

TPS482H85-Q1 48V, 85mΩ Dual-Channel Smart High-Side Switch

1 Features

- · Qualified for automotive applications
- AEC-Q100 qualified with the following results:
 - Device temperature grade 1: –40°C to 125°C ambient operating temperature range
 - Device HBM ESD classification level H3A
 - Device CDM ESD classification level C4B
- · Functional safety capable
 - Documentation available to aid functional safety system design
- Dual-channel 85-m Ω smart high-side switch with full diagnostics
- Wide operating voltage 6 V to 58 V
- Ultra-low standby current, < 2 μA per channel
- High-accuracy current sense: ±15% under > 50mA load
- Selectable current limit levels with external resistor, ±15% accuracy at 2A load
- Protection
 - Short-to-GND Protection by current limit (internal or external)
 - Absolute and relative thermal shutdown
 - Inductive Load negative voltage clamp with optimized slew rate
 - Loss-of-GND and loss-of-battery protection
- Diagnostics
 - Overcurrent and short-to-ground detection
 - Open-Load and short-to-battery detection
 - Accurate current sense
- 3.5mm x 3mm small form factor 12-pin QFN package

- Automotive display module
- · Body control module

3 Description

The TPS4H82H85-Q1 device is fully protected dual-channel smart high-side switch with two integrated $85m\Omega$ NMOS power FETs intended for 24V and 48V automotive supply systems. Protection and diagnostic features include accurate current sense, selectable current limit levels, OFF-state open-load and short-to-battery detection and thermal shutdown.

High-accuracy current sensing provides a better realtime monitoring effect and more accurate diagnostics without further calibration. The external selectable-level high-accuracy current limit allows setting the current limit value by application. The device highly improves the reliability of the system by effectively clamping the inrush current under start-up or short-circuit conditions. The TPS4H82H85-Q1 device can be used as a high-side power switch for a wide variety of resistive, inductive, and capacitive loads, including low-wattage bulbs, LEDs, relays, solenoids, and heaters.

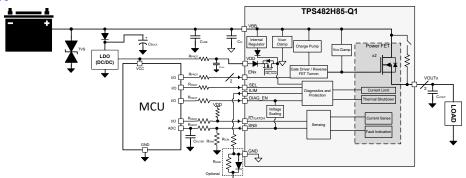
Package Information

PART NUMBER	PACKAGE ⁽¹⁾	PACKAGE SIZE ⁽²⁾
TPS482H85-Q1	CHU (VQFN-HR, 12)	3.5mm × 3mm

- For all available packages, see the orderable addendum at the end of the data sheet.
- (2) The package size (length × width) is a nominal value and includes pins, where applicable.

2 Applications

ADAS modules



Typical Application Schematic



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4 Device Comparison Table

PART NUMBER	UNIQUE PIN	NOTE	CLAMP STRUCTURE	VBB VOLTAGE TOLERANCE
TPS482H85A-Q1 ⁽¹⁾	LATCH	 User is able to configure the device behavior after a thermal fault - latch or auto-retry using the LATCH pin. Fault status can be reported through SNS pin. 	Bi-directional clamp for clamping both positive VBB or negative VOUT voltage.	Max 65V steady state. Max 100μs transient up to 80V.
TPS482H85B-Q1	open drain FLT pin, current- sense analog output	 User is able to read the global fault status through FLT pin. Device auto-retries after a thermal fault. 	Bi-directional clamp for clamping both positive VBB or negative VOUT voltage.	Max 65V steady state. Max 100μs transient up to 80V.
TPS482H85C-Q1 ⁽¹⁾	LATCH	User is able to configure the device behavior after a thermal fault - latch or auto-retry using the LATCH pin. Fault status can be reported through SNS pin.	Uni-directional clamp negative VOUT voltage from inductive discharge only.	Max 70V steady state. No transient beyond 70V.

⁽¹⁾ Device in preview. Please contact TI for more information.



5 Pin Configuration and Functions

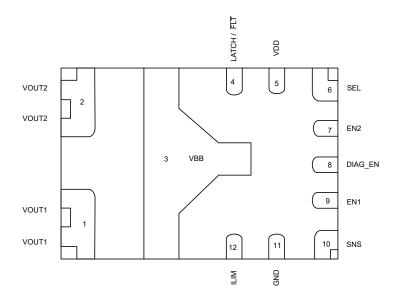


Figure 5-1. CHU Package 12-Pin VQFN-HR Top View

5.1 Pinout

See Applications Section for full list of recommended components

Pin Number	Pin Name (Ver. A/ Ver. C)	Pin Name (Ver. B)	Туре	Description
1	VOUT1	VOUT1	0	Channel 1 output.
2	VOUT2	VOUT2	0	Channel 2 output.
3	VBB	VBB	POWER	Input power supply.
4	LATCH	FLT	I for LATCH O for FLT	LATCH: High to latch OFF device after thermal shutdown; low to auto-retry. Internally pulled down. FLT: Open drain global fault pin.
5	VDD	VDD	POWER	Low voltage supply input. Float to enable the internal regulator.
6	SEL	SEL	I	Selects the channel for fault and current sense output on the SNS pin. Low to select channel 1; high to select channel 2. Internally pulled down.
7	EN2	EN2	I	Enable signal for channel 2. Internally pulled down.
8	DIAG_EN	DIAG_EN	I	High to enable ON state current sense and fault reporting through SNS pin, and OFF-state open load detection. Low to disable the diagnostics. Internally pulled down.
9	EN1	EN1	I	Enable signal for channel 1. Internally pulled down.
10	SNS	SNS	0	Output corresponding sense value based on sense ratio; also shows fault status by going high.
11	GND	GND	GND	Ground of device. Connect to resistor and diode ground network to have reverse battery protection.



See Applications Section for full list of recommended components

Pin Number	Pin Name (Ver. A/ Ver. C)	Pin Name (Ver. B)	Туре	Description
12	ILIM	ILIM	o	Adjustable current limit. Select the current limit level by connect the resistor from ILIM pin to IC GND pin. Leave the pin floating or short the pin to IC GND for two additional levels.



6 Specifications

6.1 Absolute Maximum Ratings

Over operating free-air temperature range (unless otherwise noted)(1)

		MIN	MAX	UNIT
Maximum continuous supply voltage, V _{BB} (Version A, B)	Maximum continuous supply voltage, V _{BB}		65	V
VBB Transient pulse, overvoltage voltage (Version A, B)	Max 100 µs duration		80	V
Maximum continuous supply voltage, V _{BB} (Version C)	Maximum continuous supply voltage, V _{BB}		70	V
Maximum continuous supply voltage, V _{DD}			7	V
Enable pin current, I _{ENx}	Enable pin current, I _{EN}	-1	20	mA
Enable pin voltage, V _{ENx}		-1	7	V
Diagnostic Enable pin current, I _{DIA_EN}		– 1	20	mA
Diagnostic Enable pin voltage, V _{DIA_EN}		-1	7	V
Ver A LATCH pin voltage, V _{LATCH}	LATCH pin voltage, V _{LATCH}	-1	7	V
LATCH pin current, I _{LATCH}	LATCH pin current, I _{LATCH}	-1	20	mA
SEL pin voltage, V _{SEL}	SEL pin voltage, V _{SEL}	-1	7	V
SEL pin current, I _{SEL}	SEL pin current, I _{SEL}	-1	20	mA
Sense pin current, I _{SNS}		-100	10	mA
Sense pin voltage, V _{SNS}		-1	5.5	V
FLT pin current, I _{FLT}		-30	10	mA
FLT pin voltage, V _{FLT}		-0.3	70	V
Reverse ground current, I _{GND}	V _{BB} < 0 V, Max 2ms negative supply transient		-50	mA
Storage temperature, T _{stg}		-65	150	°C

⁽¹⁾ Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

6.2 ESD Ratings

				VALUE	UNIT
V _(ESD) Electrostatic discharge ⁽¹⁾ Classification Level 2 ⁽²⁾	Human-body model (HBM), per AEC Q100-002	All pins except VBB and VOUT	±2000		
	Classification Level 2	VBB and VOUT	±4000	V	
	Charged-device model (CDM), per AEC Q100-011 Classification Level C5	All pins	±750		

- (1) All ESD strikes are with reference from the pin mentioned to GND
- (2) AEC-Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specifications.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)(1)

			MIN	MAX	UNIT
V _{VDD_NOM}	Nominal supply voltage	Nominal supply voltage	4.5	5.5	V
V _{VBB_NOM}	Nominal supply voltage		6	58	V
V _{VBB_SC}	Short circuit supply voltage capability			58	V
V _{ENx}	Enable voltage		-1	5.5	V
V _{DIA_EN}	Diagnostic Enable voltage		-1	5.5	V
V _{SEL}	Select voltage		-1	5.5	V
V _{SNS}	Sense voltage		-1	5.5	V



over operating free-air temperature range (unless otherwise noted)(1)

		MIN	MAX	UNIT
T _A	Operating free-air temperature	-40	125	°C

(1) All operating voltage conditions are measured with respect to device GND

6.4 Thermal Information

	THERMAL METRIC ⁽¹⁾ (2)	TPS482Hxx-Q1 Hotrod QFN	UNIT
R _{0JA}	Junction-to-ambient thermal resistance	72.8	°C/W
R _{0JC(top)}	Junction-to-case (top) thermal resistance	39.2	°C/W
R _{0JB}	Junction-to-board thermal resistance	19.3	°C/W
ΨЈТ	Junction-to-top characterization parameter	5.2	°C/W
ΨЈВ	Junction-to-board characterization parameter	19.2	°C/W
R _{0JC(bot)}	Junction-to-case (bottom) thermal resistance	16.8	°C/W

- (1) For more information about traditional and new thermal metrics, see the SPRA953 application report.
- (2) The thermal parameters are based on a 4-layer PCB according to the JESD51-5 and JESD51-7 standards.

