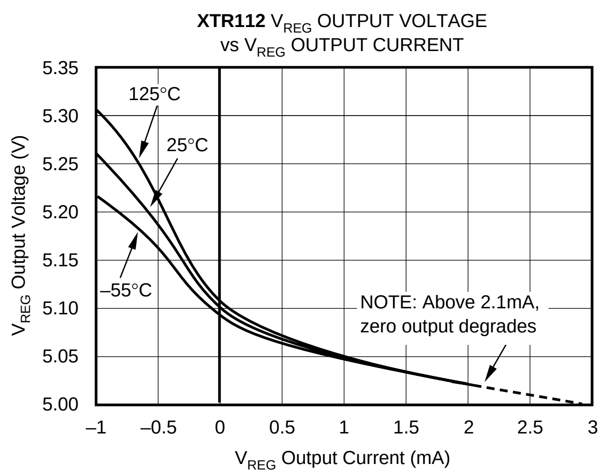
TYPICAL PERFORMANCE CURVES (CONT)

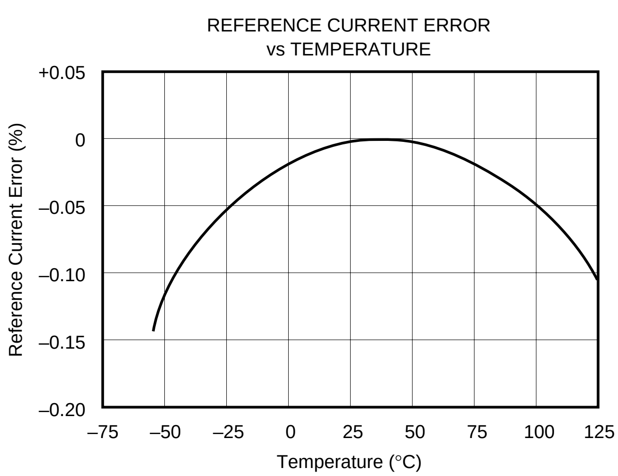
At T_A = +25°C, and V+ = 24V, unless otherwise noted.











APPLICATION INFORMATION

Figure 1 shows the basic connection diagram for the XTR112 and XTR114. The loop power supply, V_{PS}, provides power for all circuitry. Output loop current is measured as a voltage across the series load resistor, R_L.

Two matched current sources drive the RTD and zero-setting resistor, R_Z. These current sources are 250µA for the XTR112 and 100µA for the XTR114. Their instrumentation amplifier input measures the voltage difference between the RTD and R_Z. The value of R_Z is chosen to be equal to the resistance of the RTD at the low-scale (minimum) measurement temperature. R_Z can be adjusted to achieve 4mA output at the minimum measurement temperature to correct for input offset voltage and reference current mismatch of the XTR112 and XTR114.

R_{CM} provides an additional voltage drop to bias the inputs of the XTR112 and XTR114 within their common-mode input range. R_{CM} should be bypassed with a 0.01µF capacitor to minimize common-mode noise. Resistor R_G sets the gain of the instrumentation amplifier according to the desired temperature range. R_{LIN1} provides second-order linearization correction to the RTD, typically achieving a 40:1 improvement in linearity. An additional resistor is required for three-wire RTD connections, see Figure 3.

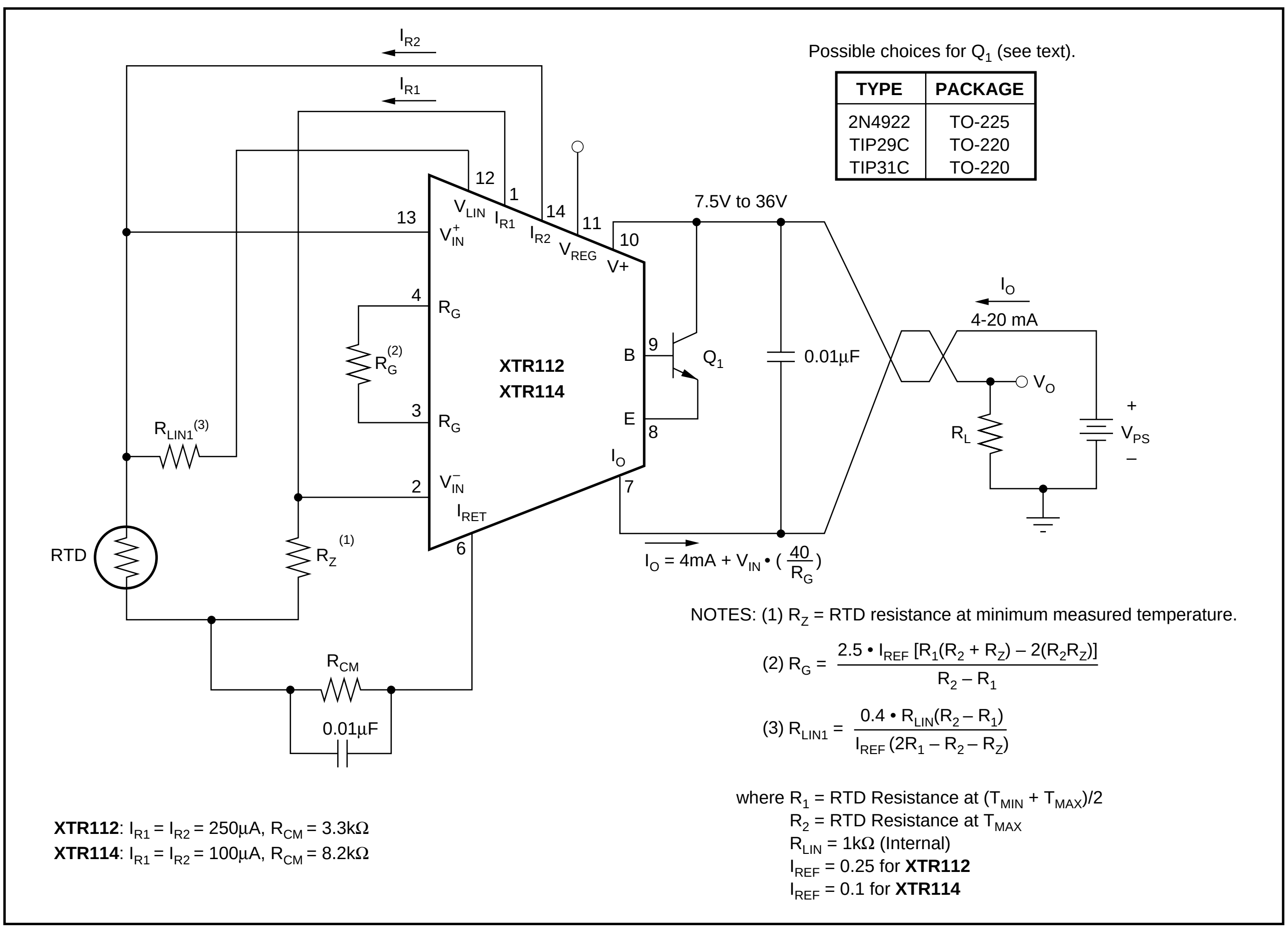
The transfer function through the complete instrumentation amplifier and voltage-to-current converter is:

$$I_O = 4mA + V_{IN} \bullet (40/R_G)$$
$$(V_{IN} \text{ in volts, } R_G \text{ in ohms})$$

where V_{IN} is the differential input voltage. As evident from the transfer function, if R_G is not used the gain is zero and the output is simply the XTR's zero current. The value of R_G varies slightly for two-wire RTD and three-wire RTD connections with linearization. R_G can be calculated from the equations given in Figure 1 (two-wire RTD connection) and Table I (three-wire RTD connection).

The I_{RET} pin is the return path for all current from the current sources and V_{REG}. The I_{RET} pin allows any current used in external circuitry to be sensed by the XTR112 and XTR114 and to be included in the output current without causing an error.

The V_{REG} pin provides an on-chip voltage source of approximately 5.1V and is suitable for powering external input circuitry (refer to Figure 6). It is a moderately accurate voltage reference—it is not the same reference used to set the precision current references. V_{REG} is capable of sourcing approximately 2.1mA of current for the XTR112 and 2.4mA for the XTR114. Exceeding these values may affect the 4mA zero output. Both products can sink approximately 1mA.



