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## 1.1 nV/VHz Noise, Low Power, Precision Operational Amplifier

Check for Samples: OPA211-HT

#### **FEATURES**

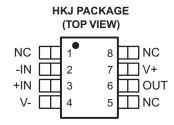
- Low Voltage Noise: 1.1 nV/√Hz at 1 kHz
- Input Voltage Noise:
   80 nV<sub>PP</sub> (0.1 Hz to 10 Hz)
- THD+N: -136dB (G = 1, f = 1 kHz)
- Offset Voltage: 240 µV (max)
- Offset Voltage Drift: 0.35 μV/°C (typ)
- Low Supply Current: 6 mA/Ch (typ)
- Unity-Gain Stable
- Gain Bandwidth Product:
   80 MHz (G = 100)
   45 MHz (G = 1)
- Slew Rate: 27 V/µs
- 16-Bit Settling: 700 ns
- Wide Supply Range:
   ±2.25 V to ±18 V, 4.5 V to 36 V
- Rail-to-rail output
- · Output current: 30 mA

## **APPLICATIONS**

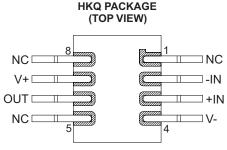
- Down-Hole Drilling
- High Temperature Environments

# SUPPORTS EXTREME TEMPERATURE APPLICATIONS

- Controlled Baseline
- One Assembly/Test Site
- One Fabrication Site
- Available in Extreme (-55°C/210°C)
   Temperature Range (1)
- Extended Product Life Cycle
- Extended Product-Change Notification
- Product Traceability
- Texas Instruments high temperature products utilize highly optimized silicon (die) solutions with design and process enhancements to maximize performance over extended temperatures.



NC denotes no internal connection



HKQ as formed or HKJ mounted dead bug

(1) Custom temperature ranges available

## DESCRIPTION

The OPA211 series of precision operational amplifiers achieves very low 1.1 nV/ $\sqrt{\text{Hz}}$  noise density with a supply current of only 3.6 mA. This series also offers rail-to-rail output swing, which maximizes dynamic range.

The extremely low voltage and low current noise, high speed, and wide output swing of the OPA211 series make these devices an excellent choice as a loop filter amplifier in PLL applications.

AA.

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.



In precision data acquisition applications, the OPA211 series of op amps provides 700-ns settling time to 16-bit accuracy throughout 10-V output swings. This ac performance, combined with only 240- $\mu$ V of offset and 0.35- $\mu$ V/°C of drift over temperature, makes the OPA211 ideal for driving high-precision 16-bit analog-to-digital converters (ADCs) or buffering the output of high-resolution digital-to-analog converters (DACs).

The OPA211 series is specified over a wide dual-power supply range of ±2.25 V to ±18 V, or for single-supply operation from 4.5 V to 36 V.

This series of op amps is specified from  $T_A = -55$ °C to 210°C.

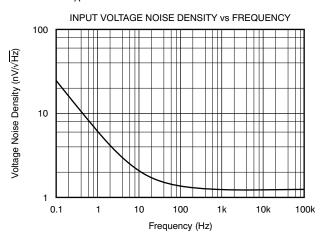


Table 1. ORDERING INFORMATION(1)

TA	PACKAGE	ORDERABLE PART NUMBER	TOP-SIDE MARKING
	HKJ	OPA211SHKJ	OPA211SHKJ
–55°C to 210°C	HKQ	OPA211SHKQ	OPA211SHKQ
	KGD	OPA211SKGD1	NA

(1) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI Web site at www.ti.com.



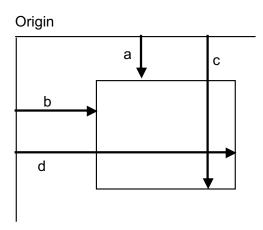
This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.



## **BARE DIE INFORMATION**

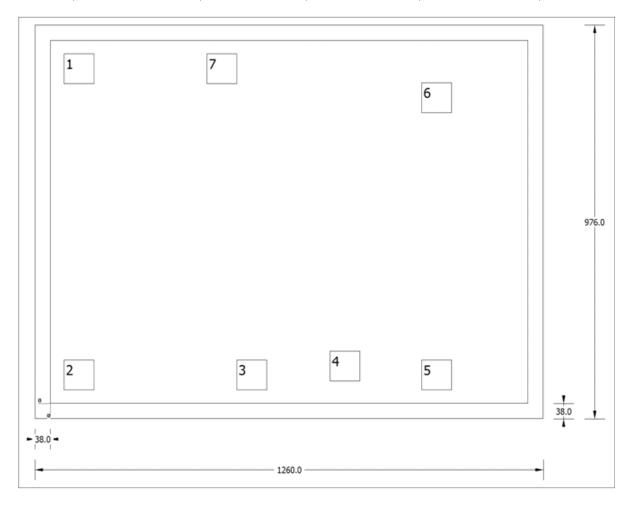
DIE THICKNESS	BACKSIDE FINISH	BACKSIDE POTENTIAL	BOND PAD METALLIZATION COMPOSITION		
15 mils.	Silicon with backgrind	V-	Al-Si-Cu (0.5%)		





## **Table 2. BOND PAD COORDINATES**

DESCRIPTION	PAD NUMBER	а	b	С	d
-IN	1	34.4000	792.000	109.400	867.000
+IN	2	34.4000	33.000	109.400	108.000
NC	3	461.850	33.000	536.850	108.000
V-	4	692.650	54.600	767.650	129.600
OUT	5	920.400	33.000	995.400	108.000
V+	6	920.400	720.150	995.400	795.150
NC	7	388.050	792.000	463.050	867.000



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## **ABSOLUTE MAXIMUM RATINGS**(1)

Over operating free-air temperature range (unless otherwise noted).

