

TPS6281xM, Extended Temperature, 2.75-V to 6-V Adjustable-Frequency Step-Down DC/DC Converter

1 Features

- Functional Safety-Capable
 - Documentation available to aid functional safety system design
- Extended junction temperature from -55°C to $+150^{\circ}\text{C}$
- Input voltage range: 2.75 V to 6 V
- Family of 1-A, 2-A, 3-A, and 4-A converters
- Quiescent current: 15 μA typical
- Output voltage from 0.6 V to 5.5 V
- Output voltage accuracy $\pm 1\%$ (FPWM operation)
- Adjustable soft start
- Start-up at -55°C
- Forced PWM or PWM and PFM operation
- Adjustable switching frequency of 1.8 MHz to 4 MHz
- Precise ENABLE input allows
 - User-defined undervoltage lockout
 - Exact sequencing
- 100% duty cycle mode
- Active output discharge
- Spread spectrum clocking - optional
- Power good output with window comparator
- Package with wettable flanks

2 Applications

- Aircraft electrical power
- Defense radio
- Seeker front end
- In-flight entertainment
- Rail transport

3 Description

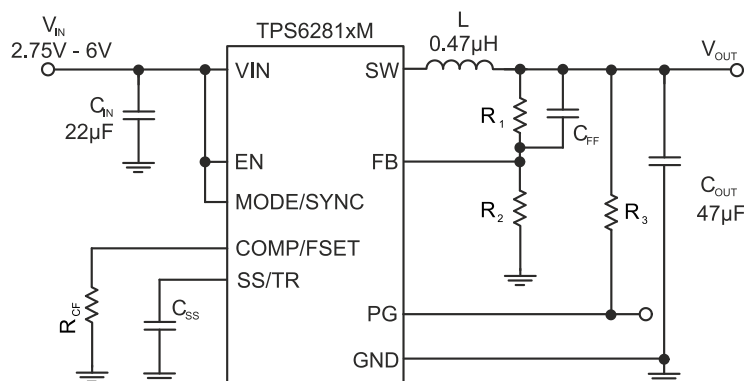
The TPS6281xM is family of pin-to-pin 1-A, 2-A, 3-A, and 4-A synchronous step-down DC/DC converters. All devices offer high efficiency and ease of use. The family of devices is based on a peak current mode control topology. Low-resistive switches allow up to 4-A continuous output current at high ambient temperature. The switching frequency is externally adjustable from 1.8 MHz to 4 MHz and can also be synchronized to an external clock in the same frequency range. The device can automatically enter power save mode (PSM) at light loads to maintain high efficiency across the whole load range. The device provides 1% output voltage accuracy in PWM mode which helps design a power supply with high output voltage accuracy. The SS/TR pin allows the user to set the start-up time or form tracking of the output voltage to an external source, allowing external sequencing of different supply rails and limiting the inrush current during start-up.

The TPS6281xM device is available in a 2-mm \times 3-mm VQFN package with wettable flanks.

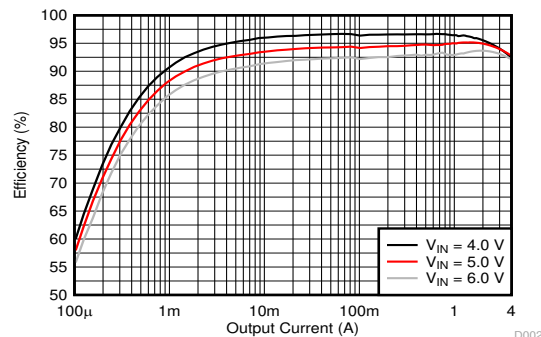
Device Information

PART NUMBER	PACKAGE ⁽¹⁾	BODY SIZE (NOM)
TPS62810M	VQFN	2 mm \times 3 mm
TPS62811M		
TPS62812M		
TPS62813M		

- (1) For all available packages, see the orderable addendum at the end of the data sheet.



Simplified Schematic



Efficiency Versus Output Current;
 $V_{\text{OUT}} = 3.3 \text{ V}$; PWM and PFM; $f_s = 2.25 \text{ MHz}$



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4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

DATE	REVISION	NOTES
March 2021	*	Initial release

5 Device Comparison Table

DEVICE NUMBER	OUTPUT CURRENT	VOUT DISCHARGE	FOLDBACK CURRENT LIMIT	SPREAD SPECTRUM CLOCKING (SSC)	OUTPUT VOLTAGE
TPS62811MWRWYR	1 A	ON	OFF	OFF	adjustable
TPS62812MWRWYR	2 A	ON	OFF	OFF	adjustable
TPS62813MWRWYR	3 A	ON	OFF	OFF	adjustable
TPS62810MWRWYR	4 A	ON	OFF	OFF	adjustable

6 Pin Configuration and Functions

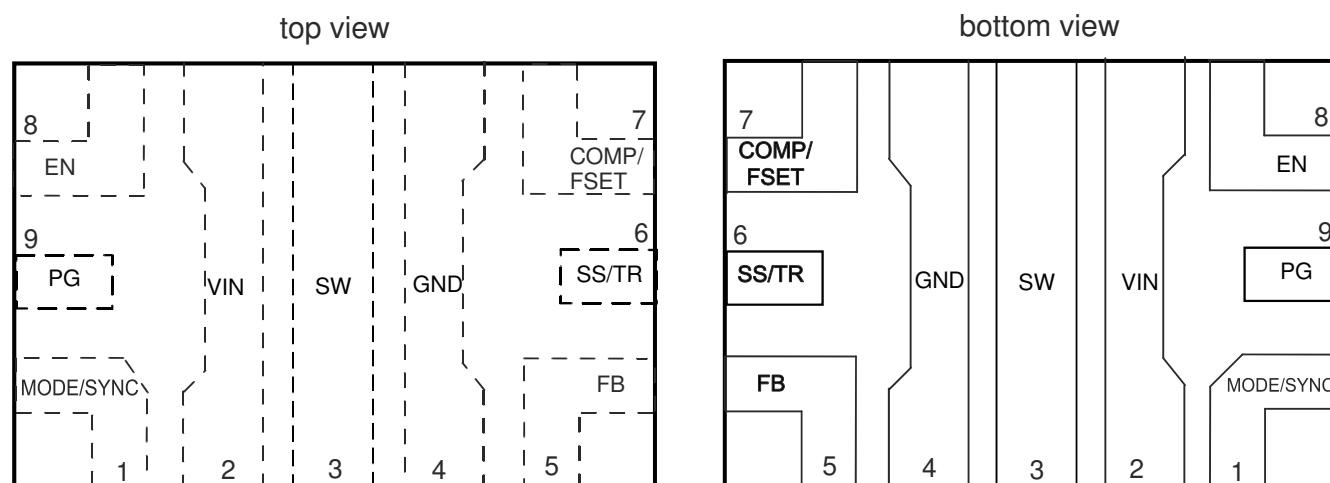


Figure 6-1. 9-Pin (VQFN) RWY Package

Table 6-1. Pin Functions

PIN		I/O	DESCRIPTION
NAME	NO.		
EN	8	I	This is the enable pin of the device. Connect to logic low to disable the device. Pull high to enable the device. Do not leave this pin unconnected.
FB	5	I	Voltage feedback input. Connect the resistive output voltage divider to this pin. For the fixed voltage versions, connect the FB pin directly to the output voltage.
GND	4		Ground pin
MODE/SYNC	1	I	The device runs in PFM/PWM mode when this pin is pulled low. If the pin is pulled high, the device runs in forced PWM mode. Do not leave this pin unconnected. The mode pin can also be used to synchronize the device to an external frequency. See Section 7 for the detailed specification of the digital signal applied to this pin for external synchronization.
COMP/FSET	7	I	Device compensation and frequency set input. A resistor from this pin to GND defines the compensation of the control loop as well as the switching frequency if not externally synchronized. If the pin is tied to GND or VIN, the switching frequency is set to 2.25 MHz. Do not leave this pin unconnected.
PG	9	O	Open-drain power-good output. Low impedance when not "power good", high impedance when "power good". This pin can be left open or be tied to GND when not used.
SS/TR	6	I	Soft Start / Tracking pin. A capacitor connected from this pin to GND defines the rise time for the internal reference voltage. The pin can also be used as an input for tracking and sequencing; see Section 9.4.7 .
SW	3		Switch pin of the converter. This pin is connected to the internal power MOSFETs.
VIN	2		Power supply input. Connect the input capacitor as close as possible between the VIN pin and GND.

7 Specifications

7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)⁽¹⁾

		MIN	MAX	UNIT
Pin voltage range ⁽¹⁾	V _{IN}	−0.3	6.5	V
	SW	−0.3	V _{IN} + 0.3	V
	SW (transient for less than 10 ns) ⁽²⁾	−3	10	V
	FB	−0.3	4	V
	PG, SS/TR, COMP/FSET	−0.3	V _{IN} + 0.3	V
Pin voltage range ⁽¹⁾	EN, MODE/SYNC	−0.3	6.5	V
Storage temperature, T _{stg}		−65	150	°C

(1) Operation outside the *Absolute Maximum Ratings* may cause permanent device damage. *Absolute Maximum Ratings* do not imply functional operation of the device at these or any other conditions beyond those listed under *Recommended Operating Conditions*. If used outside the *Recommended Operating Conditions* but within the *Absolute Maximum Ratings*, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

(2) While switching

7.2 ESD Ratings

			VALUE	UNIT
V _(ESD)	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC ⁽¹⁾	±2000	V
		Charged-device model (CDM), per JEDEC specification JESD22-C101 ⁽²⁾	±750	

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

7.3 Recommended Operating Conditions

		MIN	NOM	MAX	UNIT
V _{IN}	Supply voltage range	2.75		6	V
V _{OUT}	Output voltage range	0.6		5.5	V
L	Effective inductance for a switching frequency of 1.8 MHz to 3.5 MHz	0.32	0.47	0.9	μH
L	Effective inductance for a switching frequency of 3.5 MHz to 4 MHz	0.25	0.33	0.9	μH
C _{OUT}	Effective output capacitance for 1-A and 2-A version ⁽¹⁾	15	22	470	μF
C _{OUT}	Effective output capacitance for 3-A and 4-A version ⁽¹⁾	27	47	470	μF
C _{IN}	Effective input capacitance ⁽¹⁾	5	10		μF
R _{CF}		4.5		100	kΩ
T _J	Operating junction temperature	−55		+150	°C

(1) The values given for the capacitors in the table are effective capacitance, which includes the DC bias effect. Due to the DC bias effect of ceramic capacitors, the effective capacitance is lower than the nominal value when a voltage is applied. Please check the manufacturers DC bias curves for the effective capacitance versus DC voltage applied. Further restrictions may apply. Please see the [feature description for COMP/FSET](#) about the output capacitance versus compensation setting and output voltage.

7.4 Thermal Information

THERMAL METRIC ⁽¹⁾		TPS6281xM	UNIT
		RWY (VQFN)	
		9 PINS	
R _{θJA}	Junction-to-ambient thermal resistance	71.1	°C/W
R _{θJC(top)}	Junction-to-case (top) thermal resistance	37.2	°C/W
R _{θJB}	Junction-to-board thermal resistance	16.4	°C/W
ψ _{JT}	Junction-to-top characterization parameter	0.9	°C/W
ψ _{JB}	Junction-to-board characterization parameter	16.1	°C/W

THERMAL METRIC ⁽¹⁾		TPS6281xM	UNIT
		RWY (VQFN)	
		9 PINS	
R _{θJC(bot)}	Junction-to-case (bottom) thermal resistance	n/a	°C/W

(1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.

7.5 Electrical Characteristics

over operating junction temperature ($T_J = -55^{\circ}\text{C}$ to $+150^{\circ}\text{C}$) and $V_{IN} = 2.75\text{ V}$ to 6 V . Typical values at $V_{IN} = 5\text{ V}$ and $T_J = 25^{\circ}\text{C}$. (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY						
I _Q	Operating quiescent current	EN = high, I _{OUT} = 0 mA, device not switching, T _J = 125°C			21	μA
I _Q	Operating quiescent current	EN = high, I _{OUT} = 0 mA, device not switching		15	30	μA
I _{SD}	Shutdown current	EN = 0 V, at T _J = 125 °C			18	μA
I _{SD}	Shutdown current	EN = 0 V, nominal value at T _J = 25 °C, max value at T _J = 150°C		1.5	26	μA
V _{UVLO}	Undervoltage lockout threshold	Rising input voltage	2.5	2.6	2.75	V
		Falling input voltage	2.25	2.5	2.6	V
T _{SD}	Thermal shutdown temperature	Rising junction temperature		170		°C
	Thermal shutdown hysteresis			15		
CONTROL (EN, SS/TR, PG, MODE)						
V _{IH}	High level input voltage for MODE pin		1.1			V
V _{IL}	Low level input voltage for MODE pin				0.3	V
f _{SYNC}	Frequency range on MODE pin for synchronization	Requires a resistor from COMP/FSET to GND, see the <i>Application and Implementation</i> section	1.8		4	MHz
	Duty cycle of synchronization signal at MODE pin		40%	50%	60%	
	Time to lock to external frequency			50		μs
V _{IH}	Input threshold voltage for EN pin; rising edge		1.06	1.1	1.15	V
V _{IL}	Input threshold voltage for EN pin; falling edge		0.96	1.0	1.05	V
I _{LKG}	Input leakage current for EN, MODE/SYNC	V _{IH} = V _{IN} or V _{IL} = GND			150	nA
	Resistance from COMP/FSET to GND for logic low	Internal frequency setting with f = 2.25 MHz	0		2.5	kΩ
	Voltage on COMP/FSET for logic high	Internal frequency setting with f = 2.25 MHz		V _{IN}		V
V _{TH_PG}	UVP power good threshold voltage; dc level	Rising (%V _{FB})	92%	95%	98%	
	UVP power good threshold voltage; dc level	Falling (%V _{FB})	87%	90%	93%	
	OVP power good threshold; dc level	Rising (%V _{FB})	107%	110%	113%	
	OVP power good threshold; dc level	Falling (%V _{FB})	104%	107%	111%	
	Power good de-glitch time	For a high level to low level transition on power good		40		μs
V _{OL_PG}	Power good output low voltage	I _{PG} = 2 mA		0.07	0.3	V
I _{LKG_PG}	Input leakage current (PG)	V _{PG} = 5 V			100	nA
I _{SS/TR}	SS/TR pin source current		2.1	2.5	2.8	μA
	Tracking gain	V _{FB} /V _{SS/TR}		1		