6.5 Electrical Characteristics

 V_{BB} = 8 V to 58 V, T_A = -40°C to 150°C (unless otherwise noted)

	PARAMETER	TEST CO	NDITIONS	MIN	TYP	MAX	UNIT
INPUT VOL	TAGE AND CURRENT						
V _{Clamp}	VDS clamp voltage	VBB = 8V, Ids = 1A	$T_J = -40^{\circ}\text{C} \text{ to } 150^{\circ}\text{C}$			68	V
V _{Clamp}	VDS clamp voltage	VBB = 48V, Ids = 1A	$T_J = -40^{\circ}\text{C} \text{ to } 150^{\circ}\text{C}$	58		75	V
V _{UVLOR}	V _{BB} undervoltage lockout rising (not indicated on FLT or SNS pin)	Magaurad with respect to	the CND pin of the device	6.0	6.3	6.6	V
V _{UVLOF}	V _{BB} undervoltage lockout falling (not indicated on FLT or SNS pin)	ineasured with respect to	Measured with respect to the GND pin of the device —		5.6	5.9	V
	Standby current (total		T _J = 25°C			2	μΑ
I _{SLEEP}	device leakage including	$V_{BB} \le 54V$, $V_{EN} = V_{DIA_EN}$ = 0V, $V_{OUT} = 0V$	T _J = 85°C			4	μA
	both MOSFET channels)	21,1001	T _J = 125°C			10	μΑ
1	Output leakage current	V _{BB} ≤ 54V, V _{EN} = V _{DIA EN}	T _J = 25°C		0.01	0.3	μΑ
I _{OUT(standby)}	per channel	= 0V, V _{OUT} = 0V	T _J = 85°C			8.0	μΑ
I _{DIA}	Current consumption in diagnostic mode, channels OFF		ISNS = 0 mA, VDD floating VEN = 0V, VDIA_EN = 5V, VOUT = 0V		1.2	1.5	mA
I _{DIA}	Current consumption in diagnostic mode, channels OFF	I _{SNS} = 0mA, VDD = 5V V _{EN} = 0V, V _{DIA_EN} = 5V, V ₀	_{DUT} = 0V		0.5	0.8	mA
I _{Q_1CH,DIAG}	Quiescent current one channel enabled with external VDD	ISNS = 0 mA, VOUT floating, VDD =5V, VEN1 = 5V, VDIA_EN = 5V	ISNS = 0 mA, VOUT floating, VDD =5V, VEN1 = 5V, VDIA_EN = 5V		1.4	1.6	mA
I _{Q_1CH,DIAG}	Quiescent current one channel enabled with internal VDD	ISNS = 0mA, VOUT floating, VDD floating, VEN1 = 5V, VDIA_EN = 5V	ISNS = 0mA, VOUT floating, VDD floating, VEN1 = 5V, VDIA_EN = 5V		1.4	1.6	mA
I _{Q,DIAG}	Quiescent current both channels enabled, diagnostic enabled	V _{EN} = V _{DIA_EN} = 5V, I _{OUT} = 0A VDD = 5V	V _{EN} = V _{DIA_EN} = 5 V, I _{OUT} = 0 A VDD = 5V		0.8	1	mA



 V_{BB} = 8 V to 58 V, T_{A} = -40°C to 150°C (unless otherwise noted)

	PARAMETER	TEST CO	NDITIONS	MIN	TYP	MAX	UNIT
$I_{Q,DIAG}$	Quiescent current both channels enabled, diagnostic enabled	V _{EN} = V _{DIA_EN} = 5V, I _{OUT} = 0A VDD not connected	V _{EN} = V _{DIA_EN} = 5 V, I _{OUT} = 0 A VDD not connected		1.7	2	mA
I _{Q, VDD}	VDD Quiescent current when both channels enabled, diagnostic enabled	V _{EN} = V _{DIA_EN} = 5 V, I _{OUT}	= 0 A VDD = 5V		TBD		mA
RON CHAP	RACTERISTICS		,			'	
R _{ON}	On-resistance per channel	8 V ≤ V _{BB} ≤ 54 V, I _{OUT} = 1 A	T _J = 25°C		76		mΩ
R _{ON}	On-resistance per channel	8 V ≤ V _{BB} ≤ 54 V, I _{OUT} = 1 A	T _J = 150°C			165	mΩ
R _{ON_par}	2-channels Paralleled On-resistance	8 V ≤ V _{BB} ≤ 54 V, I _{OUT} = 1 A	T _J = 25°C		38		mΩ
R _{ON_par}	2-channels Paralleled On-resistance	8 V ≤ V _{BB} ≤ 54 V, I _{OUT} = 1 A	T _J = 150°C			82	mΩ
R _{ON}	Reverse Polarity On- resistance	-28 V ≤ V _{BB} ≤ -8 V, I _{OUT} = 1 A, EN2 = 0V	T _J = 25°C		85		mΩ
R _{ON}	Reverse Polarity On- resistance	-28 V ≤ V _{BB} ≤ -8 V, I _{OUT} = 1 A, EN2 = 0V	T _J = 150°C			174	mΩ
ΔR _{ON}	Delta On-resistance between channels	8 V ≤ V _{BB} ≤ 28 V, I _{OUT} = 1 A	T _J = -40°C to 150°C			5	%
IL _{NOM}	Continuous load current, per channel	Two channels enabled, T _{AMB} = 85°C	Two channels enabled, T _{AMB} = 85°C		2.2		Α
IL _{NOM}	Continuous load current, per channel	One channel enabled, T _{Al}	_{MB} = 85°C		3.2		Α
CURRENT	SENSE CHARACTERISTIC	CS		·			
K _{SNS}	Current sense ratio	I _{OUT} = 1A			2000		
I _{SNS_SAT}	Saturated sense current (Current clamp setting)			4	4.5		mA
I _{SNSI}	Current sense current	$V_{EN} = V_{DIA_EN} = 5 V$	I _{OUT} = 4 A		2		mA
I _{SNSI}	Current sense current	$V_{EN} = V_{DIA_EN} = 5 V$	I _{OUT} = 2 A		1		mA
I _{SNSI}	Current sense current	V _{EN} = V _{DIA_EN} = 5 V	I _{OUT} = 1 A		0.5		mA
I _{SNSI}	Current sense current	V _{EN} = V _{DIA_EN} = 5 V	I _{OUT} = 500 mA		0.25		mA
I _{SNSI}	Current sense current	V _{EN} = V _{DIA_EN} = 5 V	I _{OUT} = 200 mA		0.1		mA
I _{SNSI}	Current sense current	V _{EN} = V _{DIA_EN} = 5 V	I _{OUT} = 100 mA		0.05		mA
I _{SNSI}	Current sense current	V _{EN} = V _{DIA_EN} = 5 V	I _{OUT} = 50 mA		0.025		mA
I _{SNSI}	Current sense current	V _{EN} = V _{DIA_EN} = 5 V	I _{OUT} = 10 mA		0.005		mA
SNS CHAR	ACTERISTICS					'	
V _{SNSFH}	V _{SNS} fault high-level	V _{DIA_EN} = 5V	V _{DIA_EN} = 5V	4.5	5.0	5.77	V
V _{SNSFH}	V _{SNS} fault high-level	V _{DIA_EN} = 3.3 V, V _{DIA_EN} > V _{IH,DIAG_EN}	V _{DIA_EN} = 3.3 V, V _{DIA_EN} > V _{IH,DIAG_EN}	3.0	3.3	3.82	V
I _{SNSFH_max}	I _{SNS} fault high-level	V _{DIA_EN} > V _{IH,DIAG_EN}		4.5		4.8	mA
	I _{SNS} leakage with no load		T _A = 25°C			5	μA
SNSleak	current	$V_{DIA_EN} = 5 \text{ V, IL} = 0 \text{ mA}$	T _A = 125°C			5	μΑ
V _{BB_ISNS}	V _{BB} headroom needed for full current sense and fault functionality	V _{DIAG_EN} = 3.3 V		6			٧

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 V_{BB} = 8 V to 58 V, T_A = -40°C to 150°C (unless otherwise noted)

	PARAMETER	TEST CO	MIN	TYP	MAX	UNIT	
V_{BB_ISNS}	V _{BB} headroom needed for full current sense and fault functionality	V _{DIAG_EN} = 5 V	6.5			٧	
CURRENT	LIMIT CHARACTERISTICS	3					
R _{ILIM,SHORT}	RLIM Short Circuit Detection Range					1	kΩ
R _{ILIM,OPEN}	RLIM Open Detection Range			70			kΩ
			R _{ILIM} = Open	8.8	10	10.5	Α
			R _{ILIM} = Short	8.1	9	9.7	Α
			R _{ILIM} = 2.74 kΩ	7.3	8	8.6	Α
		Regulated current at	R _{ILIM} = 6.65 kΩ	6.4	7	7.5	Α
	CHx I _{CL} Current limit	short circuit R _L < 200	R _{ILIM} = 11.5 kΩ	5.4	6	6.5	Α
I _{CLx}	regulation level	mΩ when Enabled. $T_J = -40$ °C to 150°C	R _{ILIM} = 18.7 kΩ	4.6	5	5.4	Α
			R _{ILIM} = 26.1 kΩ	3.7	4	4.4	Α
			R _{ILIM} = 34.8 kΩ	2.8	3	3.3	Α
			R _{ILIM} = 45.3 kΩ	1.8	2	2.2	Α
			$R_{ILIM} = 59 \text{ k}\Omega$	0.8	1	1.1	Α
I _{CLx_LINPK}	CHx I _{CL} current limit threshold before current limiting - overload condition. Ratio to the regulated current limit level.	dl/dt<0.01A/ms. T _J = – 40°C to 150°C	all R _{ILIM}		1	.25 x I _{CL}	
I _{ENPS}	Peak current enabling into permanent short. Ratio to the regulated current limit level.	$Z_L = 100 \text{ m}\Omega + 1.4 \mu\text{H. T}_J$ = -40°C to 150°C	I _{ILIM} < 3A			1.8 x I _{CL}	
I _{ENPS}	Peak current enabling into permanent short. Ratio to the regulated current limit level.	$Z_L = 100 \text{ m}\Omega + 1.4 \mu\text{H. T}_J$ = -40°C to 150°C	I _{ILIM} >= 3A			1.5 x I _{CL}	
I _{OVCR}	OVCR Peak current threshold when short is applied while switch enabled	$Z_L = 100 \text{ m}\Omega + 1.4 \mu\text{H. T}_J$ = -40°C to 150°C	all R _{ILIM}			40	А
FAULT CHA	RACTERISTICS					'	
V _{OL}	Open-load detection voltage (VDS voltage)	V _{EN} = 0 V, V _{DIA_EN} = 5 V, r	neasure VDS voltage	1.7	2.0	2.3	٧
V _{OL_HYS}	Open-load detection voltage (VDS voltage) comparator hysteresis	V _{EN} = 0 V, V _{DIA_EN} = 5 V,	V _{EN} = 0 V, V _{DIA_EN} = 5 V,		360		mV
R _{VOL}	Open-load detection internal pull-up resistor per channel	V _{EN} = 0 V, V _{DIA_EN} = 5 V		260	315	360	kΩ
t _{OL_OFF}	Open-load indication-time from EN falling	$V_{EN} = 5 \text{ V to } 0 \text{ V}, V_{DIA_EN} = 5 \text{ V}$ $I_{OUT} = 0 \text{ mA}, V_{OUT} = \overline{V}_{BB} - V_{OL}$			350		μs
t _{OL_OFF1}	Open-load detection deglitch time	$V_{EN} = 0 \text{ V}, V_{DIA_EN} = 5 \text{ V}, V_{DIA_EN}$ duration longer than t_{OL} .	When V _{BB} – V _{OUT} < V _{OL} , Open load detected.			1.6	ms
t _{OL_OFF2}	Open-load indication-time from DIA_EN rising	$V_{EN} = 0 \text{ V}, V_{DIA_EN} = 0 \text{ V to}$ $I_{OUT} = 0 \text{ mA}, V_{OUT} = V_{BB} - 0 \text{ V to}$	o 5 V			1.6	ms
T _{ABS}	Thermal shutdown	, , , , , , , , , , , , , , , , , , , ,			169		°C