Possible choices for Q_1 (see text).

TYPE	PACKAGE
2N4922	TO-225
TIP29C	TO-220
TIP31C	TO-220

$$I_O = 4mA + V_{IN} \bullet \left(\frac{40}{R_G}\right)$$

NOTES: (1) R_Z = RTD resistance at minimum measured temperature.

(2) $R_G = \dfrac{2.5 \bullet I_{REF}\,[R_1(R_2 + R_Z) - 2(R_2R_Z)]}{R_2 - R_1}$

(3) $R_{LIN1} = \dfrac{0.4 \bullet R_{LIN}(R_2 - R_1)}{I_{REF}\,(2R_1 - R_2 - R_Z)}$

where R_1 = RTD Resistance at $(T_{MIN} + T_{MAX})/2$
R_2 = RTD Resistance at T_{MAX}
R_{LIN} = 1kΩ (Internal)
I_{REF} = 0.25 for **XTR112**
I_{REF} = 0.1 for **XTR114**

XTR112: $I_{R1} = I_{R2}$ = 250µA, R_{CM} = 3.3kΩ
XTR114: $I_{R1} = I_{R2}$ = 100µA, R_{CM} = 8.2kΩ

FIGURE 1. Basic Two-Wire RTD Temperature Measurement Circuit with Linearization.

A negative input voltage, V_{IN}, will cause the output current to be less than 4mA. Increasingly negative V_{IN} will cause the output current to limit at approximately 1.3mA for the XTR112 and 1mA for the XTR114. Refer to the typical curve "Under-Scale Current vs Temperature."

Increasingly positive input voltage (greater than the full-scale input) will produce increasing output current according to the transfer function, up to the output current limit of approximately 27mA. Refer to the typical curve "Over-Scale Current vs Temperature."

EXTERNAL TRANSISTOR

Transistor Q_1 conducts the majority of the signal-dependent 4-20mA loop current. Using an external transistor isolates the majority of the power dissipation from the precision input and reference circuitry of the XTR112 and XTR114, maintaining excellent accuracy.

Since the external transistor is inside a feedback loop its characteristics are not critical. Requirements are: V_{CEO} = 45V min, β = 40 min and P_D = 800mW. Power dissipation requirements may be lower if the loop power supply voltage is less than 36V. Some possible choices for Q_1 are listed in Figure 1.

The XTR112 and XTR114 can be operated without this external transistor, however, accuracy will be somewhat degraded due to the internal power dissipation. Operation without Q_1 is not recommended for extended temperature ranges. A resistor (R = 3.3kΩ) connected between the I_{RET} pin and the E (emitter) pin may be needed for operation below 0°C without Q_1 to guarantee the full 20mA full-scale output, especially with V+ near 7.5V.

LOOP POWER SUPPLY

The voltage applied to the XTR112 and XTR114, V+, is measured with respect to the I_O connection, pin 7. V+ can range from 7.5V to 36V. The loop supply voltage, V_{PS}, will differ from the applied voltage according to the voltage drop on the current sensing resistor, R_L (plus any other voltage drop in the line).

If a low loop supply voltage is used, R_L (including the loop wiring resistance) must be made a relatively low value to assure that V+ remains 7.5V or greater for the maximum loop current of 20mA:

$$R_L \text{ max} = \left(\frac{(V+) - 7.5V}{20mA}\right) - R_{WIRING}$$

It is recommended to design for V+ equal or greater than 7.5V with loop currents up to 30mA to allow for out-of-range input conditions.

The low operating voltage (7.5V) of the XTR112 and XTR114 allow operation directly from personal computer power supplies (12V ±5%). When used with the RCV420 Current Loop Receiver (Figure 7), load resistor voltage drop is limited to 3V.

ADJUSTING INITIAL ERRORS

Many applications require adjustment of initial errors. Input offset and reference current mismatch errors can be corrected by adjustment of the zero resistor, R_Z. Adjusting the gain-setting resistor, R_G, corrects any errors associated with gain.

TWO-WIRE AND THREE-WIRE RTD CONNECTIONS

In Figure 1, the RTD can be located remotely simply by extending the two connections to the RTD. With this remote two-wire connection to the RTD, line resistance will introduce error. This error can be partially corrected by adjusting the values of R_Z, R_G, and R_{LIN1}.

A better method for remotely located RTDs is the three-wire RTD connection shown in Figure 3. This circuit offers improved accuracy. R_Z's current is routed through a third wire to the RTD. Assuming line resistance is equal in RTD lines 1 and 2, this produces a small common-mode voltage which is rejected by the XTR112 and XTR114. A second resistor, R_{LIN2}, is required for linearization.

Note that although the two-wire and three-wire RTD connection circuits are very similar, the gain-setting resistor, R_G, has slightly different equations:

$$\text{Two-wire: } R_G = \frac{2.5 \bullet I_{REF}\left[R_1(R_2 + R_Z) - 2(R_2 R_Z)\right]}{R_2 - R_1}$$

$$\text{Three-wire: } R_G = \frac{2.5 \bullet I_{REF}(R_2 - R_Z)(R_1 - R_Z)}{R_2 - R_1}$$

where R_Z = RTD resistance at T_{MIN}
R_1 = RTD resistance at $(T_{MIN} + T_{MAX})/2$
R_2 = RTD resistance at T_{MAX}
I_{REF} = 0.25 for XTR112
I_{REF} = 0.1 for XTR114

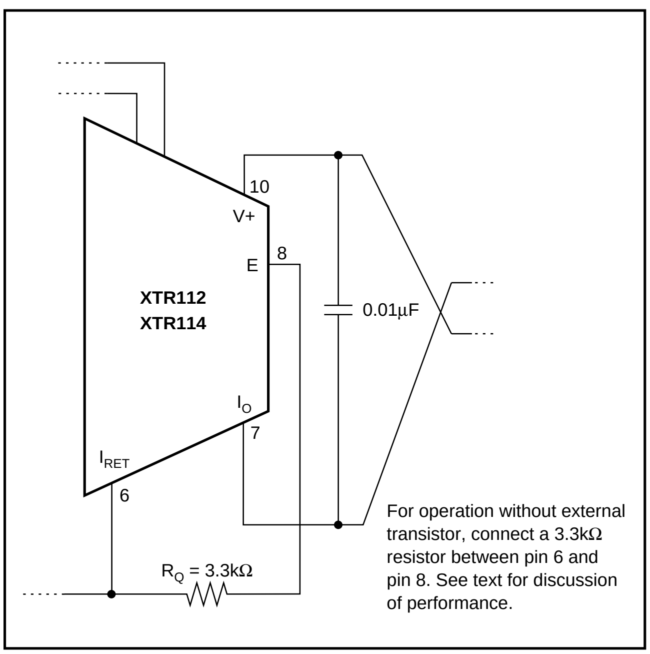


FIGURE 2. Operation Without External Transistor.

Table I summarizes the resistor equations for two-wire and three-wire RTD connections. An example calculation is also provided. To maintain good accuracy, at least 1% (or better) resistors should be used for R_G. Table II provides standard 1% R_G values for a three-wire Pt1000 RTD connection with linearization for the XTR112. Table III gives R_G values for the XTR114.

LINEARIZATION

RTD temperature sensors are inherently (but predictably) nonlinear. With the addition of one or two external resistors, R_{LIN1} and R_{LIN2}, it is possible to compensate for most of this nonlinearity resulting in 40:1 improvement in linearity over the uncompensated output.