TPS62810M, TPS62811M, TPS62812M, TPS62813M

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over operating junction temperature ($T_J = -55^{\circ}\text{C}$ to $+150^{\circ}\text{C}$) and $V_{IN} = 2.75\text{ V}$ to 6 V . Typical values at $V_{IN} = 5\text{ V}$ and $T_J = 25^{\circ}\text{C}$. (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
	Tracking offset	Feedback voltage with $V_{SS/TR} = 0\text{ V}$		17		mV
POWER SWITCH						
$R_{DS(ON)}$	High-side MOSFET ON-resistance	$V_{IN} \geq 5\text{ V}$		37	60	m Ω
$R_{DS(ON)}$	Low-side MOSFET ON-resistance	$V_{IN} \geq 5\text{ V}$		15	35	m Ω
	High-side MOSFET leakage current	$V_{IN} = 6\text{ V}$; $V(SW) = 0\text{ V}$			30	μA
	Low-side MOSFET leakage current	$V(SW) = 6\text{ V}$			55	μA
	SW leakage	$V(SW) = 0.6\text{ V}$; current into SW pin	-0.025		30	μA
I_{LIMH}	High-side MOSFET current limit	DC value, for TPS62810; $V_{IN} = 3\text{ V}$ to 6 V	4.8	5.6	6.65	A
I_{LIMH}	High-side MOSFET current limit	DC value, for TPS62813; $V_{IN} = 3\text{ V}$ to 6 V	3.9	4.5	5.35	A
I_{LIMH}	High-side MOSFET current limit	DC value, for TPS62812; $V_{IN} = 3\text{ V}$ to 6 V	2.8	3.4	4.3	A
I_{LIMH}	High-side MOSFET current limit	DC value, for TPS62811; $V_{IN} = 3\text{ V}$ to 6 V	2.0	2.6	3.35	A
I_{LIMNEG}	Negative valley current limit	DC value		-1.8		A
f_S	PWM switching frequency range		1.8	2.25	4	MHz
f_S	PWM switching frequency	With COMP/FSET tied to V_{IN} or GND	2.025	2.25	2.475	MHz
	PWM switching frequency tolerance	Using a resistor from COMP/FSET to GND, $f_S = 1.8\text{ MHz}$ to 4 MHz	-19%		18%	
$t_{on,min}$	Minimum on time of HS FET	$T_J = -40^{\circ}\text{C}$ to 125°C , $V_{IN} = 3.3\text{ V}$		50	75	ns
$t_{on,min}$	Minimum on time of LS FET	$V_{IN} = 3.3\text{ V}$		30		ns
OUTPUT						
V_{FB}	Feedback voltage			0.6		V
I_{LKG_FB}	Input leakage current (FB)	$V_{FB} = 0.6\text{ V}$		1	70	nA
V_{FB}	Feedback voltage accuracy	$V_{IN} \geq V_{OUT} + 1\text{ V}$	PWM mode	-1%	1%	
		$V_{IN} \geq V_{OUT} + 1\text{ V}$; $V_{OUT} \geq 1.5\text{ V}$	PFM mode; $C_{o,eff} \geq 22\text{ }\mu\text{F}$, $L = 0.47\text{ }\mu\text{H}$	-1%	2%	
		$1\text{ V} \leq V_{OUT} < 1.5\text{ V}$	PFM mode; $C_{o,eff} \geq 47\text{ }\mu\text{F}$, $L = 0.47\text{ }\mu\text{H}$	-1%	2.5%	
V_{FB}	Feedback voltage accuracy with voltage tracking	$V_{IN} \geq V_{OUT} + 1\text{ V}$; $V_{SS/TR} = 0.3\text{ V}$	PWM mode	-1%	7%	
	Load regulation	PWM mode operation		0.05		%/A
	Line regulation	PWM mode operation, $I_{OUT} = 1\text{ A}$, $V_{IN} \geq V_{OUT} + 1\text{ V}$		0.02		%/V
	Output discharge resistance				50	Ω
t_{delay}	Start-up delay time	$I_{OUT} = 0\text{ mA}$, time from EN = high to start switching; V_{IN} applied already	135	250	650	μs
t_{ramp}	Ramp time; SS/TR pin open	$I_{OUT} = 0\text{ mA}$, time from first switching pulse until 95% of nominal output voltage; device not in current limit	100	150	200	μs

7.6 Typical Characteristics

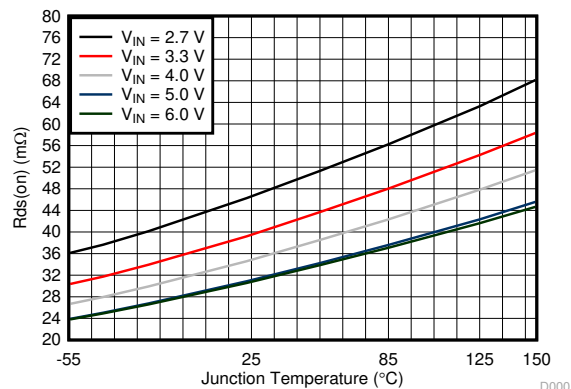


Figure 7-1. $R_{ds(on)}$ of High-side Switch

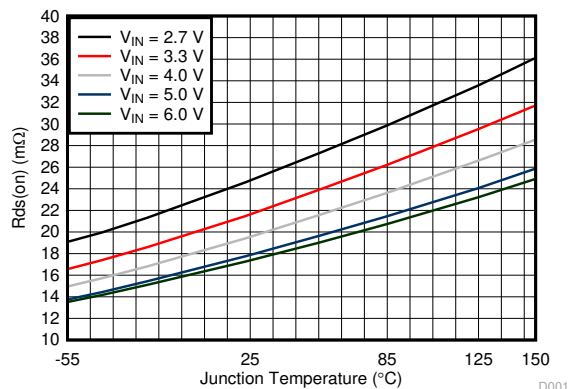


Figure 7-2. $R_{ds(on)}$ of Low-side Switch

8 Parameter Measurement Information

8.1 Schematic

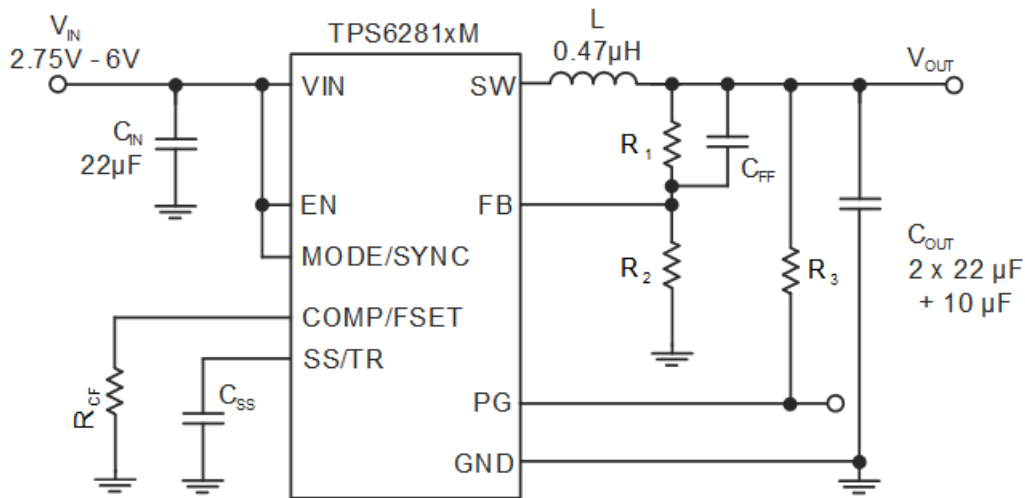


Figure 8-1. Measurement Setup for TPS62810M (4 A) and TPS62813M (3 A)

Table 8-1. List of Components

REFERENCE	DESCRIPTION	MANUFACTURER ⁽¹⁾
IC	TPS62810M or TPS62813M	Texas Instruments
L	0.47-µH inductor; XEL4030-471MEB	Coilcraft
C _{IN}	22 µF / 10 V; GCM31CR71A226KE02L	Murata
C _{OUT}	2 × 22 µF / 10 V; GCM31CR71A226KE02L + 1 × 10 µF, 6.3 V; GCM188D70J106ME36	Murata
C _{SS}	4.7 nF (equal to 1-ms start-up ramp)	Any
R _{CF}	8.06 kΩ	Any
C _{FF}	10 pF	Any
R ₁	Depending on V _{OUT}	Any
R ₂	Depending on V _{OUT}	Any
R ₃	100 kΩ	Any

(1) See the [Third-party Products Disclaimer](#).

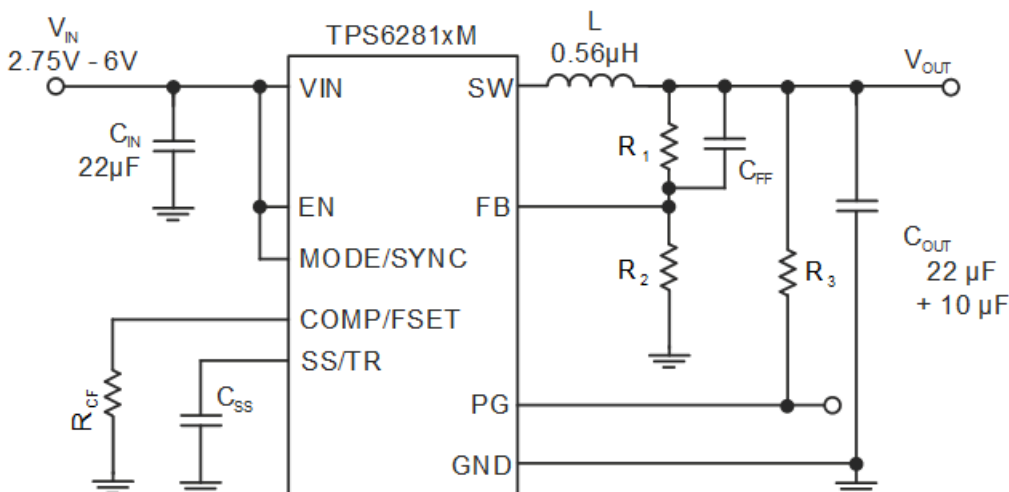


Figure 8-2. Measurement Setup for TPS62811M (1 A) and TPS62812M (2 A)

Table 8-2. List of Components

REFERENCE	DESCRIPTION	MANUFACTURER ⁽¹⁾
IC	TPS62812M or TPS62811M	Texas Instruments
L	0.56-µH inductor; XEL4020-561MEB	Coilcraft
C _{IN}	22 µF / 10 V; GCM31CR71A226KE02L	Murata
C _{OUT}	1 × 22 µF / 10 V; GCM31CR71A226KE02L + 1 × 10 µF, 6.3 V; GCM188D70J106ME36	Murata
C _{SS}	4.7 nF (equal to 1-ms start-up ramp)	Any
R _{CF}	8.06 kΩ	Any
C _{FF}	10 pF	Any
R ₁	Depending on V _{OUT}	Any
R ₂	Depending on V _{OUT}	Any
R ₃	100 kΩ	Any

(1) See the [Third-party Products Disclaimer](#).

Table 8-3. List of Key Components, Operation at –55°C

REFERENCE	DESCRIPTION	MANUFACTURER ⁽¹⁾
IC	TPS62810M, TPS62811M, TPS62812M, or TPS62813M	Texas Instruments
L	0.47-µH inductor; TFM252012ALMAR47MTAA	TDK
C _{IN}	22 µF / 10 V; GCJ31CL8ED226KE07	Murata
C _{OUT}	2 × 22 µF / 10 V; GCJ31CL8ED226KE07 + 1 × 10 µF, 16 V; GCJ32ER91C106KE01	Murata

(1) See the [Third-party Products Disclaimer](#).

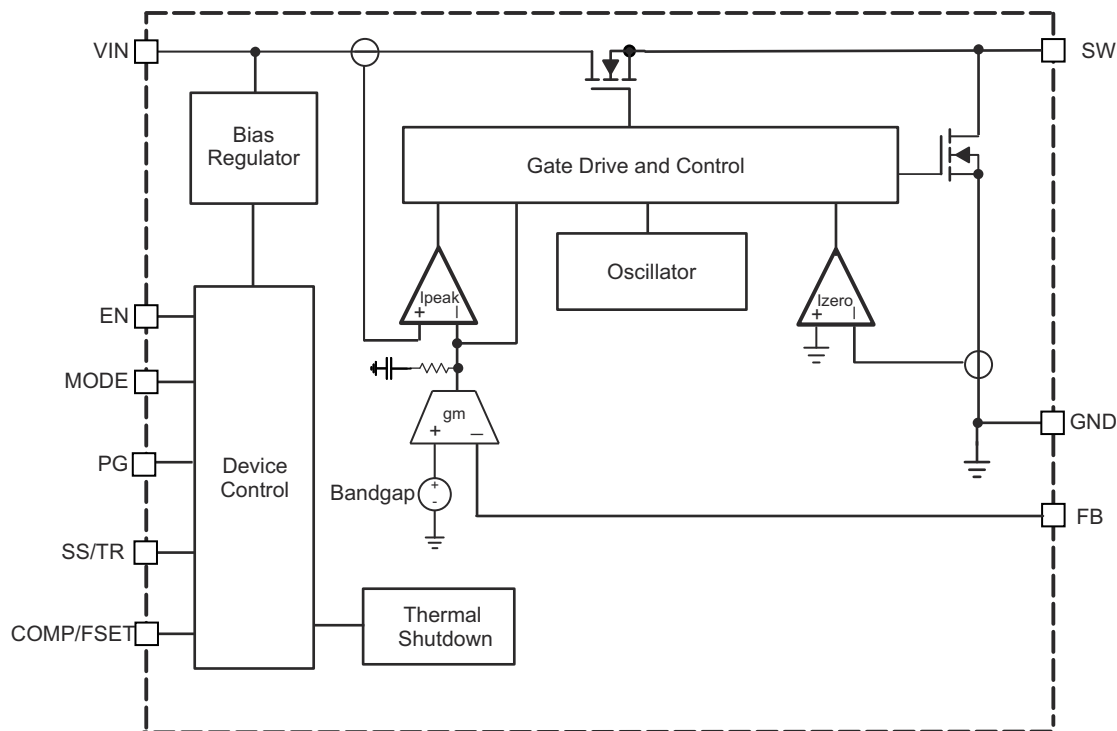
9 Detailed Description

9.1 Overview

The TPS6281xM synchronous switch mode DC/DC converter is based on a peak current mode control topology. The control loop is internally compensated. To optimize the bandwidth of the control loop to the wide range of output capacitance that can be used with the TPS6281xM, one of three internal compensation settings can be selected. See [Section 9.3.2](#). The compensation setting is selected either by a resistor from COMP/FSET to GND, or by the logic state of this pin. The regulation network achieves fast and stable operation with small external components and low-ESR ceramic output capacitors. The device can be operated without a feedforward capacitor on the output voltage divider, however, using a 10-pF (typical) feedforward capacitor improves transient response.

The device support forced fixed-frequency PWM operation with the MODE pin tied to a logic high level. The frequency is defined as either internally fixed 2.25 MHz when COMP/FSET is tied to GND or VIN, or in a range of 1.8 MHz to 4 MHz defined by a resistor from COMP/FSET to GND. Alternatively, the devices can be synchronized to an external clock signal in a range from 1.8 MHz to 4 MHz, applied to the MODE pin with no need for additional passive components. External synchronization is only possible if a resistor from COMP/FSET to GND is used. If COMP/FSET is directly tied to GND or VIN, the device cannot be synchronized externally. An internal PLL allows a change from an internal clock to an external clock during operation. The synchronization to the external clock is done on a falling edge of the clock applied at MODE to the rising edge on the SW pin. This allows roughly a 180° phase shift when the SW pin is used to generate the synchronization signal for a second converter. When the MODE pin is set to a logic low level, the devices operate in power save mode (PFM) at low output current and automatically transfer to fixed-frequency PWM mode at higher output current. In PFM mode, the switching frequency decreases linearly based on the load to sustain high efficiency down to very low output current.

9.2 Functional Block Diagram



9.3 Feature Description

9.3.1 Precise Enable

The voltage applied at the enable pin of the TPS6281xM device is compared to a fixed threshold of 1.1 V for a rising voltage. This lets the user drive the pin with a slowly changing voltage and enables the use of an external RC network to achieve a power-up delay.

The precise enable input provides a user-programmable undervoltage lockout by adding a resistor divider to the input of the enable pin.

The enable input threshold for a falling edge is typically 100 mV lower than the rising edge threshold. The TPS6281xM device starts operation when the rising threshold is exceeded. For proper operation, the EN pin must be terminated and must not be left floating. Pulling the EN pin low forces the device into shutdown with a shutdown current of typically 1 μ A. In this mode, the internal high-side and low-side MOSFETs are turned off and the entire internal control circuitry is switched off.

9.3.2 COMP/FSET

This pin lets the user set two different parameters independently:

- Internal compensation settings for the control loop
- The switching frequency in PWM mode from 1.8 MHz to 4 MHz

A resistor from COMP/FSET to GND changes the compensation and switching frequency. The change in compensation allows the user to adapt the device to different values of output capacitance. The resistor must be placed close to the pin to keep the parasitic capacitance on the pin to a minimum. The compensation setting is sampled when the converter starts up, so a change in the resistor during operation only has an effect on the switching frequency, but not on the compensation.

To save external components, the pin can also be directly tied to VIN or GND to set a pre-defined switching frequency or compensation. Do not leave the pin floating.

The switching frequency has to be selected based on the input voltage and the output voltage to meet the specifications for the minimum on time and minimum off time.

