







UCC27423-Q1, UCC27424-Q1, UCC27425-Q1 SGLS274I - SEPTEMBER 2008 - REVISED NOVEMBER 2023

# UCC2742x-Q1 Dual 4-A High-Speed Low-Side MOSFET Drivers With Enable

### 1 Features

- Qualified for Automotive Applications
- AEC-Q100 Qualified With the Following Results:
  - Device Temperature Grade 1: –40°C to +125°C Ambient Operating Temperature Range
  - Device HBM ESD Classification Level 2
  - Device CDM ESD Classification Level C6
- Industry-Standard Pinout
- **Enable Functions for Each Driver**
- High-Current Drive Capability of ±4 A
- Unique Bipolar and CMOS True Drive Output Stage Provides High Current at MOSFET Miller Thresholds
- Inputs Independent of Supply Voltage Compatible With TTL and CMOS
- 20-ns Typical Rise and 15-ns Typical Fall Times With 1.8-nF Load
- Typical Propagation Delay Times of 25 ns With Input Falling and 35 ns With Input Rising
- 4-V to 15-V Supply Voltage
- Dual Outputs Can Be Paralleled for Higher Drive
- Available in Thermally Enhanced MSOP PowerPAD™ Package
- Rated From -40°C to +125°C

# 2 Applications

- Switch Mode Power Supplies
- **DC-DC Converters**
- **Motor Controllers**
- Line Drivers
- Class D Switching Amplifiers

# 3 Description

The UCC2742x-Q1 family of devices are high-speed dual MOSFET drivers capable of delivering large peak currents into capacitive loads. Two standard logic options are offered: dual inverting and dual noninverting drivers. They are offered in the standard 8-pin SOIC (D) package. The thermally enhanced 8-pin PowerPAD Package MSOP package (DGN) drastically lowers the thermal resistance to improve long-term reliability.

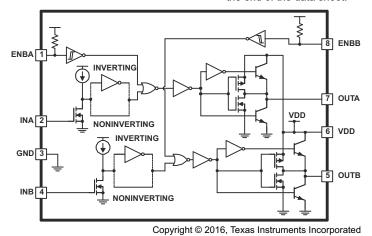
Using a design that inherently minimizes shootthrough current, these drivers deliver 4-A current where it is needed most, at the Miller plateau region, during the MOSFET switching transition. A unique bipolar and MOSFET hybrid output stage in parallel also allows efficient current sourcing and sinking at low supply voltages.

The UCC2742x-Q1 provide enable (ENBL) functions to have better control of the operation of the driver applications. ENBA and ENBB are implemented on pins 1 and 8, which were previously left unused in the industry standard pinout. They are internally pulled up to V<sub>DD</sub> for active-high logic and can be left open for standard operation.

### **Device Information**

PART NUMBER <sup>(1)</sup>	PACKAGE	BODY SIZE (NOM)
	SOIC (8)	4.90 mm × 3.91 mm
UCC2742x-Q1	MSOP With PowerPAD (8)	3.00 mm × 3.00 mm

For all available packages, see the orderable addendum at the end of the data sheet.





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# **4 Device Comparison Table**

ORDERABLE PART NUMBER <sup>(1)</sup>	CONFIGURATION
UCC27423QDGNRQ1	Dual Inverting
UCC27424QDGNRQ1	Dual Noninverting
UCC27423QDRQ1	Dual Inverting
UCC27424QDRQ1	Dual Noninverting
UCC27425QDRQ1	One Inverting, One Noninverting

<sup>(1)</sup> For the most current package and ordering information, see Section 13, or see the TI web site at www.ti.com.



# **5 Pin Configuration and Functions**

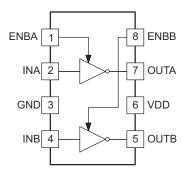


Figure 5-1. UCC27423-Q1: D or DGN Package 8-Pin SOIC or MSOP With PowerPAD Dual Inverting, Top View

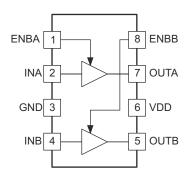


Figure 5-2. UCC27424-Q1: D or DGN Package 8-Pin SOIC or MSOP With PowerPAD Dual Noninverting, Top View

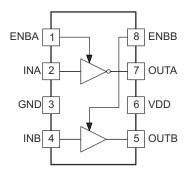


Figure 5-3. UCC27425-Q1: D Package 8-Pin SOIC One Inverting, One Noninverting, Top View

Table 5-1. Pin Functions

	PIN DESCRIPTION		DESCRIPTION
NO.	NAME	1/0	DESCRIPTION
1	ENBA	ı	Enable input for the driver A with logic-compatible threshold and hysteresis. The driver output can be enabled and disabled with this pin. It is internally pulled up to $V_{DD}$ with 100-k $\Omega$ resistor for active high operation. The output state when the device is disabled is low, regardless of the input state.
2	INA	INA I Input A. Input signal of the A driver which has logic-compatible threshold and hysteresis. If not used, this input must be tied to either V <sub>DD</sub> or GND. It must not be left floating.	
3	GND	_	Common ground. This ground must be connected very closely to the source of the power MOSFET which the driver is driving.
4	INB	I	Input B. Input signal of the B driver which has logic-compatible threshold and hysteresis. If not used, this input must be tied to either V <sub>DD</sub> or GND. It must not be left floating.
5	OUTB	0	Driver output B. The output stage is capable of providing 4-A drive current to the gate of a power MOSFET.
6	VDD	_	Supply voltage and the power input connection for this device.



# **Table 5-1. Pin Functions (continued)**

	PIN		PIN		DESCRIPTION
NO. NAME I/O DESCRIPTION		DESCRIPTION			
7	OUTA	0	Driver output A. The output stage is capable of providing 4-A drive current to the gate of a power MOSFET.		
8	ENBB	I	Enable input for the driver B with logic-compatible threshold and hysteresis. The driver output can be enabled and disabled with this pin. It is internally pulled up to $V_{DD}$ with 100-k $\Omega$ resistor for active-high operation. The output state when the device is disabled is low, regardless of the input state.		



# **6 Specifications**

# **6.1 Absolute Maximum Ratings**

over operating free-air temperature range (unless otherwise noted)(1) (2)

			MIN	MAX	UNIT
$V_{DD}$	Supply voltage		-0.3	16	V
	Output current	DC		0.3	Α
I <sub>OUT</sub>	Output current  Input voltage  Enable voltage	Pulsed, 0.5 μs		4.5	A
V <sub>IN</sub>	Input voltage	INA, INB	-5	$6^{(3)}$ or $(V_{DD} + 0.3)^{(3)}$	V
V <sub>EN</sub>	Enable voltage	ENBA, ENBB	-0.3	$6^{(3)}$ or $(V_{DD} + 0.3)^{(3)}$	V
D	Dower dissination	T <sub>A</sub> = 25°C (D package)		650	mW
P <sub>D</sub>	Power dissipation	T <sub>A</sub> = 25°C (DGN package)		3	W
TJ	Junction operating tempera	ature	-55	150	°C
T <sub>stg</sub>	Storage temperature		-65	150	°C

<sup>(1)</sup> Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

# 6.2 ESD Ratings

			VALUE	UNIT
V	Electrostatic discharge	Human-body model (HBM), per AEC Q100-002 <sup>(1)</sup>	±2000	V
V <sub>(ESD)</sub> Electrostatic dis	Electrostatic discharge	Charged-device model (CDM), per AEC Q100-011	±1000	<b>v</b>

<sup>(1)</sup> AEC Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specification.