	TWO-WIRE		THREE-WIRE		
	R_G	R_{LIN1}	R_G	R_{LIN1}	R_{LIN2}
General Equations	$= \frac{I_{REF} \cdot 2.5 [R_1 (R_2 + R_Z) - 2 (R_2R_Z)]}{(R_2 - R_1)}$	$= \frac{0.4 \cdot R_{LIN} (R_2 - R_1)}{I_{REF} \cdot (2R_1 - R_2 - R_Z)}$	$= \frac{I_{REF} \cdot 2.5 (R_2 - R_Z) (R_1 - R_Z)]}{(R_2 - R_1)}$	$= \frac{0.4 \cdot R_{LIN} (R_2 - R_1)}{I_{REF} \cdot (2R_1 - R_2 - R_Z)}$	$= \frac{0.4 \cdot (R_{LIN} + R_G)(R_2 - R_1)}{I_{REF} \cdot (2R_1 - R_2 - R_Z)}$
XTR112 (I_{REF} = 0.25) (see Table II)	$= \frac{0.625 \cdot [R_1 (R_2 + R_Z) - 2 (R_2R_Z)]}{(R_2 - R_1)}$	$= \frac{1.6 \cdot R_{LIN} (R_2 - R_1)}{(2R_1 - R_2 - R_Z)}$	$= \frac{0.625 \cdot (R_2 - R_Z) (R_1 - R_Z)]}{(R_2 - R_1)}$	$= \frac{1.6 \cdot R_{LIN} (R_2 - R_1)}{(2R_1 - R_2 - R_Z)}$	$= \frac{1.6 \cdot (R_{LIN} + R_G)(R_2 - R_1)}{(2R_1 - R_2 - R_Z)}$
XTR114 (I_{REF} = 0.1) (see Table III)	$= \frac{0.25 \cdot [R_1 (R_2 + R_Z) - 2 (R_2R_Z)]}{(R_2 - R_1)}$	$= \frac{4 \cdot R_{LIN} (R_2 - R_1)}{(2R_1 - R_2 - R_Z)}$	$= \frac{0.25 \cdot (R_2 - R_Z) (R_1 - R_Z)]}{(R_2 - R_1)}$	$= \frac{4 \cdot R_{LIN} (R_2 - R_1)}{(2R_1 - R_2 - R_Z)}$	$= \frac{4 \cdot (R_{LIN} + R_G)(R_2 - R_1)}{(2R_1 - R_2 - R_Z)}$

where R_Z = RTD resistance at the minimum measured temperature, T_{MIN}

R_1 = RTD resistance at the midpoint measured temperature, $T_{MID} = (T_{MIN} + T_{MAX})/2$

R_2 = RTD resistance at maximum measured temperature, T_{MAX}

R_{LIN} = 1kΩ (internal)

XTR112 RESISTOR EXAMPLE:

The measurement range is –100°C to +200°C for a 3-wire Pt100 RTD connection. Determine the values for R_S, R_G, R_{LIN1}, and R_{LIN2}. Look up the values from the chart or calculate the values according to the equations provided.

METHOD 1: TABLE LOOK UP

T_{MIN} = –100°C and ΔT = 300°C (T_{MAX} = +200°C),
Using Table II the 1% values are:

R_Z = 604Ω R_{LIN1} = 33.2kΩ

R_G = 750Ω R_{LIN2} = 59kΩ

METHOD 2: CALCULATION

Step 1: Determine R_Z, R_1, and R_2.

R_Z is the RTD resistance at the minimum measured temperature, T_{MIN} = –100°C. Using Equation (1) at right gives R_Z = 602.5Ω (1% value is 604Ω).

R_2 is the RTD resistance at the maximum measured temperature, T_{MAX} = 200°C. Using Equation (2) at right gives R_2 = 1758.4Ω.

R_1 is the RTD resistance at the midpoint measured temperature, $T_{MID} = (T_{MIN} + T_{MAX})/2$ = (–100 + 200)/2 = 50°C. R_1 is NOT the average of R_Z and R_2. Using Equation (2) at right gives R_1 = 1194Ω.

Step 2: Calculate R_G, R_{LIN1}, and R_{LIN2} using equations above.

R_G = 757Ω (1% value is 750Ω)
R_{LIN1} = 33.322kΩ (1% value is 33.2kΩ)
R_{LIN2} = 58.548kΩ (1% value is 59kΩ)

Calculation of Pt1000 Resistance Values
(according to DIN IEC 751)

Equation (1) Temperature range from –200°C to 0°C:
$R_{(T)} = 1000 [1 + 3.90802 \cdot 10^{-3} \cdot T - 0.5802 \cdot 10^{-6} \cdot T^2 - 4.27350 \cdot 10^{-12} \cdot (T - 100) \cdot T^3]$

Equation (2) Temperature range from 0°C to +850°C:
$R_{(T)} = 1000 (1 + 3.90802 \cdot 10^{-3} \cdot T - 0.5802 \cdot 10^{-6} \cdot T^2)$

where: $R_{(T)}$ is the resistance in Ω at temperature T.
T is the temperature in °C.

NOTE: Most RTD manufacturers provide reference tables for resistance values at various temperatures.

Resistor values for other RTD types (such as Pt2000) can be calculated using the XTR resistor selection program in the Applications Section on Burr-Brown's web site (www.burr-brown.com)

TABLE I. Summary of Resistor Equations for Two-Wire and Three-Wire Pt1000 RTD Connections.

XTR112 1% RESISTOR VALUES FOR A THREE-WIRE RTD CONNECTION

MEASUREMENT TEMPERATURE SPAN ΔT (°C)

T_{MIN}	100°C	200°C	300°C	400°C	500°C	600°C	700°C	800°C	900°C	1000°C
–200°C	187/267 48700 61900	187/536 31600 48700	187/806 25500 46400	187/1050 21500 44200	187/1330 17800 41200	187/1580 15000 39200	187/1820 13000 36500	187/2100 11300 34800	187/2370 9760 33200	187/2670 8660 31600
–100°C	604/255 86600 110000	604/499 49900 75000	604/4750 33200 59000	604/1000 24900 49900	604/1270 19600 44200	604/1500 15800 40200	604/1780 13300 37400	604/2050 11500 34800	604/2260 10000 32400	
0°C	1000/243 105000 130000	1000/487 51100 76800	1000/732 33200 57600	1000/976 24300 48700	1000/1210 19100 42200	1000/1470 15400 38300	1000/1740 13000 35700	1000/1960 11000 33200		
100°C	1370/237 102000 127000	1370/475 49900 73200	1370/715 32400 56200	1370/953 23700 46400	1370/1180 18700 40200	1370/1430 15000 36500	1370/1690 12400 33200			
200°C	1740/232 100000 121000	1740/464 48700 69800	1740/698 31600 53600	1740/931 23200 44200	1740/1150 17800 38300	1740/1400 14300 34800				
300°C	2100/221 95300 118000	2100/442 46400 68100	2100/665 30100 51100	2100/887 22100 42200	2100/1130 17400 36500					
400°C	2490/215 93100 113000	2490/432 45300 64900	2490/649 29400 48700	2490/866 21500 40200						
500°C	2800/210 887000 107000	2800/412 43200 61900	2800/619 28000 45300							
600°C	3160/200 86600 102000	3160/402 42200 59000								
700°C	3480/191 82500 100000									
800°C	3740/187 80600 95300									

R_Z/R_G
R_{LIN1}
R_{LIN2}

NOTE: The values listed in the table are 1% resistors (in Ω). Exact values may be calculated from the following equations:

R_Z = RTD resistance at minimum measured temperature, T_{MIN}.

$$R_G = \frac{0.625 \bullet (R_2 - R_Z)(R_1 - R_Z)}{(R_2 - R_1)}$$

$$R_{LIN1} = \frac{1.6 \bullet R_{LIN}(R_2 - R_1)}{(2R_1 - R_2 - R_Z)}$$

$$R_{LIN2} = \frac{1.6 \bullet (R_{LIN} + R_G)(R_2 - R_1)}{(2R_1 - R_2 - R_Z)}$$

where R_1 = RTD resistance at the midpoint measured temperature, $(T_{MIN} + T_{MAX})/2$

R_2 = RTD resistance at T_{MAX}

R_{LIN} = 1kΩ (Internal)

TABLE II. XTR112 R_Z, R_G, R_{LIN1}, and R_{LIN2} Standard 1% Resistor Values for Three-Wire Pt1000 RTD Connection with Linearization.