For example: $V_{IN} = 5\text{ V}$, $V_{OUT} = 1\text{ V}$ --> duty cycle (DC) = $1\text{ V} / 5\text{ V} = 0.2$

- with $t_{on} = DC \times T$ --> $t_{on,min} = 1 / f_{s,max} \times DC$
- --> $f_{s,max} = 1 / t_{on,min} \times DC = 1 / 0.075\text{ }\mu\text{s} \times 0.2 = 2.67\text{ MHz}$

The compensation range has to be chosen based on the minimum capacitance used. The capacitance can be increased from the minimum value as given in [Table 9-1](#) and [Table 9-2](#), up to a maximum of 470 μ F in all of the three compensation ranges. If the capacitance of an output changes during operation, for example, when load switches are used to connect or disconnect parts of the circuitry, the compensation must be chosen for the minimum capacitance on the output. With large output capacitance, the compensation must be done based on that large capacitance to get the best load transient response. Compensating for large output capacitance, but placing less capacitance on the output, can lead to instability.

The switching frequency for the different compensation settings is determined by the following equations.

For compensation (comp) setting 1:

$$R_{CF}(k\Omega) = \frac{18\text{MHz} \cdot k\Omega}{f_s(\text{MHz})} \quad (1)$$

For compensation (comp) setting 2:

$$R_{CF}(k\Omega) = \frac{60MHz \cdot k\Omega}{f_s(MHz)} \quad (2)$$

For compensation (comp) setting 3:

$$R_{CF}(k\Omega) = \frac{180MHz \cdot k\Omega}{f_s(MHz)} \quad (3)$$

Table 9-1. Switching Frequency and Compensation for TPS62810M (4 A) and TPS62813M (3 A)

COMPENSATION	R _{CF}	SWITCHING FREQUENCY	MINIMUM OUTPUT CAPACITANCE FOR V _{OUT} < 1 V	MINIMUM OUTPUT CAPACITANCE FOR 1 V ≤ V _{OUT} < 3.3 V	MINIMUM OUTPUT CAPACITANCE FOR V _{OUT} ≥ 3.3 V
for the smallest output capacitance (comp setting 1)	10 kΩ ... 4.5 kΩ	1.8 MHz (10 kΩ) ... 4 MHz (4.5 kΩ) according to Equation 1	53 μF	32 μF	27 μF
for medium output capacitance (comp setting 2)	33 kΩ ... 15 kΩ	1.8 MHz (33 kΩ) ... 4 MHz (15 kΩ) according to Equation 2	100 μF	60 μF	50 μF
for large output capacitance (comp setting 3)	100 kΩ ... 45 kΩ	1.8 MHz (100 kΩ) ... 4 MHz (45 kΩ) according to Equation 3	200 μF	120 μF	100 μF
for the smallest output capacitance (comp setting 1)	tied to GND	internally fixed 2.25 MHz	53 μF	32 μF	27 μF
for large output capacitance (comp setting 3)	tied to V _{IN}	internally fixed 2.25 MHz	200 μF	120 μF	100 μF

Table 9-2. Switching Frequency and Compensation for TPS62812M (2 A) and TPS62811M (1 A)

COMPENSATION	R _{CF}	SWITCHING FREQUENCY	MINIMUM OUTPUT CAPACITANCE FOR V _{OUT} < 1 V	MINIMUM OUTPUT CAPACITANCE FOR 1 V ≤ V _{OUT} < 3.3 V	MINIMUM OUTPUT CAPACITANCE FOR V _{OUT} ≥ 3.3 V
for the smallest output capacitance (comp setting 1)	10 kΩ ... 4.5 kΩ	1.8 MHz (10 kΩ) ... 4 MHz (4.5 kΩ) according to Equation 1	30 μF	18 μF	15 μF
for medium output capacitance (comp setting 2)	33 kΩ ... 15 kΩ	1.8 MHz (33 kΩ) ... 4 MHz (15 kΩ) according to Equation 2	60 μF	36 μF	30 μF
for large output capacitance (comp setting 3)	100 kΩ ... 45 kΩ	1.8MHz (100 kΩ) ...4 MHz (45 kΩ) according to Equation 3	130 μF	80 μF	68 μF
for the smallest output capacitance (comp setting 1)	tied to GND	internally fixed 2.25 MHz	30 μF	18 μF	15 μF
for large output capacitance (comp setting 3)	tied to V _{IN}	internally fixed 2.25 MHz	130 μF	80 μF	68 μF

Refer to [Section 10.1.3.2](#) for further details on the required output capacitance required depending on the output voltage.

A too-high resistor value for R_{CF} is decoded as "tied to V_{IN}". A value below the lowest range is decoded as "tied to GND". The minimum output capacitance in [Table 9-1](#) and [Table 9-2](#) is for capacitors close to the output of the device. If the capacitance is distributed, a lower compensation setting can be required. All values are effective capacitance including, but not limited to:

- All tolerances
- Aging

- DC bias effect

9.3.3 MODE/SYNC

When MODE/SYNC is set low, the device operates in PWM or PFM mode, depending on the output current. The MODE/SYNC pin lets the user force PWM mode when set high. The pin also lets the user apply an external clock in a frequency range from 1.8 MHz to 4 MHz for external synchronization. Similar to COMP/FSET, take the specifications for the minimum on time and minimum off time into account when setting the external frequency. For use with external synchronization on the MODE/SYNC pin, the internal switching frequency must be set by R_{CF} to a similar value of the externally applied clock. This ensures a fast settling to the external clock and, if the external clock fails, the switching frequency stays in the same range and the compensation settings are still valid. When there is no resistor from COMP/FSET to GND but the pin is pulled high or low, external synchronization is not possible.

9.3.4 Spread Spectrum Clocking (SSC)

For device versions with SSC enabled, the switching frequency is randomly changed in PWM mode when the internal clock is used. The frequency variation is typically between the nominal switching frequency and up to 288 kHz above the nominal switching frequency. When the device is externally synchronized by applying a clock signal to the MODE/SYNC pin, the TPS6281xM device follows the external clock and the internal spread spectrum block is turned off. SSC is also disabled during soft start.

9.3.5 Undervoltage Lockout (UVLO)

If the input voltage drops, the undervoltage lockout prevents mis-operation of the device by switching off both of the power FETs. The device is fully operational for voltages above the rising UVLO threshold and turns off if the input voltage trips below the threshold for a falling supply voltage.

9.3.6 Power Good Output (PG)

Power good is an open-drain output driven by a window comparator. PG is held low when the device is disabled, in undervoltage lockout, and in thermal shutdown. When the output voltage is in regulation hence, within the window defined in the electrical characteristics, the output is high impedance.

Table 9-3. PG Status

EN	DEVICE STATUS	PG STATE
X	$V_{IN} < 2.75\text{ V}$	undefined
low	$V_{IN} < 2.75\text{ V}$	undefined
high	$V_{IN} < 2.25\text{ V}$	undefined
low	$V_{IN} \geq 2.75\text{ V}$	low
high	$2.25\text{ V} \leq V_{IN} \leq \text{UVLO}$ OR in thermal shutdown OR V_{OUT} not in regulation	low
high	V_{OUT} in regulation	high impedance

9.3.7 Thermal Shutdown

The junction temperature (T_J) of the device is monitored by an internal temperature sensor. If T_J exceeds 170°C (typ), the device goes into thermal shutdown. Both the high-side and low-side power FETs are turned off and PG goes low. When T_J decreases by the hysteresis amount of typically 15°C, the device resumes normal operation, beginning with soft start. During a PFM pause, the thermal shutdown is not active. After a PFM pause, the device needs up to 9 μs to detect a too-high junction temperature. If the PFM burst is shorter than this delay, the device does not detect a too-high junction temperature.

9.4 Device Functional Modes

9.4.1 Pulse Width Modulation (PWM) Operation

The TPS6281xM device has two operating modes: forced PWM mode (discussed in this section) and PWM/PFM (discussed in [Section 9.4.2](#)).

With the MODE/SYNC pin set to high, the TPS6281xM device operates with pulse width modulation in continuous conduction mode (CCM). The switching frequency is either defined by a resistor from the COMP pin to GND or by an external clock signal applied to the MODE/SYNC pin. With an external clock is applied to MODE/SYNC, the device follows the frequency applied to the pin. To maintain regulation, the frequency needs to be in a range the device can operate at, taking the minimum on time into account.

9.4.2 Power Save Mode Operation (PWM/PFM)

When the MODE/SYNC pin is low, power save mode is allowed. The device operates in PWM mode as long as the peak inductor current is above the approximately 1.2-A PFM threshold. When the peak inductor current drops below the PFM threshold, the device starts to skip switching pulses. In power save mode, the switching frequency decreases with the load current maintaining high efficiency.

9.4.3 100% Duty-Cycle Operation

The duty cycle of a buck converter operated in PWM mode is given as $D = V_{OUT} / V_{IN}$. The duty cycle increases as the input voltage comes close to the output voltage and the off time gets smaller. When the approximately 30-ns minimum off time is reached, the TPS6281xM device skips switching cycles while it approaches 100% mode. In 100% mode, the device keeps the high-side switch on continuously. The high-side switch stays turned on as long as the output voltage is below the target. In 100% mode, the low-side switch is turned off. The maximum dropout voltage in 100% mode is the product of the on-resistance of the high-side switch plus the series resistance of the inductor and the load current.

9.4.4 Current Limit and Short Circuit Protection

The TPS6281xM device is protected against overload and short circuit events. If the inductor current exceeds the current limit I_{LIMH} , the high-side switch is turned off and the low-side switch is turned on to ramp down the inductor current. The high-side switch turns on again only if the current in the low-side switch has decreased below the low-side current limit. Due to internal propagation delay, the actual current can exceed the static current limit. The dynamic current limit is given as:

$$I_{peak(yp)} = I_{LIMH} + \frac{V_L}{L} \cdot t_{PD} \quad (4)$$

where

- I_{LIMH} is the static current limit as specified in the [Electrical Characteristics](#)
- L is the effective inductance at the peak current
- V_L is the voltage across the inductor ($V_{IN} - V_{OUT}$)
- t_{PD} is the internal propagation delay of typically 50 ns

The current limit can exceed static values, especially if the input voltage is high and very small inductances are used. The dynamic high-side switch peak current can be calculated as:

$$I_{peak(yp)} = I_{LIMH} + \frac{V_{IN} - V_{OUT}}{L} \cdot 50ns \quad (5)$$

9.4.5 Foldback Current Limit and Short Circuit Protection

This is valid for devices where foldback current limit is enabled.

When the device detects current limit for more than 1024 subsequent switching cycles, it reduces the current limit from its nominal value to typically 1.8 A. Foldback current limit is left when the current limit indication goes away. If device operation continues in current limit, after 3072 switching cycles, the device tries for full current limit again after 1024 switching cycles.

9.4.6 Output Discharge

The purpose of the discharge function is to ensure a defined down ramp of the output voltage when the device is being disabled and to keep the output voltage close to 0 V when the device is off. The output discharge feature

is only active once the TPS6281xM device has been enabled at least once since the supply voltage was applied. The discharge function is enabled as soon as the device is disabled, in thermal shutdown, or in undervoltage lockout. The minimum supply voltage required for the discharge function to remain active is typically 2 V. Output discharge is not activated during a current limit or foldback current limit event.

9.4.7 Soft Start/Tracking (SS/TR)

The internal soft-start circuitry controls the output voltage slope during start-up. This avoids excessive inrush current and ensures a controlled output voltage rise time. It also prevents unwanted voltage drops from high impedance power sources or batteries. When EN is set high to start operation, the device starts switching after a delay of about 200 μ s, then the internal reference and hence, V_{OUT} , rises with a slope controlled by an external capacitor connected to the SS/TR pin.

Leaving the SS/TR pin un-connected provides the fastest start-up ramp with typically 150 μ s. A capacitor connected from SS/TR to GND is charged with 2.5 μ A by an internal current source during soft start until it reaches the 0.6-V reference voltage. The capacitance required to set a certain ramp-time (t_{ramp}) is:

$$C_{SS}[nF] = \frac{2.5\mu A \cdot t_{ramp}[ms]}{0.6V} \quad (6)$$

If the device is set to shutdown (EN = GND), undervoltage lockout, or thermal shutdown, an internal resistor pulls the SS/TR pin to GND to ensure a proper low level. Returning from those states causes a new start-up sequence.

A voltage applied at SS/TR can be used to track a main voltage. The output voltage follows this voltage up and down in forced PWM mode. In PFM mode, the output voltage decreases based on the load current. The SS/TR pin must not be connected to the SS/TR pin of other devices. An external voltage applied on SS/TR is internally clamped to the feedback voltage (0.6 V). It is recommended to set the target for the external voltage on SS/TR slightly above the feedback voltage. Given the tolerances of the resistor divider R_5 and R_6 on SS/TR, this ensures the device "switches" to the internal reference voltage when the power-up sequencing is finished. See [Figure 10-57](#).

10 Application and Implementation

Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

10.1 Application Information

10.1.1 Programming the Output Voltage

The output voltage of the TPS6281xM device is adjustable. It can be programmed for output voltages from 0.6 V to 5.5 V using a resistor divider from VOUT to GND. The voltage at the FB pin is regulated to 600 mV. The value of the output voltage is set by the selection of the resistor divider from [Equation 7](#). It is recommended to choose resistor values that allow a current of at least 2 µA, meaning the value of R₂ must not exceed 400 kΩ. Lower resistor values are recommended for the highest accuracy and most robust design.

$$R_1 = R_2 \cdot \left(\frac{V_{OUT}}{V_{FB}} - 1 \right) \quad (7)$$

10.1.2 Inductor Selection

The TPS6281xM device is designed for a nominal 0.47-µH inductor with a typical switching frequency of 2.25 MHz. Larger values can be used to achieve a lower inductor current ripple, but they can have a negative impact on efficiency and transient response. Smaller values than 0.47 µH cause a larger inductor current ripple, which causes larger negative inductor current in forced PWM mode at low or no output current. For a higher or lower nominal switching frequency, the inductance must be changed accordingly.

The inductor selection is affected by several effects like the following:

- Inductor ripple current
- Output ripple voltage
- PWM-to-PFM transition point
- Efficiency

In addition, the selected inductor has to be rated for appropriate saturation current and DC resistance (DCR). [Equation 8](#) calculates the maximum inductor current.

$$I_{L(max)} = I_{OUT(max)} + \frac{\Delta I_{L(max)}}{2} \quad (8)$$

$$\Delta I_{L(max)} = \frac{V_{OUT} \cdot \left(1 - \frac{V_{OUT}}{V_{IN}} \right)}{L_{min}} \cdot \frac{1}{f_{SW}} \quad (9)$$

where

- I_{L(max)} is the maximum inductor current
- ΔI_{L(max)} is the peak-to-peak inductor ripple current
- L_{min} is the minimum inductance at the operating point

Table 10-1. Typical Inductors

TYPE	INDUCTANCE [μH]	CURRENT [A] ⁽¹⁾	FOR DEVICE	NOMINAL SWITCHING FREQUENCY	DIMENSIONS [LxBxH] mm	MANUFACTURER ⁽²⁾	OPERATION AT – 55°C
ML433PYA601MLZ	0.6 μH, ±20%	10.4	TPS62810M, TPS62813M, TPS62812M	2.25 MHz	4 × 4 × 2.1	Coilcraft	yes
ML433PYA401MLZ	0.4 μH, ±20%	12.5	TPS62810M, TPS62813M, TPS62812M	2.25 MHz	4 × 4 × 2.1	Coilcraft	yes
XFL4015-471ME	0.47 μH, ±20%	3.5	TPS62813M, TPS62812M	2.25 MHz	4 × 4 × 1.6	Coilcraft	no
XEL4020-561ME	0.56 μH, ±20%	9.9	TPS62810M, TPS62813M, TPS62812M	2.25 MHz	4 × 4 × 2.1	Coilcraft	no
XEL4030-471ME	0.47 μH, ±20%	12.3	TPS62810M, TPS62813M, TPS62812M	2.25 MHz	4 × 4 × 3.1	Coilcraft	no
XEL3515-561ME	0.56 μH, ±20%	4.5	TPS62813M, TPS62812M	2.25 MHz	3.5 × 3.2 × 1.5	Coilcraft	no
XFL3012-331MEB	0.33 μH, ±20%	2.6	TPS62811M, TPS62812M	≥ 3.5 MHz	3 × 3 × 1.3	Coilcraft	no
XPL2010-681ML	0.68 μH, ±20%	1.5	TPS62811M	2.25 MHz	2 × 1.9 × 1	Coilcraft	no
DFE252012PD- R47M	0.47 μH, ±20%	see data sheet	TPS62811M, TPS62813M, TPS62812M	2.25 MHz	2.5 × 2 × 1.2	Murata	no

(1) Lower of I_{RMS} at 20°C rise or I_{SAT} at 20% drop

(2) See the [Third-party Products Disclaimer](#).

