







OPA396 SBOSA65 - JULY 2021

OPA396 Precision, Low I_Q, Low Input Bias Current Op Amp

1 Features

Low Io: 23.5 µA

Gain bandwidth product: 1 MHz

Low input bias current: 10 fA (typical)

Low offset voltage: ±100 µV (maximum)

Low drift: ±1.2 µV/°C

Low supply voltage operation: 1.7 V to 5.5 V

Input common mode range ±100 mV beyond rail

Fast slew rate: 1 V/us

High load capacitance drive

High output current drive: 60 mA

Rail-to-rail output

EMI/RFI filtered inputs

Small packages: SC70 and WCSP (Preview)

2 Applications

- Portable electronics
- Flow transmitter
- Blood glucose monitor
- Process analytics (pH, gas, force, humidity)
- Temperature transmitter
- Pressure transmitter
- Medical sensor patches
- **Building automation**
- Wearable fitness and activity monitor
- Gas detector
- Analog security camera

3 Description

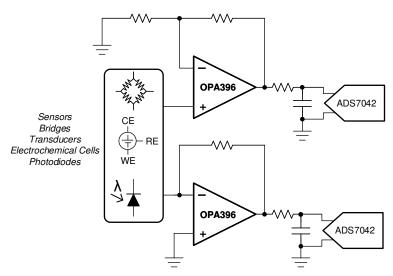
The OPA396 features a combination of high bandwidth (1 MHz) along with very low quiescent current (23.5 µA) in a high-precision amplifier. These features combined with rail-to-rail input and output make this device an exceptional choice in high-gain, low-power applications. Ultra-low input bias current of 10 fA, 100 μV of offset (maximum), and 1.2 μV/°C of drift over temperature help maintain high precision in ratiometric and amperometric sensor front ends that have demanding low-power requirements.

The OPA396 uses Texas Instrument's proprietary e-trim[™] operational amplifier technology, enabling a unique combination of ultra-low offset and low input offset drift without the need for any input switching or auto-zero techniques. The CMOS-based technology platform also features a modern, robust output stage design that is tolerant of high output capacitance, alleviating stability problems that are common in typical low-power amplifiers.

Device Information

PART NUMBER	PACKAGE ⁽¹⁾	BODY SIZE (NOM)
OPA396	SC-70 (5)	2.00 mm x 1.25 mm

For all available packages, see the package option addendum at the end of the data sheet.



High-Input-Impedance, Low-Offset Buffer



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4 Revision History

DATE	REVISION	NOTES
July 2021	*	Initial Release



5 Pin Configuration and Functions

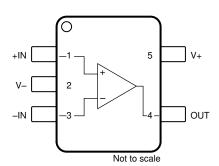


Figure 5-1. DCK Package, 5-Pin SC70, Top View

Table 5-1. Pin Functions

PIN		I/O	DESCRIPTION	
NAME	NO.	1/0	DESCRIPTION	
-IN	3	I	Inverting input	
+IN	1	I	Noninverting input	
OUT	4	0	Output	
V-	2	_	Negative (lowest) power supply	
V+	5	_	Positive (highest) power supply	



6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)(1)

			MIN	MAX	UNIT
Vs	Supply veltage V = (VI) (VI)	Single-supply		6	V
VS	Supply voltage, $V_S = (V+) - (V-)$	Dual-supply		±3	V
	Input voltage, all pins	Common-mode	(V-) - 0.5	(V+) + 0.5	V
	Input voltage, all pills	Differential		(V+) - (V-) + 0.5	
	Input current, all pins			±10	mA
	Output short circuit ⁽²⁾		Continuous	Continuous	
T _A	Operating temperature		-55	150	°C
T _{stg}	Storage temperature		-65	150	°C

⁽¹⁾ Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

6.2 ESD Ratings

			VALUE	UNIT
V _(ESD) Electrostatic discharge		Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	±2000	V
V _(ESD)	Electrostatic discharge	Charged-device model (CDM), per JEDEC specification JESD22-C101 ⁽²⁾	±500	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \

¹⁾ JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

	3 1 3 1				
			MIN	NOM MAX	UNIT
V-	Supply voltage, $V_S = (V+) - (V-)$	Single-supply	1.7	5.5	V
V _S Su	Supply voltage, $v_S = (v_T) = (v_T)$	Dual-supply	±0.85	±2.75	\
	Input voltage	Differential	-0.5	+0.5	
T _A	Specified temperature		-40	125	°C

6.4 Thermal Information

		OPA396	
	THERMAL METRIC ⁽¹⁾	DCK (SC70)	UNIT
		5 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	214	°C/W
R _{θJC(top)}	Junction-to-case (top) thermal resistance	115	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	58	°C/W
Ψ_{JT}	Junction-to-top characterization parameter	29	°C/W
Ψ_{JB}	Junction-to-board characterization parameter	58	°C/W
R _{θJC(bot)}	Junction-to-case (bottom) thermal resistance	N/A	°C/W

For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.

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⁽²⁾ Short-circuit to ground, one amplifier per package.

⁽²⁾ JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.