XTR114 1% RESISTOR VALUES FOR A THREE-WIRE RTD CONNECTION

MEASUREMENT TEMPERATURE SPAN ΔT (°C)

T_{MIN}	100°C	200°C	300°C	400°C	500°C	600°C	700°C	800°C	900°C	1000°C
–200°C	187/107 121000 133000	187/215 78700 95300	187/316 64900 84500	187/422 53600 76800	187/523 45300 68100	187/634 38300 68100	187/732 32400 56200	187/845 28000 52300	187/953 24900 47500	187/1050 21500 45300
–100°C	604/102 221000 243000	604/200 124000 150000	604/301 84500 110000	604/402 61900 86600	604/511 48700 73200	604/604 40200 63400	604/715 33200 57600	604/806 28700 52300	604/909 24900 47500	
0°C	1000/97.6 261000 287000	1000/196 130000 154000	1000/294 84500 107000	1000/392 61900 84500	1000/487 47500 71500	1000/590 39200 61900	1000/681 32400 54900	1000/787 27400 49900		
100°C	1370/95.3 255000 280000	1370/191 124000 147000	1370/287 80600 105000	1370/383 59000 82500	1370/475 46400 68100	1370/576 37400 59000	1370/665 31600 52300			
200°C	1740/90.9 249000 267000	1740/182 121000 143000	1740/274 78700 100000	1740/365 57600 78700	1740/464 44200 64900	1740/549 36500 56200				
300°C	2100/88.9 237000 261000	2100/178 118000 137000	2100/267 75000 95300	2100/357 54900 75000	2100/348 43200 61900					
400°C	2490/86.6 232000 249000	2490/174 113000 133000	2490/261 73200 93100	2490/249 53600 71500						
500°C	2800/82.5 221000 243000	2800/165 110000 127000	2800/49 69800 88700							
600°C	3160/80.6 215000 215000	3160/162 105000 121000								
700°C	3480/76.8 205000 221000									
800°C	3740/75 200000 215000									

R_Z/R_G
R_{LIN1}
R_{LIN2}

NOTE: The values listed in the table are 1% resistors (in Ω). Exact values may be calculated from the following equations:

R_Z = RTD resistance at minimum measured temperature, T_{MIN}.

$$R_G = \frac{0.25 \bullet (R_2 - R_Z)(R_1 - R_Z)}{(R_2 - R_1)}$$

$$R_{LIN1} = \frac{4 \bullet R_{LIN}(R_2 - R_1)}{(2R_1 - R_2 - R_Z)}$$

$$R_{LIN2} = \frac{4 \bullet (R_{LIN} + R_G)(R_2 - R_1)}{(2R_1 - R_2 - R_Z)}$$

where R_1 = RTD resistance at the midpoint measured temperature, $(T_{MIN} + T_{MAX})/2$

R_2 = RTD resistance at T_{MAX}

R_{LIN} = 1kΩ (Internal)

TABLE III. XTR114 R_Z, R_G, R_{LIN1}, and R_{LIN2} Standard 1% Resistor Values for Three-Wire Pt1000 RTD Connection with Linearization.

A typical two-wire RTD application with linearization is shown in Figure 1. Resistor R_{LIN1} provides positive feedback and controls linearity correction. R_{LIN1} is chosen according to the desired temperature range. An equation is given in Figure 1.

In three-wire RTD connections, an additional resistor, R_{LIN2}, is required. As with the two-wire RTD application, R_{LIN1} provides positive feedback for linearization. R_{LIN2} provides an offset canceling current to compensate for wiring resistance encountered in remotely located RTDs. R_{LIN1} and R_{LIN2} are chosen such that their currents are equal. This makes the voltage drop in the wiring resistance to the RTD a common-mode signal which is rejected by the XTR112 and XTR114. The nearest standard 1% resistor values for R_{LIN1} and R_{LIN2} should be adequate for most applications. Tables II and III provide the 1% resistor values for a three-wire Pt1000 RTD connection.

If no linearity correction is desired, the V_{LIN} pin should be left open. With no linearization, $R_G = 2500 \cdot V_{FS}$, where V_{FS} = full-scale input range.

RTDs

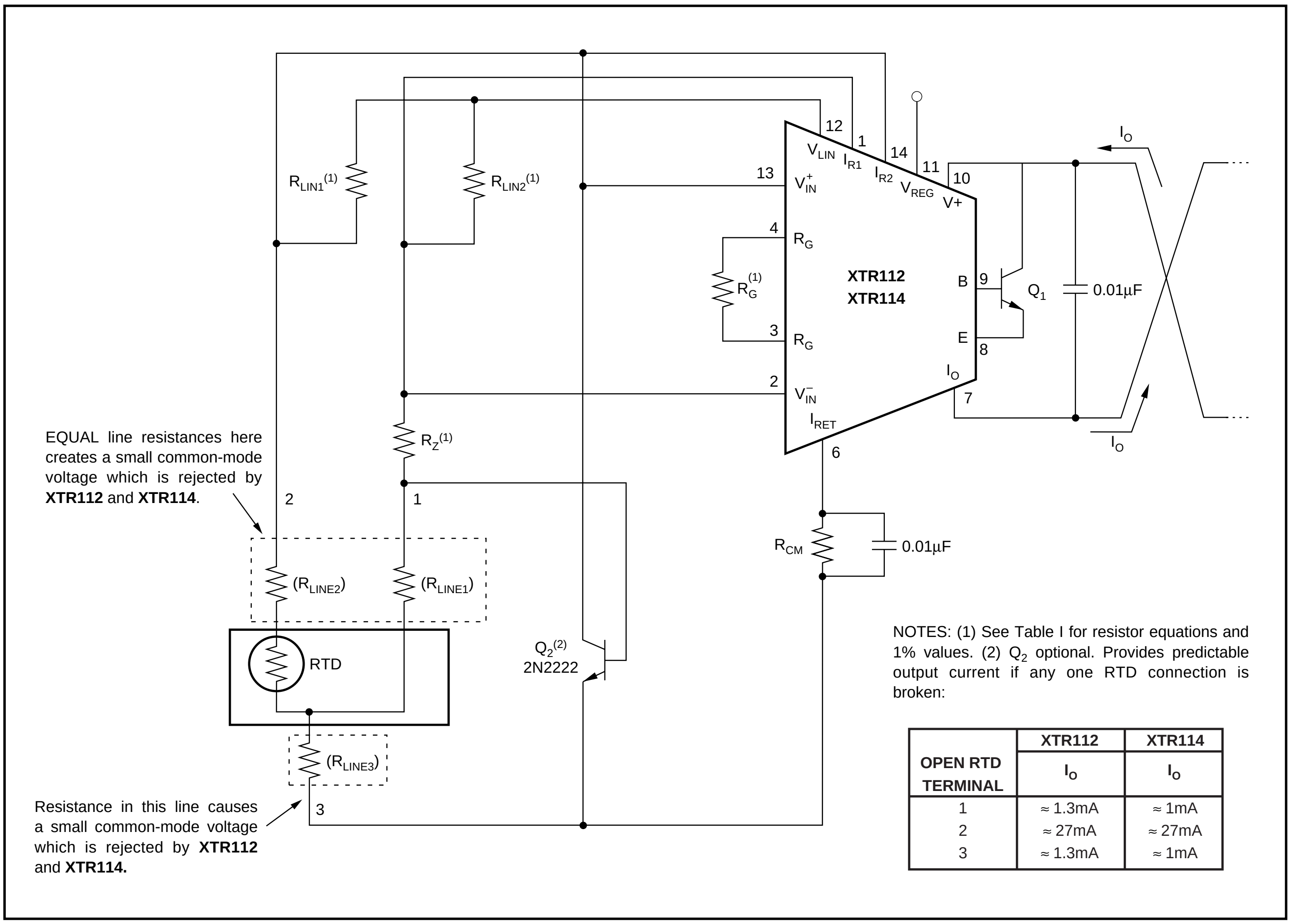
The text and figures thus far have assumed a Pt1000 RTD. With higher resistance RTDs, the temperature range and input voltage variation should be evaluated to ensure proper common-mode biasing of the inputs. As mentioned earlier, R_{CM} can be adjusted to provide an additional voltage drop to bias the inputs of the XTR112 and XTR114 within their common-mode input range.