			VALUE	UNIT	
V <sub>S</sub> = (V=) - (V-)	Supply Voltage		40	V	
V <sub>IN</sub>	Input Voltage	Input Voltage			
I <sub>IN</sub>	Input Current (Any pin except power-	ower-supply pins) ±10			
	Output Short-Circuit <sup>(2)</sup>	Output Short-Circuit <sup>(2)</sup>			
T <sub>A</sub>	Operating Temperature	Operating Temperature			
T <sub>STG</sub>	Storage Temperature		-65 to 210	°C	
TJ	Junction Temperature		210	°C	
		Human Body Model (HBM)	3000	V	
	ESD Ratings	Charged Device Model (CDM)	1000	V	

<sup>(1)</sup> Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those specified is not supported.

#### THERMAL CHARACTERISTICS FOR HKJ OR HKQ PACKAGE

over operating free-air temperature range (unless otherwise noted)

	PARAME	MIN	TYP	MAX	UNIT	
0	0	to ceramic side of case			5.7	°C/W
θ <sub>JC</sub> Junction-to-ca	Junction-to-case thermal resistance			13.7	C/VV	

Product Folder Links: OPA211-HT

<sup>(2)</sup> Short-circuit to V<sub>S</sub>/2 (ground in symmetrical dual supply setups), one amplifier per package.



## ELECTRICAL CHARACTERISTICS: V<sub>S</sub> = ±2.25 V to ±18 V

At  $T_A = 25$ °C,  $R_L = 10~k\Omega$  connected to midsupply,  $V_{CM} = V_{OUT} =$  midsupply, unless otherwise noted.

. д ,		CIWI C	T <sub>A</sub>	= -55 to 1	25°C		T <sub>A</sub> = 210°C	:	
PARAMETER		CONDITIONS	MIN	TYP	MAX	MIN	TYP	MAX	UNIT
OFFSET VOLTAGE									
Input Offset Voltage	Vos	$V_S = \pm 15V$		±30	±180		±70	±260	μV
Drift	dV <sub>os</sub> /dT			0.35	1.5		0.35	2.0	μV/°C
vs Power Supply	PSRR	$V_S = \pm 2.25V \text{ to } \pm 18V$		0.1	3		0.1	3	μV/V
INPUT BIAS CURRENT									
Input Bias Current	$I_{B}$	$V_{CM} = 0V$		±60	±200		±60	±250	nA
Offset Current	Ios	$V_{CM} = 0V$		±25	±150		±25	±150	nA
NOISE									
Input Voltage Noise	$\mathbf{e}_{n}$	f = 0.1Hz to 10Hz		80			80		$nV_{PP}$
Input Voltage Noise Density		f = 10Hz		2			2		nV/√Hz
		f = 100Hz		1.4			1.4		nV/√Hz
		f = 1kHz		1.1			1.1		nV/√ <del>Hz</del>
Input Current Noise Density	In	f = 10Hz		3.2			3.2		pA/√ <del>Hz</del>
		f = 1kHz		1.7			1.7		pA/√ <del>Hz</del>
INPUT VOLTAGE RANGE <sup>(1)</sup>									
Common-Mode Voltage Range	$V_{\text{CM}}$	V <sub>S</sub> ≥ ±5V	(V-) + 1.8		(V+) - 1.4	(V-) + 1.8		(V+) - 1.4	V
		$V_S < \pm 5V$	(V-) + 2		(V+) - 1.4	(V-) + 2		(V+) - 1.4	V
Common-Mode Rejection Ratio	CMRR	$V_{S} \ge \pm 5V$ , $(V-) + 2V \le V_{CM} \le (V+) - 2V$	114	120		113	120		dB
		$V_S < \pm 5V, (V-) + 2V \le V_{CM} \le (V+) - 2V$	108	120		93	100		dB
INPUT IMPEDANCE									
Differential				20k    8			20k    8		Ω    pF
Common-Mode				10 <sup>9</sup>    2			10 <sup>9</sup>    2		Ω    pF
OPEN-LOOP GAIN									
Open-Loop Voltage Gain	$A_{OL}$	$(V-) + 0.2V \le V_0 \le (V+) - 0.2V,$ $R_L = 10k\Omega$	114	130		112	118		dB
	$A_OL$	$(V-) + 0.6V \le V_0 \le (V+) - 0.6V,$ $R_L = 600\Omega$	110	114		90	93		dB
FREQUENCY RESPONSE									
Gain-Bandwidth Product	GBW	G = 100		80			80		MHz
		G = 1		45			45		MHz
Slew Rate	SR			27			27		V/µs
Settling Time, 0.01%	t <sub>S</sub>	$V_S = \pm 15V$ , $G = -1$ , 10V Step, $C_L = 100pF$		490			580		ns
0.0015% (16-bit)		$V_S = \pm 15V$ , $G = -1$ , 10V Step, $C_L = 100pF$		700			750		ns
Overload Recovery Time		G = -10		500			500		ns
Total Harmonic Distortion + Noise	THD+N	$G = 1, f = 1kHz,$ $V_O = 3V_{RMS}, R_L = 600\Omega$		0.00001 5			0.000015		%
				-136			-136		dB

<sup>(1)</sup> The OPA211-HT is not intended to be used as a comparator due to its limited differential input range capability.