6.5 Electrical Characteristics

at V_S = 1.7 V to 5.5 V, T_A = 25°C, and V_{CM} = V_S / 2 (unless otherwise noted)

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
OFFSET	VOLTAGE			<u> </u>			
		V _S = 5.0 V			±10	±100	
	Input offset voltage	V _{CM} = (V+) – 0.3 V, V _S = 5.0 V			±60	±750	.,
V _{OS}		N/ 0/ \ 0.4\V			±15	±100	μV
		$V_{CM} = (V-) - 0.1 V$	$T_A = -40^{\circ}\text{C to } +125^{\circ}\text{C}^{(1)}$			±600	
dV _{OS} /dT	Input offset voltage	$T_A = 0^{\circ}C \text{ to } 85^{\circ}C^{(1)}$			±1	±5	μV/°C
uv _{OS} /u1	drift	$T_A = -40^{\circ}\text{C to } +125^{\circ}\text{C}^{(1)}$			±1.2	±6	μν/ С
PSRR	Power supply rejection ratio	V _{CM} = (V–) – 0.1 V				40	μV/V
INPUT B	IAS CURRENT						
	I	$T_A = 25^{\circ}C^{(1)}$			±0.01	10	^
I _B	Input bias current	$T_A = -40^{\circ}\text{C to } +125^{\circ}\text{C}^{(1)}$			±3.78		рA
	Input offset surrent	$T_A = 25^{\circ}C^{(1)}$			±0.01	10	~ Λ
los	Input offset current	$T_A = -40$ °C to +125°C ⁽¹⁾			±1.00		рA
NOISE							
	Input voltage noise	f = 0.1 Hz to 10 Hz, V _{CM} = V			0.91		μV_{RMS}
Input voltage noise		1 - 0.1 HZ tO 10 HZ, V _{CM} -	0.1112 to 10112, V _{CM}		6.0		μV_{PP}
		f = 10 Hz			130		
e _n	Input voltage noise density	f = 1 kHz			60		nV/√ Hz
	,	f = 10 kHz			55		
i _n	Input current noise density	f = 1 kHz			30		fA/\sqrt{Hz}
INPUT V	OLTAGE						
V _{CM}	Common-mode voltage	$T_A = -40^{\circ}\text{C to } +125^{\circ}\text{C}^{(1)}$		(V–) – 0.1 V		(V+) + 0.1 V	V
		$(V-) - 0.1 V \le V_{CM} \le (V+)$	– 1.5 V	89	100		
CMDD	Common-mode	$(V-) - 0.1 V \le V_{CM} \le$		100	121		٩D
CMRR	rejection ratio	$(V+) - 1.5 \text{ V}, \text{ V}_S = 5.5 \text{ V}$	$T_A = -40^{\circ}\text{C to } + 125^{\circ}\text{C}^{(1)}$	90	100		dB
		$(V+) - 0.6 V \le V_{CM} \le (V+)$	+ 0.1 V		69		
INPUT IN	MPEDANCE						
Z _{id}	Differential input impedance				0.1 1		GΩ pF
Z _{ic}	Common-mode input impedance				1 1		TΩ pF



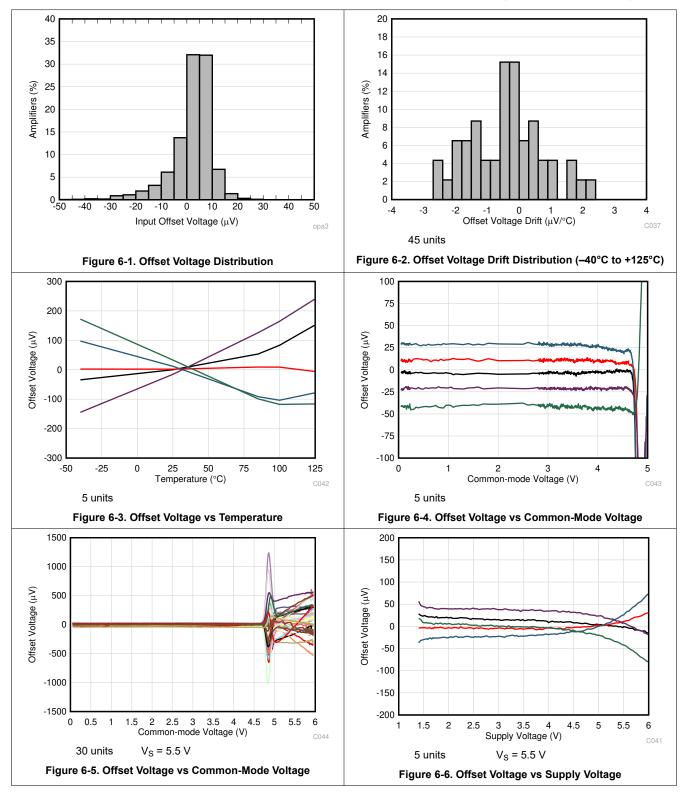
6.5 Electrical Characteristics (continued)

at V_S = 1.7 V to 5.5 V, T_A = 25°C, and V_{CM} = V_S / 2 (unless otherwise noted)