Calculating the maximum inductor current using the actual operating conditions gives the minimum saturation current of the inductor needed. A margin of about 20% is recommended to add. A larger inductor value is also useful to get lower ripple current, but increases the transient response time and size as well.

10.1.3 Capacitor Selection

10.1.3.1 Input Capacitor

For most applications, 22 μF nominal is sufficient and is recommended. The input capacitor buffers the input voltage for transient events and decouples the converter from the supply. A low-ESR multilayer ceramic capacitor (MLCC) is recommended for the best filtering and must be placed between VIN and GND as close as possible to those pins.

10.1.3.2 Output Capacitor

The architecture of the TPS6281xM device allows the use of tiny ceramic output capacitors with low equivalent series resistance (ESR). These capacitors provide low output voltage ripple and are recommended. To keep its low resistance up to high frequencies and to get narrow capacitance variation with temperature, it is recommended to use dielectric X7R, X7T, or an equivalent. Using a higher value has advantages like smaller voltage ripple and tighter DC output accuracy in power save mode. By changing the device compensation with a resistor from COMP/FSET to GND, the device can be compensated in three steps based on the minimum capacitance used on the output. The maximum capacitance is 470 μF in any of the compensation settings.

The minimum capacitance required on the output depends on the compensation setting as well as on the current rating of the device. The TPS62810M and TPS62813M devices require a minimum output capacitance of 27 μF while the lower current versions (the TPS62812M and TPS62811M devices) require 15 μF at minimum. The required output capacitance also changes with the output voltage.

For output voltages below 1 V, the minimum increases linearly from 32 μF at 1 V to 53 μF at 0.6 V for the TPS62810M device. Use the TPS62813M device with the compensation setting for smallest output capacitance. Other compensation ranges and ranges for TPS62811M and TPS62812M are equivalent. See [Table 9-1](#) and [Table 9-2](#) for details.

10.2 Typical Application

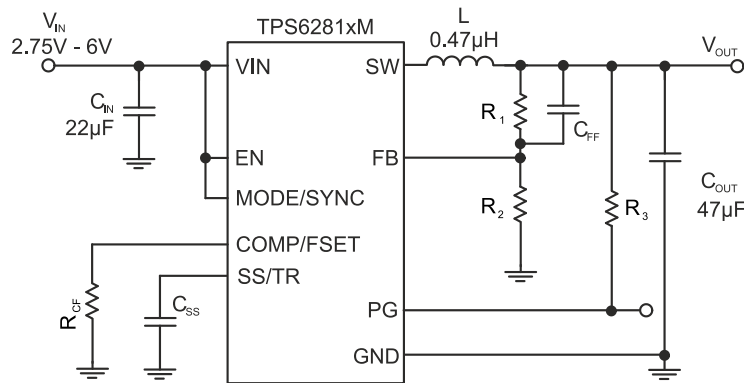


Figure 10-1. Typical Application

10.2.1 Design Requirements

The design guidelines provide a component selection to operate the device within the recommended operating conditions.

10.2.2 Detailed Design Procedure

$$R_1 = R_2 \cdot \left(\frac{V_{OUT}}{V_{FB}} - 1 \right) \quad (10)$$

With $V_{FB} = 0.6 \text{ V}$:

Table 10-2. Setting the Output Voltage

NOMINAL OUTPUT VOLTAGE V_{OUT}	R_1	R_2	C_{FF}	EXACT OUTPUT VOLTAGE
0.8 V	16.9 kΩ	51 kΩ	10 pF	0.7988 V
1.0 V	20 kΩ	30 kΩ	10 pF	1.0 V
1.1 V	39.2 kΩ	47 kΩ	10 pF	1.101 V
1.2 V	68 kΩ	68 kΩ	10 pF	1.2 V
1.5 V	76.8 kΩ	51 kΩ	10 pF	1.5 V
1.8 V	80.6 kΩ	40.2 kΩ	10 pF	1.803 V
2.5 V	47.5 kΩ	15 kΩ	10 pF	2.5 V
3.3 V	88.7 kΩ	19.6 kΩ	10 pF	3.315 V

10.2.3 Application Curves

All plots have been taken with a nominal switching frequency of 2.25 MHz when set to PWM mode, unless otherwise noted. The BOM is according to [Table 8-1](#).