## ELECTRICAL CHARACTERISTICS: V<sub>S</sub> = ±2.25 V to ±18 V (continued)

At  $T_A = 25$ °C,  $R_L = 10 \text{ k}\Omega$  connected to midsupply,  $V_{CM} = V_{OUT} = \text{midsupply}$ , unless otherwise noted.

		T <sub>A</sub> = -55 to 125°C							
PARAMETER		CONDITIONS	MIN	TYP	MAX	MIN	TYP	MAX	UNIT
OUTPUT									
Voltage Output	$V_{OUT}$	$R_L = 10k\Omega, A_{OL} \ge 114dB$	(V-) + 0.2		(V+) - 0.2	(V-) + 0.2		(V+) - 0.2	V
		$R_L = 600\Omega$ , $A_{OL} \ge 110dB$ , $\pm 18V$	(V-) + 0.6		(V+) - 0.6	(V-) + 1.2		(V+) - 0.6	V
Short-Circuit Current	I <sub>sc</sub>			+35/-50			+30/-45		mA
Capacitive Load Drive	$C_{LOAD}$				See Typi	cal Characteris	tics		
Open-Loop Output Impedance	Z <sub>O</sub>	f = 1MHz		5					Ω
POWER SUPPLY									
Specified Voltage	Vs		±2.25		±18	±2.25		±18	V
Quiescent Current (per channel)	lα	I <sub>OUT</sub> = 0A		3.6 6			6.0	7.5	mA
TEMPERATURE RANGE									
Specified range		–55°C to 210°C							
Operating range		-55°C to 210°C							

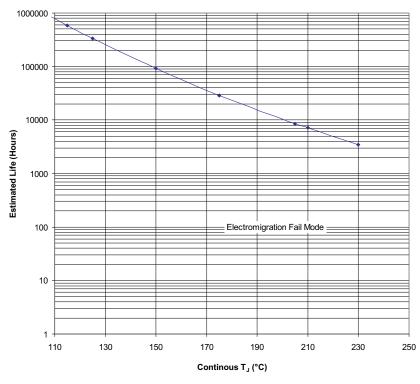


Figure 1. OPA211SKGD1 Operating Life Derating Chart

#### Notes:

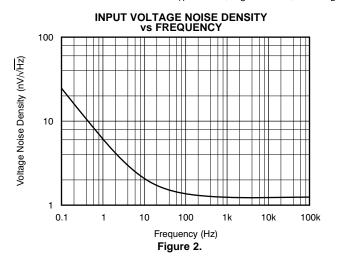
- 1. See datasheet for absolute maximum and minimum recommended operating conditions.
- 2. Silicon operating life design goal is 10 years at 105°C junction temperature (does not include package interconnect life).

Product Folder Links: OPA211-HT



#### **TYPICAL CHARACTERISTICS**

At  $T_A$  = 25°C,  $V_S$  = ±18 V, and  $R_L$  = 10 k $\Omega$ , unless otherwise noted.



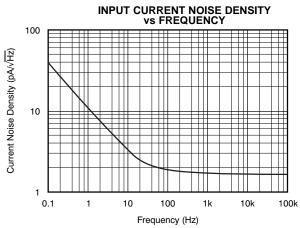
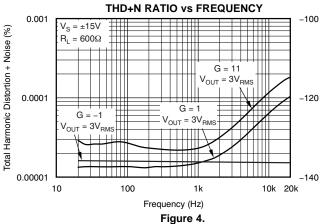
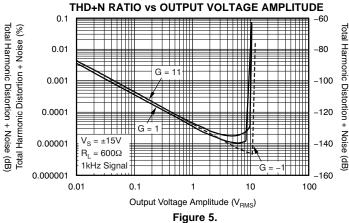


Figure 3.





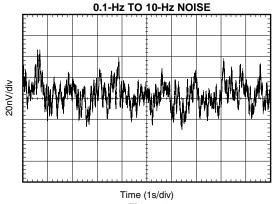
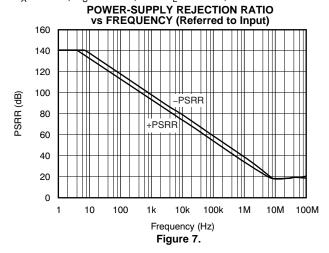
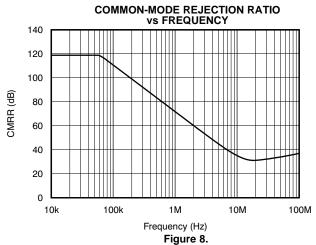


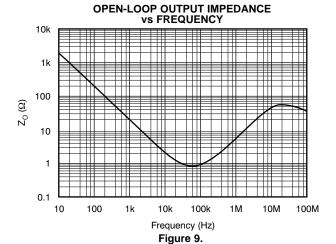
Figure 6.

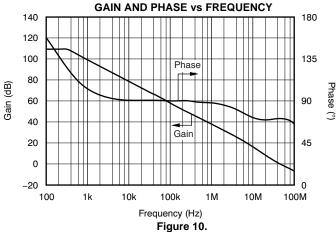


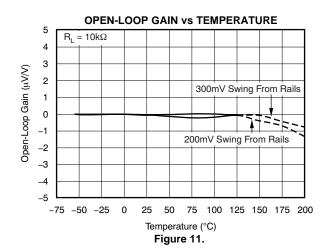
At  $T_{A}$  = 25°C,  $V_{S}$  = ±18 V, and  $R_{L}$  = 10  $k\Omega,$  unless otherwise noted.