# 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	MAX	UNIT
$V_{DD}$	Supply voltage	4	15	V
INA	lanut valtaga	-2	15	V
INB	Input voltage	-2	15	V
ENA	Fnahla valtaga	0	15	V
ENB	Enable voltage	U	15	V
T <sub>J</sub>	Operating junction temperature	-40	125	°C

### **6.4 Thermal Information**

			UCC2742x-Q1	
	THERMAL METRIC <sup>(1)</sup>	D (SOIC)	DGN (MSOP With PowerPAD)	UNIT
		8 PINS	8 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	112.6	63	°C/W
R <sub>0</sub> JC(top)	Junction-to-case (top) thermal resistance	61.5	53.8	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	52.8	35.6	°C/W
ΨЈТ	Junction-to-top characterization parameter	15.8	1.9	°C/W
ΨЈВ	Junction-to-board characterization parameter	52.3	35.3	°C/W

<sup>(2)</sup> All voltages are with respect to GND. Currents are positive into, negative out of, the specified terminal.

<sup>(3)</sup> Whichever is larger.



# 6.4 Thermal Information (continued)

		l	JCC2742x-Q1	
	THERMAL METRIC <sup>(1)</sup>		DGN (MSOP With PowerPAD)	UNIT
		8 PINS	8 PINS	
$R_{\theta JC(bot)}$	Junction-to-case (bottom) thermal resistance	_	11.9	°C/W

<sup>(1)</sup> For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.



### 6.5 Electrical Characteristics

 $V_{DD}$  = 4.5 V to 15 V,  $T_A$  = -40°C to 125°C,  $T_A$  =  $T_J$  (unless otherwise noted)

- 00	PARA	METER	1 1	TEST CONDITION	ONS	MIN	TYP	MAX	UNIT							
INPUT	(INA, INB)		•													
V <sub>IH</sub>	Logic 1 input thr	eshold				1.6	2.2	2.5	V							
V <sub>IL</sub>	Logic 0 input thr	eshold				0.8	1.2	1.5	V							
I <sub>IN</sub>	Input current		V <sub>IN</sub> = 0 V to V <sub>DD</sub>	)		-10	0	10	μΑ							
OUTPU	JT (OUTA, OUTB)	)														
I <sub>OUT</sub>	Output current		V <sub>DD</sub> = 14 V <sup>(1)</sup>				4		Α							
R <sub>OH</sub>	Output resistance	e high	I <sub>OUT</sub> = -10 mA,	(2)			1.2	2.5	Ω							
R <sub>OL</sub>	Output resistance	ce low	I <sub>OUT</sub> = 10 mA, <sup>(2</sup>	)			0.7	1.2	Ω							
ENABI	LE (ENBA, ENBB	)														
V <sub>IN_H</sub>	High-level input	voltage	Low-to-high tran	sition		1.7	2.4	2.9	V							
$V_{IN\_L}$	Low-level input v	voltage	High-to-low tran	sition		1.1	1.8	2.2	V							
	Hysteresis					0.15	0.55	0.9	V							
R <sub>ENBL</sub>	Enable impedan	ce	V <sub>DD</sub> = 14 V, ENE	BL = GND		75	100	145	kΩ							
OVERA	ALL															
				INA = 0 V	INB = 0 V		900	1350								
			UCC27423-Q1	IIVA – 0 V	INB = High		750	1100								
			UCC21423-Q1	00027425-Q1	00027425-Q1	00027425-Q1	00027425-Q1	00027425-Q1	00021420-Q1	00021425-Q1	INA = High	INB = 0 V		750	1.5	
				IIVA – Fligh	INB = High		600	2.2 2.5   1.2 1.5   0 10   4   1.2 2.5   0.7 1.2   2.4 2.9   1.8 2.2   .55 0.9   100 145   200 1350   750 1100    750 1100    750 1100    750 1100    750 1100    750 1100    750 1100    750 1100    750 1100    750 1100    750 1100    750 1100    750 1100    750 1100    750 1100    750 1100    750 1100    750 1100    750 1100    750 1100     750 1100     750 1100     750 1100     750 1100     750 1100								
				INA = 0 V	INB = 0 V		300	450								
		Static, V <sub>DD</sub> = 15 V,	UCC27424-Q1	IIVA – U V	INB = High		750	1100								
		ENBA = ENBB = 15 V	00027424-Q1	INA = High	INB = 0 V		750	10 2.5 1.2 2.9 2.2 0.9 145 1350 1100 1100 900 450 1100 1800 900 1600 700 1350 450 700 700								
	Operating			IINA – HIGH	INB = High		1200	1800								
I <sub>DD</sub>	current			INA = 0 V	INB = 0 V		600	900	μA							
			UCC27425-Q1	IIVA – U V	INB = High		1050	1600								
			0CC27425-Q1	INA = High	INB = 0 V		450	700								
				IINA – HIGH	INB = High		900	2.5 1.2 2.9 2.2 0.9 145 1350 1100 900 450 1100 1800 900 1600 700 1350 450 700 700								
				INA = 0 V	INB = 0 V		300	450								
		Disabled, V <sub>DD</sub> = 15 V,	All	11NA - U V	INB = High		450	700								
		ENBA = ENBB = 0 V		INA = High	INB = 0 V	1.2 2.5 0.7 1.2  1.7 2.4 2.9 1.1 1.8 2.2 0.15 0.55 0.9 75 100 145  900 1350 750 1100	700									
				IIVA - FIIGH	INB = High		600	900								

<sup>(1)</sup> Parameter not tested in production

<sup>(2)</sup> Output pullup resistance in this table is a DC measurement that measures resistance of PMOS structure only (not N-channel structure).

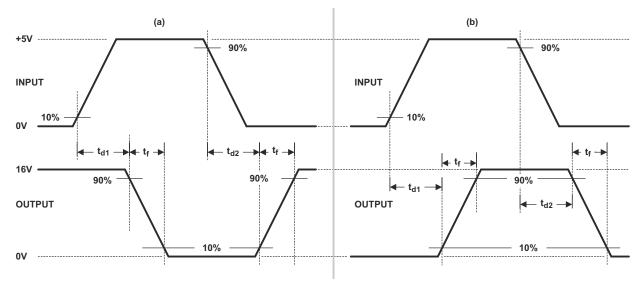


# 6.6 Switching Characteristics

over operating free-air temperature range (unless otherwise noted)

	PARAMETER	TEST C	ONDITIONS	MIN	TYP	MAX	UNIT
SWITC	CHING TIME						
t <sub>r</sub>	Rise time (OUTA, OUTB)	$C_{LOAD} = 1.8 \text{ nF}^{(1)}$			20	40	ns
t <sub>f</sub>	Fall time (OUTA, OUTB)	$C_{LOAD} = 1.8 \text{ nF}^{(1)}$			15	40	ns
t <sub>D1</sub>	Delay time, IN rising (IN to OUT)	$C_{LOAD} = 1.8 \text{ nF}^{(1)}$			25	50	ns
t <sub>D2</sub>	Delay time, IN falling (IN to	$C_{LOAD} = 1.8 \text{ nF}^{(1)}$	UCC27423-Q1, UCC27424-Q1		35	60	ns
	OUT)		UCC27425-Q1		35	70	
ENAB	LE (ENBA, ENBB)						
t <sub>D3</sub>	Propagation delay time <sup>(3)</sup>	$C_{LOAD} = 1.8 \text{ nF}^{(1)} (2)$			30	60	ns
t <sub>D4</sub>	Propagation delay time <sup>(3)</sup>	$C_{LOAD} = 1.8 \text{ nF}^{(1)} (2)$			100	150	ns

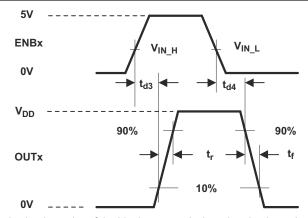
- (1) Specified by design
- (2) Not production tested
- (3) See Figure 6-2



The 10% and 90% thresholds depict the dynamics of the bipolar output devices that dominate the power MOSFET transition through the Miller regions of operation.