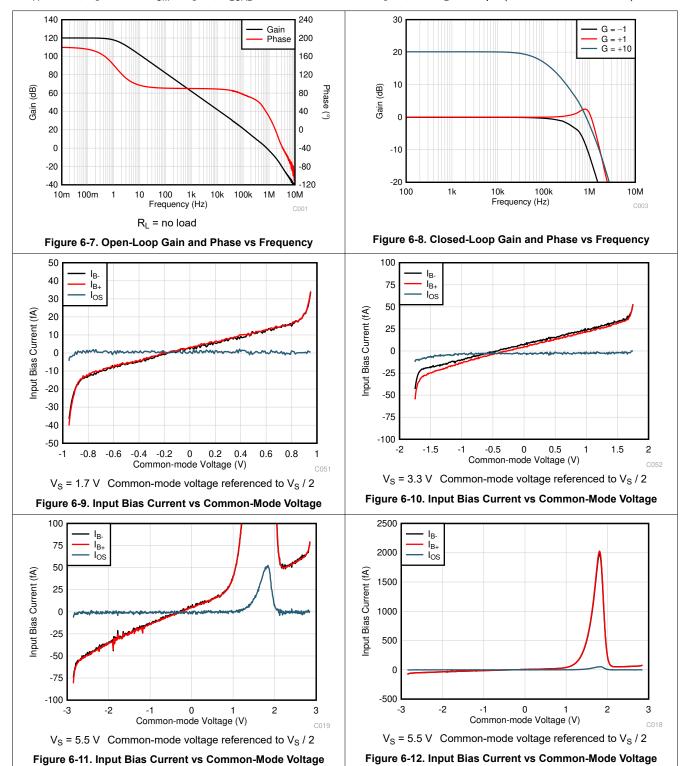
	PARAMETER	1	TEST CONDITIONS	MIN	TYP	MAX	UNIT	
OPEN-L	LOOP GAIN							
		V _S = 5.5 V	$(V-) + 0.1 V < V_O < (V+) - 0.1 V,$ $V_{CM} = (V-) -100 \text{ mV},$ $R_L = 10 \text{ k}\Omega$	100	121			
٨	Open-loop voltage	V _S - 5.5 V		100	121		dB	
A _{OL}	gain	V = 4.7.V	$(V-) + 0.1 V < V_O < (V+) - 0.1 V,$ $V_{CM} = (V+) - 1.5 V,$ $R_L = 10 k\Omega$	90	113		αБ	
		V _S = 1.7 V	$(V-) + 0.45 V < V_O < (V+) - 0.45 V,$ $V_{CM} = (V+) - 1.5 V,$ $R_L = 2 k\Omega$	90	107			
FREQU	ENCY RESPONSE							
			I_{OUT} = 0 μA, R_L = 10 k Ω		450		kHz	
UGB	Unity-gain bandwidth	G = 1	I_{OUT} = 0 μA, R_L = 50 k Ω		0.85		MHz	
			I_{OUT} = 100 μA, R_{L} = 10 kΩ		0.75		IVITZ	
GBW	Gain-bandwidth product				1		MHz	
SR	Slew rate	G = -1, 4-V step			1		V/µs	
t _S	Settling time	To 0.1%, V _S = 5.5, G =	1, 1-V step		8		μs	
t _{OR}	Overload recovery time	V _{IN} x G = V _S			15		μs	
OUTPU	Т							
		No load				3		
\/	Voltage output	R _L = 10 kΩ				10	m\/	
Vo	swing from rail	$R_L = 2 \text{ k}\Omega$ $T_A = -40^{\circ}\text{C to } +125^{\circ}\text{C}$, both rails, $R_L = 10 \text{ k}\Omega^{(1)}$				40	mV	
						10		
I _{SC}	Short-circuit current	V _S = 5.5 V	/ _S = 5.5 V		60		mA	
Z _O	Open-loop output impedance	= 1 MHz, I _{OUT} = 100 μA			4		kΩ	
POWER	R SUPPLY		-					
l _Q	Quiescent current per amplifier	V _{CM} = (V+) – 1.5 V	$T_A = -40^{\circ}\text{C to } +125^{\circ}\text{C}^{(1)}$		23.5	30 32	μA	

⁽¹⁾ Specification established from device population bench system measurements across multiple lots.