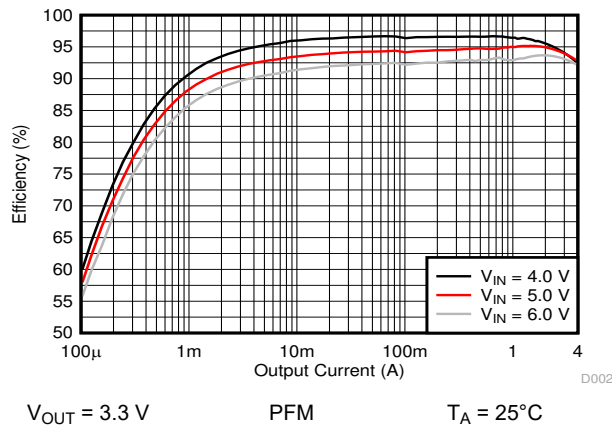


Figure 10-2. Efficiency versus Output Current

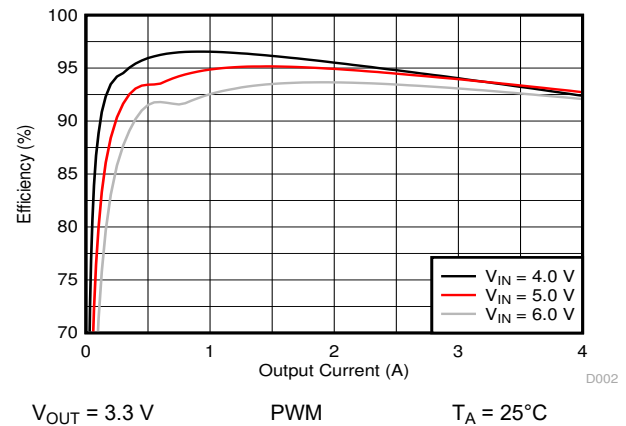


Figure 10-3. Efficiency versus Output Current

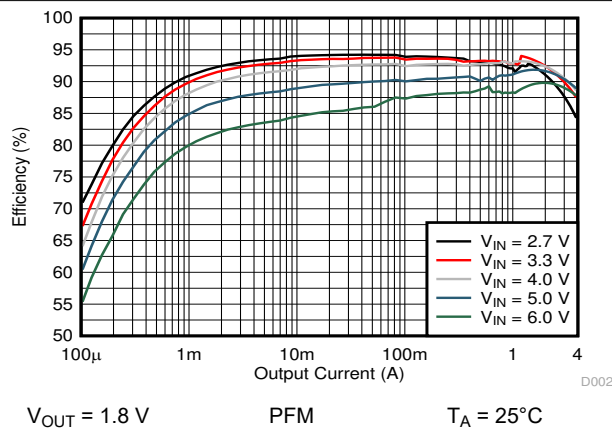


Figure 10-4. Efficiency versus Output Current

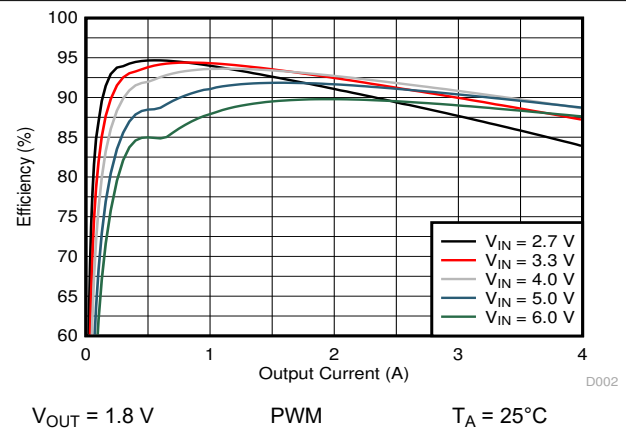


Figure 10-5. Efficiency versus Output Current

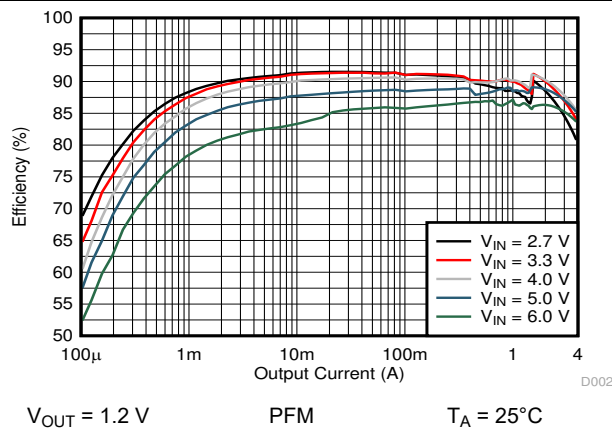


Figure 10-6. Efficiency versus Output Current

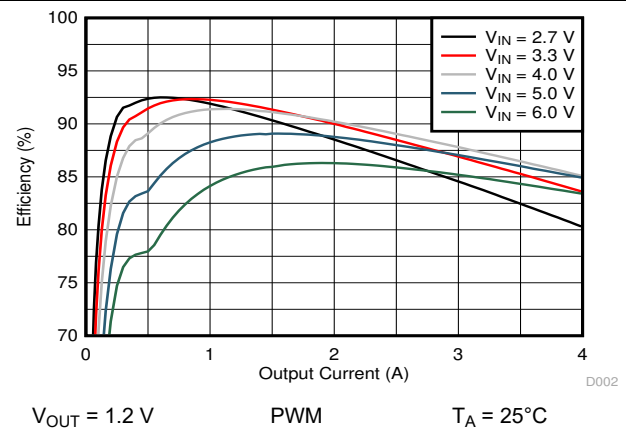


Figure 10-7. Efficiency versus Output Current

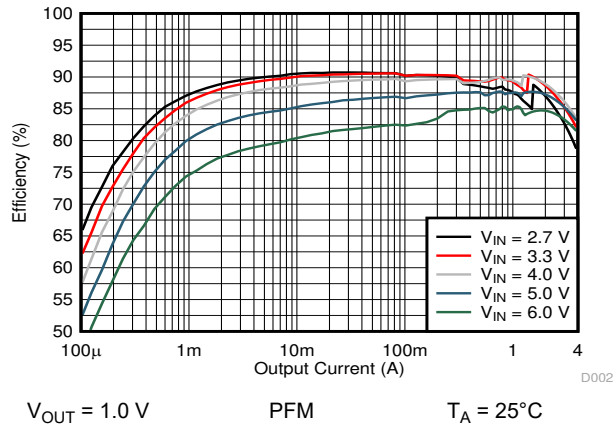


Figure 10-8. Efficiency versus Output Current

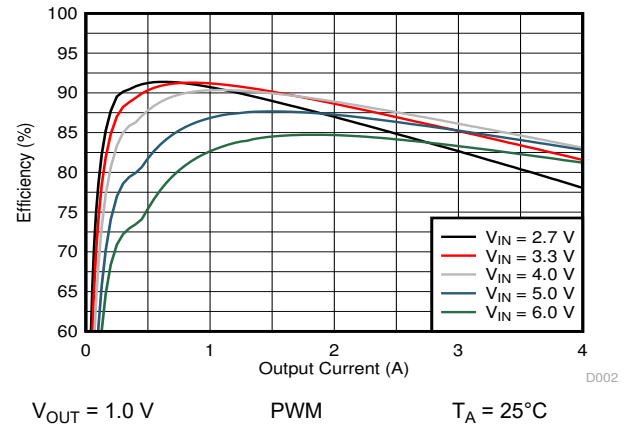


Figure 10-9. Efficiency versus Output Current

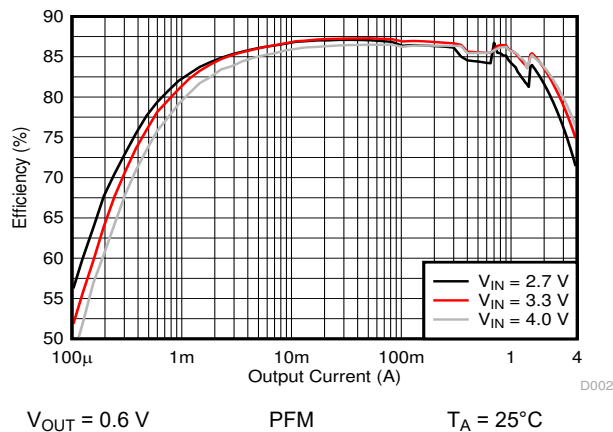


Figure 10-10. Efficiency versus Output Current

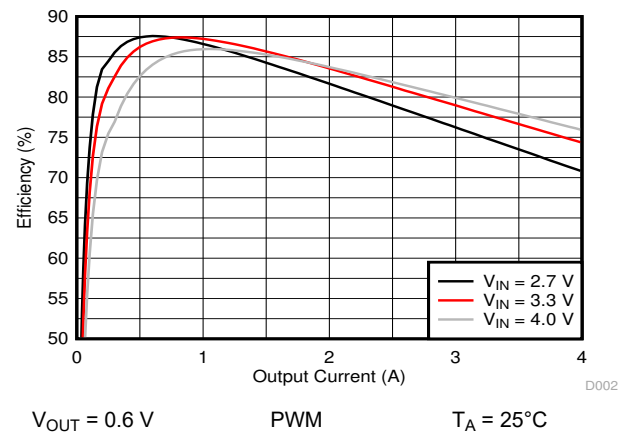


Figure 10-11. Efficiency versus Output Current

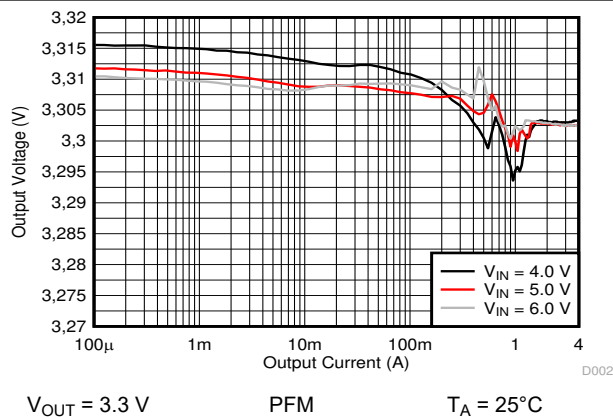


Figure 10-12. Output Voltage versus Output Current

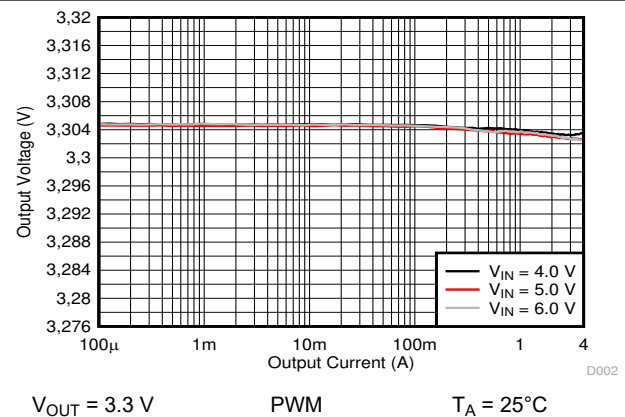


Figure 10-13. Output Voltage versus Output Current

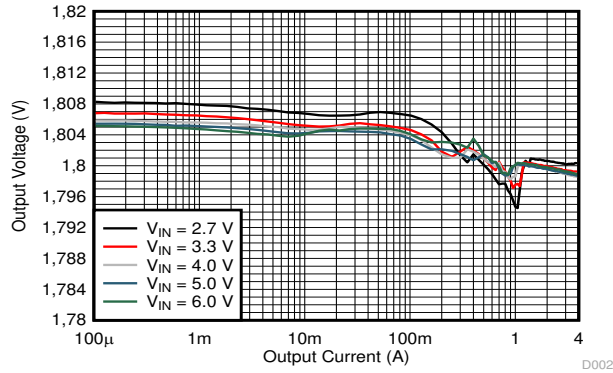


Figure 10-14. Output Voltage versus Output Current

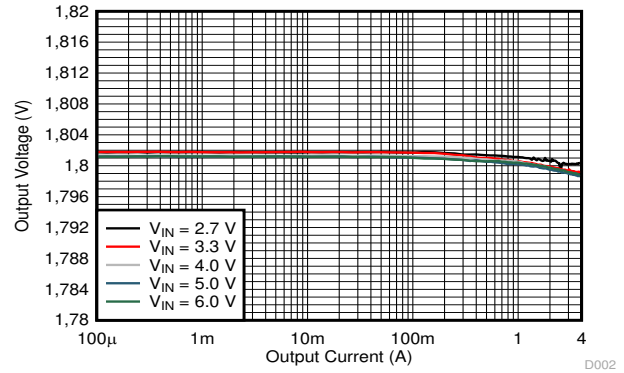


Figure 10-15. Output Voltage versus Output Current

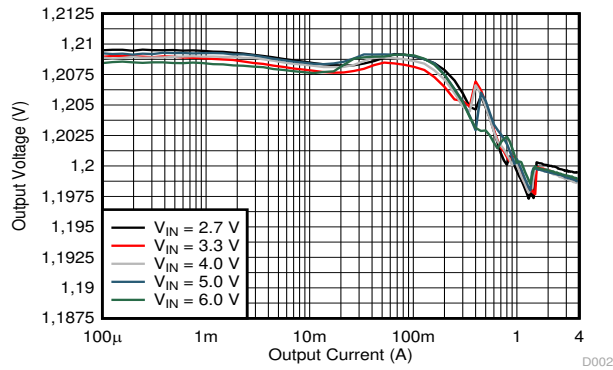


Figure 10-16. Output Voltage versus Output Current

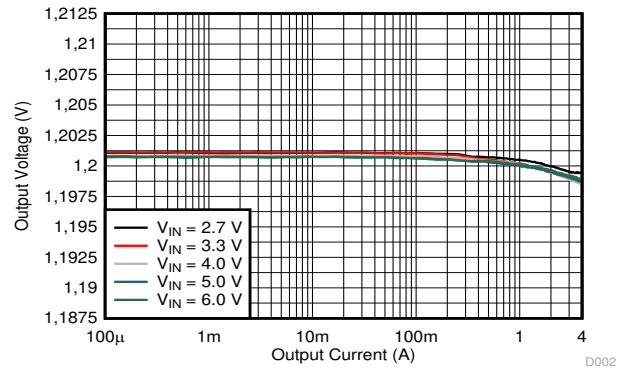


Figure 10-17. Output Voltage versus Output Current

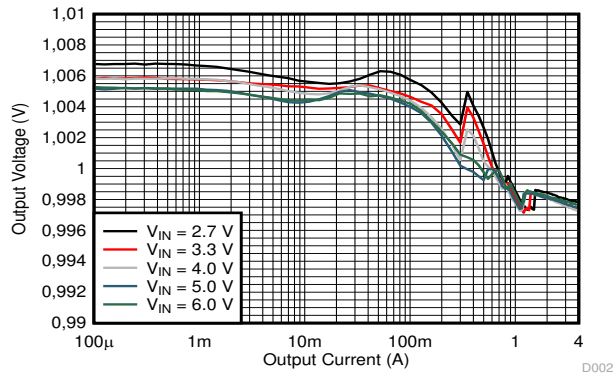


Figure 10-18. Output Voltage versus Output Current

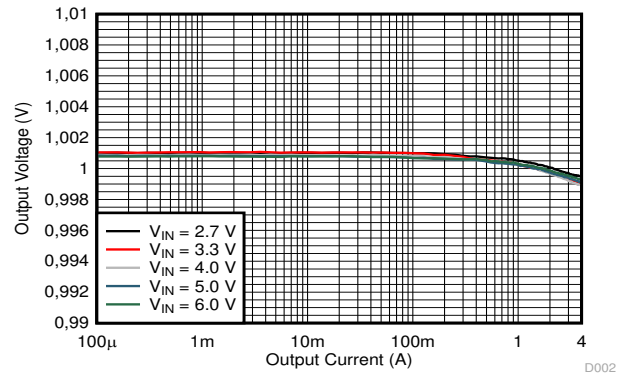


Figure 10-19. Output Voltage versus Output Current

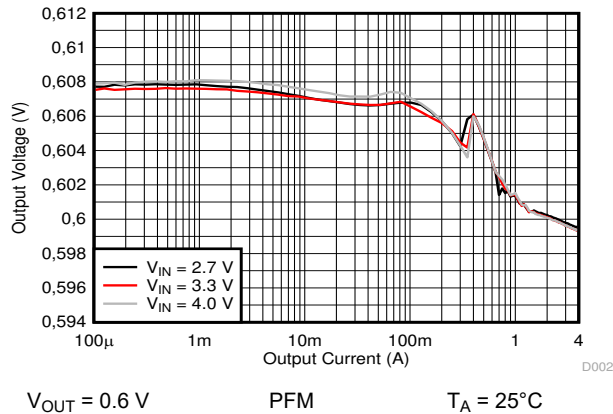


Figure 10-20. Output Voltage versus Output Current

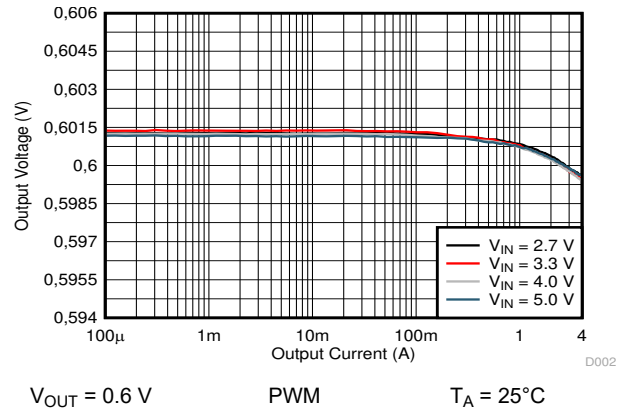


Figure 10-21. Output Voltage versus Output Current

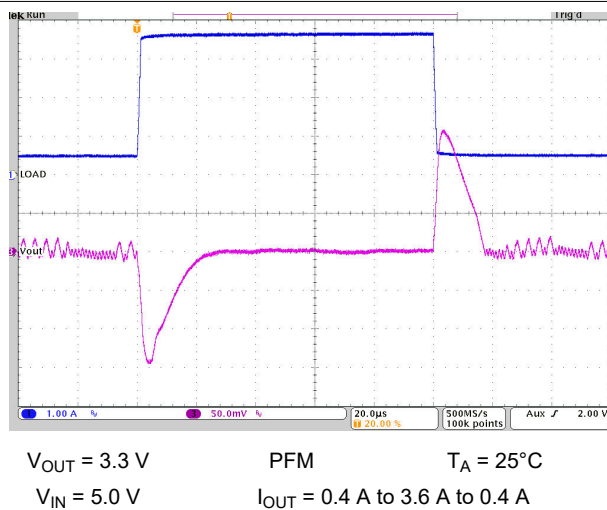


Figure 10-22. Load Transient Response

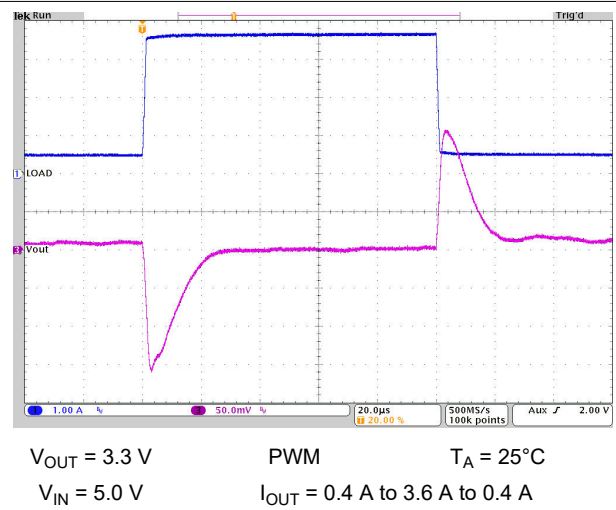


Figure 10-23. Load Transient Response

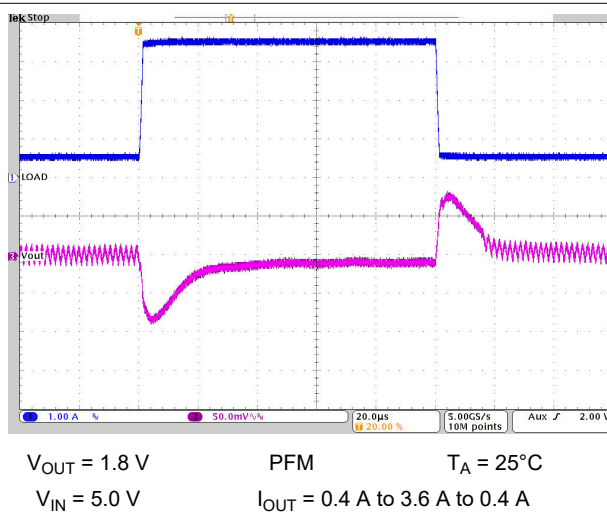


Figure 10-24. Load Transient Response

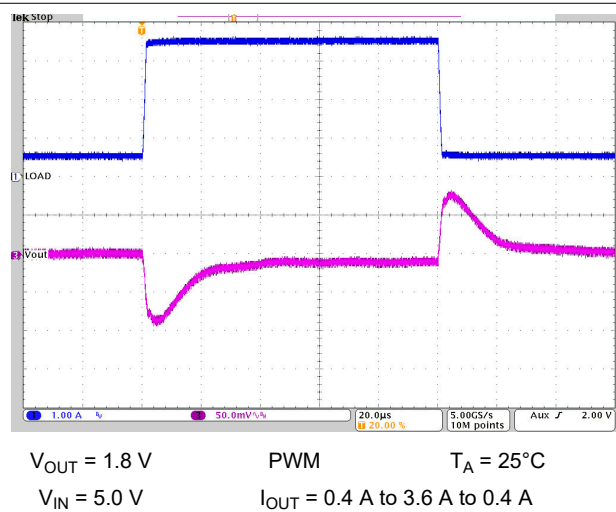
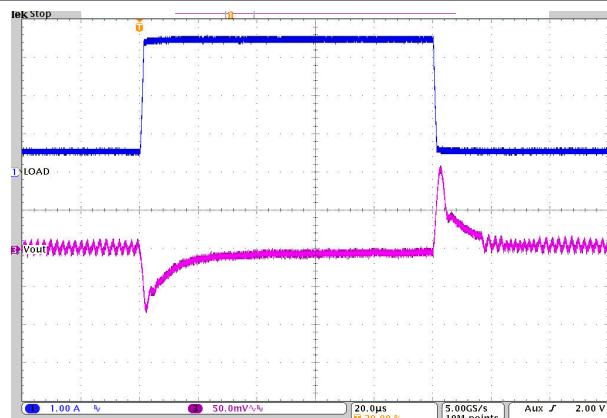
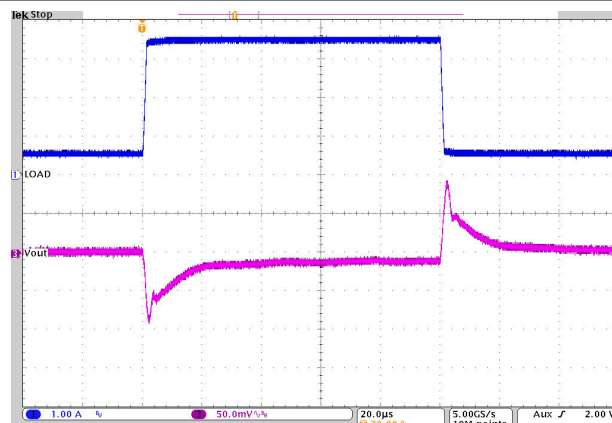


Figure 10-25. Load Transient Response



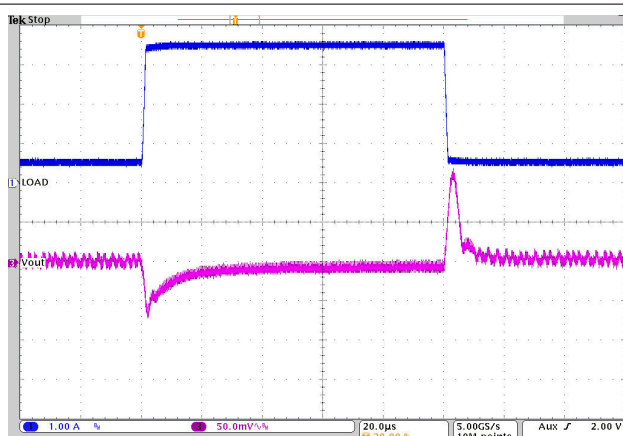
$V_{OUT} = 1.2 \text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5.0 \text{ V}$ $I_{OUT} = 0.4 \text{ A to } 3.6 \text{ A to } 0.4 \text{ A}$

Figure 10-26. Load Transient Response



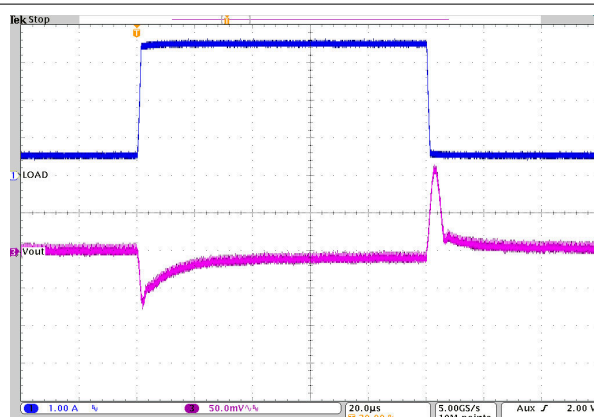
$V_{OUT} = 1.2 \text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5.0 \text{ V}$ $I_{OUT} = 0.4 \text{ A to } 3.6 \text{ A to } 0.4 \text{ A}$

Figure 10-27. Load Transient Response



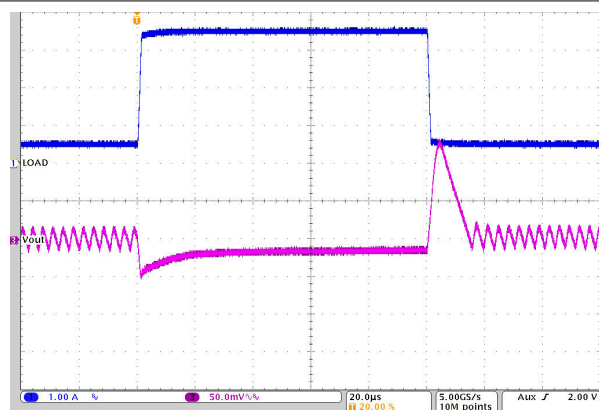
$V_{OUT} = 1.0 \text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5.0 \text{ V}$ $I_{OUT} = 0.4 \text{ A to } 3.6 \text{ A to } 0.4 \text{ A}$