Figure 6-1. Switching Waveforms for (a) Inverting Driver and (b) Noninverting Driver





The 10% and 90% thresholds depict the dynamics of the bipolar output devices that dominate the power MOSFET transition through the Miller regions of operation.

Figure 6-2. Switching Waveform for Enable to Output

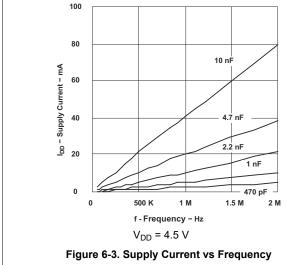
### 6.7 Dissipation Ratings

PACKAGE	θ <sub>JC</sub> (°C/W)	θ <sub>JA</sub> (°C/W)	POWER RATING T <sub>A</sub> = 70°C (mW) <sup>(1)</sup>			
D (SOIC-8)	42	84 to 160 <sup>(2)</sup>	344 to 655 <sup>(2)</sup>			
DGN (MSOP PowerPAD)(3)	11.9	63	873			

- (1) 125°C operating junction temperature is used for power rating calculations.
- (2) The range of values indicates the effect of the PCB. These values are intended to give the system designer an indication of the best-and worst-case conditions. In general, the system designer should attempt to use larger traces on the PCB, where possible, to spread the heat away form the device more effectively.
- (3) The PowerPAD is not directly connected to any leads of the package. However, it is electronically and thermally connected to the substrate which is the ground of the device.



# **6.8 Typical Characteristics**



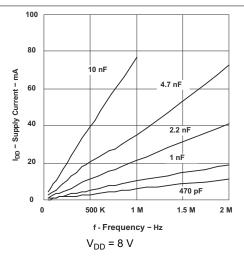


Figure 6-4. Supply Current vs Frequency

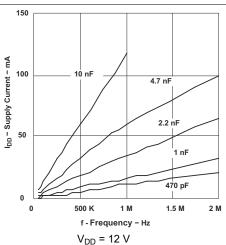


Figure 6-5. Supply Current vs Frequency

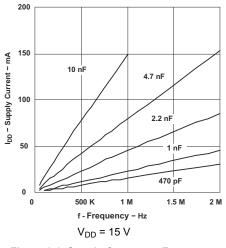


Figure 6-6. Supply Current vs Frequency

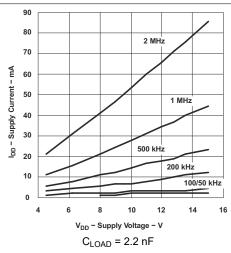


Figure 6-7. Supply Current vs Supply Voltage

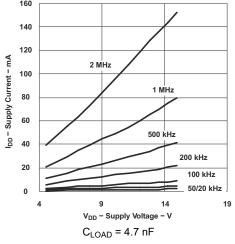
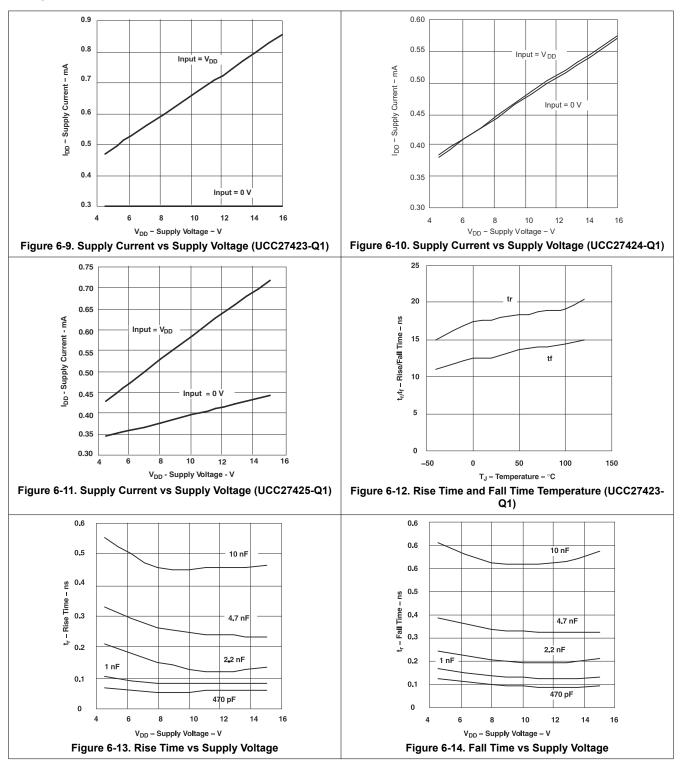


Figure 6-8. Supply Current vs Supply Voltage







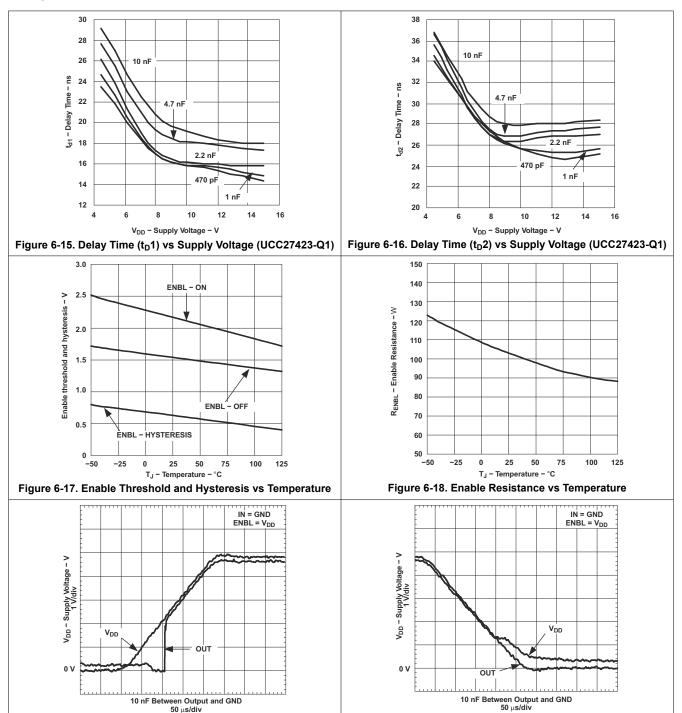
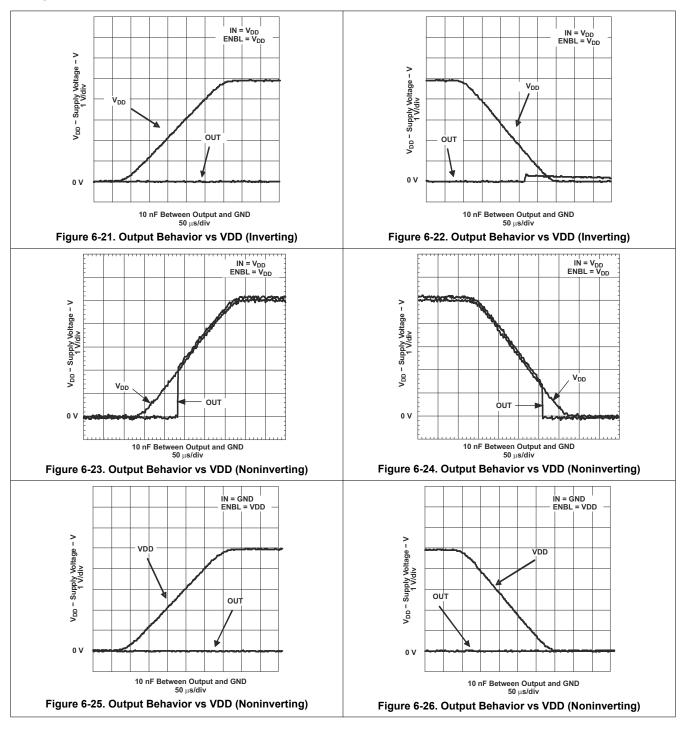