 V_{BB} = 8 V to 58 V, T_A = -40°C to 150°C (unless otherwise noted)

	PARAMETER	TEST	CONDITIONS	MIN	TYP	MAX	UNIT
T _{REL}	Relative thermal shutdown				60		°C
T _{HYS_ABS}	Thermal shutdown hysteresis				20		°C
t _{FAULT_FLT}	Fault indication-time, Ver B	V _{DIA_EN} = 5 V Time between fault ar	nd FLT asserting			60	μs
t _{FAULT_SNS}	Fault indication-time through SNS pin	V _{DIA_EN} = 5 V Time between fault ar	nd I _{SNS} settling at V _{SNSFH}			60	μs
t _{RETRY}	Retry time	Time from fault shutde (thermal shutdown).	own until switch re-enable	1	2	3	ms
EN PIN CH	ARACTERISTICS						
V _{IL, ENx}	Input voltage low-level	Relative to IC GND				0.8	V
V _{IH, ENx}	Input voltage high-level	Relative to IC GND		1.8			V
V _{IHYS, ENx}	Input voltage hysteresis				280		mV
R _{ENx}	Internal pulldown resistor	V _{EN} = 0.8 V		700	1000	1400	kΩ
I _{IL, ENx}	Input current low-level	V _{EN} = 0.8 V				4	μA
I _{IH, ENx}	Input current high-level	V _{EN} = 5 V				20	μA
DIA_EN PI	N CHARACTERISTICS						
V _{IL, DIA_EN}	Input voltage low-level					0.8	V
V _{IH, DIA_EN}	Input voltage high-level			1.5			V
V _{IHYS} ,	Input voltage hysteresis						mV
R _{DIA_EN}	Internal pulldown resistor	V _{DIA_EN} = 0.8 V		600	1000	1300	kΩ
I _{IL_DIA_EN}	Input current low-level	V _{DIA_EN} = -1 V		-10		0	μA
I _{IL, DIA_EN}	Input current low-level	V _{DIA EN} = 0.8 V				4	μA
I _{IH, DIA_EN}	Input current high-level	V _{DIA_EN} = 5 V				20	μA
	HARACTERISTICS	_					
V _{IL, SEL}	Input voltage low-level					0.8	V
V _{IH, SEL}	Input voltage high-level			1.5			V
V _{IHYS, SEL}	Input voltage hysteresis			150	280	400	mV
R _{SEL}	Internal pulldown resistor	V _{SEL} = 0.8 V	V _{DIA EN} = 0.8 V	700	1000	1300	kΩ
I _{IL, SEL}	Input current low-level	V _{SEL} = 0.8 V	V _{DIA_EN} = 0.8 V			1.1	μA
I _{IH, SEL}	Input current high-level	V _{SEL} = 5V	V _{DIA_EN} = 5 V			7	μA
	CHARACTERISTICS	ı				I	
V _{IH, LATCH}	Input voltage high-level			1.5			V
V _{IL, LATCH}	Input voltage low-level					0.8	V
I _{IL,LATCH}	Input current low-level	V _{LATCH} = 0.8 V	V _{DIA_EN} = 0.8 V			1.8	μA
I _{IH,LATCH}	Input current high-level	V _{LATCH} = 5V	V _{DIA EN} = 5 V			10	μA
V _{IHYS,LATCH}	-		_	150	280	400	mV
R _{LATCH}	Internal pulldown resistor	V _{LATCH} = 0.8 V	V _{DIA_EN} = 0.8 V	400	500	600	kΩ

6.6 SNS Timing Characteristics

 V_{BB} = 6 V to 18 V, T_{J} = -40°C to +150°C (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
SNS TIMING - CURRENT SENSE					



 V_{BB} = 6 V to 18 V, T_{J} = -40°C to +150°C (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
t	Settling time from rising edge of DIA_EN	V_{ENx} = 5 V, V_{DIA_EN} = 0 V to 5 V R _{SNS} = 1 k Ω , I _L = 0.32A			12	μs
t _{SNSION1}	50% of V _{DIA_EN} to 90% of settled ISNS	$V_{EN} = 5 \text{ V}, V_{DIA_EN} = 0 \text{ V to } 5 \text{ V}$ $R_{SNS} = 1 \text{ k}\Omega, I_L = 16\text{mA}$			6	μs
t _{SNSION2}	Settling time from rising edge of EN and DIA_EN 50% of V _{DIA_EN} V _{EN} to 90% of settled ISNS	$V_{EN} = V_{DIA_EN} = 0 \text{ V to 5 V}$ VBB = 48 \overline{V} R _{SNS} = 1 k Ω , I _L = 0.32A			160	μs
t _{SNSION3}	Settling time from rising edge of EN with DIA_EN HI; 50% of V _{DIA_EN} V _{EN} to 90% of settled ISNS	$V_{EN} = 0 \text{ V to 5 V}, V_{DIA_EN} = 5 \text{ V VBB} = 48 \text{ V}$ $R_{SNS} = 1 \text{ k}\Omega, I_L = 0.32 \text{A}$			160	μs
t _{SNSIOFF}	Settling time from falling edge of DIA_EN; 50% of V _{DIA_EN} to 5% of settled ISNS	$V_{EN} = 5 \text{ V}, V_{DIA_EN} = 5 \text{ V to } 0 \text{ V VBB}$ = 48 V $R_{SNS} = 1 \text{ k}\Omega, I_L = 0.32 \text{A}$			6	μs
t _{SETTLEH}	Settling time from rising edge of load step	$V_{EN} = 5 \text{ V}, V_{DIA_EN} = 5 \text{ V}$ $R_{SNS} = 1 \text{ k}\Omega, I_L = 16\text{mA}$			3	μs
t _{SETTLEL}	Settling time from falling edge of load step	$V_{EN} = 5 \text{ V}, V_{DIA_EN} = 5 \text{ V}$ $R_{SNS} = 1 \text{ k}\Omega, I_L = 0.32 \text{A to } 16 \text{mA}$			4	μs
t _{MUX}	Settling time from switching from CHx to CHy	$V_{EN} = 5 \text{ V}, V_{DIA_EN} = 5 \text{ V}$ $R_{SNS} = 1 \text{ k}\Omega, \text{ SEL} = 0 \text{ V to } 5 \text{ V}$ CH1 = 0.48A, CH2 = 3.2A			14	μs
t _{MUX}	Settling time from switching from CHx to CHy	$V_{EN1} = 5 \text{ V}, V_{EN2} = 0 \text{ V}, V_{DIA_EN} = 5 \text{ V}$ $R_{SNS} = 1 \text{ k}\Omega, \text{ SEL} = 0 \text{ V} \text{ to } 5 \text{ V}$ CH1 = 0.48A, CH2 = V_{SNSFH}			10	μs

6.7 Switching Characteristics_24V

 $V_{BB} = 48V$, $T_J = -40$ °C to +150°C (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP MAX	UNIT
t _{DR}	Channel Turn-on delay time (from Standby)	V_{BB} = 24 V, R_L = 20 Ω 50% of EN to 20% of VOUT		100	μs
t _{DR}	Channel Turn-on delay time (from Active)	V_{BB} = 24 V, R_L = 20 Ω 50% of EN to 20% of VOUT		50	μs
t _{DF}	Channel Turn-off delay time	V_{BB} = 24 V, R_L = 20 Ω 50% of EN to 80% of VOUT		50	μs
SR _R	VOUT rising slew rate	V_{BB} = 24 V, 20% to 80% of V_{OUT} , R_L = 20 Ω	0.26	0.52	V/µs
SR _F	VOUT falling slew rate	ew rate $ \begin{array}{c} 80\% \text{ to } 20\% \text{ of V}_{\text{OUT}}, \\ R_{\text{L}} = 20 \ \Omega \end{array} \qquad \qquad 0.12 $		0.62	V/µs
f _{max}	Maximum PWM frequency		0.75		kHz
t _{ON}	Channel Turn-on time	V_{BB} = 24 V, R_L = 20 Ω 50% of EN to 80% of VOUT		140	μs
t _{OFF}	Channel Turn-off time	V_{BB} = 24 V, R_L = 20 Ω 50% of EN to 20% of VOUT		86	μs
		1-ms enable pulse V_{BB} = 24 V, R_{L} = 20 Ω	-15	20	μs
t _{ON} – t _{OFF} Turn-on and off matching		200-μs enable pulse in Active state, V_{BB} =24 V, R_L = 20 Ω	-40	40	μs
E _{ON}	Switching energy losses during turn- on	V _{BB} = 24 V, R _L = 50 Ω		0.15	mJ
E _{OFF}	Switching energy losses during turn-off	V _{BB} = 24 V, R _L = 50 Ω		0.15	mJ