Figure 10-28. Load Transient Response



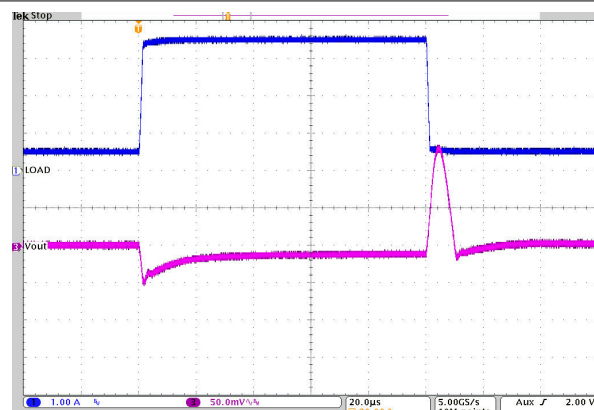
$V_{OUT} = 1.0 \text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5.0 \text{ V}$ $I_{OUT} = 0.4 \text{ A to } 3.6 \text{ A to } 0.4 \text{ A}$

Figure 10-29. Load Transient Response



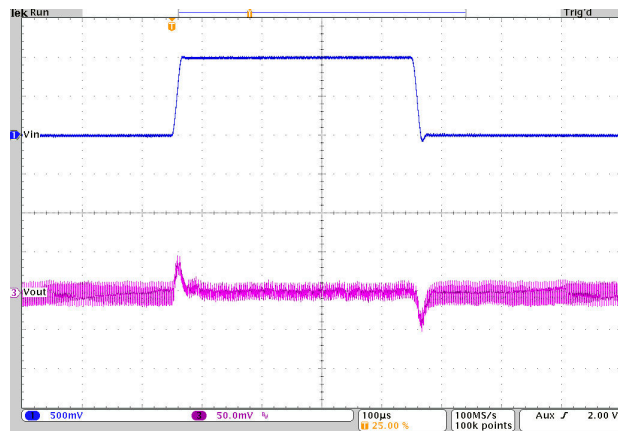
$V_{OUT} = 0.6 \text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 3.3 \text{ V}$ $I_{OUT} = 0.4 \text{ A to } 3.6 \text{ A to } 0.4 \text{ A}$

Figure 10-30. Load Transient Response



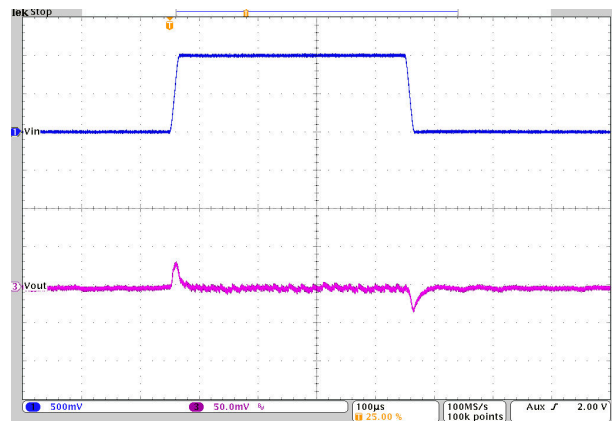
$V_{OUT} = 0.6 \text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $V_{IN} = 3.3 \text{ V}$ $I_{OUT} = 0.4 \text{ A to } 3.6 \text{ A to } 0.4 \text{ A}$

Figure 10-31. Load Transient Response



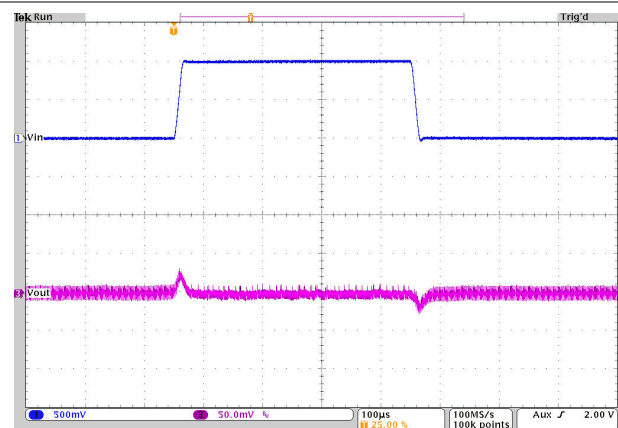
$V_{OUT} = 3.3\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.5\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-32. Line Transient Response



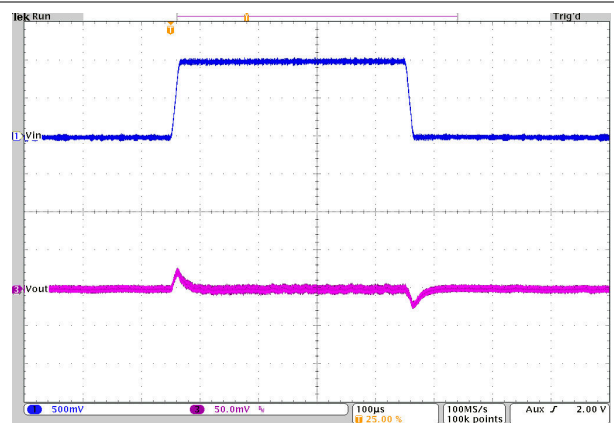
$V_{OUT} = 3.3\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-33. Line Transient Response



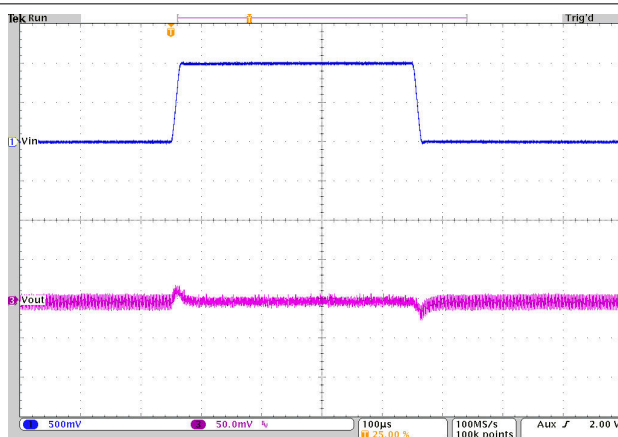
$V_{OUT} = 1.8\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.5\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-34. Line Transient Response



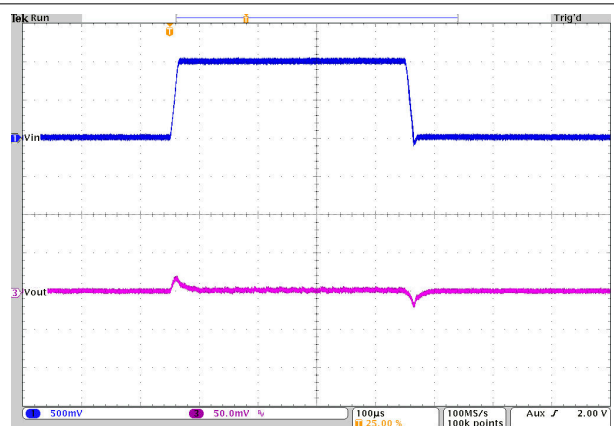
$V_{OUT} = 1.8\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-35. Line Transient Response



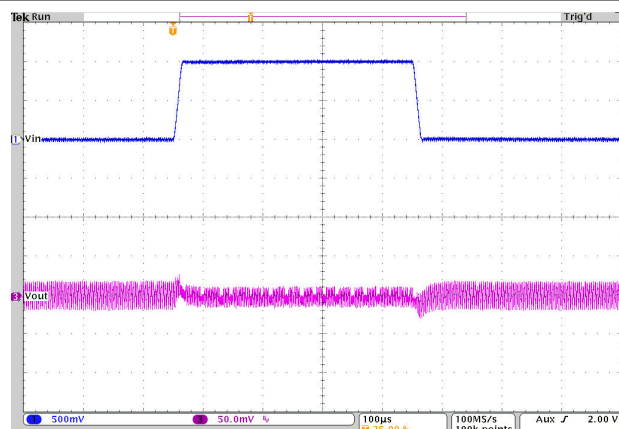
$V_{OUT} = 1.2\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.5\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-36. Line Transient Response



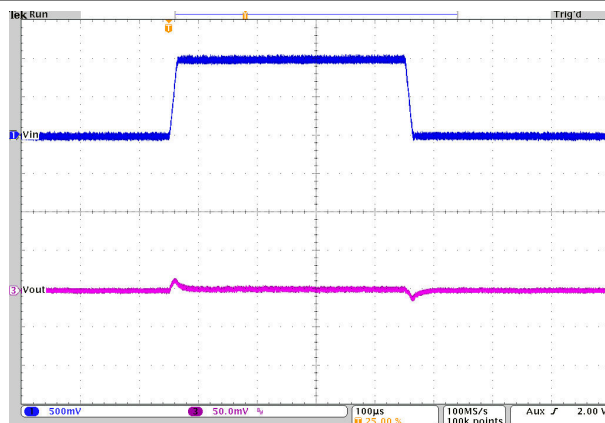
$V_{OUT} = 1.2\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-37. Line Transient Response



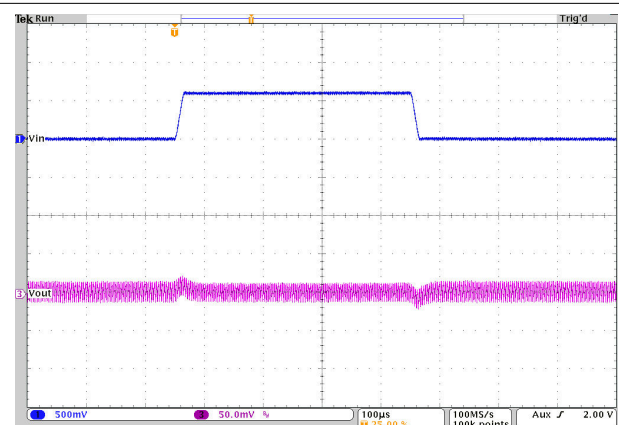
$V_{OUT} = 1.0\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.5\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-38. Line Transient Response



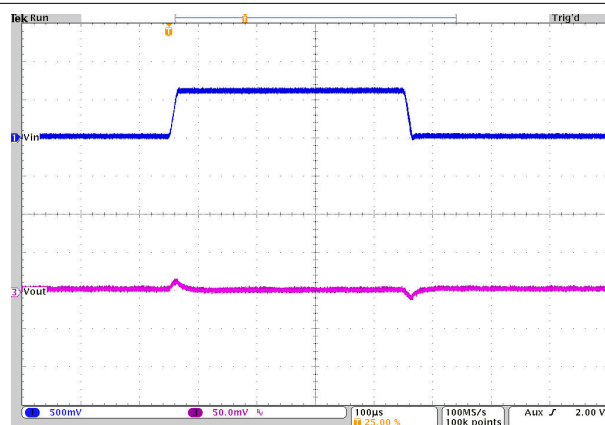
$V_{OUT} = 1.0\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-39. Line Transient Response



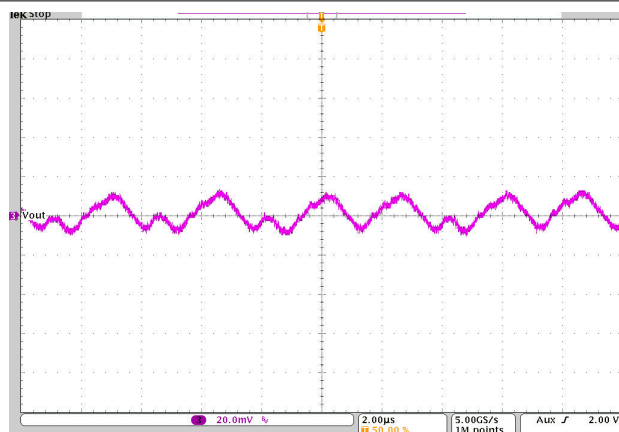
$V_{OUT} = 0.6\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.5\text{ A}$ $V_{IN} = 3.0\text{ V to } 3.6\text{ V to } 3.0\text{ V}$

Figure 10-40. Line Transient Response



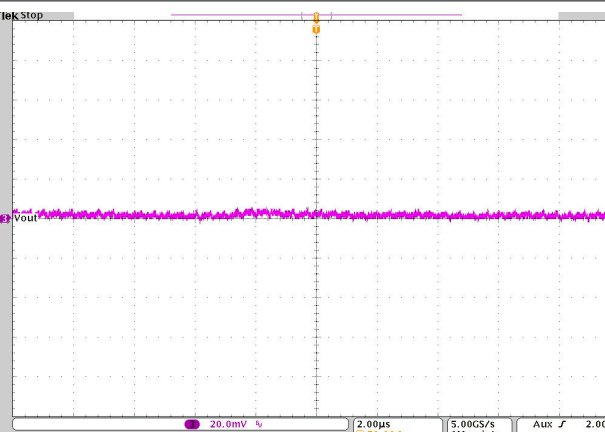
$V_{OUT} = 0.6\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 3.0\text{ V to } 3.6\text{ V to } 3.0\text{ V}$

Figure 10-41. Line Transient Response



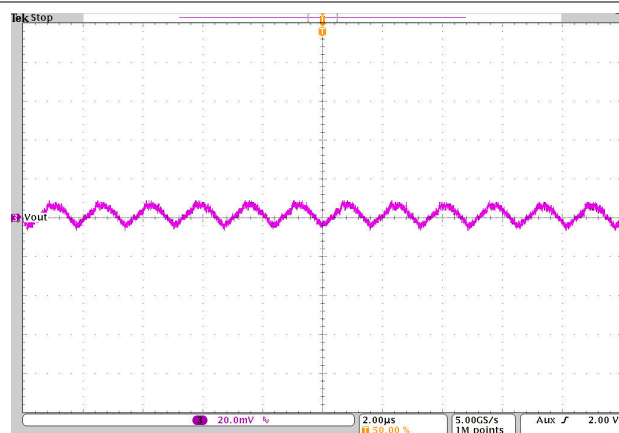
$V_{OUT} = 3.3\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.5\text{ A}$ $V_{IN} = 5.0\text{ V}$ BW = 20 MHz

Figure 10-42. Output Voltage Ripple



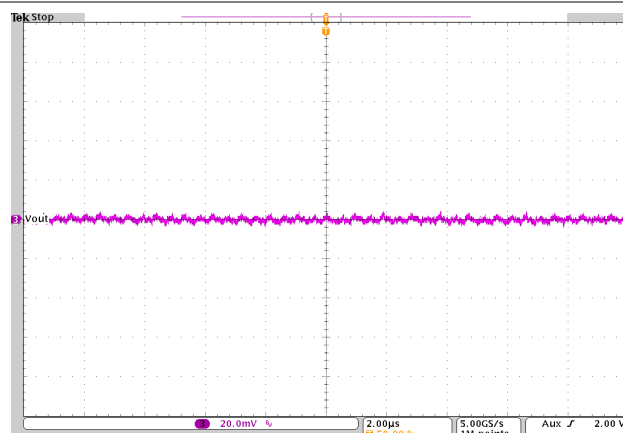
$V_{OUT} = 3.3\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 5.0\text{ V}$ BW = 20 MHz

Figure 10-43. Output Voltage Ripple



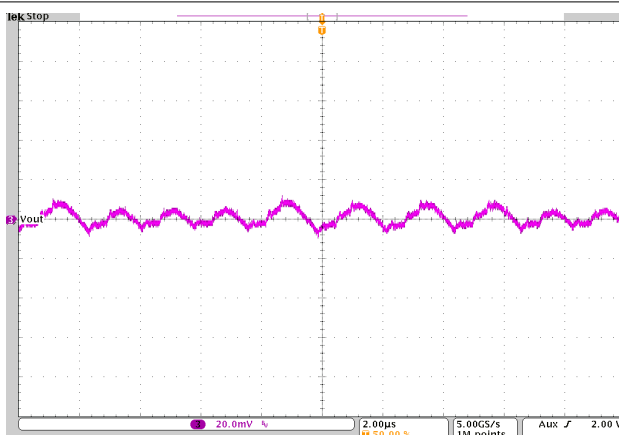
$V_{OUT} = 1.8\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.5\text{ A}$ $V_{IN} = 5.0\text{ V}$ BW = 20 MHz