ERROR ANALYSIS

Table IV shows how to calculate the effect various error sources have on circuit accuracy. A sample error calculation for a typical RTD measurement circuit (Pt1000 RTD, 200°C measurement span) is provided. The results reveal the XTR112's and XTR114's excellent accuracy, in this case 1% unadjusted for the XTR112, 1.16% for the XTR114. Adjusting resistors R_G and R_Z for gain and offset errors improves the XTR112's accuracy to 0.28% (0.31% for the XTR114). Note that these are worst-case errors; guaranteed maximum values were used in the calculations and all errors were assumed to be positive (additive). The XTR112 and XTR114 achieve performance which is difficult to obtain with discrete circuitry and requires less space.

OPEN-CIRCUIT PROTECTION

The optional transistor Q_2 in Figure 3 provides predictable behavior with open-circuit RTD connections. It assures that if any one of the three RTD connections is broken, the XTR's output current will go to either its high current limit (≈ 27mA) or low current limit (≈ 1.3mA for XTR112 and ≈ 1mA for XTR114). This is easily detected as an out-of-range condition.



NOTES: (1) See Table I for resistor equations and 1% values. (2) Q_2 optional. Provides predictable output current if any one RTD connection is broken:

OPEN RTD TERMINAL	XTR112 I_O	XTR114 I_O
1	≈ 1.3mA	≈ 1mA
2	≈ 27mA	≈ 27mA
3	≈ 1.3mA	≈ 1mA

FIGURE 3. Three-Wire Connection for Remotely Located RTDs.

SAMPLE ERROR CALCULATION FOR XTR112[1]

RTD value at 4mA Output ($R_{RTD\ MIN}$)	1000Ω
RTD Measurement Range	200°C
Ambient Temperature Range (ΔT_A)	20°C
Supply Voltage Change (ΔV+)	5V
Common-Mode Voltage Change (ΔCM)	0.1V

ERROR SOURCE	ERROR EQUATION	SAMPLE ERROR CALCULATION[2]	ERROR (ppm of Full Scale) UNADJ.	ERROR (ppm of Full Scale) ADJUST.
INPUT				
Input Offset Voltage	$V_{OS}/(V_{IN\ MAX}) \cdot 10^6$	$100\mu V/(250\mu A \cdot 3.8\Omega/°C \cdot 200°C) \cdot 10^6$	526	0
vs Common-Mode	$CMRR \cdot \Delta CM/(V_{IN\ MAX}) \cdot 10^6$	$50\mu V/V \cdot 0.1V/(250\mu A \cdot 3.8\Omega/°C \cdot 200°C) \cdot 10^6$	26	26
Input Bias Current	$I_B/I_{REF} \cdot 10^6$	$0.025\mu A/250\mu A \cdot 10^6$	100	0
Input Offset Current	$I_{OS} \cdot R_{RTD\ MIN}/(V_{IN\ MAX}) \cdot 10^6$	$3nA \cdot 1000\Omega/(250\mu A \cdot 3.8\Omega/°C \cdot 200°C) \cdot 10^6$	16	0
		Total Input Error:	**668**	**26**
EXCITATION				
Current Reference Accuracy	I_{REF} Accuracy (%)/100% • 10^6	0.2%/100% • 10^6	2000	0
vs Supply	(I_{REF} vs V+) • ΔV+	25ppm/V • 5V	125	125
Current Reference Matching	I_{REF} Matching (%)/100% • I_{REF} • $R_{RTD\ MIN}/(V_{IN\ MAX})$ • 10^6	$0.1\%/100\% \cdot 250\mu A \cdot 1000\Omega/(250\mu A \cdot 3.8\Omega/°C \cdot 200°C) \cdot 10^6$	1316	0
vs Supply	(I_{REF} matching vs V+) • ΔV+ • $R_{RTD\ MIN}/(V_{IN\ MAX})$	$10ppm/V \cdot 5V \cdot 250\mu A \cdot 1000\Omega/(250\mu A \cdot 3.8\Omega/°C \cdot 200°C)$	66	66
		Total Excitation Error:	**3507**	**191**
GAIN				
Span	Span Error (%)/100% • 10^6	0.2%/100% • 10^6	2000	0
Nonlinearity	Nonlinearity (%)/100% • 10^6	0.01%/100% • 10^6	100	100
		Total Gain Error:	**2100**	**100**
OUTPUT				
Zero Output	$(I_{ZERO} - 4mA)/16000\mu A \cdot 10^6$	$25\mu A/16000\mu A \cdot 10^6$	1563	0
vs Supply	$(I_{ZERO}$ vs V+) • ΔV+/16000µA • 10^6	$0.2\mu A/V \cdot 5V/16000\mu A \cdot 10^6$	63	63
		Total Output Error:	**1626**	**63**
DRIFT (ΔT_A = 20°C)				
Input Offset Voltage	$Drift \cdot \Delta T_A/(V_{IN\ MAX}) \cdot 10^6$	$1.5\mu V/°C \cdot 20°C/(250\mu A \cdot 3.8\Omega/°C \cdot 200°C) \cdot 10^6$	158	158
Input Bias Current (typical)	$Drift \cdot \Delta T_A/I_{REF} \cdot 10^6$	$20pA/°C \cdot 20°C/250\mu A \cdot 10^6$	2	2
Input Offset Current (typical)	$Drift \cdot \Delta T_A \cdot R_{RTD\ MIN}/(V_{IN\ MAX}) \cdot 10^6$	$5pA/°C \cdot 20°C \cdot 1000\Omega/(250\mu A \cdot 3.8\Omega/°C \cdot 200°C) \cdot 10^6$	0.5	0.5
Current Reference Accuracy	$Drift \cdot \Delta T_A$	35ppm/°C • 20°C	700	700
Current Reference Matching	$Drift \cdot \Delta T_A \cdot I_{REF} \cdot R_{RTD\ MIN}/(V_{IN\ MAX})$	$15ppm/°C \cdot 20°C \cdot 250\mu A \cdot 1000\Omega/(250\mu A \cdot 3.8\Omega/°C \cdot 200°C)$	395	395
Span	$Drift \cdot \Delta T_A$	25ppm/°C • 20°C	500	500
Zero Output	$Drift \cdot \Delta T_A/16000\mu A \cdot 10^6$	$0.5\mu A/°C \cdot 20°C/16000\mu A \cdot 10^6$	626	626
		Total Drift Error:	**2382**	**2382**
NOISE (0.1Hz to 10Hz, typ)				
Input Offset Voltage	$v_n/(V_{IN\ MAX}) \cdot 10^6$	$0.6\mu V/(250\mu A \cdot 3.8\Omega/°C \cdot 200°C) \cdot 10^6$	3	3
Current Reference	I_{REF} Noise • $R_{RTD\ MIN}/(V_{IN\ MAX}) \cdot 10^6$	$3nA \cdot 1000\Omega/(250\mu A \cdot 3.8\Omega/°C \cdot 200°C) \cdot 10^6$	16	16
Zero Output	I_{ZERO} Noise/16000µA • 10^6	$0.03\mu A/16000\mu A \cdot 10^6$	2	2
		Total Noise Error:	**21**	**21**
		TOTAL ERROR:	**10304 (1.03%)**	**2783 (0.28%)**

NOTES: (1) For XTR114, I_{REF} = 100µA. Total unadjusted error is 1.16%, adjusted error 0.31%. (2) All errors are min/max and referred to input, unless otherwise stated.

TABLE IV. Error Calculation.

REVERSE-VOLTAGE PROTECTION

The XTR112's and XTR114's low compliance rating (7.5V) permits the use of various voltage protection methods without compromising operating range. Figure 4 shows a diode bridge circuit which allows normal operation even when the voltage connection lines are reversed. The bridge causes a two diode drop (approximately 1.4V) loss in loop supply voltage. This results in a compliance voltage of approximately 9V—satisfactory for most applications. If 1.4V drop in loop supply is too much, a diode can be inserted in series with the loop supply voltage and the V+ pin. This protects against reverse output connection lines with only a 0.7V loss in loop supply voltage.

SURGE PROTECTION

Remote connections to current transmitters can sometimes be subjected to voltage surges. It is prudent to limit the maximum surge voltage applied to the XTR to as low as practical. Various zener diode and surge clamping diodes are specially designed for this purpose. Select a clamp diode with as low a voltage rating as possible for best protection. For example, a 36V protection diode will assure proper transmitter operation at normal loop voltages, yet will provide an appropriate level of protection against voltage surges. Characterization tests on three production lots showed no damage to the XTR112 or XTR114 within loop supply voltages up to 65V.