6.8 Switching Characteristics_48V

 V_{BB} = 48V, T_J = -40°C to +150°C (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP MAX	UNIT
Channel Turn-on delay time (from Standby)	V_{BB} = 48 V, R_{L} = 20 Ω 50% of EN to 20% of VOUT		105	μs
Channel Turn-on delay time (from Active)	V_{BB} = 48 V, R_{L} = 20 Ω 50% of EN to 20% of VOUT		56	μs
Channel Turn-off delay time	V_{BB} = 48 V, R_{L} = 20 Ω 50% of EN to 80% of VOUT		65	μs
VOUT rising slew rate	V_{BB} = 48 V, 20% to 80% of V_{OUT} , R_L = 20 Ω	0.34	0.68	V/µs
VOUT falling slew rate	80% to 20% of V_{OUT} , R_L = 20 Ω	0.34	0.73	V/µs
Maximum PWM frequency		0.75		kHz
Channel Turn-on time	V_{BB} = 48 V, R_L = 20 Ω 50% of EN to 80% of VOUT		180	μs
Channel Turn-off time	V_{BB} = 48 V, R_L = 20 Ω 50% of EN to 20% of VOUT		140	μs
	1-ms enable pulse V_{BB} = 48 V, R_{L} = 20 Ω	-30	30	μs
Turn-on and off matching	200-μs enable pulse in Active state, V_{BB} = 48 V, R_{L} = 20 Ω	-30	30	μs
PWM accuracy - average load	400-μs enable pulse (2-ms period) in Active state, V_{BB} = 48 V, R_{L} = 20 Ω	-15	15	%
current	\leq 500 Hz, 50% Duty cycle V _{BB} = 48 V, R _L = 20 Ω	-10	10	%
Switching energy losses during turn- on	V _{BB} = 48 V, R _L = 50 Ω		1	mJ
Switching energy losses during turn-off	$V_{BB} = 48 \text{ V}, R_{L} = 50 \Omega$		0.9	mJ
	Channel Turn-on delay time (from Standby) Channel Turn-on delay time (from Active) Channel Turn-off delay time VOUT rising slew rate VOUT falling slew rate Maximum PWM frequency Channel Turn-on time Channel Turn-off time Turn-on and off matching PWM accuracy - average load current Switching energy losses during turn-on Switching energy losses during turn-on	Channel Turn-on delay time (from Standby) $V_{BB} = 48 \text{ V}, R_L = 20 \Omega 50\%$ of EN to 20% of VOUTChannel Turn-on delay time (from Active) $V_{BB} = 48 \text{ V}, R_L = 20 \Omega 50\%$ of EN to 20% of VOUTChannel Turn-off delay time $V_{BB} = 48 \text{ V}, R_L = 20 \Omega 50\%$ of EN to 80% of VOUTVOUT rising slew rate $V_{BB} = 48 \text{ V}, 20\%$ to 80% of V_{OUT} , $R_L = 20 \Omega$ VOUT falling slew rate 80% to 20% of V_{OUT} , $R_L = 20 \Omega$ Maximum PWM frequency $V_{BB} = 48 \text{ V}, R_L = 20 \Omega 50\%$ of EN to 80% of VOUTChannel Turn-on time $V_{BB} = 48 \text{ V}, R_L = 20 \Omega 50\%$ of EN to 20% of VOUTChannel Turn-off time $V_{BB} = 48 \text{ V}, R_L = 20 \Omega 50\%$ of EN to 20% of VOUT1-ms enable pulse $V_{BB} = 48 \text{ V}, R_L = 20 \Omega$ 200-µs enable pulse in Active state, $V_{BB} = 48 \text{ V}, R_L = 20 \Omega$ 200-µs enable pulse (2-ms period) in Active state, $V_{BB} = 48 \text{ V}, R_L = 20 \Omega$ Switching energy losses during turn-on $V_{BB} = 48 \text{ V}, R_L = 50 \Omega$ Switching energy losses during turn-on $V_{AB} = 48 \text{ V}, R_L = 50 \Omega$	Channel Turn-on delay time (from Standby) VBB = 48 V, RL = 20 Ω 50% of EN to 20% of VOUT Channel Turn-on delay time (from Active) VBB = 48 V, RL = 20 Ω 50% of EN to 20% of VOUT Channel Turn-off delay time VBB = 48 V, RL = 20 Ω 50% of EN to 80% of VOUT VOUT rising slew rate VBB = 48 V, 20% to 80% of VOUT, RL = 20 Ω VOUT falling slew rate 80% to 20% of VOUT, RL = 20 Ω Maximum PWM frequency 0.75 Channel Turn-on time VBB = 48 V, RL = 20 Ω 50% of EN to 80% of VOUT Channel Turn-off time VBB = 48 V, RL = 20 Ω 50% of EN to 20% of VOUT Turn-on and off matching VBB = 48 V, RL = 20 Ω 50% of EN to 20% of VOUT Turn-on and off matching VBB = 48 V, RL = 20 Ω 50% of EN to 20% of VOUT Turn-on and off matching VBB = 48 V, RL = 20 Ω 50% of EN to 20% of VOUT Turn-on and off matching VBB = 48 V, RL = 20 Ω 50% of EN to 20% of VOUT Turn-on and off matching 400-μs enable pulse VBB = 48 V, RL = 20 Ω 50% of EN to 20% of VOUT PWM accuracy - average load current 400-μs enable pulse (2-ms period) in Active state, VBB = 48 V, RL = 20 Ω 50% of VOUT -15 Switching energy losses during turn-on VBB = 48 V, RL = 50 Ω -10 Switching energy losses during turn-on VBB = 48 V, RL = 50 Ω -10	



7 Detailed Description

7.1 Overview

The TPS482H85-Q1 device is a smart high-side switch, with internal charge pump and dual-channel integrated NMOS power FETs. Full diagnostics and high-accuracy current-sense features enable intelligent control of the load. The adjustable current-limit function greatly improves the reliability of whole system.

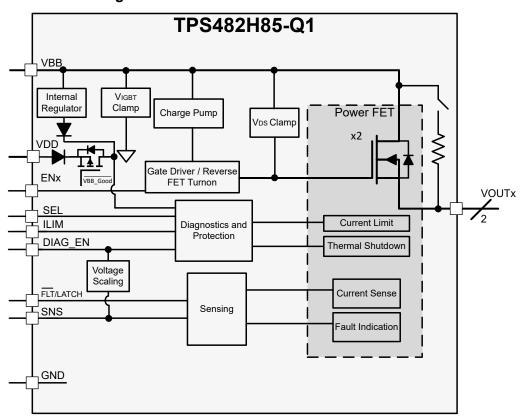
The device has logic pins to enable each of the two channels and a separate pin to enable the diagnostic output with SEL pin to select the channel to be output on the analog current SNS pin. A and C versions provide a LATCH pin to select between latch and auto-retry behavior after thermal shutdown, while B version provides a global FLT pin to indicate a fault in the device.

The external high-accuracy current limit allows setting the current-limit value by applications. When overcurrent occurs, the device improves system reliability by clamping the inrush current effectively. The device can also save system cost by reducing the size of PCB traces and connectors, and the capacity of the preceding power stage.

For inductive loads (relays, solenoids, valves), the device implements an active clamp between drain and source to protect itself. During the inductive switching-off cycle, both the energy of the power supply and the load are dissipated on the high-side switch. The device also optimizes the switching-off slew rate when the clamp is active, which helps the system design by keeping the effects of transient power and EMI to a minimum.

The TPS482H85-Q1 device is a smart high-side switch for a wide variety of resistive, inductive, and capacitive loads, including low-wattage bulbs, LEDs, relays, solenoids, heaters, and sub-modules.

7.2 Functional Block Diagram





7.3 Feature Description

7.3.1 Pin Current and Voltage Conventions

For reference purposes throughout the data sheet, current directions on their respective pins are as shown by the arrows in Figure 7-1. The direction is used to indicate the polarities of current in Specifications, but not to represent the actual current flow direction of each pin. All voltages are measured relative to the ground plane.

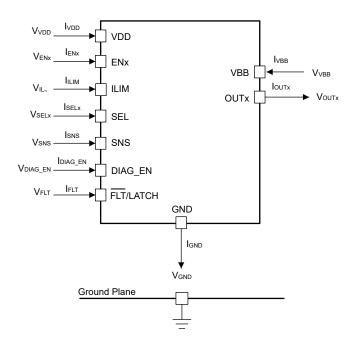


Figure 7-1. Voltage and Current Conventions

7.3.2 Accurate Current Sense

The high-accuracy current-sense function is internally implemented, which allows a better real-time monitoring effect and more-accurate diagnostics without further calibration. A current mirror is used to source 1 / K_{SNS} of the load current, flowing out to the external resistor between the SNS pin and GND, and reflected as voltage on the SNS pin.

 K_{SNS} is the ratio of the output current and the sense current. The accuracy values of K_{SNS} quoted in the electrical characteristics do take into consideration temperature and supply voltage. Each device was internally calibrated while in production, so post-calibration by users is not required in most cases.

The maximum voltage out on the SNS pin is clamped to V_{SNSFH} , which is the fault voltage level. To make sure that this voltage is not higher than the system can tolerate, the max voltage at the DIAG_EN pin has been limited to the voltage at the SNS pin. If DIAG_EN is between V_{IH} and 3.3V, the maximum output on the SNS pin is approximately 3.3V. However, if the voltage at DIAG_EN is above 3.3V, then the fault SNS voltage, V_{SNSFH} , tracks that voltage up to 5V. Tracking is done because the GPIO voltage output that is powering the diagnostics through DIAG_EN is close to the maximum acceptable ADC voltage within the same microcontroller. Therefore, the sense resistor value, R_{SNS} , can be chosen to maximize the range of currents needed to be measured by the system. The R_{SNS} value must be chosen based on application need. The maximum usable R_{SNS} value is bounded by the ADC minimum acceptable voltage, $V_{ADC,min}$, for the smallest load current needed to be measured by the system, $I_{LOAD,min}$. The minimum acceptable R_{SNS} value has to ensure the V_{SNS} voltage is below the V_{SNSFH} value so that the system can correctly determine faults. This difference between the maximum readable current through the SNS pin, $I_{LOAD,max} \times R_{SNS}$, and the V_{SNSFH} is called the headroom voltage, V_{HR} .



The headroom voltage is determined by the system but is important so that there is a difference between the maximum readable current and a fault condition. Therefore, the minimum R_{SNS} value has to be the V_{SNSFH} minus the V_{HR} times the sense current ratio, K_{SNS} divided by the maximum load current the system must measure, $I_{LOAD,max}$. Use the following equation to set the boundary equation.

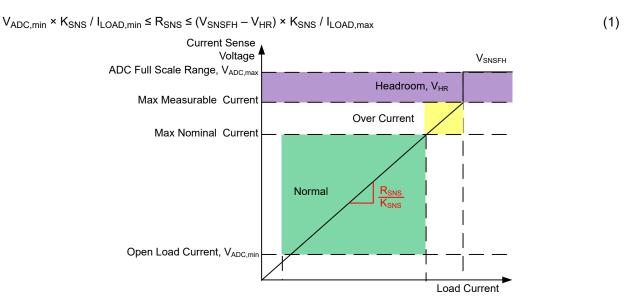


Figure 7-2. Voltage Indication on the Current-Sense Pin

The maximum current the system wants to read, $I_{LOAD,max}$, must be below the current-limit threshold because after the current-limit threshold is tripped the V_{SNS} value goes to V_{SNSFH} .

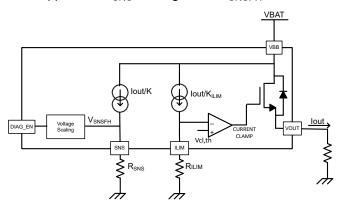


Figure 7-3. Current-Sense and Current-Limit Block Diagram

Because this scheme adapts based on the voltage coming in from the MCU, there is no need to have a Zener diode on the SNS pin to protect from high voltages.

7.3.3 Adjustable Current Limit

A high-accuracy adjustable current limit allows higher reliability, which protects the power supply and wires during short circuit or power up by being programed to an acceptable level. Also, current limiting can save system costs by reducing PCB traces, connector size, capacity of the preceding power stage and possibly reducing wire gauge.

Current limit offers protection from over-stressing to the load and integrated power FET. the current limit regulates the output current to the set value, asserts the $\overline{\text{FLT}}$ pin, and pulls up the SNS pin to V_{SNSFH} if the device is set up to output that channel on the SNS pin.



The device can be programmed to different current limit values through an external resistor on the ILIM pin. There are 10 current limit settings which can be set based on resistors values in Current Limit Setting Through External Resistor. A shift of ≥2% from the resistor value listed in Current Limit Setting Through External Resistor can potentially cause ILIM threshold shift. ≤1% tolerance resistors should be used for R_{ILIM} resistor.

Table 7-1. Current Limit Setting Through External Resistor

ALLOWED RESISTOR VALUE (1)	ILIM THRESHOLD
59kΩ	1A
45.3kΩ	2A
34.8kΩ	3A
26.1kΩ	4A
18.7kΩ	5A
11.5kΩ	6A
6.65kΩ	7A
2.74kΩ	8A
Short to GND (<1.1kΩ)	9A
Open (>60 kΩ)	10A

Note

Any resistor settings that are not listed in this table can be interpreted as one of the adjacent levels, which is not a recommended configuration.