Figure 10-44. Output Voltage Ripple



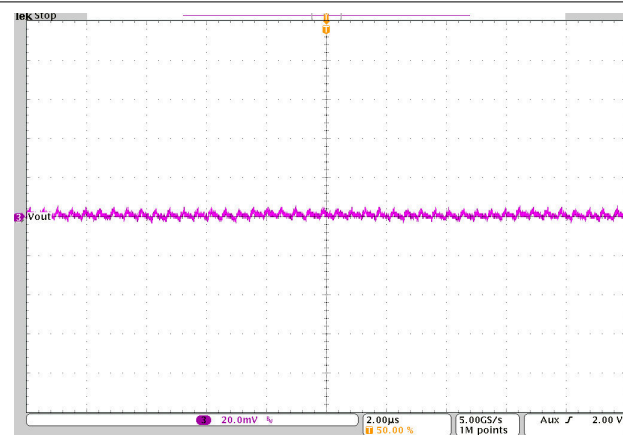
$V_{OUT} = 1.8\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 5.0\text{ V}$ BW = 20 MHz

Figure 10-45. Output Voltage Ripple



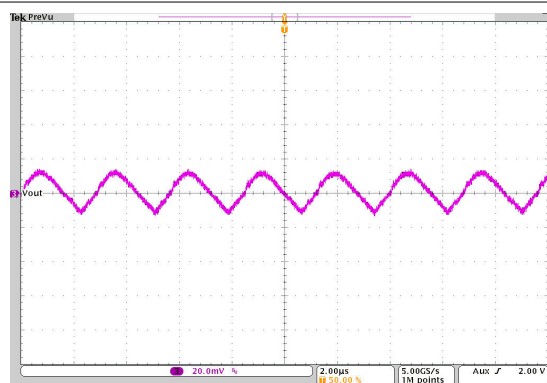
$V_{OUT} = 1.2\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.5\text{ A}$ $V_{IN} = 5.0\text{ V}$ BW = 20 MHz

Figure 10-46. Output Voltage Ripple



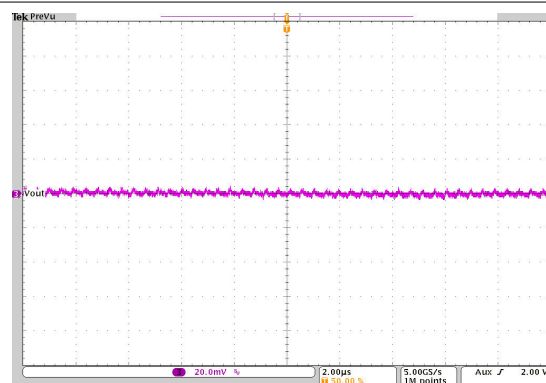
$V_{OUT} = 1.2\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 5.0\text{ V}$ BW = 20 MHz

Figure 10-47. Output Voltage Ripple



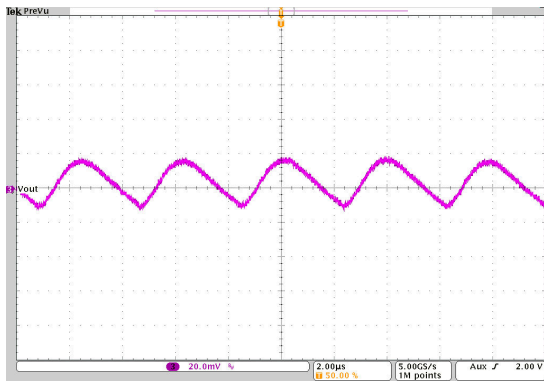
$V_{OUT} = 1.0\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.5\text{ A}$ $V_{IN} = 5.0\text{ V}$ BW = 20 MHz

Figure 10-48. Output Voltage Ripple



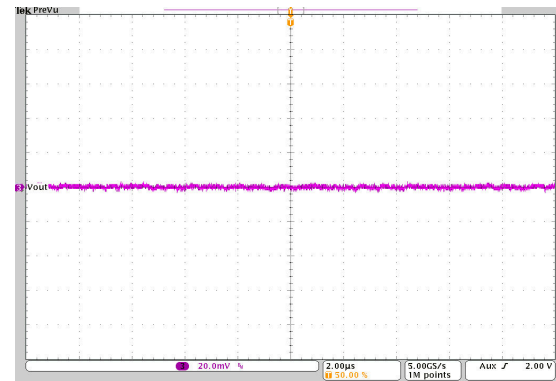
$V_{OUT} = 1.0\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 5.0\text{ V}$ BW = 20 MHz

Figure 10-49. Output Voltage Ripple



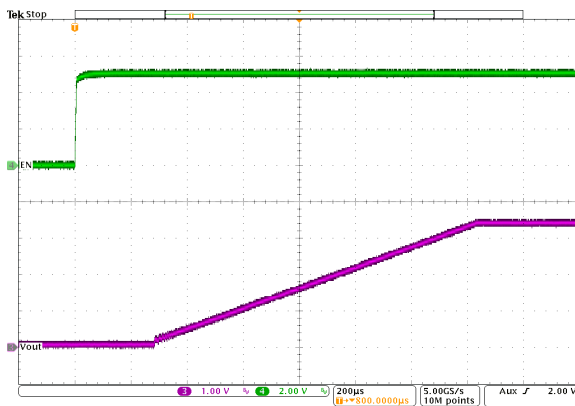
$V_{OUT} = 0.6\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.5\text{ A}$ $V_{IN} = 3.3\text{ V}$ BW = 20 MHz

Figure 10-50. Output Voltage Ripple



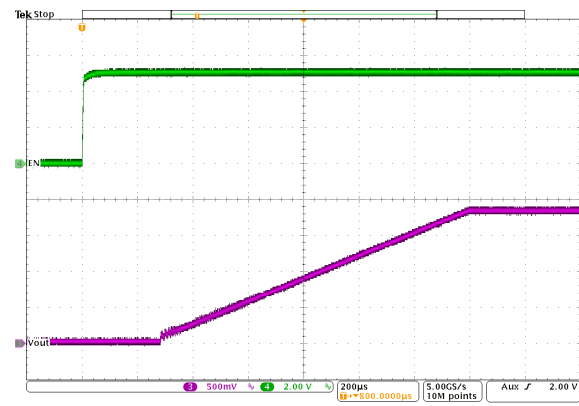
$V_{OUT} = 0.6\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 3.3\text{ V}$ BW = 20 MHz

Figure 10-51. Output Voltage Ripple



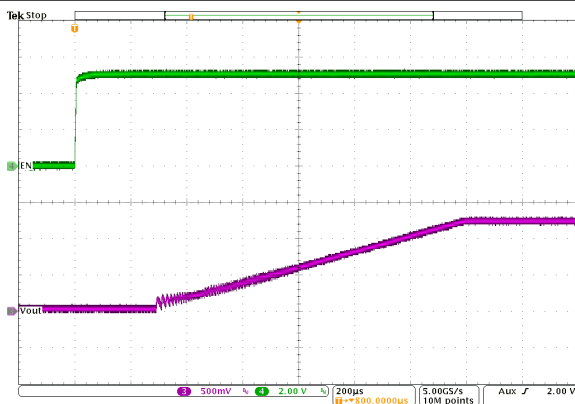
$V_{OUT} = 3.3\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 5\text{ V}$ $C_{SS} = 4.7\text{ nF}$

Figure 10-52. Start-Up Timing



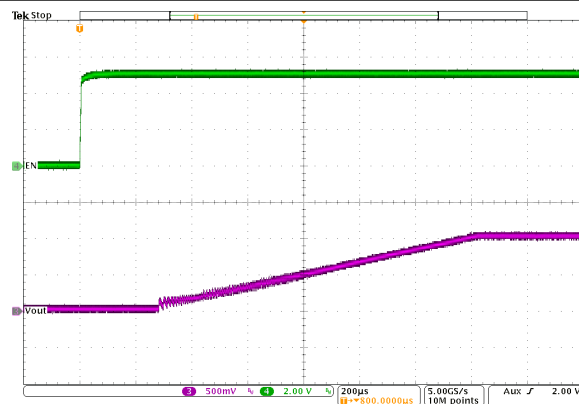
$V_{OUT} = 1.8\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 5\text{ V}$ $C_{SS} = 4.7\text{ nF}$

Figure 10-53. Start-Up Timing



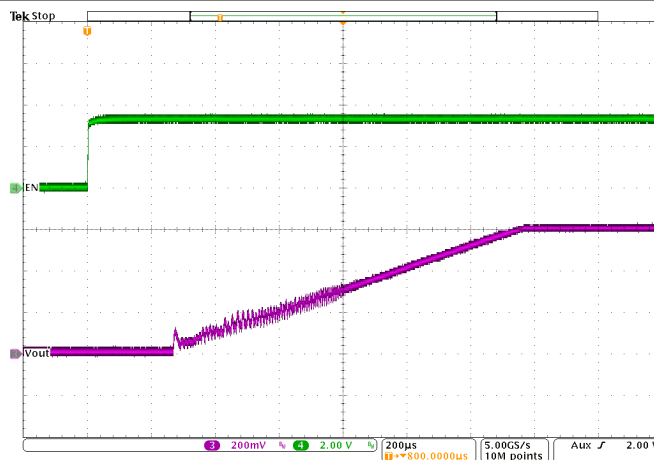
$V_{OUT} = 1.2\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 5\text{ V}$ $C_{SS} = 4.7\text{ nF}$

Figure 10-54. Start-Up Timing



$V_{OUT} = 1.0\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 5\text{ V}$ $C_{SS} = 4.7\text{ nF}$

Figure 10-55. Start-Up Timing



$V_{OUT} = 0.6\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 4\text{ A}$ $V_{IN} = 3.3\text{ V}$ $C_{SS} = 4.7\text{ nF}$

Figure 10-56. Start-Up Timing

10.3 System Examples

10.3.1 Voltage Tracking

The TPS6281xM device follows the voltage applied to the SS/TR pin. A voltage ramp on SS/TR to 0.6 V ramps the output voltage according to the 0.6-V feedback voltage.

Tracking the 3.3 V of device 1, such that both rails reach their target voltage at the same time, requires a resistor divider on SS/TR of device 2 equal to the output voltage divider of device 1. The output current of 2.5 μ A on the SS/TR pin causes an offset voltage on the resistor divider formed by R_5 and R_6 . The equivalent resistance of $R_5 \parallel R_6$, so it must be kept below 15 k Ω . The current from SS/TR causes a slightly higher voltage across R_6 than 0.6 V, which is desired because device 2 switches to its internal reference as soon as the voltage at SS/TR is higher than 0.6 V.

In case both devices need to run in forced PWM mode, it is recommended to tie the MODE pin of device 2 to the output voltage or the power good signal of device 1, the main device. The TPS6281xM device has a duty cycle limitation defined by the minimum on time. For tracking down to low output voltages, device 2 cannot follow once the minimum duty cycle is reached. Enabling PFM mode while tracking is in progress allows the user to ramp down the output voltage close to 0 V.

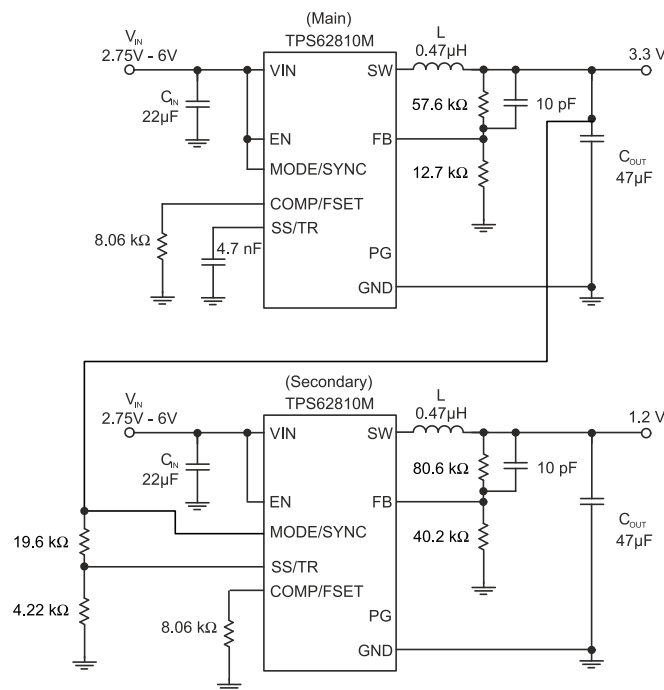


Figure 10-57. Schematic for Output Voltage Tracking

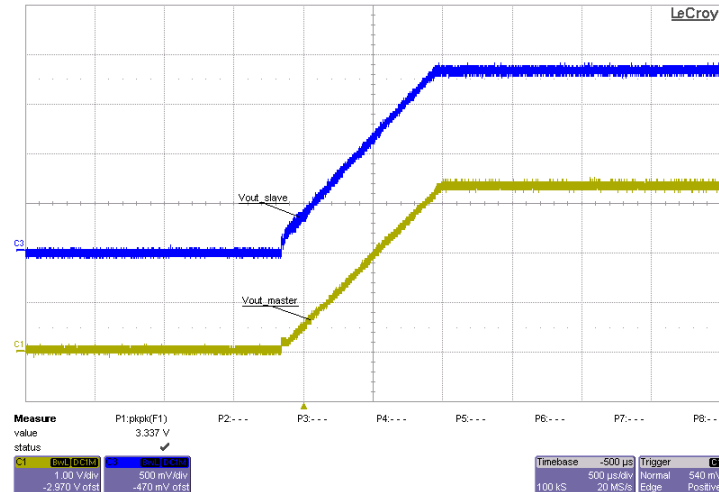


Figure 10-58. Scope Plot for Output Voltage Tracking

10.3.2 Synchronizing to an External Clock

The TPS6281xM device can be externally synchronized by applying an external clock on the MODE/SYNC pin. There is no need for any additional circuitry as long as the input signal meets the requirements given in the electrical specifications. The clock can be applied or removed during operation, letting the user switch from an externally defined fixed frequency to power save mode or to an internally fixed-frequency operation. The value of the R_{CF} resistor must be chosen so that the internally defined frequency and the externally applied frequency are close to each other. This ensures a smooth transition from internal to external frequency and vice versa.

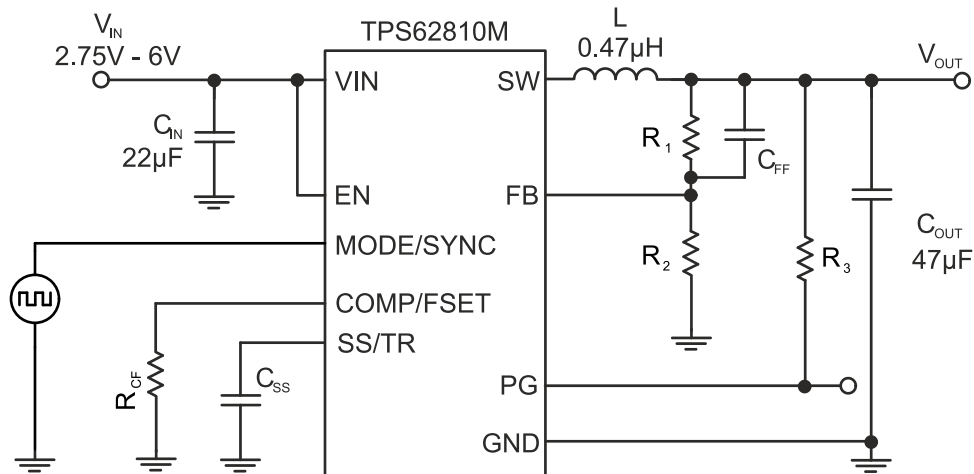
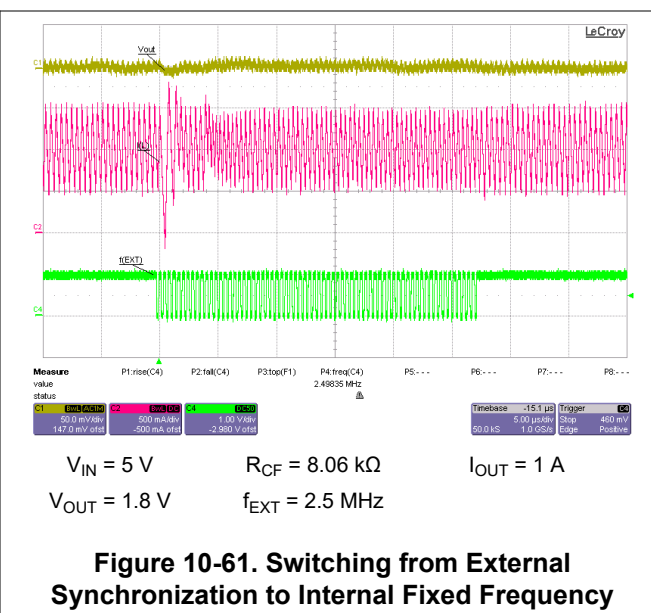
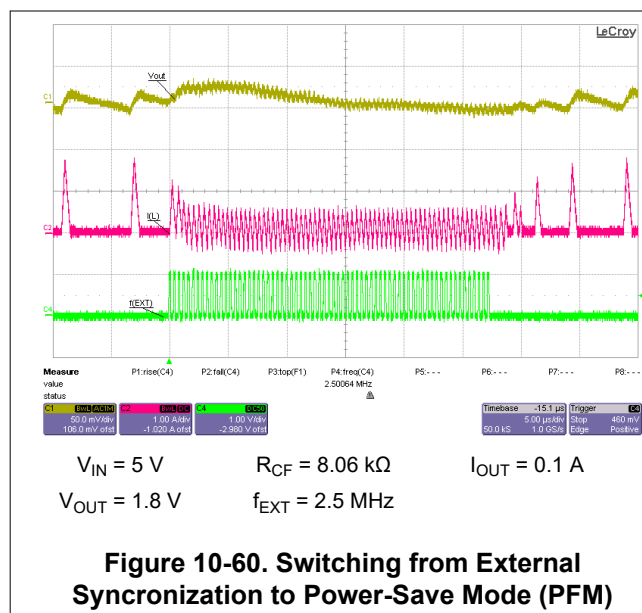


Figure 10-59. Schematic Using External Synchronization



11 Power Supply Recommendations

The TPS6281xM device family has no special requirements for its input power supply. The output current of the input power supply needs to be rated according to the supply voltage, output voltage, and output current of the TPS6281xM device.