Most surge protection zener diodes have a diode characteristic in the forward direction that will conduct excessive current, possibly damaging receiving-side circuitry if the loop connections are reversed. If a surge protection diode is used, a series diode or diode bridge should be used for protection against reversed connections.

RADIO FREQUENCY INTERFERENCE

The long wire lengths of current loops invite radio frequency interference. RF can be rectified by the sensitive input circuitry of the XTR112 and XTR114 causing errors. This generally appears as an unstable output current that varies with the position of loop supply or input wiring.

If the RTD sensor is remotely located, the interference may enter at the input terminals. For integrated transmitter assemblies with short connection to the sensor, the interference more likely comes from the current loop connections.

Bypass capacitors on the input reduce or eliminate this input interference. Connect these bypass capacitors to the I_{RET} terminal as shown in Figure 5. Although the dc voltage at the I_{RET} terminal is not equal to 0V (at the loop supply, V_{PS}) this circuit point can be considered the transmitter's "ground." The 0.01µF capacitor connected between V+ and I_O may help minimize output interference.

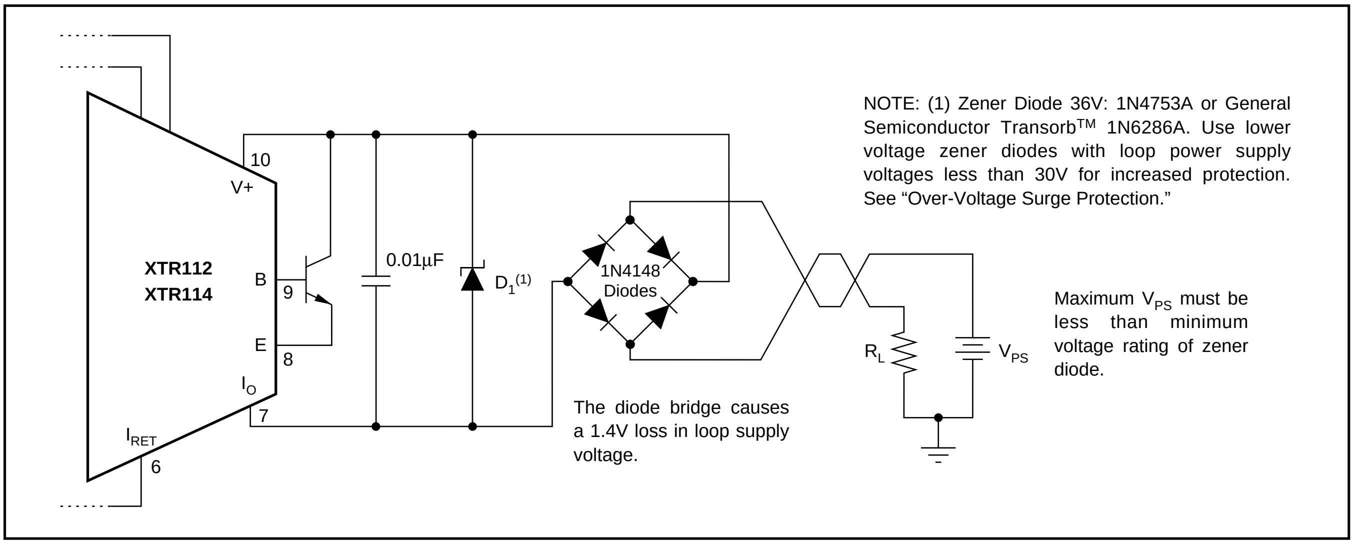


FIGURE 4. Reverse Voltage Operation and Over-Voltage Surge Protection.

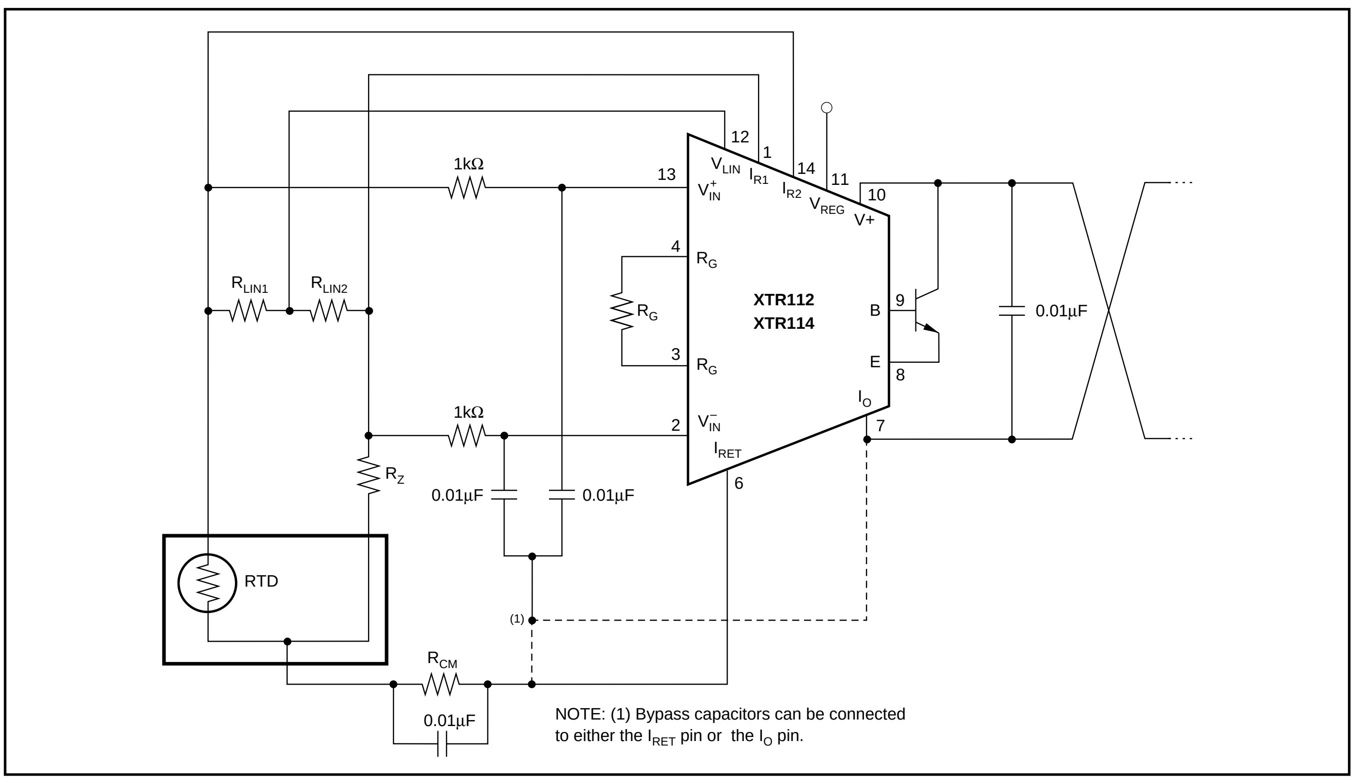


FIGURE 5. Input Bypassing Technique with Linearization.