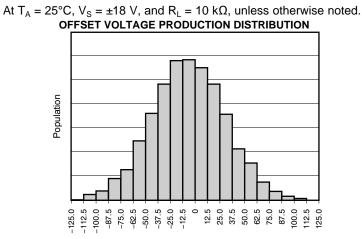






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Offset Voltage (µV) Figure 12.

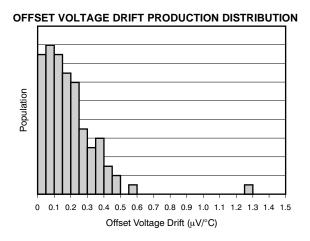
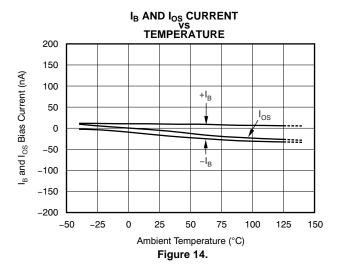
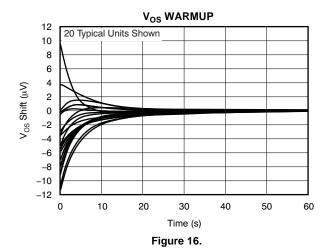
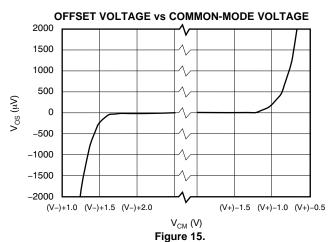


Figure 13.







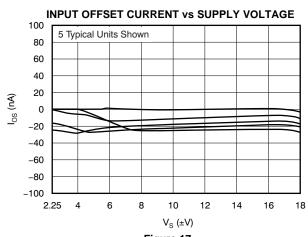
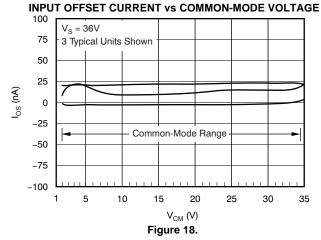
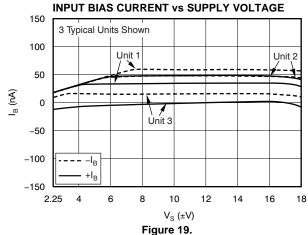


Figure 17.

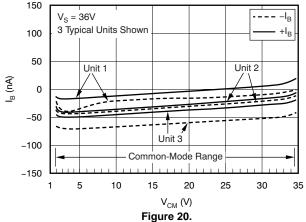


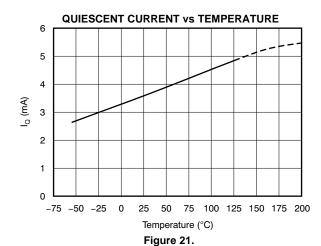
At  $T_{A}$  = 25°C,  $V_{S}$  = ±18 V, and  $R_{L}$  = 10  $k\Omega,$  unless otherwise noted.











#### QUIESCENT CURRENT vs SUPPLY VOLTAGE

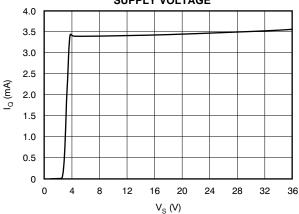


Figure 22.

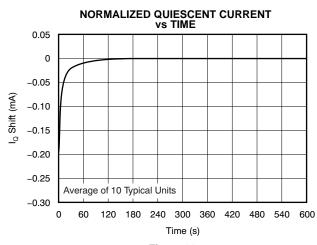
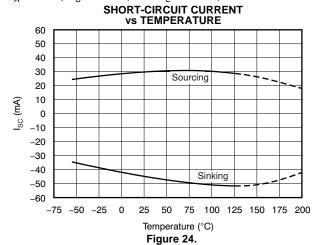


Figure 23.



At  $T_A$  = 25°C,  $V_S$  = ±18 V, and  $R_L$  = 10 k $\Omega$ , unless otherwise noted.



SMALL-SIGNAL STEP RESPONSE (100 mV) G = -1  $C_L = 10pF$   $G_{\theta} = -1$   $G_{\theta} = -1$ 

Figure 25.

Time (0.1µs/div)

SMALL-SIGNAL STEP RESPONSE (100 mV)

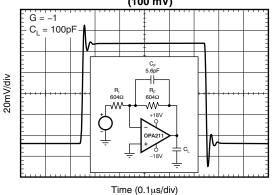


Figure 26.

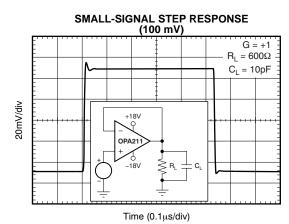


Figure 27.

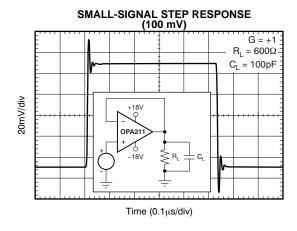
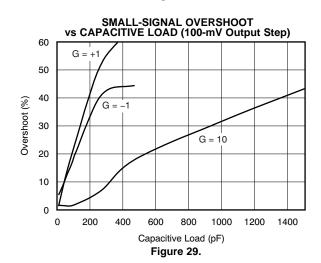
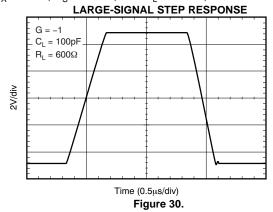


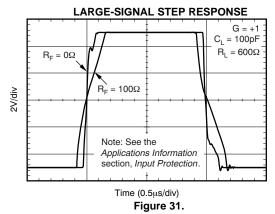
Figure 28.