To set a different inrush current limit and steady state current limit, the current limit resistor can be changed dynamically when the device is ON. MOSFET based control scheme can be adopted for changing the current limit on the fly. However, the components and the layout at ILIM pin need to be considered carefully to minimize the capacitance at the pin. If switching the ILIM threshold on-the-fly, any capacitance ≥ 100pF at ILIM pin might affect the transition speed from one ILIM resistor to another, which can lead to unwanted shutdown. MOSFET with low input capacitance needs to be selected for dynamic current limit change.

A current limit event occurs when I_{OUTx} reaches the regulation threshold level, I_{CL} . When I_{OUT} reaches the current limit threshold, I_{CL} , the device can remain enabled and limit I_{OUTx} to I_{CL} . When the device remains enabled (and limits I_{OUT}), thermal shutdown may be triggered due to the high amount of power dissipation in the FET. The regulation loop response when the device is enabled into a short circuit is shown in Enable Into Short Current Limit (auto-retry). The figure is showing the scenario with the auto-retry versions or LATCH pin version with LATCH = LOW listed in Device Comparison Table. The LATCH pin version with LATCH = HIGH will latch off after the first thermal shutdown. Please note that the current may peak at a higher value (I_{CL_ENPS}) than the regulation threshold (I_{CL}).

When an over-current event occurs, the current limit must respond quickly in order to limit the peak current seen on short circuits (both hot and enabling into a short). The peak has to be limited to ensure that the supply does not droop for a given amount of supply capacitance. This is especially important in applications where the device is powered from a DC/DC instead of car battery.



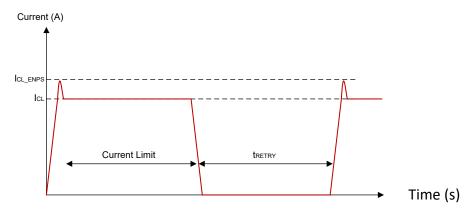


Figure 7-4. Enable Into Short Current Limit (auto-retry)

However, a higher (I_{CL_LINPK}) output current than the current limit regulation loop threshold (I_{CL}) may be available from the switch during an overload condition before the current limitation is applied.

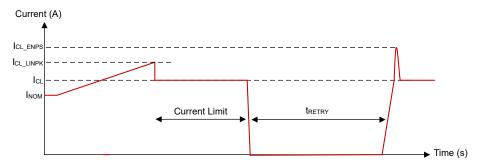


Figure 7-5. Linear Peak From Soft Short (auto-retry)

The device applies a strong pulldown to limit the current during the short circuit event while the switch is enabled. The current will then drop down to zero before the current limit regulation loop engages and the switch turn-on and the behavior will be similar to the enable into a short circuit case.

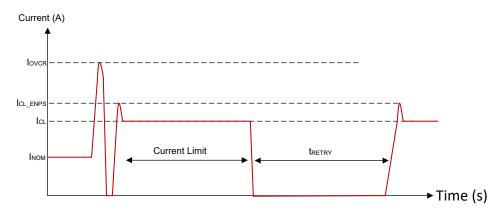


Figure 7-6. Hot Short Event (auto-retry)

7.3.4 Inductive-Load Switching-Off Clamp

When switching an inductive load off, the inductive reactance tends to pull the output voltage negative. Excessive negative voltage could cause the power FET to break down. To protect the power FET, an internal clamp between drain and source is implemented, namely V_{DS(clamp)}.

$$V_{DS(clamp)} = V_{VS} - V_{OUT}$$
 (2)

During the period of demagnetization (t_{decay}), the power FET is turned on for inductance-energy dissipation. The total energy is dissipated in the high-side switch. Total energy includes the energy of the power supply ($E_{(VS)}$) and the energy of the load ($E_{(load)}$). If resistance is in series with inductance, some of the load energy is dissipated on the resistance.

$$E_{(HSS)} = E_{(VS)} + E_{(load)} = E_{(VS)} + E_{(L)} - E_{(R)}$$
(3)

When an inductive load switches off, $E_{(HSS)}$ causes high thermal stressing on the device. The upper limit of the power dissipation depends on the device intrinsic capacity, ambient temperature, and board dissipation condition.

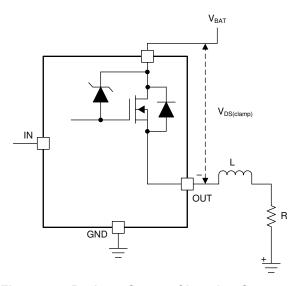


Figure 7-7. Drain-to-Source Clamping Structure

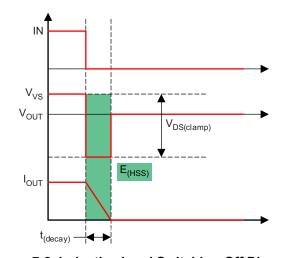


Figure 7-8. Inductive Load Switching-Off Diagram

From the perspective of the high-side switch, $E_{(HSS)}$ equals the integration value during the demagnetization period.

ADVANCE INFORMATION



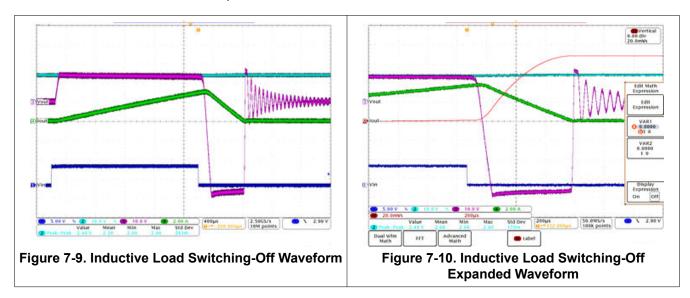
$$\begin{split} E_{(HSS)} &= \int_{0}^{t_{(decay)}} V_{DS(clamp)} \times I_{OUT}(t) dt \\ t_{(decay)} &= \frac{L}{R} \times In \left(\frac{R \times I_{OUT(max)} + |V_{OUT}|}{|V_{OUT}|} \right) \\ E_{(HSS)} &= L \times \frac{V_{VS} + |V_{OUT}|}{R^2} \times \left[R \times I_{OUT(max)} - |V_{OUT}| \ In \left(\frac{R \times I_{OUT(max)} + |V_{OUT}|}{|V_{OUT}|} \right) \right] \end{split} \tag{4}$$

When R approximately equals 0, $E_{(HSD)}$ can be given simply as:

$$E_{(HSS)} = \frac{1}{2} \times L \times I_{OUT(max)}^2 \frac{V_{VS} + |V_{OUT}|}{|V_{OUT}|}$$
(5)

Figure 7-9 is a waveform of the device driving an inductive load, and Figure 7-10 is waveform with an expanded time scale. Channel 1 is the IN signal, channel 2 is the supply voltage V_{VS} , channel 3 is the output voltage V_{OUT} , channel 4 is the output current I_{OUT} , and channel M is the measured power dissipation $E_{(HSS)}$.

On the waveform, the duration of V_{OUT} from V_{VS} to $(V_{VS}-V_{DS(clamp)})$ is around 120 μ s. The device also optimizes the switching-off slew rate when the clamp is active. This optimization can help the system design by keeping the effects of transient power and EMI to a minimum. As shown in Figure 7-9 and Figure 7-10, the controlled slew rate is around 0.5 V/μ s.



Note that for PWM-controlled inductive loads, it is recommended to add the external freewheeling circuitry shown in Figure 7-11 to protect the device from repetitive power stressing. TVS is used to achieve the fast decay. See Figure 7-11 for more details.



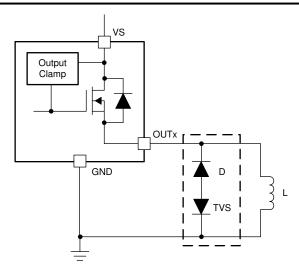


Figure 7-11. Protection With External Circuitry

7.3.5 Fault Detection and Reporting

7.3.5.1 Diagnostic Enable Function

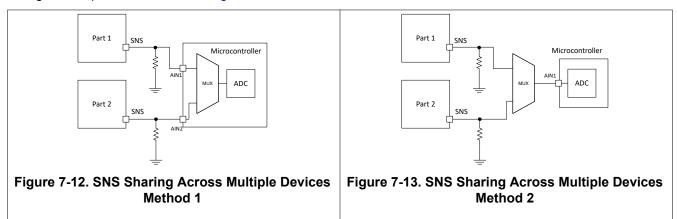
The DIAG_EN pin enables or disables the diagnostic functions. If multiple devices are used, but the ADC resource is limited in the microcontroller, the MCU can use GPIOs to set DIAG_EN high to enable the diagnostics of one device while disabling the diagnostics of the other devices by setting DIAG_EN low. In addition, the device can keep the power consumption to a minimum by setting DIAG_EN and ENx low.

7.3.5.2 Multiplexing of Current Sense

SEL pin is used to multiplex the shared current-sense function among the two channels within the same device. Pulling each pin high or low sets the corresponding channel to be output on the SNS pin if DIAG_EN is high. FLT still represents a global interrupt that goes low if a fault occurs on any channel.

If current sense information needs to be multiplexed across different devices, then it is not recommended to directly tie the SNS pins together across multiple devices. When the DIAG_EN is LOW, there is an internal clamp at SNS pin that clamps the voltage to approximately 2V. One device SNS pin might affect the other devices SNS readback if tied directly.

To use SNS pin across multiple devices, it is recommended to connect individual SNS pin to different analog input pins of MCU, as illustrated in Figure 7-12. Alternatively, an external analog MUX can be used to connect to a single MCU pin, as illustrated in Figure 7-13.



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Table 7-2. Diagnosis Configuration Table

DIAG_EN	ENx	SEL	SNS ACTIVATED CHANNEL	SNS	FLT	PROTECTIONS AND DIAGNOSTICS
L	Н	_	_	0V. Clamp to 2V internally if external	See Fault Table	SNS disabled, FLT reporting, full protection
	L			voltage is applied to the pin.	High-Z	Diagnostics disabled, no protection
Н		0	Channel 1	Fault Table	See Fault	See Fault Table
	_	1	Channel 2	Tault lable	Table	See Fault Table

7.3.5.3 FAULT Reporting

For the variants with the global \overline{FLT} pin, the \overline{FLT} output monitors the global fault condition among all the channels. When a fault condition occurs on any channel, the \overline{FLT} pin is pulled down to GND. A 3.3-V or 5-V external pullup is required to match the supply level of the microcontroller. The \overline{FLT} pin reports faults on any channel as long as the device is not in the SLEEP mode.

After the FAULT report, the microcontroller can check and identify the channel in fault status by multiplexed current sensing. Alternately for the variants without the global FLT pin, the SNS pin also works as a fault report with an internal pullup voltage, V_{SNSFH} if DIAG_EN is high.