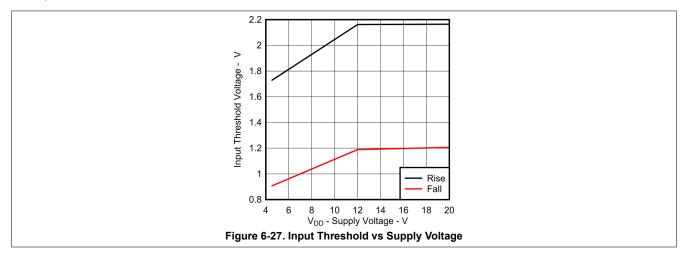
Figure 6-19. Output Behavior vs Supply Voltage (Inverting)

Figure 6-20. Output Behavior vs Supply Voltage (Inverting)









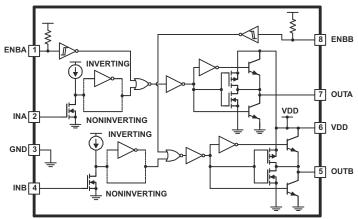


# 7 Detailed Description

### 7.1 Overview

The UCC2742x-Q1 family of high-speed dual MOSFET drivers can deliver large peak currents into capacitive loads. The UCC27423-Q1 offers these standard logic options: dual-inverting drivers, dual noninverting drivers, and one inverting, one noninverting driver. The thermally enhanced 8-pin PowerPAD MSOP package (DGN) drastically lowers the thermal resistance to improve long-term reliability. It is also offered in the standard 8-pin SOIC (D) package. Using a design that inherently minimizes shoot-through current, these drivers deliver 4 A of current where it is needed most at the Miller plateau region during the MOSFET switching transition. A unique Bipolar and MOSFET hybrid output stage in parallel also allows efficient current sourcing and sinking at low supply voltages.

### 7.2 Functional Block Diagram



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### 7.3 Feature Description

### 7.3.1 Input Stage

The input thresholds have a 3.3-V logic sensitivity over the full range of  $V_{DD}$  voltages; yet it is equally compatible with 0 to  $V_{DD}$  signals. The inputs of UCC2742x-Q1 drivers are designed to withstand 500-mA reverse current without either damage to the IC for logic upset. The input stage of each driver must be driven by a signal with a short rise or fall time. This condition is satisfied in typical power supply applications, where the input signals are provided by a PWM controller or logic gates with fast transition times (< 200 ns). The input stages to the drivers function as a digital gate, and they are not intended for applications where a slow changing input voltage is used to generate a switching output when the logic threshold of the input section is reached. While this may not be harmful to the driver, the output of the driver may switch repeatedly at a high frequency.

Users should not attempt to shape the input signals to the driver in an attempt to slow down (or delay) the signal at the output. If limiting the rise or fall times to the power device is desired, limit the rise or fall times to the power device, then an external resistance can be added between the output of the driver and the load device, which is generally a power MOSFET gate. The external resistor may also help remove power dissipation from the device package, as discussed in the Section 10.3.

### 7.3.2 Output Stage

Inverting outputs of the UCC2742x-Q1 are intended to drive external P-channel MOSFETs. Noninverting outputs of the UCC2742x-Q1 are intended to drive external N-channel MOSFETs.

Each output stage is capable of supplying  $\pm 4$ -A peak current pulses and swings to both  $V_{DD}$  and GND. The pullup and pulldown circuits of the driver are constructed of bipolar and MOSFET transistors in parallel. The peak output current rating is the combined current from the bipolar and MOSFET transistors. The output resistance is the  $R_{DS(on)}$  of the MOSFET transistor when the voltage on the driver output is less than the saturation voltage of the bipolar transistor. Each output stage also provides a very low impedance to overshoot



and undershoot due to the body diode of the external MOSFET. This means that in many cases, external Schottky-clamp diodes are not required.

The UCC2742x-Q1 family delivers the 4-A gate drive where it is most needed during the MOSFET switching transition—at the Miller plateau region—providing improved efficiency gains. A unique bipolar and MOSFET hybrid output stage in parallel also allows efficient current sourcing at low supply voltages.

### 7.3.3 Enable

The UCC2742x-Q1 devices provide dual enable inputs for improved control of each driver channel operation. The inputs incorporate logic-compatible thresholds with hysteresis. They are internally pulled up to  $V_{DD}$  with 100-k $\Omega$  resistor for active-high operation. When ENBA and ENBB are driven high, the drivers are enabled; when ENBA and ENBB are low, the drivers are disabled. The default state of the enable pin is to enable the driver and, therefore, can be left open for standard operation. The output states when the drivers are disabled is low, regardless of the input state. See Table 7-1 for operation using enable logic.

Enable inputs are compatible with both logic signals and slowly-changing analog signals. They can be directly driven, or a power-up delay can be programmed with a capacitor between ENBA/ENBB and GND. ENBA and ENBB control input A and input B, respectively.

### 7.3.4 Parallel Outputs

The A and B drivers may be combined into a single driver by connecting the INA/INB inputs together and the OUTA/OUTB outputs together. Then, a single signal can control the paralleled combination as shown in Figure 7-1.

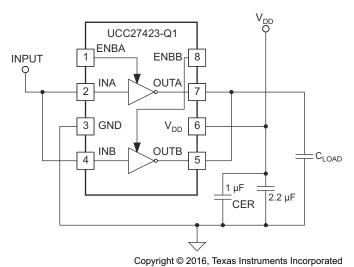


Figure 7-1. Parallel Outputs

### 7.3.5 Operational Waveforms and Circuit Layout

Figure 7-2 shows the circuit performance achievable with a single driver (half of the 8-pin IC) driving a 10-nF load. The input pulse width (not shown) is set to 300 ns to show both transitions in the output waveform. Note the linear rise and fall edges of the switching waveforms. This is due to the constant output current characteristic of the driver as opposed to the resistive output impedance of traditional MOSFET-based gate drivers.



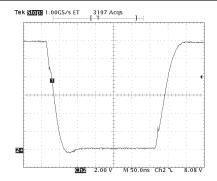


Figure 7-2. Pulse Response

In a power driver operating at high frequency, it is a significant challenge to get clean waveforms without much overshoot or undershoot and ringing. The low output impedance of these drivers produces waveforms with high di/dt. This tends to induce ringing in the parasitic inductances. Use the upmost care in the circuit layout. It is advantageous to connect the driver IC as close as possible to the leads. The driver IC layout has ground on the opposite side of the output, so the ground must be connected to the bypass capacitors and the load with copper trace as wide as possible. These connections must also be made with a small enclosed loop area to minimize the inductance.

### 7.3.6 V<sub>DD</sub>

Although quiescent  $V_{DD}$  current is very low, total supply current is higher, depending on OUTA and OUTB current and the programmed oscillator frequency. Total  $V_{DD}$  current is the sum of quiescent  $V_{DD}$  current and the average OUT current. Knowing the operating frequency and the MOSFET gate charge ( $Q_g$ ), average OUT current can be calculated from Equation 1.

$$I_{OUT} = Q_g \times f \tag{1}$$

where

### · f is frequency

For the best high-speed circuit performance, TI recommends two  $V_{DD}$  bypass capacitors to prevent noise problems. TI highly recommends using surface-mount components. A 0.1- $\mu$ F ceramic capacitor must be located closest to the  $V_{DD}$  to ground connection. In addition, a larger capacitor (such as 1  $\mu$ F) with relatively low ESR must be connected in parallel, to help deliver the high current peaks to the load. The parallel combination of capacitors must present a low impedance characteristic for the expected current levels in the driver application.

# 7.4 Device Functional Modes

With  $V_{DD}$  power supply in the range of 4 V to 16 V, the output stage is dependent on the states of the HI and LI pins. Table 7-1 shows the UCC2742x-Q1 truth table.