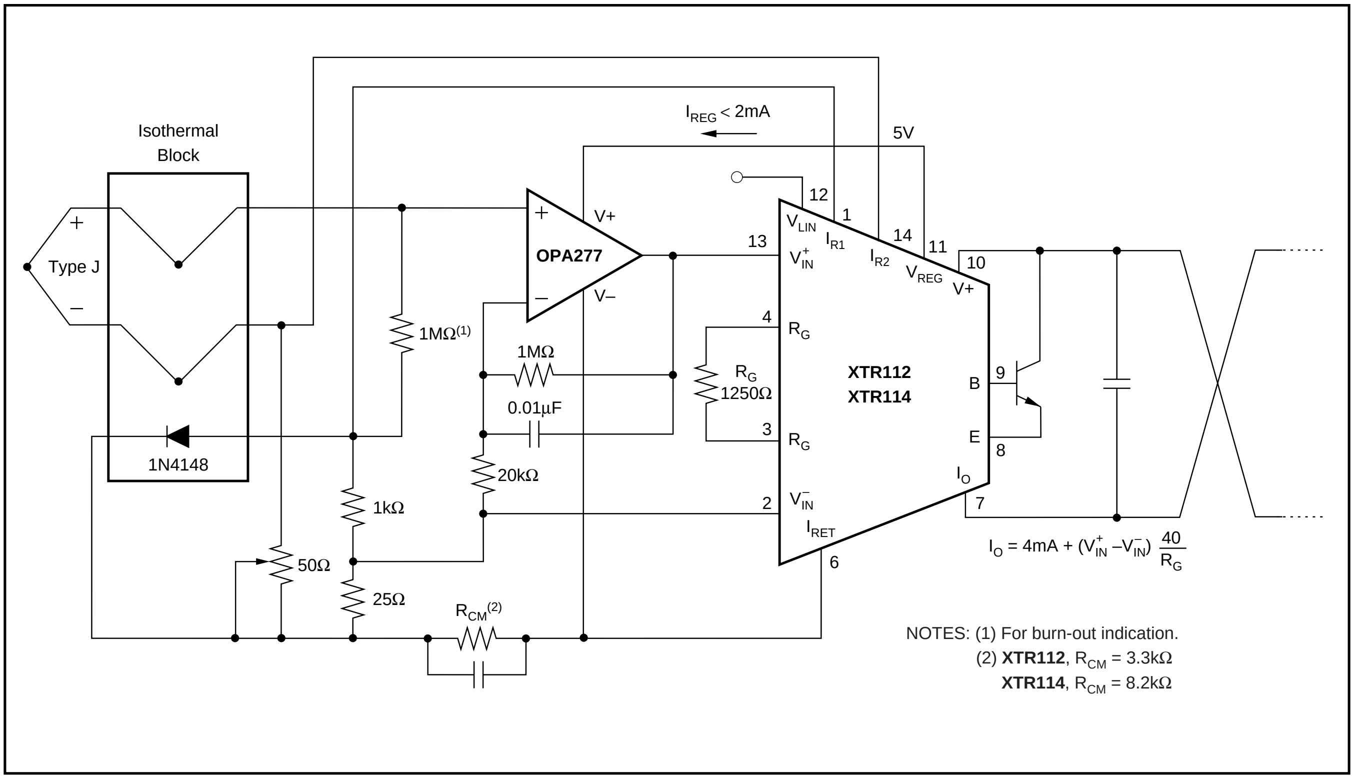


FIGURE 6. Thermocouple Low Offset, Low Drift Loop Measurement with Diode Cold-Junction Compensation.

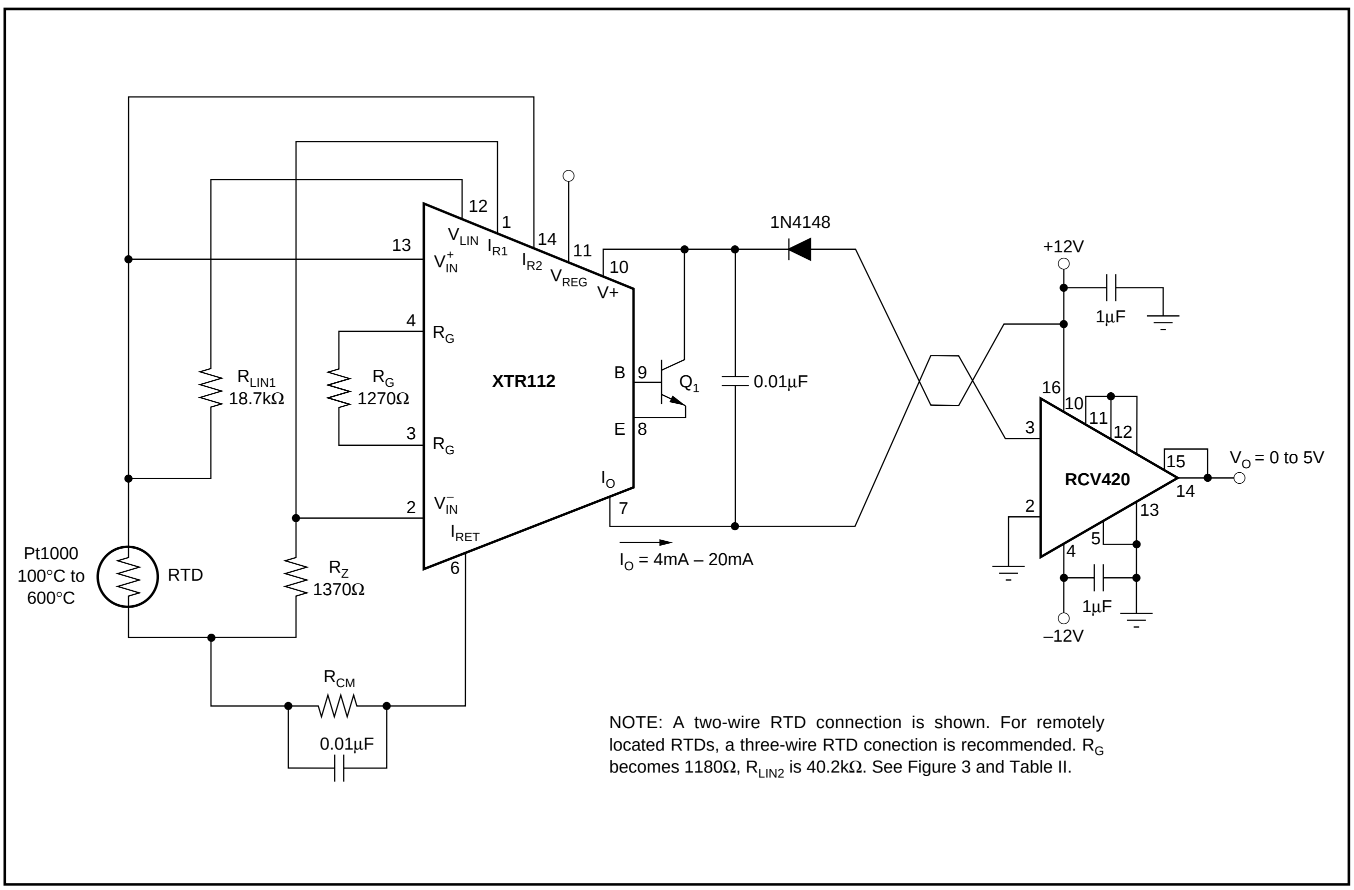


FIGURE 7. ±12V Powered Transmitter/Receiver Loop.