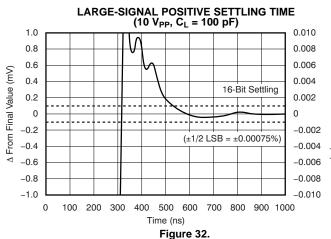


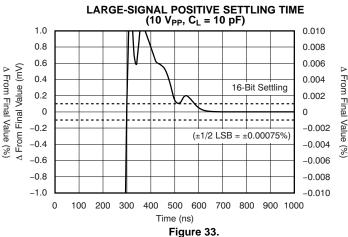


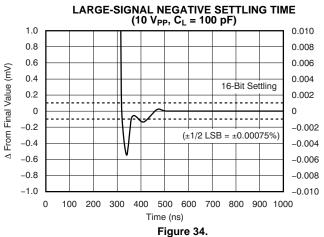
At  $T_A$  = 25°C,  $V_S$  = ±18 V, and  $R_L$  = 10 k $\Omega$ , unless otherwise noted.

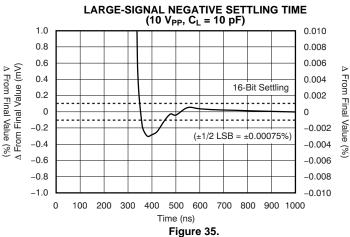












4. rigur



At  $T_A$  = 25°C,  $V_S$  = ±18 V, and  $R_L$  = 10 k $\Omega$ , unless otherwise noted.

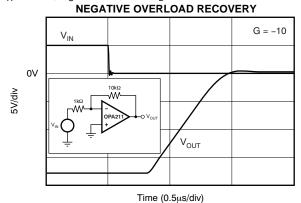


Figure 36.

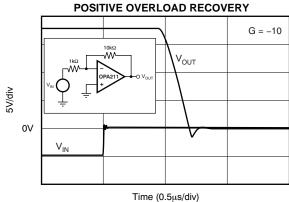
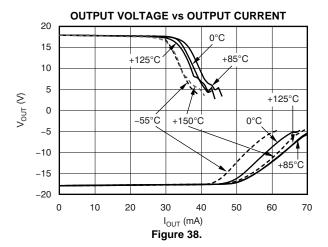


Figure 37.



**TURN-OFF TRANSIENT** 20 15 10 Output Signal 5 5V/div 0 -5 -10Shutdown Signal -15  $V_S = \pm 15V$ -20 Time (2µs/div) Figure 40.

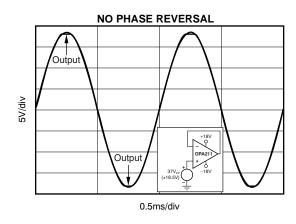
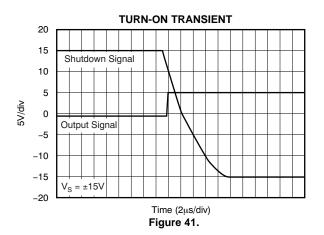
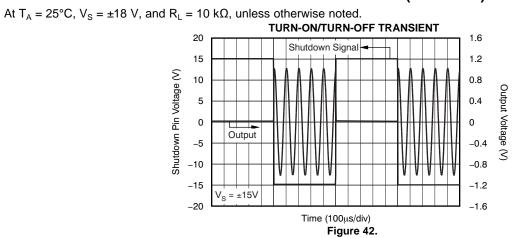


Figure 39.









#### **APPLICATION INFORMATION**

The OPA211 is a unity-gain stable, precision op amp with very low noise. Applications with noisy or high-impedance power supplies require decoupling capacitors close to the device pins. In most cases, 0.1-µF capacitors are adequate. Figure 43 shows a simplified schematic of the OPA211. This die uses a SiGe bipolar process and contains 180 transistors.

#### **OPERATING VOLTAGE**

OPA211 series op amps operate from ±2.25-V to ±18-V supplies while maintaining excellent performance. The OPA211 series can operate with as little as 4.5 V between the supplies and with up to 36 V between the supplies. However, some applications

do not require equal positive and negative output voltage swing. With the OPA211 series, power-supply voltages do not need to be equal. For example, the positive supply could be set to 25 V with the negative supply at –5 V or vice-versa.

The common-mode voltage must be maintained within the specified range. In addition, key parameters are assured over the specified temperature range,  $T_A = -55^{\circ}\text{C}$  to 210°C. Parameters that vary significantly with operating voltage or temperature are shown in the Typical Characteristics.