INPUTS (VIN\_L, VIN\_H) UCC27423-Q1 UCC27424-Q1 UCC27425-Q1 **ENBA ENBB** INA INB **OUTA OUTB OUTA OUTB OUTA OUTB** Н Н L L Н Н L L Н L Н Н L Н Н L L Н Н Н Н Н Н L L Н Н L L L Н Н Н Н L L Н Н L Н Х Χ L

Table 7-1. Input and Output Logic Table

Importantly, if INA and INB are not used, they must be tied to either VDD or GND; they must not be left floating.



# 8 Application and Implementation

### Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

### 8.1 Application Information

High-frequency power supplies often require high-speed, high-current drivers such as the UCC2742x-Q1 family. A leading application is the need to provide a high-power buffer stage between the PWM output of the control IC and the gates of the primary power MOSFET or IGBT switching devices. In other cases, the driver IC is used to drive the power device gates through a drive transformer. Synchronous rectification supplies also have the need to simultaneously drive multiple devices which can present an extremely large load to the control circuitry.

Driver ICs are used when it is not feasible to have the primary PWM regulator IC directly drive the switching devices for one or more reasons. The PWM IC may not have the brute drive capability required for the intended switching MOSFET, limiting the switching performance in the application. In other cases, there may be a desire to minimize the effect of high-frequency switching noise by placing the high current driver physically close to the load. Also, newer ICs that target the highest operating frequencies may not incorporate onboard gate drivers at all. Their PWM outputs are only intended to drive the high impedance input to a driver such as the UCC2742x-Q1. Finally, the control IC may be under thermal stress due to power dissipation, and an external driver can help by moving the heat from the controller to an external package.

### 8.2 Typical Application

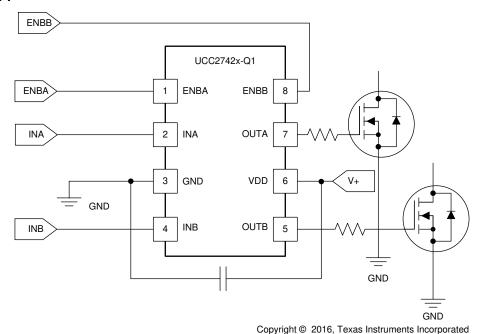


Figure 8-1. UCC2742x-Q1 Driving Two Independent MOSFETs

### 8.2.1 Design Requirements

To select proper device from UCC2742x-Q1 family, TI recommends first checking the appropriate logic for the outputs. The UCC27423-Q1 has dual inverting outputs, the UCC27424-Q1 has dual noninverting outputs, and the UCC27425-Q1 has an inverting channel A and noninverting channel B. Moreover, evaluate some



considerations to make the most appropriate selection. Among these considerations are  $V_{DD}$ , drive current, and power dissipation.

### 8.2.2 Detailed Design Procedure

### 8.2.2.1 Source and Sink Capabilities During Miller Plateau

Large power MOSFETs present a large load to the control circuitry. Proper drive is required for efficient, reliable operation. The UCC2742x-Q1 drivers have been optimized to provide maximum drive to a power MOSFET during the Miller plateau region of the switching transition. This interval occurs while the drain voltage is swinging between the voltage levels dictated by the power topology, requiring the charging and discharging of the drain-gate capacitance with current supplied or removed by the driver device.

Two circuits are used to test the current capabilities of the UCC2742x-Q1 driver. In each case, external circuitry is added to clamp the output near 5 V while the IC is sinking or sourcing current. An input pulse of 250 ns is applied at a frequency of 1 kHz in the proper polarity for the respective test. In each test, there is a transient period where the current peaked up and then settled down to a steady-state value. The noted current measurements are made at a time of 200 ns after the input pulse is applied, after the initial transient.

The circuit in Figure 8-2 is used to verify the current sink capability when the output of the driver is clamped around 5 V, a typical value of gate-source voltage during the Miller plateau region. The UCC2742x-Q1 is found to sink 4.5 A at  $V_{DD}$  = 15 V and 4.28 A at  $V_{DD}$  = 12 V.

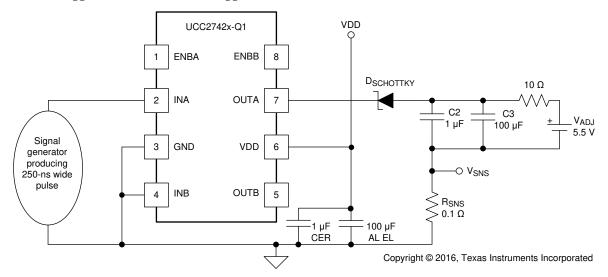


Figure 8-2. Current Sink Capability Test

The circuit show in Figure 8-3 is used to test the current source capability with the output clamped around 5 V with a string of Zener diodes. The UCC2742x-Q1 is found to source 4.8 A at  $V_{DD}$  = 15 V and 3.7 A at  $V_{DD}$  = 12 V.



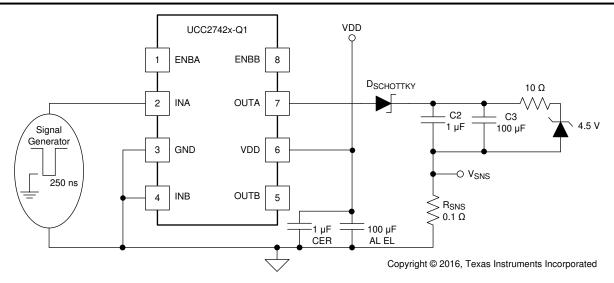


Figure 8-3. Current Source Capability Test

### 8.2.2.2 Drive Current and Power Requirements

The UCC2742x-Q1 family of drivers are capable of delivering 4 A of current to a MOSFET gate for a period of several hundred nanoseconds. High-peak current is required to turn the device ON quickly. Then, to turn the device OFF, the driver is required to sink a similar amount of current to ground. This repeats at the operating frequency of the power device. A MOSFET is used in this discussion because it is the most common type of switching device used in high frequency power conversion equipment.

Reference 1 in the Section 11.2.1 section discuss the current required to drive a power MOSFET and other capacitive-input switching devices. Reference 1 in includes information on the previous generation of bipolar IC gate drivers.

When a driver IC is tested with a discrete, capacitive load, it is a fairly simple matter to calculate the power that is required from the bias supply. The energy that must be transferred from the bias supply to charge the capacitor is given by Equation 2.

$$E = \frac{1}{2}CV^2 \tag{2}$$

where

- C = load capacitor
- V = bias voltage (feeding the driver)

There is an equal amount of energy transferred to ground when the capacitor is discharged. This leads to a power loss given by Equation 3.

$$P = CV^2 \times f \tag{3}$$

where

f = switching frequency

This power is dissipated in the resistive elements of the circuit. Thus, with no external resistor between the driver and gate, this power is dissipated inside the driver. Half of the total power is dissipated when the capacitor is charged, and the other half is dissipated when the capacitor is discharged. An actual example using the conditions of the previous gate drive waveform should help clarify this.

With V<sub>DD</sub> = 12 V, C<sub>I OAD</sub> = 10 nF, and f = 300 kHz, the power loss can be calculated as Equation 4.



$$P = 10 \text{ nF} \times (12 \text{ V})^2 \times (300 \text{ kHz}) = 0.432 \text{ W}$$
 (4)

With a 12-V supply, this would equate to a current of Equation 5.

$$I = \frac{P}{V} = \frac{0.432 \text{ W}}{12 \text{ V}} = 36 \text{ mA}$$
 (5)

The actual current measured from the supply was 0.037 A, and is very close to the predicted value. But, consider the  $I_{DD}$  current that is due to the IC internal consumption. With no load, the IC current draw is 0.0027 A. Under this condition, the output rise and fall times are faster than with a load. This could lead to an almost insignificant, yet measurable current due to cross-conduction in the output stages of the driver. However, these small current differences are buried in the high-frequency switching spikes, and are beyond the measurement capabilities of a basic lab setup. The measured current with 10-nF load is reasonably close to that expected.