7.3.5.4 Fault Table

Table 7-3. Fault Table

CONDITIONS	ENx	OUTx	SNS (If DIAG_EN is high)	FLT #none# (with external pull-up)	BEHAVIOR	FAULT RECOVERY
	L	L	0	Н	Normal	_
Normal	Н	V _{BB} - I _{LOAD} × R _{ON}	I _{LOAD} / K _{SNS}	Н	Normal	_
Overcurrent	н	V _{BB} - I _{LIM} × R _{ON}	V_{SNSFH}	L	Holds the current at the current limit until thermal shutdown or when the overcurrent event is removed.	Auto
Open load, short to battery, reverse	L	Н	V_{SNSFH}	L	Internal pull-up resistor is active. Fault is asserted when V _{VS} – V _{OUTx} < V _(ol,off)	Auto
polarity	Н	Н	I _{LOAD} / K _{SNS} ≈ 0	Н	Normal behavior. User can make judgement based on SNS pin output.	_
Hot short	Н	L	V_{SNSFH}	L	Device will immediately shutdown, and reenable into current limit.	Auto-retry into current limit until thermal shutdown. Auto-retry version will repeat until the fault goes away. Latch version will need toggle EN after first thermal shutdown.
Enable into permanent short	L→H	L	V_{SNSFH}	L	Device will enable into current limit until thermal shutdown.	Enable into current limit until thermal shutdown. Auto-retry version will repeat until the fault goes away. Latch version will need toggle EN after first thermal shutdown.



Table 7-3. Fault Table (continued)

14410 1 011 4411 14410 (0011111404)							
CONDITIONS	ENx	OUTx	SNS (If DIAG_EN is high)	FLT #none# (with external pull-up)	BEHAVIOR	FAULT RECOVERY	
Absolute thermal shutdown, Relative thermal shutdown	Н	L	V _{SNSFH}	L	Shuts down when devices hits relative or absolute thermal shutdown.	For auto-retry version, output auto- retry after t _{RETRY} . Fault recovers when T _J < T _{HYS} or when ENx toggles. Latch version can recover only when EN toggles.	
Reverse polarity	x	x	x		X	Channel turns on to lower power dissipation. Current into ground pin needs to be limited by external ground network.	

Note

FLT output only on the variants that include FLT pin.

7.3.6 Full Diagnostics

7.3.6.1 Short-to-GND and Overload Detection

When a channel is on, a short to GND or overload condition causes overcurrent. If the overcurrent triggers either the internal or external current-limit threshold, the fault condition is reported out. The microcontroller can handle the overcurrent by turning off the switch. The device will clamp the current to I_{CL} until thermal shutdown. TPS2HC120A automatically recovers when the fault condition is removed.

In a hot short condition, when the short-circuit is applied when the EN is HIGH, the device will shutdown immediately and auto-retry the same as enable into permanent short condition, as shown in Figure 7-6.

7.3.6.2 Open-Load Detection

7.3.6.2.1 Channel On

When a channel is ON, benefiting from the high-accuracy current sense in the small current range, if an open-load event occurs, it can be detected as an ultra low V_{SNS} and handled by the microcontroller. Note that the detection is not reported on the \overline{FAULT} pin or the fault registers. The microcontroller must multiplex the SEL pins to output the correct channel out on the SNS pin.

7.3.6.2.2 Channel Off

In the OFF state, when DIAG_EN is high, there is an internal pull-up resistor R_{OL} that pulls up a channel to V_{BB}. The specific channel that gets pulled up is based on the selection of SEL, and the other channels do not have the pull-up resistor engaged.

If there is load present at the selected channel, then the output voltage is pulled to around 0V, as the load is much stronger than the R_{OL} . In the case of an open load, the output voltage will be pulled close to the supply voltage by the R_{OL} . If V_{BB} - V_{OUT} < $V_{OL,off}$ for the selected channel, the \overline{FLT} pin goes low to indicate the fault to the MCU, and the SNS pin is pulled up to I_{SNSFH} .



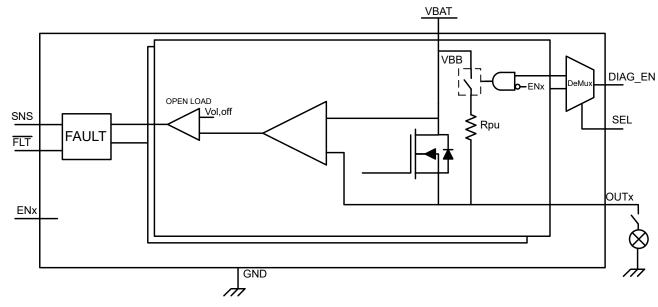


Figure 7-14. Open-Load Detection in Off-State

7.3.6.3 Short-to-Battery Detection

Short-to-battery has the same detection mechanism and behavior as open-load detection, in both the on-state and off-state. See Fault Table for more details.

7.3.6.4 Reverse-Polarity and Battery Protection

Reverse-polarity, commonly referred to as reverse battery, occurs when the ground of the device goes to the battery potential, $V_{GND} = V_{BAT}$, and the supply pin goes to ground, $V_{BB} = 0V$. In this case, if the EN1 pin has a path to the *ground* plane, then the FET turns on to lower the power dissipation through the main channel and prevent current flow through the body diode. Note that the resistor/diode ground network (if there is not a central blocking diode on the supply) must be present for the device to protect itself during a reverse battery event.

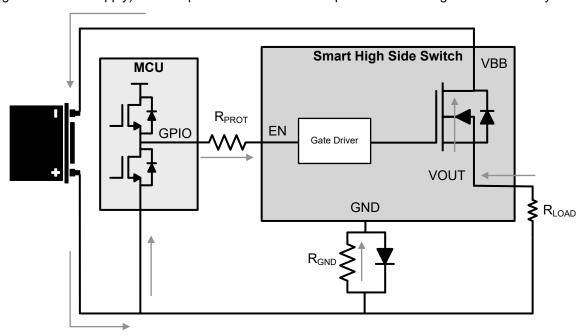


Figure 7-15. Reverse Battery Circuit



For more external protection circuitry information, see Section 7.3.7.5. See the fault truth table in Fault Table for more details.

7.3.6.5 Thermal Fault Detection

To protect the device in severe power stressing cases, the device implements two types of thermal fault detection, absolute temperature protection (absolute thermal shutdown) and dynamic temperature protection (relative thermal shutdown). Respective temperature sensors are integrated close to each power FET, so the thermal fault is reported by each channel. This arrangement can help the device keep the cross-channel effect to a minimum when some channels are in a thermal fault condition.

7.3.6.5.1 Thermal Protection Behavior

The thermal protection behavior can be split up into three categories of events that can happen. Figure 7-16 shows each of these categories.

- 1. **Relative thermal shutdown**: the device is enabled into an overcurrent event. The output current rises up to the I_{ILIM} level and the \overline{FLT} goes low. With this large amount of current going through the junction temperature of the FET increases rapidly with respect to the controller temperature. When the power FET temperature rises T_{REL} amount above the controller junction temperature $\Delta T = T_{FET} T_{CON} > T_{REL}$, the device shuts down. For auto-retry version, after t_{RETRY} , the part tries to restart itself. Latch version will require EN to be toggled to re-enable the channel. The \overline{FLT} is asserted until the fault condition is cleared. The first plot in Figure 7-16 shows the relative thermal shutdown behavior for the auto-retry version.
- 2. Absolute thermal shutdown: the device is still enabled in an overcurrent event. However, in this case the junction temperature rises up and hits an absolute reference temperature, T_{ABS}, and then shuts down. For auto-retry version, the device does not recover until both T_J < T_{ABS} T_{hys} and the t_{RETRY} timer has expired. For latch version, toggling EN is required to re-enable the channel. The second plot in Figure 7-16 shows the absolute thermal shutdown behavior for the auto-retry version.
- 3. **Latch behavior**: the device is enabled into an overcurrent event. The DIAG_EN pin is high so that diagnostics can be monitored on SNS and FLT. For the latched version of the device, if the part shuts down due to a thermal fault, either relative thermal shutdown or absolute thermal shutdown, the device does not enable the channel until the EN pin is toggled. The third plot in Figure 7-16 shows the relative thermal shutdown behavior for the variants with LATCH pin when LATCH pin is HIGH.



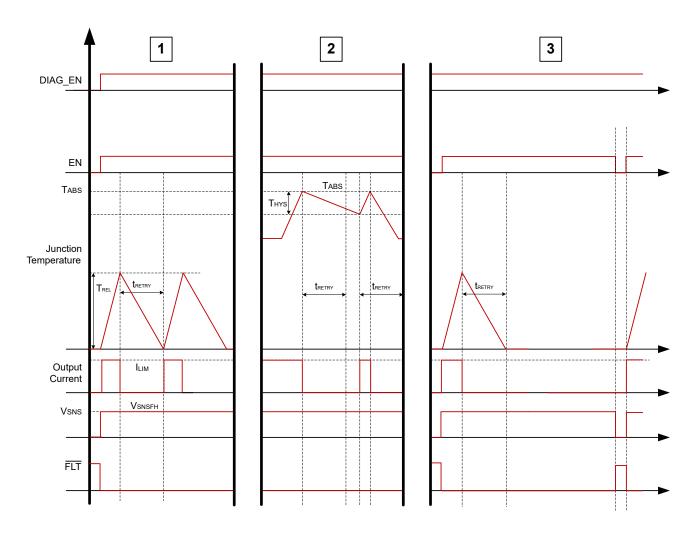


Figure 7-16. Thermal Behavior

7.3.7 Full Protections

7.3.7.1 UVLO Protection

The device monitors the supply voltage V_{VBB} , to prevent unpredicted behaviors when V_{VBB} is too low. When V_{VBB} falls down to V_{UVLOF} , the device shuts down. When V_{VBB} rises up to V_{UVLOR} , the device turns on.



7.3.7.2 Loss of GND Protection

When loss of GND occurs, all the channels are disabled regardless of control pin status, and the part is not powered.

Case 1 (loss of device GND): loss of GND protection is active when the thermal pad (Tab), I_{C_GND}, and current limit ground are one trace connected to the system ground, as shown in Figure 7-17.

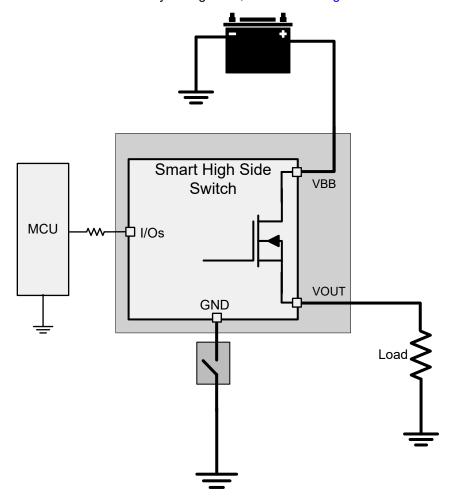


Figure 7-17. Loss of Device GND

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Case 2 (loss of module GND): when the whole ECU module GND is lost, protections are also active. At this condition, the load GND remains connected.