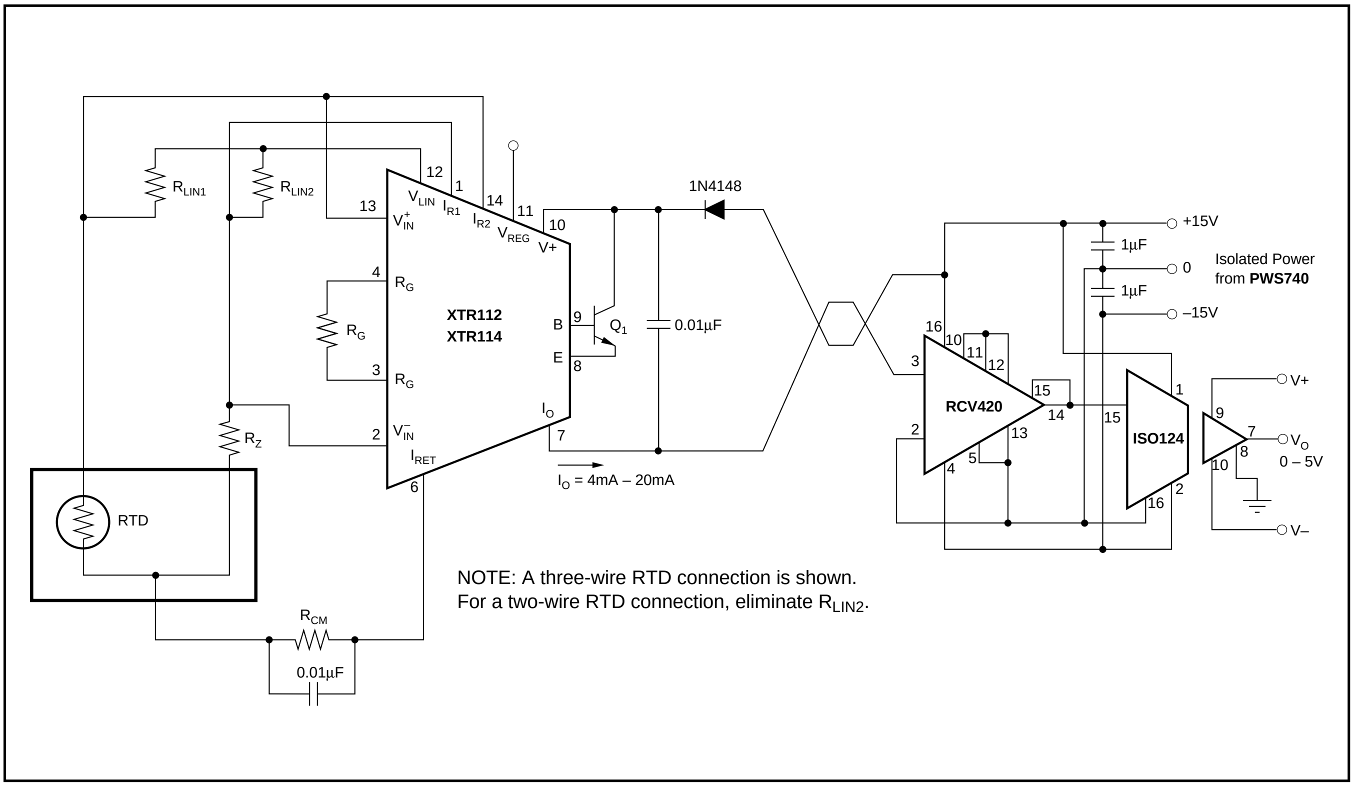


FIGURE 8. Isolated Transmitter/Receiver Loop.

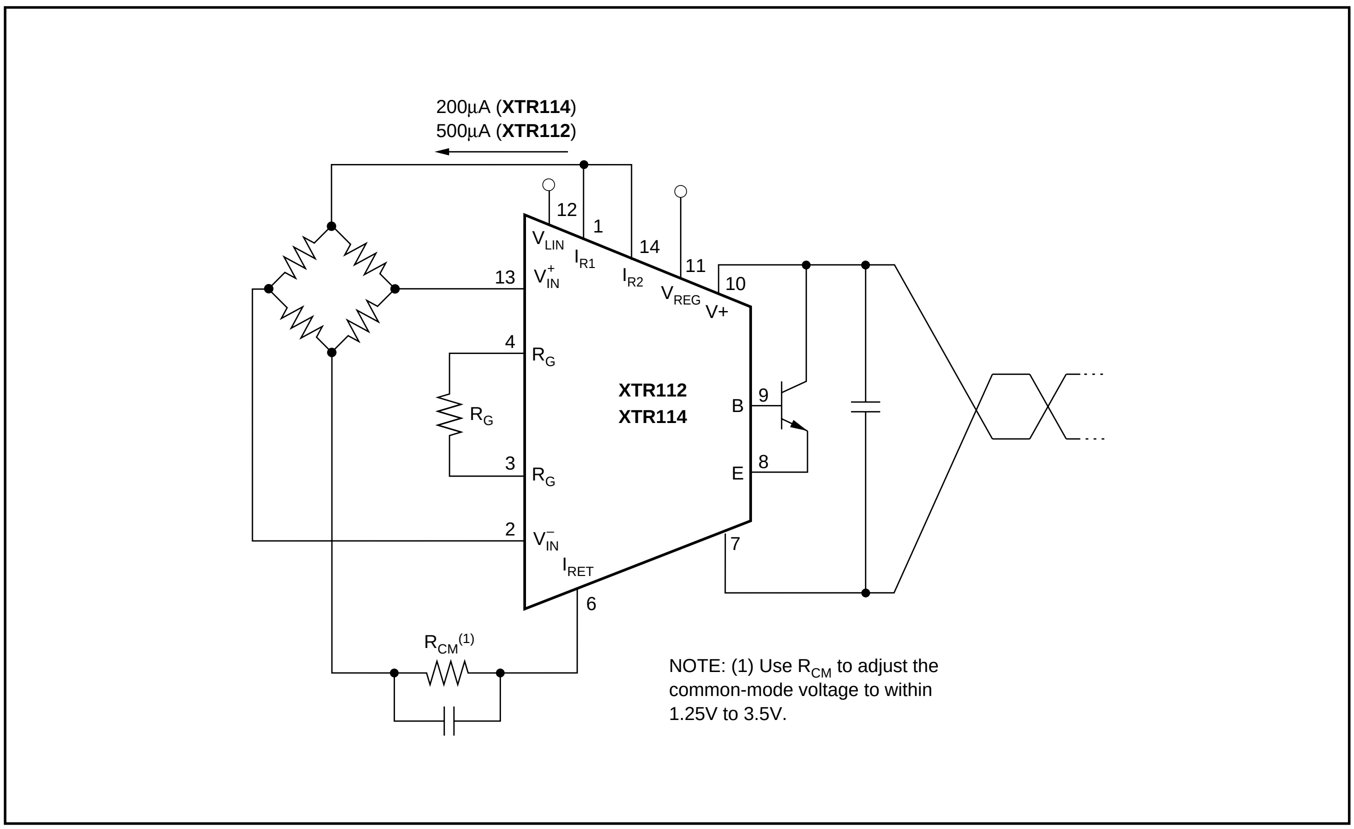


FIGURE 9. Bridge Input, Current Excitation.

PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package | Pins	Package qty | Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
XTR112U	Active	Production	SOIC (D) | 14	50 | TUBE	Yes	Call TI	Level-3-260C-168 HR	-40 to 85	XTR112U
XTR112U.A	Active	Production	SOIC (D) | 14	50 | TUBE	Yes	Call TI	Level-3-260C-168 HR	-40 to 85	XTR112U
XTR112UA	Active	Production	SOIC (D) | 14	50 | TUBE	Yes	Call TI	Level-3-260C-168 HR	-40 to 85	XTR112U A
XTR112UA.A	Active	Production	SOIC (D) | 14	50 | TUBE	Yes	Call TI	Level-3-260C-168 HR	-40 to 85	XTR112U A

(1) **Status:** For more details on status, see our product life cycle.

(2) **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

(3) **RoHS values:** Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

(4) **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

(5) **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

(6) **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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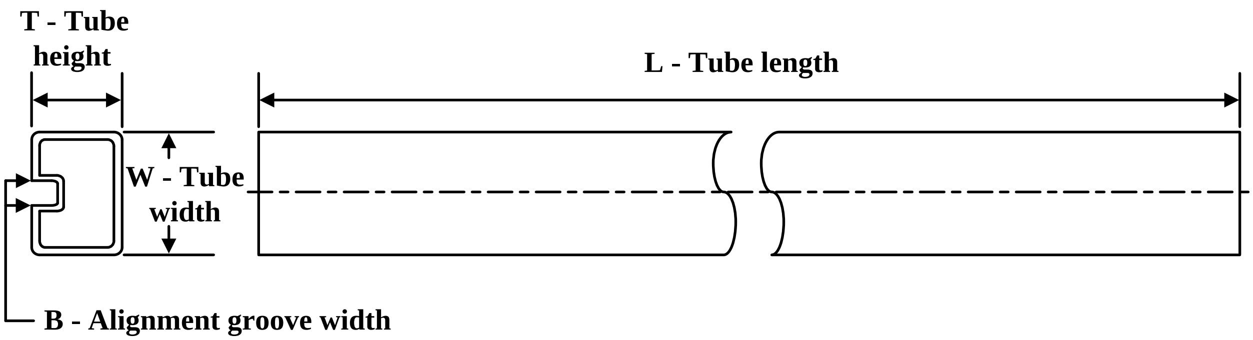
TUBE



*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	T (µm)	B (mm)
XTR112U	D	SOIC	14	50	506.6	8	3940	4.32
XTR112U.A	D	SOIC	14	50	506.6	8	3940	4.32
XTR112UA	D	SOIC	14	50	506.6	8	3940	4.32
XTR112UA.A	D	SOIC	14	50	506.6	8	3940	4.32