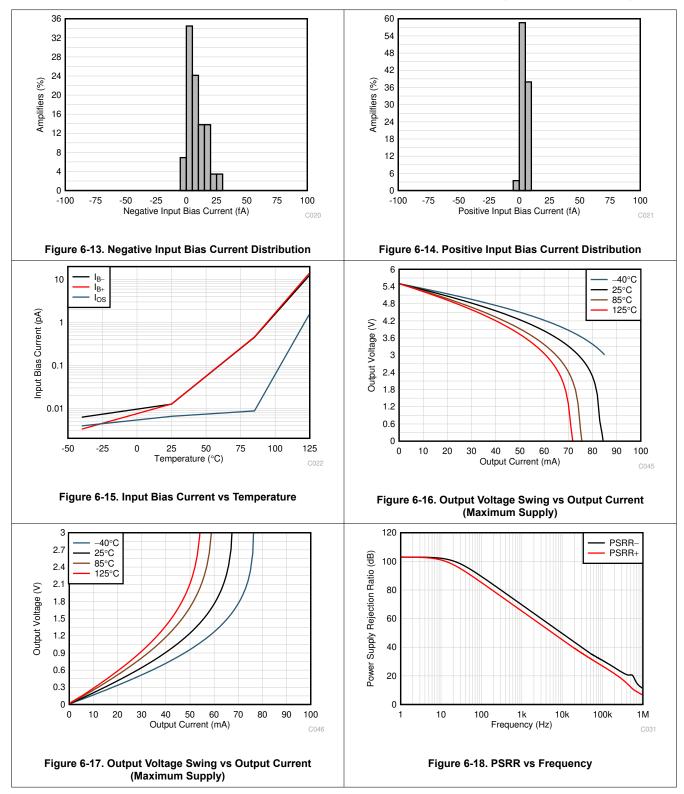
6.6 Typical Characteristics



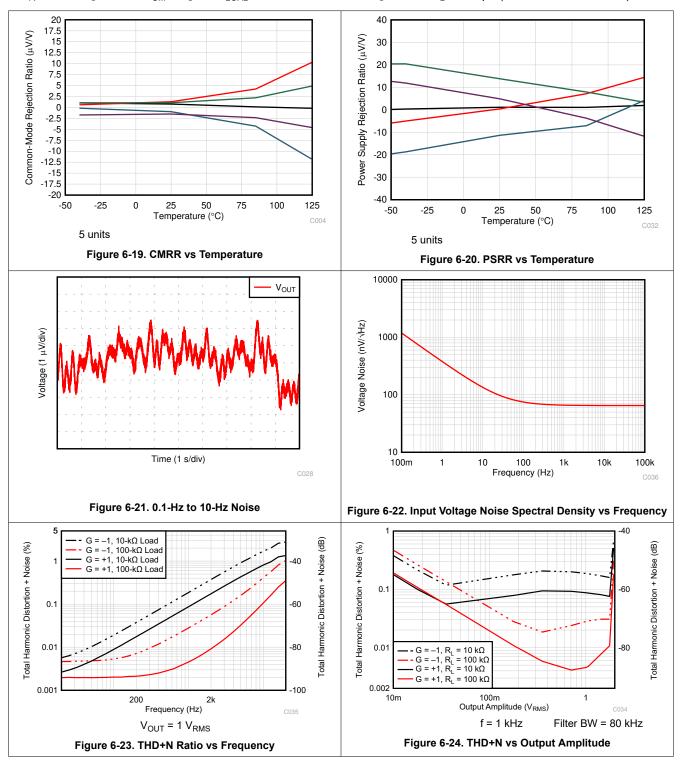




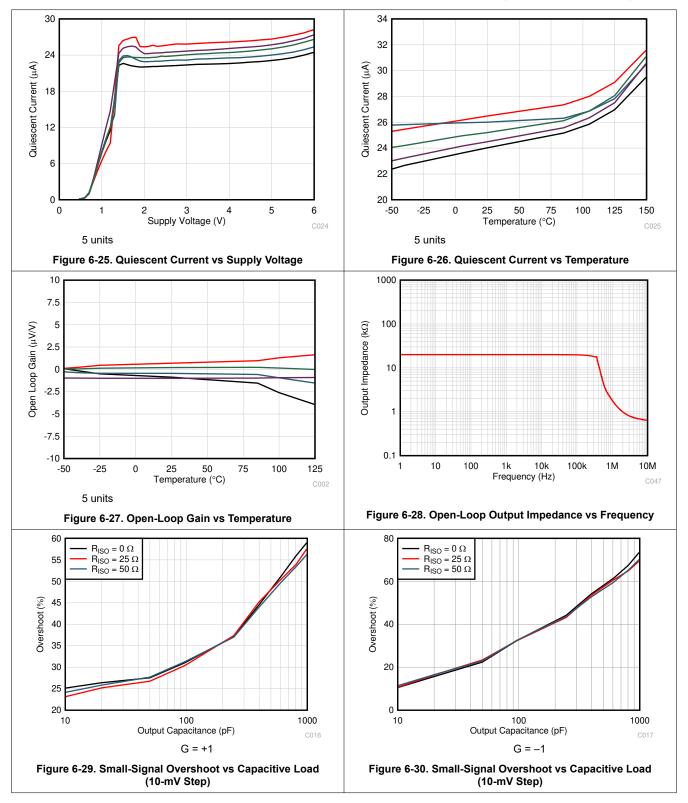




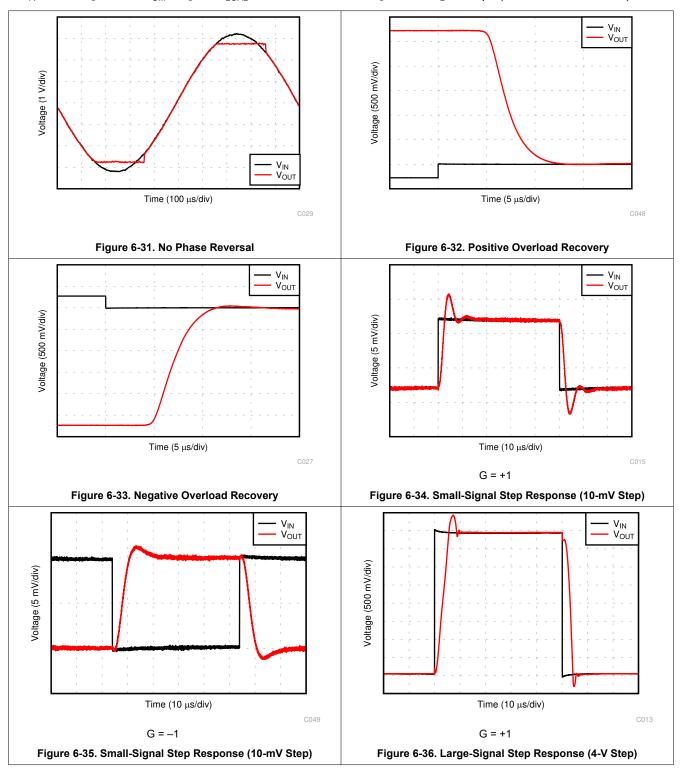




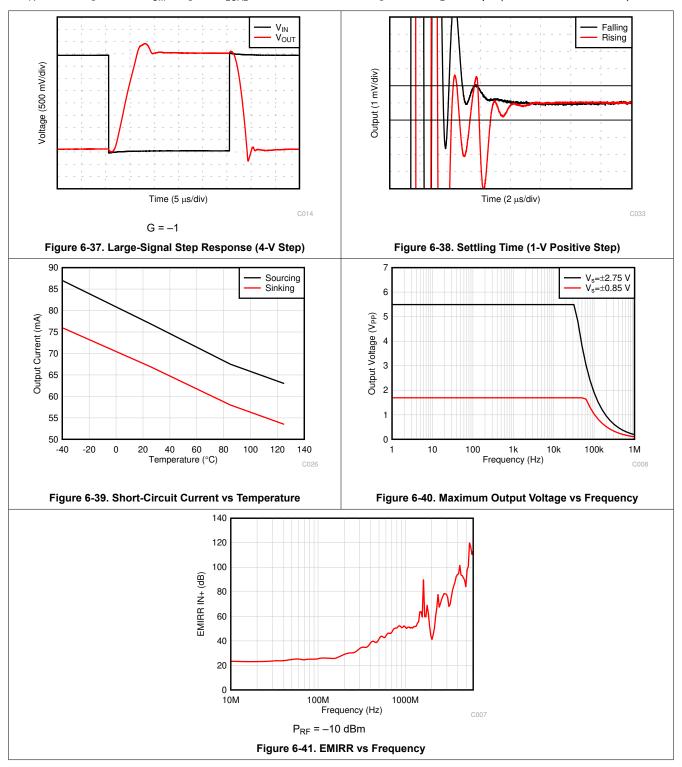














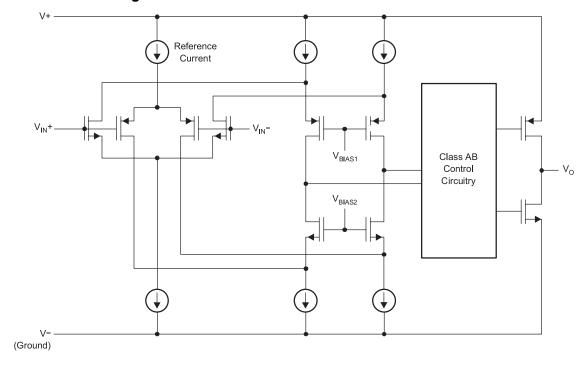
7 Detailed Description

7.1 Overview

The OPA396 is a low-offset, low-power e-trim operational amplifier (op amp) that uses a proprietary offset trim technique. This op amp offers ultra-low input offset voltage, drift and input bias current while achieving an excellent bandwidth-to-quiescient-current ratio. The OPA396 operates from 1.7 V to 5.5 V, is unity-gain stable, and is designed for a wide range of general-purpose and precision applications.

The output features an advanced output stage that tolerates high capacitive loading for solid and stable performance. The OPA396 strengths make this device an excellent amplifier for high-impedance sensors, where input bias current, offset voltage, and power consumption are critical.

7.2 Functional Block Diagram





7.3 Feature Description

7.3.1 Low Input Bias Current

The OPA396 achieves very low input bias current as a results of CMOS inputs and advanced ESD protection circuitry. Input bias current (I_B) is primarily a function of the input protection scheme in CMOS input amplifiers. If careful consideration is not taken with the ESD cells, a CMOS input device can exhibit large input bias currents, especially over temperature. The OPA396 achieves excellent input bias current ratings of ± 30 pA maximum at 125° C.

7.3.2 Input Differential Voltage

The OPA396 does not have any diodes connected between the input nodes, allowing for input voltages anywhere between the supply voltage. The input structure can be seen in Figure 7-1. Although the device can tolerate any differential input voltage that does not exceed the supply voltage, do not operate continuously at differential input voltages greater than 0.5 V.