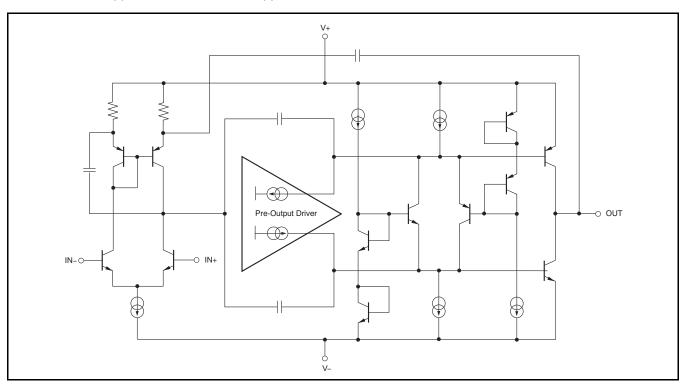


Figure 43. OPA211 Simplified Schematic

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#### INPUT PROTECTION

The input terminals of the OPA211 are protected from excessive differential voltage with back-to-back diodes, as shown in Figure 44. In most circuit applications, the input protection circuitry has no consequence. However, in low-gain or G = 1 circuits, fast ramping input signals can forward bias these diodes because the output of the amplifier cannot respond rapidly enough to the input ramp. This effect illustrated in Figure 31 of the Typical Characteristics. If the input signal is fast enough to create this forward bias condition, the input signal current must be limited to 10mA or less. If the input signal current is not inherently limited, an input series resistor can be used to limit the signal input current. This input series resistor degrades the low-noise performance of the OPA211, and is discussed in the Noise Performance section of this data sheet. Figure 44 shows an example implementing a currentlimiting feedback resistor.

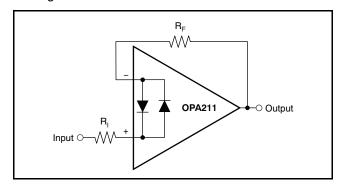


Figure 44. Pulsed Operation

## NOISE PERFORMANCE (1)

Figure 45 shows total circuit noise for varying source impedances with the op amp in a unity-gain configuration (no feedback resistor network, and therefore no additional noise contributions). Two different op amps are shown with total circuit noise calculated. The OPA211 has very low voltage noise, making it ideal for low source impedances (less than  $2 k\Omega$ ). A similar precision op amp, the OPA227, has somewhat higher voltage noise but lower current noise. It provides excellent noise performance at moderate source impedance (10 k $\Omega$  to 100 k $\Omega$ ). Above 100 k $\Omega$ , a FET-input op amp such as the OPA132 (very low current noise) may provide improved performance. The equation in Figure 45 is shown for the calculation of the total circuit noise. Note that  $e_n$  = voltage noise,  $I_n$  = current noise, R<sub>S</sub> = source impedance, k = Boltzmann's constant =  $1.38 \times 10^{-23}$  J/K, and T is temperature in K.

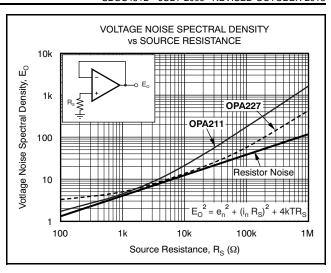


Figure 45. Noise Performance of the OPA211 and OPA227 in Unity-Gain Buffer Configuration

#### **BASIC NOISE CALCULATIONS**

Design of low-noise op amp circuits requires careful consideration of a variety of possible noise contributors: noise from the signal source, noise generated in the op amp, and noise from the feedback network resistors. The total noise of the circuit is the root-sum-square combination of all noise components.

The resistive portion of the source impedance produces thermal noise proportional to the square root of the resistance. This function is plotted in Figure 45. The source impedance is usually fixed; consequently, select the op amp and the feedback resistors to minimize the respective contributions to the total noise.

Figure 45 depicts total noise for varying source impedances with the op amp in a unity-gain configuration (no feedback resistor network, and therefore no additional noise contributions). The operational amplifier itself contributes both a voltage noise component and a current noise component. The voltage noise is commonly modeled as a timevarying component of the offset voltage. The current noise is modeled as the time-varying component of the input bias current and reacts with the source resistance to create a voltage component of noise. Therefore, the lowest noise op amp for a given application depends on the source impedance. For low source impedance, current noise is negligible and voltage noise generally dominates. For high source impedance, current noise may dominate.

 OPA227 and OPA132 have not been characterized or tested at 210°C.



Figure 46 illustrates both inverting and noninverting op amp circuit configurations with gain. In circuit configurations with gain, the feedback network resistors also contribute noise. The current noise of the op amp reacts with the feedback resistors to create additional noise components. The feedback resistor values can generally be chosen to make these noise sources negligible. The equations for total noise are shown for both configurations.

# TOTAL HARMONIC DISTORTION MEASUREMENTS

OPA211 series op amps have excellent distortion characteristics. THD + Noise is below 0.0001% (G = 1,  $V_O$  = 3  $V_{RMS}$ ) throughout the audio frequency range, 20 Hz to 20 kHz, with a 600-Ω load.

The distortion produced by OPA211 series op amps is below the measurement limit of many commercially available distortion analyzers. However, a special test circuit illustrated in Figure 47 can be used to extend the measurement capabilities.

Op amp distortion can be considered an internal error source that can be referred to the input. Figure 47 shows a circuit that causes the op amp distortion to be 101 times greater than that normally produced by the op amp. The addition of  $R_3$  to the otherwise standard noninverting amplifier configuration alters the feedback factor or noise gain of the circuit. The closed-loop gain is unchanged, but the feedback available for error correction is reduced by a factor of

101, thus extending the resolution by 101. Note that the input signal and load applied to the op amp are the same as with conventional feedback without  $R_3$ . The value of  $R_3$  should be kept small to minimize its effect on the distortion measurements.

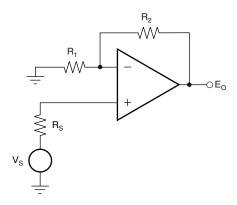
Validity of this technique can be verified by duplicating measurements at high gain and/or high frequency where the distortion is within the measurement capability of the test equipment. Measurements for this data sheet were made with an Audio Precision System Two distortion/noise analyzer, which greatly simplifies such repetitive measurements. The measurement technique can, however, be performed with manual distortion measurement instruments.