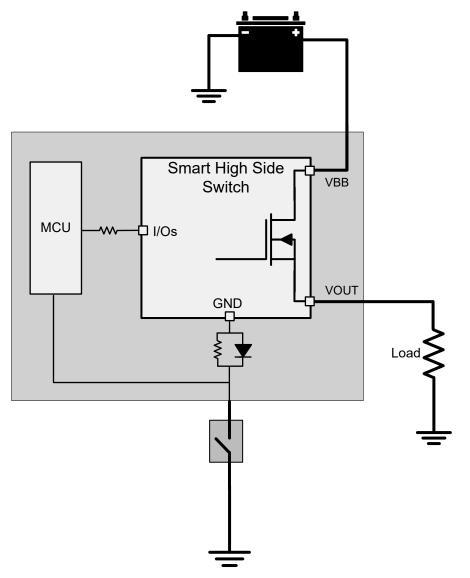


Figure 7-18. Loss of Module GND



7.3.7.3 Loss of Power Supply Protection

When loss of supply occurs, output is turned off regardless of whether the input is high or low. For a resistive or capacitive load, loss of supply protection is easy to achieve due to no more power. The worst case is a charged inductive load. In this case, the current is driven from all of the IOs to maintain the inductance output loop. TI recommends either the MCU serial resistor plus the GND network (diode and resistor in parallel) or external free-wheeling circuitry.

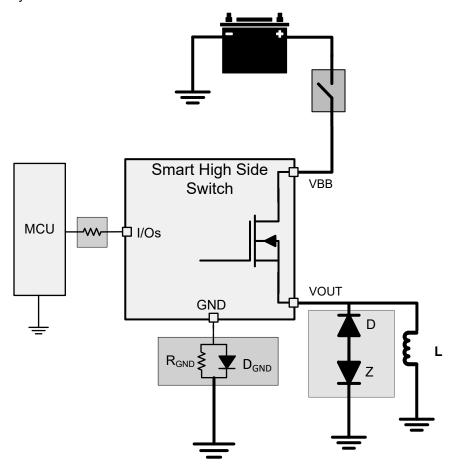


Figure 7-19. Loss of Battery

7.3.7.4 Loss of VDD

In the case of a loss of VDD supply input, the device continues to operate normally normally without any change in state. The only impact of the loss of VDD supply is an increase in quiescent current consumption through the VBB pin.



7.3.7.5 Reverse Current Protection

Method 1: block diode connected with V_{BB} . Both the device and load are protected when in reverse polarity. The blocking diode does not allow any of the current to flow during reverse battery condition.

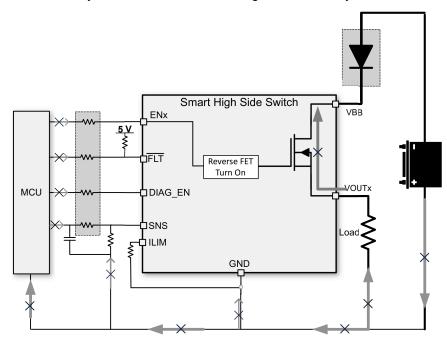


Figure 7-20. Reverse Protection With Block Diode

ADVANCE INFORMATION

Method 2 (GND network protection): only the high-side device is protected under this connection. The load reverse current is limited by the impedance of the load itself. Note when reverse polarity happens, the continuous reverse current through the power FET must not make the heat build up be greater than the absolute maximum junction temperature. This can be calculated using the $R_{ON(REV)}$ value and the $R_{\theta JA}$ specification. In the reverse battery condition it is important that the FET comes on to lower the power dissipation. This action is achieved through the path from EN to system ground where the positive voltage is being applied. No matter what types of connection are between the device GND and the board GND, if a GND voltage shift happens, ensure the following proper connections for the normal operation:

Connect the current limit programmable resistor to the device GND.

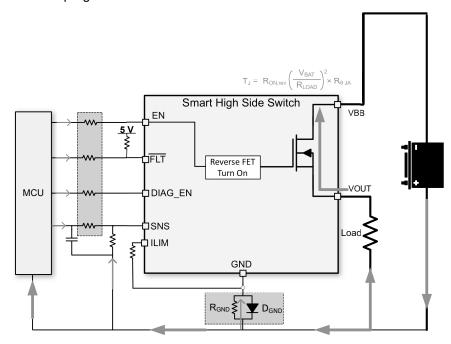


Figure 7-21. Reverse Protection With GND Network

Recommendation – resistor and diode in parallel: a peak negative spike can occur when the inductive
load is switching off, which can damage the HSD or the diode. So, TI recommends a resistor in parallel with
the diode when driving an inductive load. The recommended selection are a 1-kΩ resistor in parallel with
an I_F > 100-mA diode. If multiple high-side switches are used, the resistor and diode can be shared among
devices.

If multiple high-side power switches are used, the resistor can be shared among devices.

• **Ground Resistor:** The higher resistor value contributes to a better current limit effect when the reverse battery or negative ISO pulses.

$$R_{GND} \ge \frac{\left(-V_{CC}\right)}{\left(-I_{GND}\right)} \tag{6}$$

where

- V_{CC} is the maximum reverse battery voltage (typically –16 V).
- I_{GND} is the maximum reverse current the ground pin can withstand, which is available in the *Absolute Maximum Ratings*.
- Ground Diode: A diode is needed to block the reverse voltage, which also brings a ground shift (≈ 600 mV).
 Additionally, the diode must be ≈ 200-V reverse voltage for the ISO 7637 pulse 1 testing so that it does not get biased.

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7.3.7.6 Protection for MCU I/Os

In many conditions, such as the negative ISO pulse, or the loss of battery with an inductive load, a negative potential on the device GND pin can damage the MCU I/O pins (more likely, the internal circuitry connected to the pins). Therefore, the serial resistors between MCU and HSS are required.

Also, for proper protection against loss of GND, TI recommends 10-k Ω resistance for the R_{PROT} resistors.

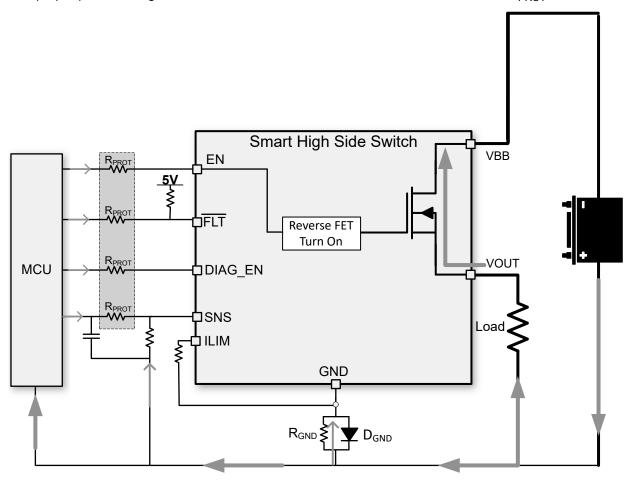


Figure 7-22. MCU I/O Protections

7.4 Device Functional Modes

7.4.1 Operatiional Modes

The device has several states to transition into based on the ENx pins and the DIAG_EN pin.



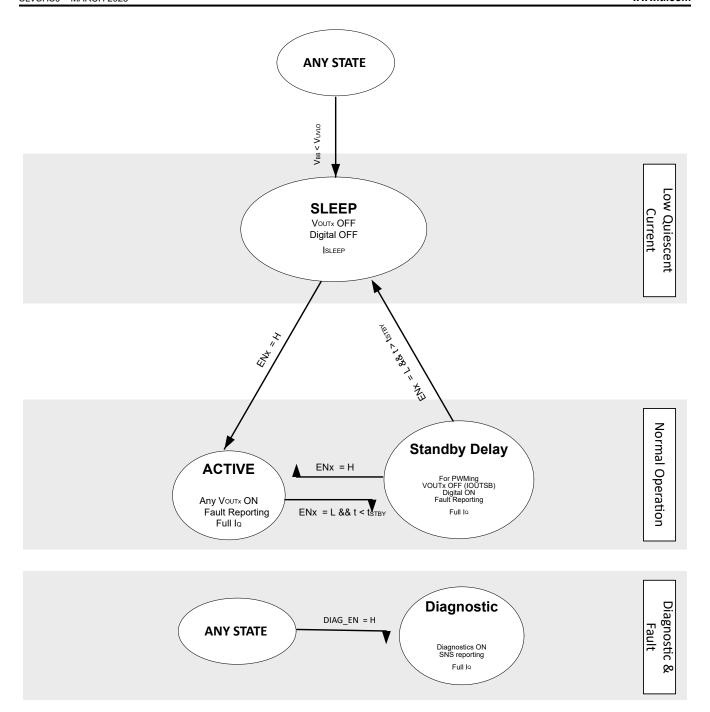


Figure 7-23. State Diagram

SLEEP

In the SLEEP state, everything inside the device is turned off and the quiscent current is the I_{SLEEP} . The device can only transition out of the SLEEP state if the ENx pins or DIAG_EN pin gets pulled high. From SLEEP, the device can transfer into the ACTIVE state if any of the ENx pins are pulled high, or the DIAGNOSTIC state if the DIAG_EN pin, without any of the ENx pins, goes high. Additionally, if the device is in any of the states and VBB drops below V_{BBUVLO} , the device transitions into SLEEP state.

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DIAGNOSTIC

The DIAGNOSTIC state is when the device is outputting diagnostics on the SNS and FLT pins. This can happen when the device is in any previous state and the DIAG_EN pin goes high. The off-state diagnostics are comprised of open load detection in off state and short to battery detection. The FLT pin asserts if there is a fault on any of the channels, but the SNS pin only outputs a fault for the channel associated to the SELx pin values. From the DIAGNOSTIC state, the device can transfer into the ACTIVE state if the DIAG_EN pin goes back low and any channel is on or the STANDBY DELAY state if all channels are OFF.

ACTIVE

The ACTIVE state is when any of the channel outputs are on by the ENx pin associated. In the ACTIVE state, the current limit value is set by the external resistor on the ILIM pin. If the DIAG_EN pin is pulled high while in the ACTIVE state, the SNS pin outputs a proportional current to the load current of the channel associated to the SELx pins configuration until a fault occurs on that channel. Additionally the FLT pin reports if there is a fault occurring on any channel. The device can transition out of the ACTIVE state by turning off all of the channels while DIAG_EN is high or low, or a fault occurring. If all of the channels turn off and DIAG_EN is high, the device transitions into the DIAGNOSTIC state. If all of the channels turn off and the DIAG_EN pin is low, then the device transfers into the STANDBY DELAY state. However, if the ENx pins are still high and a fault occurs, the device transitions into the FAULT state.

FAULT

The FAULT state occurs when the ENx pins are high but some event has caused the channel to behave differently from normal operation. These fault events include: absolute thermal shutdown, relative thermal shutdown, and current limit. Each of these fault events either directly or eventually shut off the channel to protect the device and system. After the device shuts off and waits for t_{RETRY} amount of time and has cooled below the t_{RETRY} threshold, the output/s that were on try to come back on again and the device transitions back into the ACTIVE state or DIAGNOSTIC state.