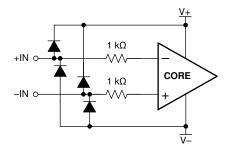


Figure 7-1. Equivalent Input Circuit

7.3.3 Capacitive Load Drive

The OPA396 features advanced output drive circuitry that can maintain stability even with capacitive loads as high as 1 nF. Many low-quiescent-current amplifiers exhibit poor stability when connected to a capacitive load as a result of the low levels of current used to bias the output stage. The OPA396 is designed with an output stage that adapts to high capacitive loads without sacrificing additional current consumption. This feature gives a highly stable device across all temperature and supply conditions, enabling robust system performance.

7.3.4 EMI Rejection

The OPA396 uses integrated electromagnetic interference (EMI) filtering to reduce the effects of EMI interference from sources such as wireless communications and densely-populated boards with a mix of analog signal chain and digital components. EMI immunity can be improved with circuit design techniques; the OPA396 benefits from these design improvements. Texas Instruments has developed the ability to accurately measure and quantify the immunity of an operational amplifier over a broad frequency spectrum extending from 10 MHz to 6 GHz. Figure 7-2 shows the results of this testing on the OPA396. Table 7-1 lists the EMIRR +IN values for the OPA396 at particular frequencies commonly encountered in real-world applications. Applications listed in Table 7-1 may be centered on or operated near the particular frequency shown. Detailed information can also be found in the *EMI Rejection Ratio of Operational Amplifiers* application report, available for download from www.ti.com.