The switching load presented by a power MOSFET can be converted to an equivalent capacitance by examining the gate charge required to switch the device. This gate charge includes the effects of the input capacitance plus the added charge needed to swing the drain of the device between the ON and OFF states. Most manufacturers provide specifications that provide the typical and maximum gate charge, in nC, to switch the device under specified conditions. Using the gate charge  $Q_g$ , one can determine the power that must be dissipated when charging a capacitor. This is done by using the equivalence  $Q_g = C_{eff}V$  to provide the power loss in Equation 6.

$$P = C \times V^2 \times f = V \times Q_{\alpha} \times f \tag{6}$$

Equation 6 allows a power designer to calculate the bias power required to drive a specific MOSFET gate at a specific bias voltage.

### 8.2.3 Application Curves

Figure 8-4 and Figure 8-5 show rising and falling time and turnon and turnoff propagation delay testing waveform in room temperature for UCC27424-Q1, and waveform measurement data (see the bottom part of the waveform). Each channel, INA/INB/OUTA/OUTB, is labeled and displayed on the left hand of the waveforms.

The load capacitance testing condition is 1.8 nF,  $V_{DD}$  = 12 V, and f = 300 kHz.

HI and LI share one same input from function generator; therefore, besides the propagation delay and rising or falling time, the difference of the propagation delay between HO and LO gives the propagation delay matching data

Note the linear rise and fall edges of the switching waveforms. This is due to the constant output current characteristic of the driver as opposed to the resistive output impedance of traditional MOSFET-based gate drivers.



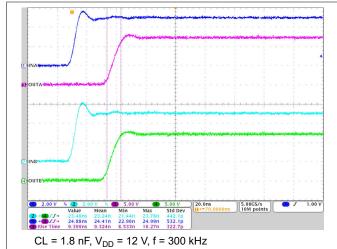


Figure 8-4. Rising Time and Turnon Propagation Delay

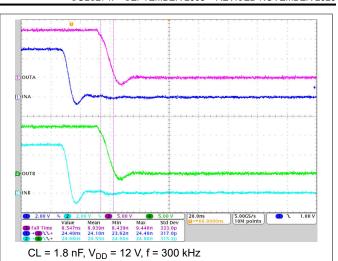


Figure 8-5. Falling Time and Turnoff Propagation Delay



# 9 Power Supply Recommendations

The recommended bias supply voltage range for UCC2742x-Q1 is from 4 V to 15 V. The upper end of this range is driven by the absolute maximum voltage rating of the  $V_{DD}$  (16 V). TI recommends keeping proper margin to allow for transient voltage spikes. A local bypass capacitor must be placed between the VDD and GND pins. And this capacitor must be placed as close to the device as possible. A low ESR, ceramic surface-mount capacitor is recommended. TI recommends using 2 capacitors across VDD and GND: a 100-nF ceramic surface-mount capacitor for high-frequency filtering placed very close to VDD and GND pin, and another surface-mount capacitor (220 nF to 10  $\mu$ F) for IC bias requirements.

### 10 Layout

# 10.1 Layout Guidelines

Optimum performance of gate drivers cannot be achieved without taking due considerations during circuit board layout. The following points are emphasized:

- 1. Low ESR or ESL capacitors must be connected close to the IC between VDD and GND pins to support high peak currents drawn from VDD during the turnon of the external MOSFETs.
- 2. Grounding considerations:
  - The first priority in designing grounding connections is to confine the high peak currents that charge
    and discharge the MOSFET gates to a minimal physical area. This decreases the loop inductance and
    minimizes noise issues on the gate terminals of the MOSFETs. The gate driver must be placed as close
    as possible to the MOSFETs.
  - Star-point grounding is a good way to minimize noise coupling from one current loop to another. The
    GND of the driver is connected to the other circuit nodes such as source of power MOSFET and ground
    of PWM controller at one, single point. The connected paths must be as short as possible to reduce
    inductance.
  - Use a ground plane to provide noise shielding. Fast rise and fall times at OUT may corrupt the input signals during transition. The ground plane must not be a conduction path for any current loop. Instead the ground plane must be connected to the star-point with one single trace to establish the ground potential. In addition to noise shielding, the ground plane can help in power dissipation as well.
- 3. In noisy environments, tying inputs of an unused channel of the UCC2742x-Q1 device to VDD or GND using short traces in order to ensure that the output is enabled and to prevent noise from causing malfunction in the output may be necessary.
- 4. Separate power traces and signal traces, such as output and input signals.



### 10.2 Layout Example

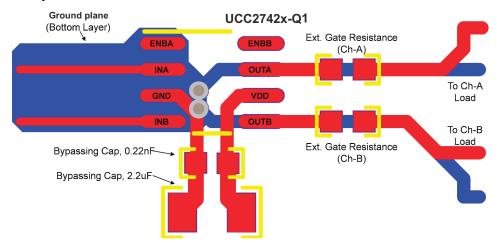


Figure 10-1. Recommended PCB Layout for UCC2742x-Q1

### 10.3 Thermal Considerations

The useful range of a driver is greatly affected by the drive power requirements of the load and the thermal characteristics of the IC package. For a power driver to be useful over a particular temperature range, the package must allow for the efficient removal of the heat produced while keeping the junction temperature within rated limits. The UCC2742x-Q1 family of drivers is available in three different packages to cover a range of application requirements.

As shown in the power dissipation rating table, the 8-pin SOIC (D) package has a power rating of around 0.5 W with  $T_A$  = 70°C. This limit is imposed in conjunction with the power derating factor also given in the Section 6.7 table. Note that the power dissipation in our earlier example is 0.432 W with a 10-nF load, 12  $V_{DD}$ , switched at 300 kHz. Thus, only one load of this size could be driven using the D package, even if the two onboard drivers are paralleled. The difficulties with heat removal limit the drive available in the older packages.

The 8-pin MSOP with PowerPAD (DGN) package significantly relieves this concern by offering an effective means of removing the heat from the semiconductor junction. As described in reference 2 of the Section 11.2.1, the PowerPAD packages offer a leadframe die pad that is exposed at the base of the package. This pad is soldered to the copper on the PCB directly underneath the IC package, reducing the  $R_{\theta\ JC(bot)}$  down to  $5.9^{\circ}C/W$ . Data is presented in reference 2 of Section 11.2.1 to show that the power dissipation can be quadrupled in the PowerPAD configuration when compared to the standard packages. The PCB must be designed with thermal lands and thermal vias to complete the heat removal subsystem. This allows a significant improvement in heat sinking over that available in the D package, and is shown to more than double the power capability of the D package. Note that the PowerPAD is not directly connected to any leads of the package. However, it is electrically and thermally connected to the substrate which is the ground of the device.



# 11 Device and Documentation Support

# 11.1 Device Support

### 11.1.1 Third-Party Products Disclaimer

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### 11.2 Documentation Support

### 11.2.1 Related Documentation

For related documentation see the following:

- Practical Considerations in High Performance MOSFET, IGBT and MCT Gate Drive Circuits
- 2. PowerPad Thermally Enhanced Package
- 3. PowerPAD Made Easy

# 11.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. Click on *Notifications* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 11.4 Support Resources

TI E2E<sup>™</sup> support forums are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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### 11.5 Trademarks

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# 11.6 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

## 11.7 Glossary

TI Glossary

This glossary lists and explains terms, acronyms, and definitions.