STANDBY DELAY

The STANDBY DELAY state is when the ENx pins are all low, outputs are all turned off and the DIAG_EN pin is also low but there has not yet been t_{STBY} amount of time. This state is included so that the channel outputs can be PWM'd without all of the internal rails being cut off and put to SLEEP mode. Once the device has waited t_{STBY} , the device completely shuts down and transitions into SLEEP. However, if during t_{STBY} , ENx were to go high, the device transitions into ACTIVE without shutting completely down. Similarly if the DIAG_EN goes high, the device transitions into DIAGNOSTIC.



8 Application and Implementation

Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

8.1 Application Information

The TPS482H85-Q1 device is capable of driving a wide variety of resistive, inductive, and capacitive loads, including the low-wattage bulbs, LEDs, relays, solenoids, heaters, and sub-modules. Full diagnostics and high-accuracy current-sense features enable intelligent control of the load. An external adjustable current limit improves the reliability of the whole system by clamping the inrush or overload current.

8.2 Typical Application

The following figure shows an example of the external circuitry connections.

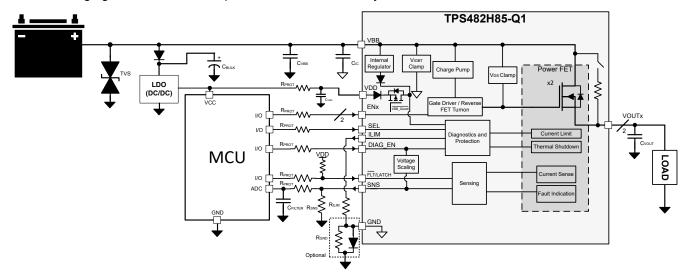


Figure 8-1. Typical Application Diagram for GPIO version

Table 8-1. Recommended Component Values

COMPONENT	DESCRIPTION	PURPOSE
TVS	SMBJ70CA	Filter voltage transients coming from battery
С _{VВВ}	5μF	Stabilize the input supply. Prevent the device from losing power during short-circuit situation.
C _{IC}	100nF	Minimal amount of capacitance on input for EMI mitigation
C _{BULK}	10μF	Help filter voltage transients on the supply rail
C _{VDD}	100nF	Stabilize the VDD supply and limit supply excursions. Needed with either external or internal VDD supplies
R _{PROT}	10kΩ	Protection resistor for microcontroller and device I/O pins
R _{LIM}	Discrete values as listed in Table 7-1	Set current limit threshold
R _{SNS}	1kΩ	Translate the sense current into sense voltage
C _{FILTER}	100pF	Coupled with RPROT on the SNS line creates a low pass filter to filter out noise going into the ADC of the MCU
C _{VOUT}	22nF	Improves EMI performance, filtering of voltage transients
R _{PULLUP}	5kΩ	Pull up resistor for open-drain pins (FLT and LPM)

Product Folder Links: TPS482H85-Q1

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Table 8-1. Recommended Component Values (continued)

COMPONENT	DESCRIPTION	PURPOSE
R_{GND}	1kΩ	Stabilize GND potential during turn-off of inductive load
D _{GND} MSX1PJ-M3/89A Diode		Keeps GND close to system ground during normal operation

8.2.1 Design Requirements

Table 8-2. Example Design Requirements

PARAMETER	VALUE
V _{DIAG_EN}	5V
I _{LOAD,max}	1A
I _{LOAD,min}	10mA
$V_{ADC,min}$	5mV
V _{HR}	1V

8.2.2 Detailed Design Procedure

To keep the 1A nominal current in the 0V to 4V current-sense range, calculate the $R_{(SNS)}$ resistor using Equation 1. To achieve better current-sense accuracy, a 1% tolerance or better resistor is preferred.

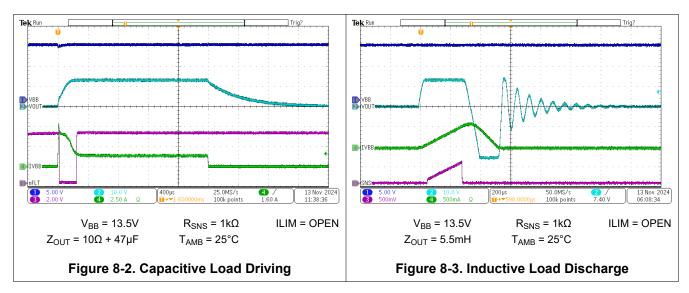
$$V_{ADC,min} \times K_{SNS} / I_{LOAD,min} \le R_{SNS} \le (V_{SNSFH} - V_{HR}) \times K_{SNS} / I_{LOAD,max}$$
(7)

The design requirement listed in Table 8-2 yields $520\Omega \le R_{SNS} \le 4160\Omega$, and $1k\Omega$ R_{SNS} satisfies the requirements.

To set the adjustable current limit value, use the $R_{(ILIM)}$ recommended in the Table 7-1. In this application, to leave enough margin for the current transient and ripple, a 45.3k Ω R_{ILIM} resistor satisfies the requirements.

8.2.3 Application Curves

Figure 8-2 shows a test example of soft-start when driving a big capacitive load. Figure 8-3 shows the VDS clamp engaging during inductive load discharge.



8.3 Power Supply Recommendations

The device is qualified for both automotive and industrial applications. The normal power supply connection is a 24V/48V automotive system.



Table 8-3. Voltage Operating Ranges

VBB VOLTAGE RANGE	NOTE
6V to 58V	Nominal 24V/48V automotive battery voltage range. All parametric specifications apply and the device is fully functional and protected.
58V to 70V for unidirectional clamp version	Extended upper 48V automotive battery operation. Device is fully functional and protected but some parametrics such as R _{ON} , current sense accuracy, current limit accuracy, and timing parameters can deviate from specifications. Check the individual specifications in Section 6.5 to confirm the voltage range it is applicable for.
58V to 65V for bidirectional clamp version	Extended upper 48V automotive battery operation. Device is fully functional and protected but some parametrics such as R _{ON} , current sense accuracy, current limit accuracy, and timing parameters can deviate from specifications. Check the individual specifications in Section 6.5 to confirm the voltage range it is applicable for.
65V to 80V for bidirectional clamp version	Max of 100µs duration is allowed in this voltage range. Device is operational and lets the pulse pass through without being damaged but does not protect against short circuits.

8.4 Layout

8.4.1 Layout Guidelines

To prevent thermal shutdown, T_J must be less than 150°C. The HTSSOP package has good thermal impedance. However, the PCB layout is very important. Good PCB design can optimize heat transfer, which is absolutely essential for the long-term reliability of the device.

- Maximize the copper coverage on the PCB to increase the thermal conductivity of the board. The major heat
 flow path from the package to the ambient is through the copper on the PCB. Maximum copper is extremely
 important when there are not any heat sinks attached to the PCB on the other side of the package.
- Add as many thermal vias as possible directly under the package ground pad to optimize the thermal conductivity of the board.
- All thermal vias should either be plated shut or plugged and capped on both sides of the board to prevent solder voids. To ensure reliability and performance, the solder coverage should be at least 85%.

8.4.2 Layout Examples

8.4.2.1 Without a GND Network

Without a GND network, tie the GND pin to the board GND copper directly. Put thermal vias under VBB pin for better thermal performance.



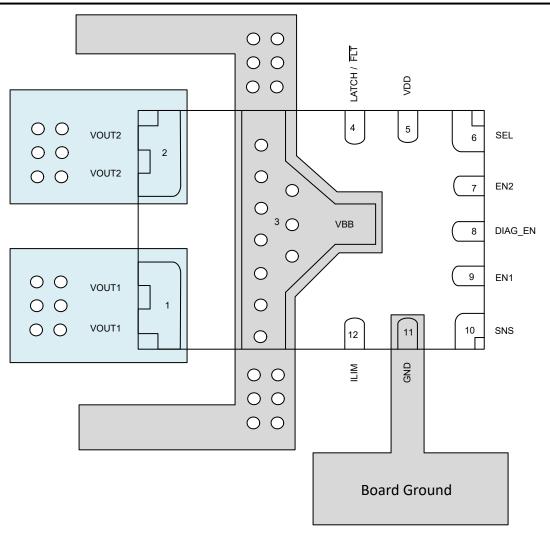


Figure 8-4. Layout Example Without a GND Network



8.4.2.2 With a GND Network

With a GND network, have the IC GND and board GND connected via the ground network. Put thermal vias under VBB pin for better thermal performance.

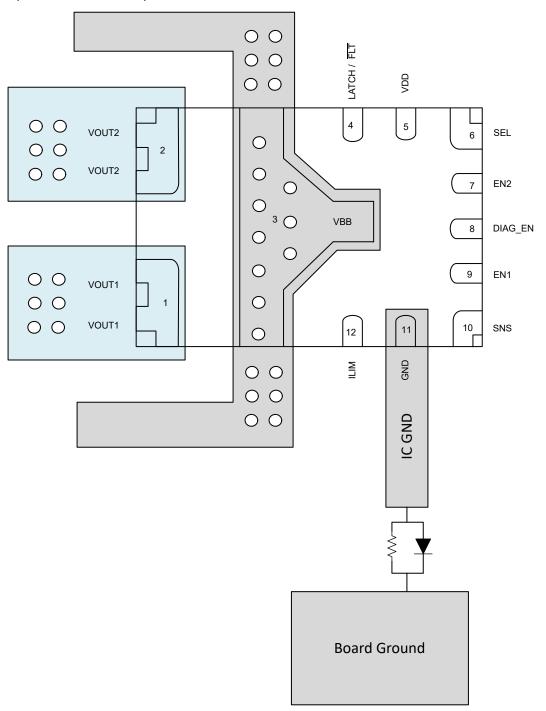


Figure 8-5. Layout Example With a GND Network



9 Device and Documentation Support

9.1 Receiving Notification of Documentation Updates

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9.5 Glossary

TI Glossary

This glossary lists and explains terms, acronyms, and definitions.

10 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

DATE	TE REVISION NOTES			
March 2025	*	Initial Release		

11 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most-current data available for the designated device. This data is subject to change without notice and without revision of this document. For browser-based versions of this data sheet, see the left-hand navigation pane.

www.ti.com 5-Jul-2025

PACKAGING INFORMATION

Orderable part number	Status	Material type	Package Pins	Package qty Carrier	RoHS (3)	Lead finish/ Ball material	MSL rating/ Peak reflow	Op temp (°C)	Part marking (6)
PTPS482H85AQCHURQ1	Active	Preproduction	VQFN-HR (CHU) 12	3000 LARGE T&R	-	Call TI	Call TI	-40 to 125	
PTPS482H85BQCHURQ1	Active	Preproduction	VQFN-HR (CHU) 12	3000 LARGE T&R	-	Call TI	Call TI	-40 to 125	
PTPS482H85BQCHURQ1.A	Active	Preproduction	VQFN-HR (CHU) 12	3000 LARGE T&R	-	Call TI	Call TI	-40 to 125	

⁽¹⁾ Status: For more details on status, see our product life cycle.

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⁽⁵⁾ MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

⁽⁶⁾ Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

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