The electromagnetic interference (EMI) rejection ratio, or EMIRR, describes the EMI immunity of operational amplifiers. An adverse effect that is common to many op amps is a change in the offset voltage as a result of RF signal rectification. An op amp that is more efficient at rejecting this change in offset as a result of EMI has a higher EMIRR and is quantified by a decibel value. Measuring EMIRR can be performed in many ways, but this section provides the EMIRR +IN, which specifically describes the EMIRR performance when the RF signal is applied to the noninverting input pin of the op amp. In general, only the noninverting input is tested for EMIRR for the following three reasons:

- 1. Op amp input pins are known to be the most sensitive to EMI, and typically rectify RF signals better than the supply or output pins.
- 2. The noninverting and inverting op amp inputs have symmetrical physical layouts and exhibit nearly matching EMIRR performance.
- 3. EMIRR is more simple to measure on noninverting pins than on other pins because the noninverting input terminal can be isolated on a PCB. This isolation allows the RF signal to be applied directly to the noninverting input terminal with no complex interactions from other components or connecting PCB traces.

High-frequency signals conducted or radiated to any pin of the operational amplifier may result in adverse effects because the amplifier does not have sufficient loop gain to correct for signals with spectral content outside the bandwidth. Conducted or radiated EMI on inputs, power supply, or output may result in unexpected dc offsets, transient voltages, or other unknown behavior. Make sure to properly shield and isolate sensitive analog nodes from noisy radio signals, digital clocks, and interfaces.

The EMIRR +IN of the OPA396 is plotted versus frequency as shown in Figure 7-2. The OPA396 unity-gain bandwidth is 1 MHz. EMIRR performance less than this frequency denotes interfering signals that fall within the op amp bandwidth.

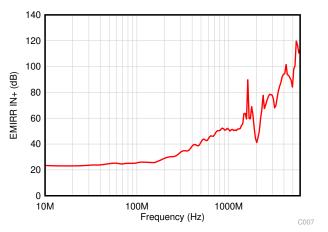


Figure 7-2. EMIRR Testing

Table 7-1. OPA396 EMIRR IN+ for Frequencies of Interest

FREQUENCY	APPLICATION AND ALLOCATION	EMIRR IN+
400 MHz	Mobile radio, mobile satellite, space operation, weather, radar, ultra-high frequency (UHF) applications	39.1 dB
900 MHz	Global system for mobile communications (GSM) applications, radio communication, navigation, GPS (to 1.6 GHz), GSM, aeronautical mobile, UHF applications	
1.8 GHz	GSM applications, mobile personal communications, broadband, satellite, L-band (1 GHz to 2 GHz)	61.3 dB
2.4 GHz	802.11b, 802.11g, 802.11n, Bluetooth®, mobile personal communications, industrial, scientific and medical (ISM) radio band, amateur radio and satellite, S-band (2 GHz to 4 GHz)	69.8 dB
3.6 GHz	Radiolocation, aero communication and navigation, satellite, mobile, S-band	82.5 dB
5 GHz	802.11a, 802.11n, aero communication and navigation, mobile communication, space and satellite operation, C-band (4 GHz to 8 GHz)	83.6 dB

7.4 Device Functional Modes

The OPA396 has a single functional mode and is operational when the power-supply voltage is greater than $1.7 \text{ V} (\pm 0.85 \text{ V})$. The maximum specified power-supply voltage for the OPA396 is $5.5 \text{ V} (\pm 2.75 \text{ V})$.

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8 Application and Implementation

Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

8.1 Application Information

The OPA396 is a unity-gain stable, precision operational amplifier free from unexpected output and phase reversal. The OPA396 is optimized for full rail-to-rail input, allowing for low-voltage, single-supply operation or split-supply use. These miniature, high-precision, low-noise amplifiers offer high-impedance inputs that have a common-mode range 100 mV beyond the supplies and can tolerate the full supply voltage across the input. The OPA396 precision amplifier is designed for sensor amplification, low-power analog signal chain applications in low or high gains, as well as a low-power discrete MOSFET or bipolar driver.

8.2 Typical Applications

8.2.1 Three-Terminal CO Gas Sensor

Figure 8-1 shows a simple micropower potentiostat circuit for use with three-terminal unbiased CO sensors. This same design is applicable to many other type of three-terminal gas sensors or electrochemical cells. The basic sensor has three electrodes: the sense or working electrode (WE), counter electrode (CE) and reference electrode (RE). A current flows between CE and WE proportional to the detected concentration. The RE monitors the potential of the internal reference point. For an unbiased sensor, the WE and RE must be maintained at the same potential by adjusting the bias on CE. Through the potentiostat circuit formed by U1, the servo feedback action maintains the RE pin at a potential set by V_{REF} . R1 maintains stability as a result of the large capacitance of the sensor. C1 and R2 form the potentiostat integrator and set the feedback time constant. U2 forms a transimpedance amplifier (TIA) to convert the resulting sensor current into a proportional voltage. The transimpedance gain, and resulting sensitivity, is set by R_F according to Equation 1:

$$V_{TIA} = (-I * R_F) + V_{REF}$$
 (1)

 R_{Load} is a load resistor with a value that is normally specified by the sensor manufacturer (typically, 10 Ω). The potential at WE is set by the applied V_{REF} .