## 12 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

C	hanges from Revision H (October 2016) to Revision I (November 2023)	Page
•	Deleted top-side marking and T <sub>A</sub> range from the Device Comparison Table. Refer to the Mechanical, Packaging, and Orderable Information for this information	3
•	Changed ESD CDM rating value from ±1500 V to ±1000 V in ESD Ratings	6
•	Changed input threshold voltage values, deleted $V_{OH}$ output high level and $V_{OL}$ output low level, change output resistance high and output resistance low values and deleted Latch-up protection from Electrical	ed
	Characteristics	8
•	Changed UCC274323 to UCC27423 in Figure 6-9, changed Figure 6-27 and added -Q1 to part numbe several graphs	
C	hanges from Revision G (May 2016) to Revision H (October 2016)	Page
•	Changed the UCC27424-Q1 pinout drawing to show two, noninverting channels	4
•	Changed the units of the capacitors in the <i>Parallel Outputs</i> figure from mF to μF	17
С	hanges from Revision F (September 2012) to Revision G (May 2016)	Page
•	Added ESD Ratings table, Feature Description section, Device Functional Modes, Application and Implementation section, Power Supply Recommendations section, Layout section, Device and	
	Documentation Support section, and Mechanical, Packaging, and Orderable Information section	1
•	Added MSOP package information to Features and Description sections	1
С	hanges from Revision E (July, 2012) to Revision F (September, 2012)	Page
•	Changed the word terminal to pin per new standards	4
•	Removed derating factor column in dissipation ratings table, and changed the $\theta_{JC}$ value from 4.7 to 11. $\theta_{JA}$ value from 50–59 to 63, and the power rating $T_A = 70^{\circ}\text{C}$ (mW) value from 1370 to 873 for the	9, the
	DGN package.	10

# 13 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

www.ti.com 23-May-2025

### PACKAGING INFORMATION

Orderable part number	Status	Material type	Package   Pins	Package qty   Carrier	RoHS	Lead finish/ Ball material	MSL rating/ Peak reflow	Op temp (°C)	Part marking
	(1)	(2)			(3)	(4)	(5)		(6)
UCC27423QDGNRQ1	Active	Production	HVSSOP (DGN)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	EADQ
UCC27423QDGNRQ1.A	Active	Production	HVSSOP (DGN)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	EADQ
UCC27423QDRQ1	Active	Production	SOIC (D)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	27423Q
UCC27423QDRQ1.A	Active	Production	SOIC (D)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	27423Q
UCC27424QDGNRQ1	Active	Production	HVSSOP (DGN)   8	2500   LARGE T&R	Yes	NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	EPJQ
UCC27424QDGNRQ1.A	Active	Production	HVSSOP (DGN)   8	2500   LARGE T&R	Yes	NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	EPJQ
UCC27424QDRQ1	Active	Production	SOIC (D)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	27424Q
UCC27424QDRQ1.A	Active	Production	SOIC (D)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	27424Q
UCC27425QDRQ1	Active	Production	SOIC (D)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	27425Q
UCC27425QDRQ1.A	Active	Production	SOIC (D)   8	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	27425Q

<sup>(1)</sup> Status: For more details on status, see our product life cycle.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

Important Information and Disclaimer: The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative

<sup>(2)</sup> Material type: When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

<sup>(3)</sup> RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

<sup>(4)</sup> Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

<sup>(5)</sup> **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

<sup>(6)</sup> Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

# PACKAGE OPTION ADDENDUM

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and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

### OTHER QUALIFIED VERSIONS OF UCC27423-Q1, UCC27424-Q1, UCC27425-Q1:

● Catalog: UCC27423, UCC27424, UCC27425

● Enhanced Product: UCC27423-EP, UCC27424-EP

NOTE: Qualified Version Definitions:

- Catalog TI's standard catalog product
- Enhanced Product Supports Defense, Aerospace and Medical Applications

# **PACKAGE MATERIALS INFORMATION**

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## TAPE AND REEL INFORMATION



# TAPE DIMENSIONS KO P1 BO W Cavity A0

A0	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



### \*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
UCC27423QDGNRQ1	HVSSOP	DGN	8	2500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
UCC27423QDRQ1	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
UCC27424QDGNRQ1	HVSSOP	DGN	8	2500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
UCC27424QDRQ1	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
UCC27424QDRQ1	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
UCC27425QDRQ1	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1



www.ti.com 18-Jul-2025



## \*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
UCC27423QDGNRQ1	HVSSOP	DGN	8	2500	353.0	353.0	32.0
UCC27423QDRQ1	SOIC	D	8	2500	353.0	353.0	32.0
UCC27424QDGNRQ1	HVSSOP	DGN	8	2500	350.0	350.0	43.0
UCC27424QDRQ1	SOIC	D	8	2500	353.0	353.0	32.0
UCC27424QDRQ1	SOIC	D	8	2500	353.0	353.0	32.0
UCC27425QDRQ1	SOIC	D	8	2500	353.0	353.0	32.0

3 x 3, 0.65 mm pitch

SMALL OUTLINE PACKAGE

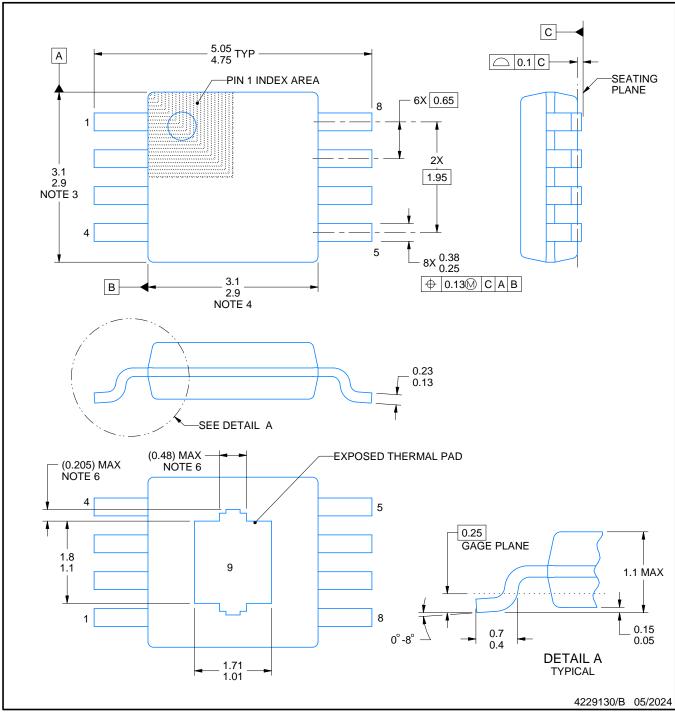
This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.



**INSTRUMENTS** www.ti.com

# PowerPAD<sup>™</sup> VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



### NOTES:

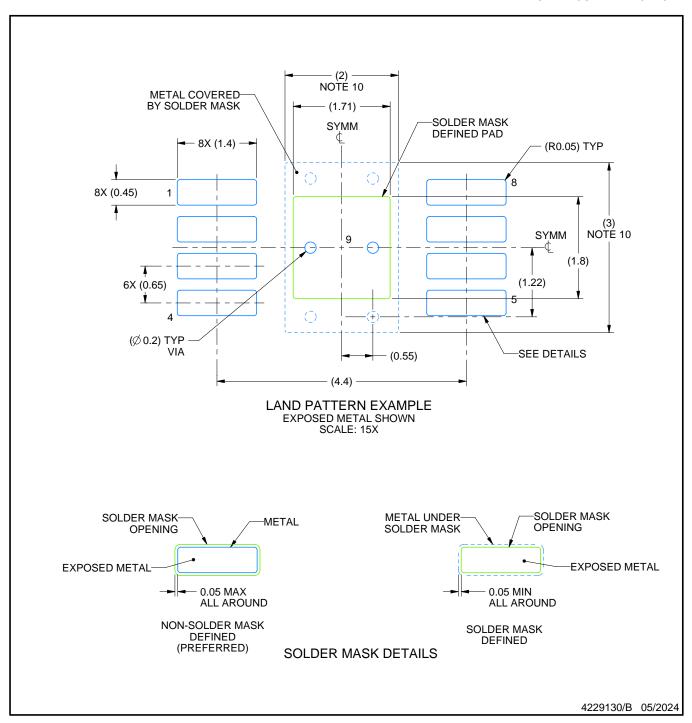
PowerPAD is a trademark of Texas Instruments.