#### SHUTDOWN

The shutdown (enable) function of the OPA211 is referenced to the positive supply voltage of the operational amplifier. A valid high disables the op amp. A valid high is defined as (V+) - 0.35 V of the positive supply applied to the shutdown pin. A valid low is defined as (V+) - 3 V below the positive supply pin. For example, with  $V_{CC}$  at  $\pm 15~V$ , the device is enabled at or below 12 V. The device is disabled at or above 14.65 V. If dual or split power supplies are used, care should be taken to ensure the valid high or valid low input signals are properly referred to the positive supply voltage. This pin must be connected to a valid high or low voltage or driven, and not left open-circuit. The enable and disable times are provided in the Typical Characteristics section (see Figure 40 through Figure 42). When disabled, the output assumes a high-impedance state.

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#### **Noise in Noninverting Gain Configuration**



Noise at the output:

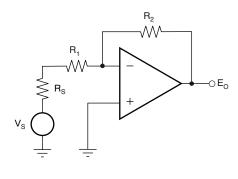
$$E_0^2 = \left(1 + \frac{R_2}{R_1}\right)^2 e_n^2 + e_1^2 + e_2^2 + (i_n R_2)^2 + e_S^2 + (i_n R_S)^2 \left(1 + \frac{R_2}{R_1}\right)^2$$

Where 
$$e_S = \sqrt{4kTR_S} \times \left[1 + \frac{R_2}{R_1}\right]$$
 = thermal noise of  $R_S$ 

$$e_1 = \sqrt{4kTR_1} \times \left[ \begin{array}{c} R_2 \\ \hline R_1 \end{array} \right] = thermal noise of R_1$$

$$e_2 = \sqrt{4kTR_2}$$
 = thermal noise of  $R_2$ 

#### **Noise in Inverting Gain Configuration**



Noise at the output:

$$E_{O}^{2} = \left[1 + \frac{R_{2}}{R_{1} + R_{S}}\right]^{2} e_{n}^{2} + e_{1}^{2} + e_{2}^{2} + (i_{n}R_{2})^{2} + e_{S}^{2}$$

Where 
$$e_S = \sqrt{4kTR_S} \times \left(\frac{R_2}{R_1 + R_S}\right)$$
 = thermal noise of  $R_S$ 

$$e_1 = \sqrt{4kTR_1} \times \left[ \frac{R_2}{R_1 + R_S} \right]$$
 = thermal noise of  $R_1$ 

$$e_2 = \sqrt{4kTR_2}$$
 = thermal noise of  $R_2$ 

For the OPA211 series op amps at 1kHz,  $e_n = 1.1 \text{nV}/\sqrt{\text{Hz}}$  and  $i_n = 1.7 \text{pA}/\sqrt{\text{Hz}}$ .

Figure 46. Noise Calculation in Gain Configurations

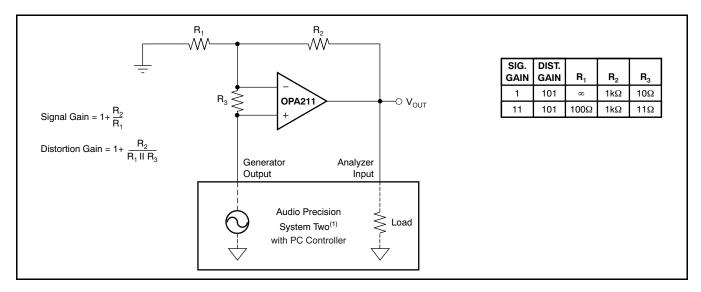


Figure 47. Distortion Test Circuit



#### **ELECTRICAL OVERSTRESS**

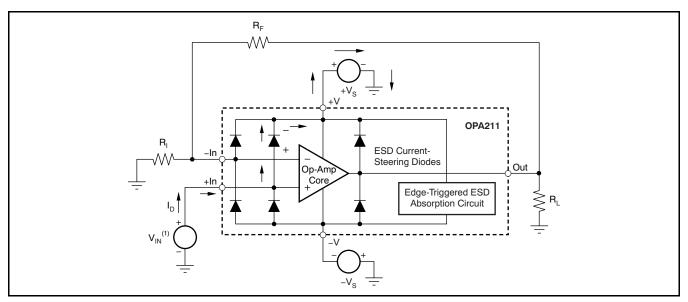
Designers often ask questions about the capability of an operational amplifier to withstand electrical overstress. These questions tend to focus on the device inputs, but may involve the supply voltage pins or even the output pin. Each of these different pin functions have electrical stress limits determined by the voltage breakdown characteristics of the particular semiconductor fabrication process and specific circuits connected to the pin. Additionally, internal electrostatic discharge (ESD) protection is built into these circuits to protect them from accidental ESD events both before and during product assembly.

It is helpful to have a good understanding of this basic ESD circuitry and its relevance to an electrical overstress event. Figure 48 illustrates the ESD circuits contained in the OPA211 (indicated by the dashed line area). The ESD protection circuitry involves several current-steering diodes connected from the input and output pins and routed back to the internal power-supply lines, where they meet at an absorption device internal to the operational amplifier. This protection circuitry is intended to remain inactive during normal circuit operation.

An ESD event produces a short duration, high-voltage pulse that is transformed into a short duration, high-current pulse as it discharges through a semiconductor device. The ESD protection circuits are designed to provide a current path around the operational amplifier core to prevent it from being damaged. The energy absorbed by the protection circuitry is then dissipated as heat.