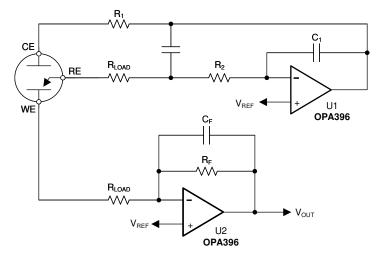


Figure 8-1. Three-Terminal CO Gas Sensor



8.2.1.1 Design Requirements

For this example, an electrical model of a CO sensor is used to simulate the sensor performance, as shown in Figure 8-2. The simulation is designed to model a CO sensor with a sensitivity of 69 nA/ppm. The supply voltage and maximum analog-to-digital converter (ADC) input voltage is 2.5 V, and the maximum concentration is 300 ppm.

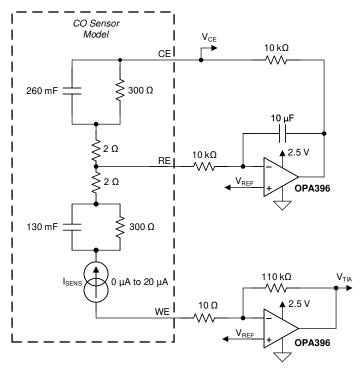


Figure 8-2. CO Sensor Simulation Schematic

8.2.1.2 Detailed Design Procedure

First, determine the V_{REF} voltage. This voltage is a compromise between maximum headroom and resolution, as well as allowance for the minimum swing on the CE terminal because the CE terminal generally goes negative in relation to the RE potential as the concentration (sensor current) increases. Bench measurements found the difference between CE and RE to be 180 mV at 300 ppm for this particular sensor. To allow for negative CE swing, footroom, and voltage drop across the 10-k Ω resistor, 300 mV is chosen for V_{RFF} .

$$V_{ZFRO} = V_{RFF} = 300 \text{ mV}$$
 (2)

where

- V_{REF} is the reference voltage (300 mV).
- V_{ZERO} is the concentration voltage (300 mV).

Next, calculate the maximum sensor current at highest expected concentration:

$$I_{SENSMAX} = I_{PERPPM} * ppmMAX = 69 \text{ nA} * 300 \text{ ppm} = 20.7 \mu A$$
 (3)

where

- I_{SENSMAX} is the maximum expected sensor current.
- I_{PERPPM} is the manufacturer specified sensor current in amperes per ppm.
- ppmMAX is the maximum required ppm reading.



Then, find the available output swing range greater than the reference voltage available for the measurement:

$$V_{SWING} = V_{OUTMAX} - V_{ZERO} = 2.5 V - 0.3 V = 2.2 V$$
 (4)

where

- V_{SWING} is the expected change in output voltage.
- V_{OUTMAX} is the maximum amplifier output swing.

Finally, calculate the transimpedance resistor (R_F) value using the maximum swing and the maximum sensor current:

$$R_F = V_{SWING} / I_{SENSMAX} = 2.2 \text{ V} / 20.7 \text{ } \mu\text{A} = 106.28 \text{ k}\Omega \text{ (use 110 k}\Omega \text{ for a common value)} \tag{5}$$

8.2.1.3 Application Curve

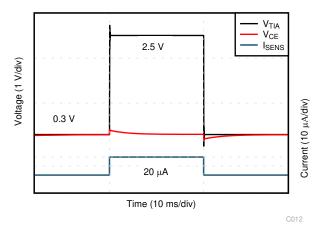


Figure 8-3. Sensor Transient Response to Simulated 300-ppm CO Exposure

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8.2.2 4-mA to 20-mA Loop Design

Factory automation systems commonly use the 4-mA to 20-mA (4-20 mA) communication protocol to enable process automation. In typical 2-wire, 4-mA to 20-mA loop applications, power to the remote transmitter is limited to less than 4 mA total consumption. As a result of the power limitations, low power consumption is essential. The OPA396 solves many design challenges in 4-mA to 20-mA loop applications, where low power, high accuracy, and high bandwidth are required.

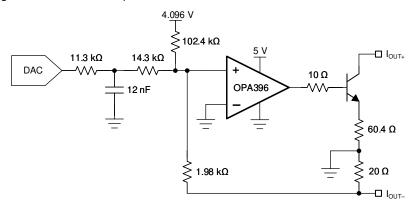


Figure 8-4. 4-20 mA Loop Interface Schematic

8.2.2.1 Design Requirements

Table 8-1. Design Parameters

PARAMETER	VALUE
Total current consumption	< 100 µA
DAC control voltage	0 V to 4.096 V
Output current	4 mA to 20 mA

8.2.2.2 Application Curve

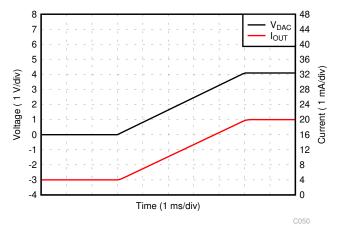


Figure 8-5. 4-mA to 20-mA Loop Response

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9 Power Supply Recommendations

The OPA396 device is specified for operation from 1.7 V to 5.5 V (±0.85 V to ±2.75 V).

10 Layout

10.1 Layout Guidelines

Paying attention to good layout practice is always recommended. Keep traces short, and when possible, use a printed-circuit board (PCB) ground plane with surface-mount components placed as close as possible to the device pins. Place a 0.1-µF capacitor closely across the supply pins. These guidelines must be applied throughout the analog circuit to improve performance and provide benefits, such as reducing the electromagnetic interference (EMI) susceptibility.