12 Layout

12.1 Layout Guidelines

A proper layout is critical for the operation of a switched mode power supply, even more so at high switching frequencies. Therefore, the PCB layout of the TPS6281xM device demands careful attention to ensure operation and to get the specified performance. A poor layout can lead to issues like poor regulation (both line and load), stability, and accuracy weaknesses increased like EMI radiation and noise sensitivity.

See [Section 12.2](#) for the recommended layout of the TPS6281xM device, which is designed for common external ground connections. The input capacitor must be placed as close as possible between the VIN and GND pin.

Provide low inductive and resistive paths for loops with high di/dt. Therefore, paths conducting the switched load current must be as short and wide as possible. Provide low capacitive paths (with respect to all other nodes) for wires with high dv/dt. Therefore, the input and output capacitance must be placed as close as possible to the IC pins and parallel wiring over long distances as well as narrow traces must be avoided. Loops that conduct an alternating current must outline an area as small as possible, as this area is proportional to the energy radiated.

Sensitive nodes like FB need to be connected with short wires and not nearby high dv/dt signals (for example SW). Since they carry information about the output voltage, they must be connected as close as possible to the actual output voltage (at the output capacitor). The capacitor on the SS/TR pin as well as the FB resistors, R_1 and R_2 , must be kept close to the IC and connect directly to those pins and the system ground plane.

The package uses the pins for power dissipation. Thermal vias on the VIN and GND pins help spread the heat into the PCB.

The recommended layout is implemented on the EVM and shown in the [TPS62810EVM-015 Evaluation Module User's Guide](#).

12.2 Layout Example

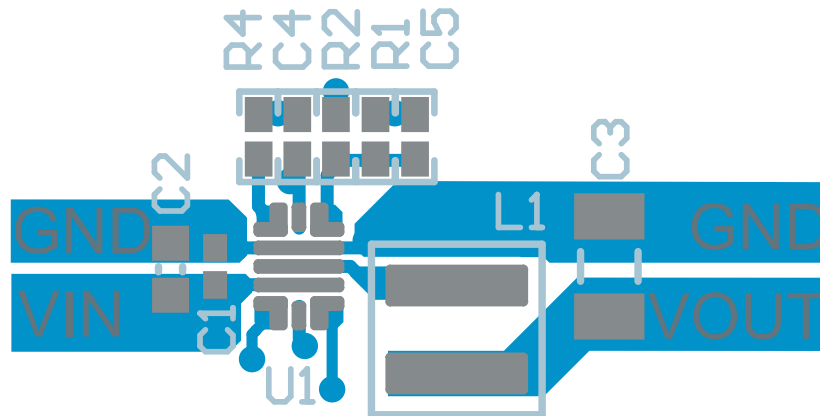


Figure 12-1. Example Layout

13 Device and Documentation Support

13.1 Device Support

13.1.1 Third-Party Products Disclaimer

TI'S PUBLICATION OF INFORMATION REGARDING THIRD-PARTY PRODUCTS OR SERVICES DOES NOT CONSTITUTE AN ENDORSEMENT REGARDING THE SUITABILITY OF SUCH PRODUCTS OR SERVICES OR A WARRANTY, REPRESENTATION OR ENDORSEMENT OF SUCH PRODUCTS OR SERVICES, EITHER ALONE OR IN COMBINATION WITH ANY TI PRODUCT OR SERVICE.

13.2 Documentation Support

13.2.1 Related Documentation

For related documentation see the following:

Texas Instruments, [TPS62810EVM-015 Evaluation Module](#), SLVUBG0

13.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on [ti.com](#). Click on *Subscribe to updates* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

13.4 Support Resources

[TI E2E™ support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

13.5 Trademarks

TI E2E™ is a trademark of Texas Instruments.

All trademarks are the property of their respective owners.

13.6 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

13.7 Glossary

[TI Glossary](#) This glossary lists and explains terms, acronyms, and definitions.

14 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package Pins	Package qty Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
TPS62810MWRWYR	Active	Production	VQFN-HR (RWY) 9	3000 LARGE T&R	Yes	SN	Level-2-260C-1 YEAR	-55 to 150	810M
TPS62811MWRWYR	Active	Production	VQFN-HR (RWY) 9	3000 LARGE T&R	Yes	SN	Level-2-260C-1 YEAR	-55 to 150	811M
TPS62812MWRWYR	Active	Production	VQFN-HR (RWY) 9	3000 LARGE T&R	Yes	SN	Level-2-260C-1 YEAR	-55 to 150	812M
TPS62813MWRWYR	Active	Production	VQFN-HR (RWY) 9	3000 LARGE T&R	Yes	SN	Level-2-260C-1 YEAR	-55 to 150	813M

⁽¹⁾ **Status:** For more details on status, see our [product life cycle](#).

⁽²⁾ **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

⁽³⁾ **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

⁽⁴⁾ **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

⁽⁵⁾ **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

⁽⁶⁾ **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

Important Information and Disclaimer: The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

TAPE AND REEL INFORMATION


*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS62810MWRWYR	VQFN-HR	RWY	9	3000	180.0	12.4	2.25	3.25	1.15	4.0	12.0	Q1
TPS62811MWRWYR	VQFN-HR	RWY	9	3000	180.0	12.4	2.25	3.25	1.15	4.0	12.0	Q1
TPS62812MWRWYR	VQFN-HR	RWY	9	3000	180.0	12.4	2.25	3.25	1.15	4.0	12.0	Q1
TPS62813MWRWYR	VQFN-HR	RWY	9	3000	180.0	12.4	2.25	3.25	1.15	4.0	12.0	Q1

TAPE AND REEL BOX DIMENSIONS



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS62810MWRWYR	VQFN-HR	RWY	9	3000	213.0	191.0	35.0
TPS62811MWRWYR	VQFN-HR	RWY	9	3000	213.0	191.0	35.0
TPS62812MWRWYR	VQFN-HR	RWY	9	3000	213.0	191.0	35.0
TPS62813MWRWYR	VQFN-HR	RWY	9	3000	213.0	191.0	35.0

GENERIC PACKAGE VIEW

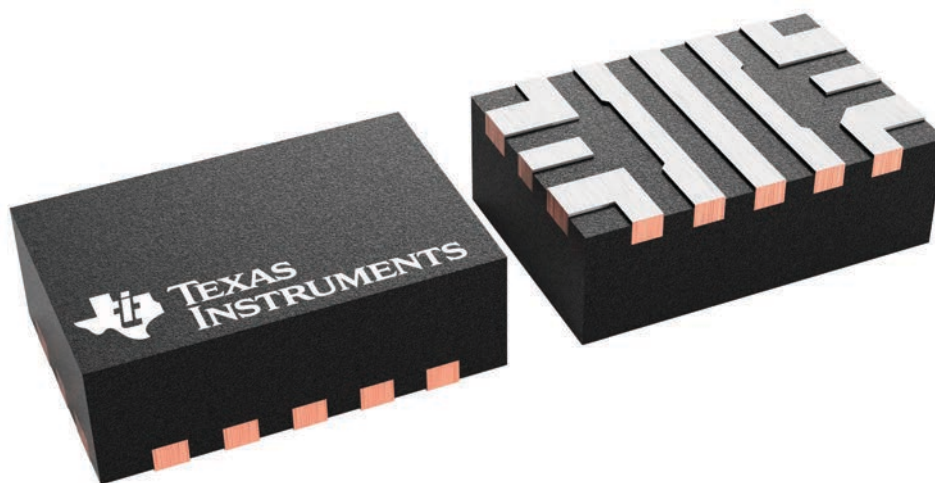
RWY 9

VQFN-HR - 1 mm max height

2 x 3, 0.5 mm pitch

PLASTIC QUAD FLATPACK - NO LEAD

This image is a representation of the package family, actual package may vary.
Refer to the product data sheet for package details.



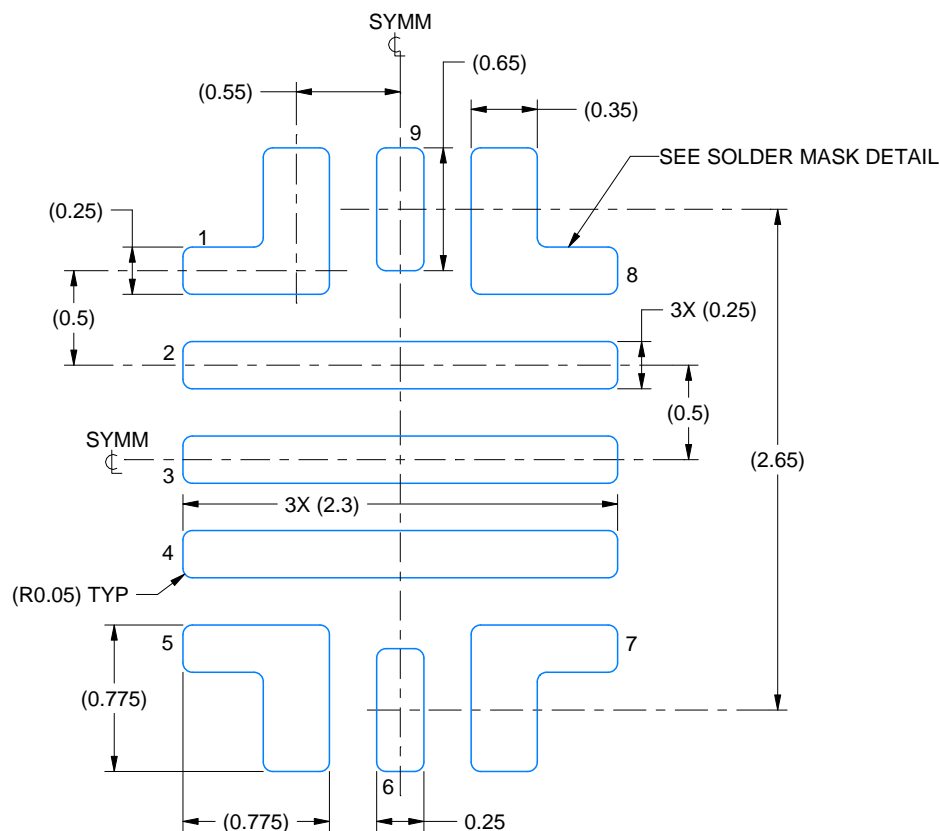
4226729/A

EXAMPLE BOARD LAYOUT

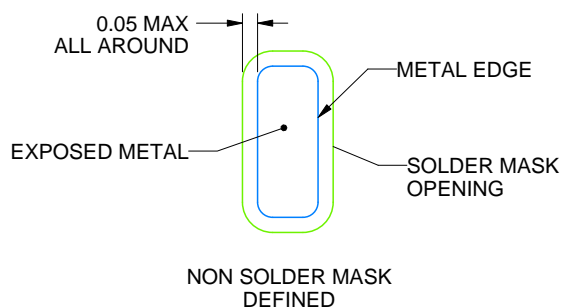
RWY0009A

VQFN-HR - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



LAND PATTERN EXAMPLE
EXPOSED METAL SHOWN
SCALE: 25X



SOLDER MASK DETAIL

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NOTES: (continued)

3. This package is designed to be soldered to thermal pads on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/sluea271).

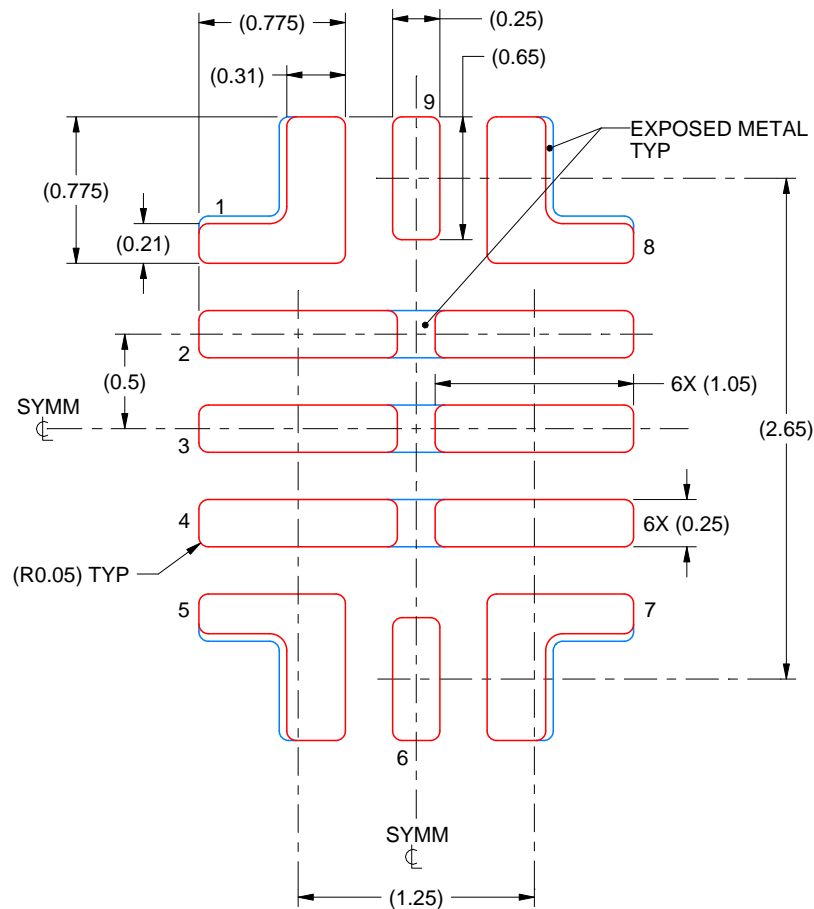
4. Vias are optional depending on application, refer to device data sheet. It is recommended that vias under paste be filled, plugged or tented.

EXAMPLE STENCIL DESIGN

RWY0009A

VQFN-HR - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



SOLDER PASTE EXAMPLE
BASED ON 0.1 mm THICK STENCIL
PADS 1, 5, 7 & 8:
90% PRINTED SOLDER COVERAGE BY AREA UNDER PACKAGE
SCALE: 25X

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NOTES: (continued)

5. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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