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.

  2. This drawing is subject to change without notice.

  3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not
- exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- 5. Reference JEDEC registration MO-187.
- 6. Features may differ or may not be present.

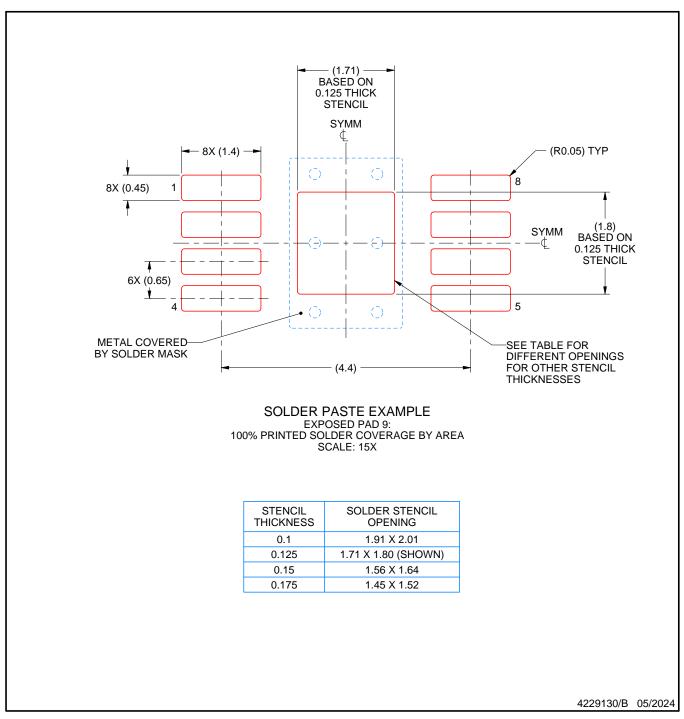




NOTES: (continued)

- 7. Publication IPC-7351 may have alternate designs.
- 8. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 9. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
- 10. Size of metal pad may vary due to creepage requirement.



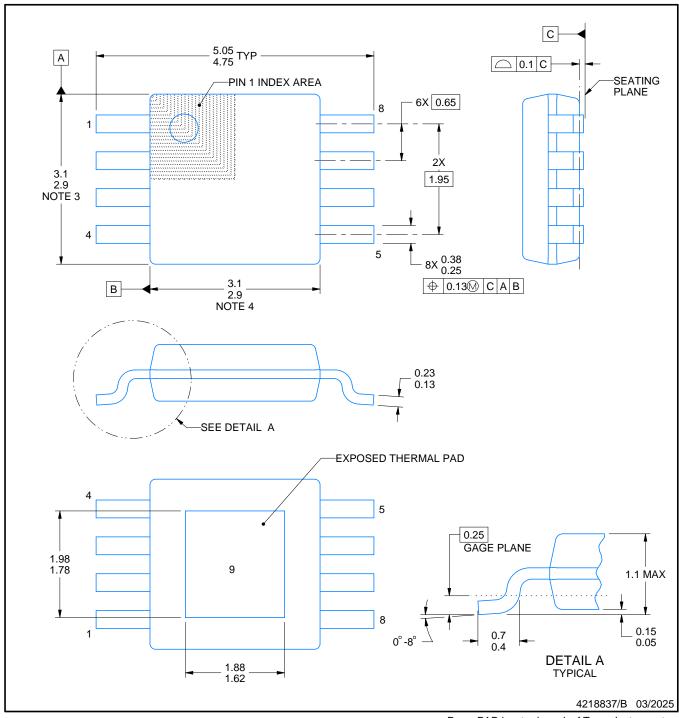


NOTES: (continued)

- 11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 12. Board assembly site may have different recommendations for stencil design.







### NOTES:

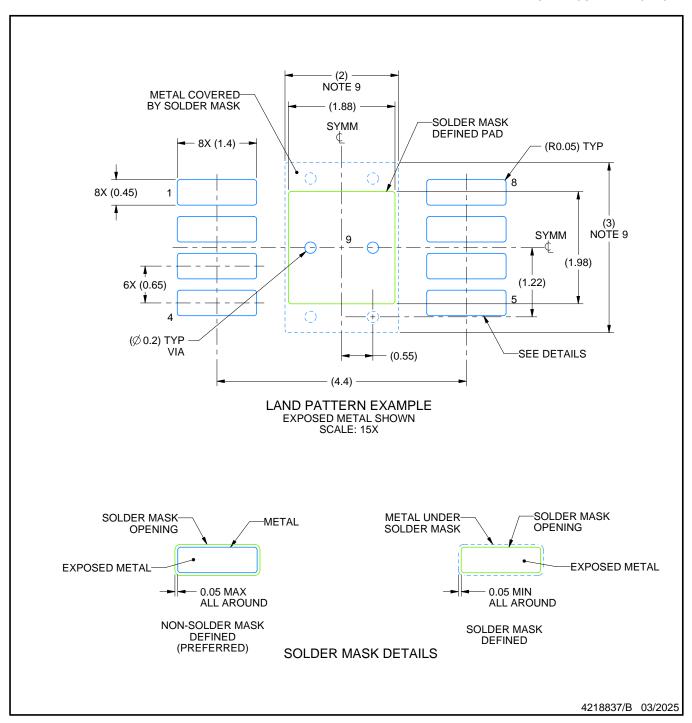
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- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.

  2. This drawing is subject to change without notice.

  3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not
- exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- 5. Reference JEDEC registration MO-187.

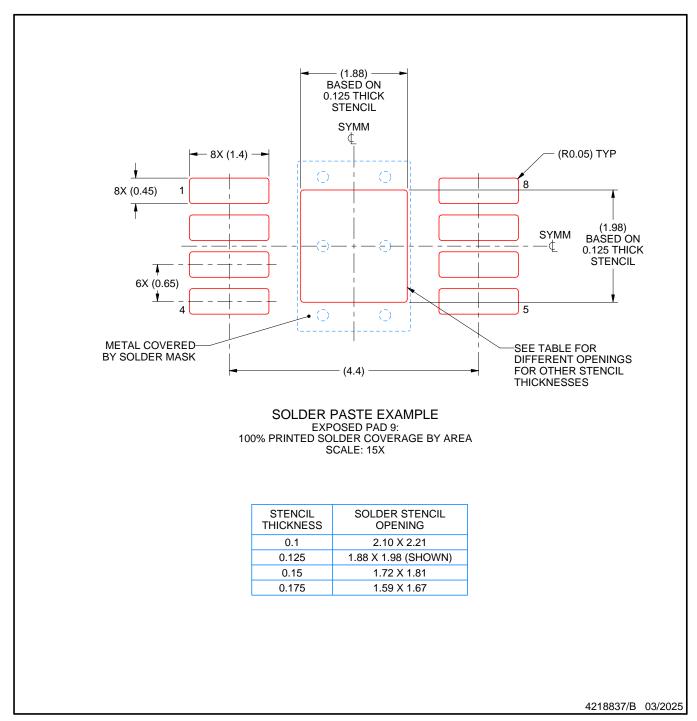




NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
- 9. Size of metal pad may vary due to creepage requirement.





NOTES: (continued)

- 10. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 11. Board assembly site may have different recommendations for stencil design.





SMALL OUTLINE INTEGRATED CIRCUIT



# NOTES:

- 1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.



SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SMALL OUTLINE INTEGRATED CIRCUIT



### NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.



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