10.2 Layout Example

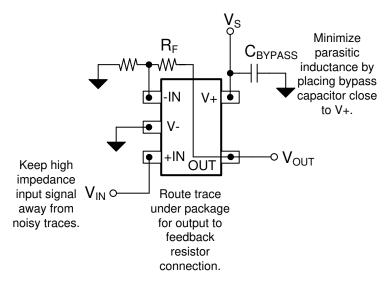


Figure 10-1. OPA396 Layout Example



11 Device and Documentation Support

11.1 Device Support

11.1.1 Development Support

11.1.1.1 TINA-TI™ Simulation Software (Free Download)

TINA-TI™ software is a simple, powerful, and easy-to-use circuit simulation program based on a SPICE engine. TINA-TI software is a free, fully-functional version of the TINA™ software, preloaded with a library of macromodels in addition to a range of both passive and active models. TINA-TI simulation software provides all the conventional dc, transient, and frequency domain analysis of SPICE, as well as additional design capabilities.

Available as a free download from the Analog eLab Design Center, TINA-TI software offers extensive post-processing capability that allows users to format results in a variety of ways. Virtual instruments offer the ability to select input waveforms and probe circuit nodes, voltages, and waveforms, creating a dynamic quick-start tool.

Note

These files require that either the TINA software (from DesignSoft[™]) or TINA-TI software be installed. Download the free TINA-TI software from the TINA-TI website.

11.2 Documentation Support

11.2.1 Related Documentation

For related documentation see the following:

- Texas Instruments, Highly-Accurate, Loop-Powered, 4mA to 20mA Field Transmitter With HART Modem reference design
- Texas Instruments, Micropower Electrochemical Gas Sensor Amplifier reference design
- Texas Instruments, Compensate Transimpedance Amplifiers Intuitively application report
- Texas Instruments, Designing With pH Electrodes application report

11.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. Click on *Subscribe to updates* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

11.4 Support Resources

TI E2E[™] support forums are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's Terms of Use.

11.5 Trademarks

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11.6 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.



11.7 Glossary

TI Glossary This glossary lists and explains terms, acronyms, and definitions.

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical packaging and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

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PACKAGING INFORMATION

Orderable part number	Status	Material type	Package Pins	Package qty Carrier	RoHS	Lead finish/	MSL rating/	Op temp (°C)	Part marking
	(1)	(2)			(3)	Ball material	Peak reflow		(6)
						(4)	(5)		
OPA396DCKR	Active	Production	SC70 (DCK) 5	3000 LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	1JJ
OPA396DCKR.A	Active	Production	SC70 (DCK) 5	3000 LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	1JJ
OPA396DCKRG4	Active	Production	SC70 (DCK) 5	3000 LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	1JJ
OPA396DCKRG4.A	Active	Production	SC70 (DCK) 5	3000 LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	1JJ
OPA396DCKT	Active	Production	SC70 (DCK) 5	250 SMALL T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	1JJ
OPA396DCKT.A	Active	Production	SC70 (DCK) 5	250 SMALL T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	1JJ

⁽¹⁾ Status: For more details on status, see our product life cycle.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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⁽²⁾ Material type: When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

⁽³⁾ RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

⁽⁴⁾ Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

⁽⁵⁾ MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

⁽⁶⁾ Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.



PACKAGE OPTION ADDENDUM

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PACKAGE MATERIALS INFORMATION

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TAPE AND REEL INFORMATION





A0	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

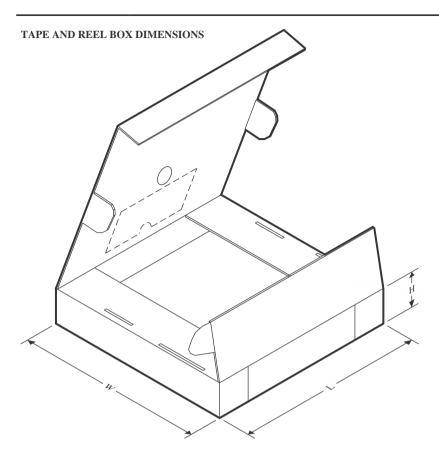
QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
OPA396DCKR	SC70	DCK	5	3000	178.0	9.0	2.4	2.5	1.2	4.0	8.0	Q3
OPA396DCKRG4	SC70	DCK	5	3000	178.0	9.0	2.4	2.5	1.2	4.0	8.0	Q3
OPA396DCKT	SC70	DCK	5	250	178.0	9.0	2.4	2.5	1.2	4.0	8.0	Q3

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*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
OPA396DCKR	SC70	DCK	5	3000	190.0	190.0	30.0
OPA396DCKRG4	SC70	DCK	5	3000	190.0	190.0	30.0
OPA396DCKT	SC70	DCK	5	250	190.0	190.0	30.0



SMALL OUTLINE TRANSISTOR



NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
 2. This drawing is subject to change without notice.
 3. Reference JEDEC MO-203.

- 4. Support pin may differ or may not be present.5. Lead width does not comply with JEDEC.
- 6. Body dimensions do not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.25mm per side



SMALL OUTLINE TRANSISTOR



NOTES: (continued)

7. Publication IPC-7351 may have alternate designs.8. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SMALL OUTLINE TRANSISTOR



NOTES: (continued)

- 9. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 10. Board assembly site may have different recommendations for stencil design.



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