When an ESD voltage develops across two or more of the amplifier device pins, current flows through one or more of the steering diodes. Depending on the path that the current takes, the absorption device may activate. The absorption device has a trigger, or threshold voltage, that is above the normal operating voltage of the OPA211 but below the device breakdown voltage level. Once this threshold is exceeded, the absorption device quickly activates and clamps the voltage across the supply rails to a safe level.

When the operational amplifier connects into a circuit such as that illustrated in Figure 48, the ESD protection components are intended to remain inactive and not become involved in the application circuit operation. However, circumstances may arise where an applied voltage exceeds the operating voltage range of a given pin. Should this condition occur, there is a risk that some of the internal ESD protection circuits may be biased on, and conduct current. Any such current flow occurs through steering diode paths and rarely involves the absorption device.



(1)  $V_{IN} = +V_S + 500$ mV.

Figure 48. Equivalent Internal ESD Circuitry and Its Relation to a Typical Circuit Application

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Figure 48 depicts a specific example where the input voltage,  $V_{IN}$ , exceeds the positive supply voltage (+V<sub>S</sub>) by 500 mV or more. Much of what happens in the circuit depends on the supply characteristics. If V<sub>S</sub> can sink the current, one of the upper input steering diodes conducts and directs current to V<sub>S</sub>. Excessively high current levels can flow with increasingly higher V<sub>IN</sub>. As a result, the datasheet specifications recommend that applications limit the input current to 10 mA.

If the supply is not capable of sinking the current,  $V_{IN}$  may begin sourcing current to the operational amplifier, and then take over as the source of positive supply voltage. The danger in this case is that the voltage can rise to levels that exceed the operational amplifier absolute maximum ratings. In extreme but rare cases, the absorption device triggers on while  $V_S$  and  $-V_S$  are applied. If this event happens, a direct current path is established between the  $V_S$  and  $-V_S$  supplies. The power dissipation of the absorption device is quickly exceeded, and the extreme internal heating destroys the operational amplifier.

Another common question involves what happens to the amplifier if an input signal is applied to the input while the power supplies  $V_{\rm S}$  and/or  $-V_{\rm S}$  are at 0 V. Again, it depends on the supply characteristic while at 0 V, or at a level below the input signal amplitude. If the supplies appear as high impedance, then the operational amplifier supply current may be supplied by the input source via the current steering diodes. This state is not a normal bias condition; the amplifier most likely will not operate normally. If the supplies are low impedance, then the current through the steering diodes can become quite high. The current level depends on the ability of the input source to deliver current, and any resistance in the input path.

#### **DFN PACKAGE**

The OPA211 is offered in an DFN-8 package (also known as SON). The DFN package is a QFN package with lead contacts on only two sides of the bottom of the package. This leadless package maximizes board space and enhances thermal and electrical characteristics through an exposed pad.

DFN packages are physically small, and have a smaller routing area, improved thermal performance, and improved electrical parasitics. Additionally, the absence of external leads eliminates bent-lead issues.

The DFN package can be easily mounted using standard printed circuit board (PCB) assembly techniques. See Application Note *QFN/SON PCB Attachment* (SLUA271) and Application Report *Quad Flatpack No-Lead Logic Packages* (SCBA017), both available for download at www.ti.com.

The exposed leadframe die pad on the bottom of the package must be connected to V-. Soldering the thermal pad improves heat dissipation and enables specified device performance.

#### **DFN LAYOUT GUIDELINES**

The exposed leadframe die pad on the DFN package should be soldered to a thermal pad on the PCB. A mechanical drawing showing an example layout is attached at the end of this data sheet. Refinements to this layout may be necessary based on assembly process requirements. Mechanical drawings located at the end of this data sheet list the physical dimensions for the package and pad. The five holes in the landing pattern are optional, and are intended for use with thermal vias that connect the leadframe die pad to the heatsink area on the PCB.

Soldering the exposed pad significantly improves board-level reliability during temperature cycling, key push, package shear, and similar board-level tests. Even with applications that have low-power dissipation, the exposed pad must be soldered to the PCB to provide structural integrity and long-term reliability.

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#### PACKAGING INFORMATION

Orderable part number	Status	Material type	Package   Pins	Package qty   Carrier	RoHS	Lead finish/	MSL rating/	Op temp (°C)	Part marking
	(1)	(2)			(3)	Ball material	Peak reflow		(6)
						(4)	(5)		
OPA211SHKJ	Active	Production	CFP (HKJ)   8	25   TUBE	Yes	Call TI	N/A for Pkg Type	-55 to 210	OPA211S HKJ
									ПКЈ
OPA211SHKQ	Active	Production	CFP (HKQ)   8	25   TUBE	Yes	AU	N/A for Pkg Type	-55 to 210	OPA211S HKQ
OPA211SKGD1	Active	Production	XCEPT (KGD)   0	400   NOT REQUIRED	Yes	Call TI	N/A for Pkg Type	-55 to 210	

<sup>(1)</sup> Status: For more details on status, see our product life cycle.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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#### OTHER QUALIFIED VERSIONS OF OPA211-HT:

<sup>(2)</sup> Material type: When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

<sup>(3)</sup> RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

<sup>(4)</sup> Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

<sup>(5)</sup> MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

<sup>(6)</sup> Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

## PACKAGE OPTION ADDENDUM

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● Enhanced Product : OPA211-EP

NOTE: Qualified Version Definitions:

- Catalog TI's standard catalog product
- Enhanced Product Supports Defense, Aerospace and Medical Applications

## **PACKAGE MATERIALS INFORMATION**

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## **TUBE**

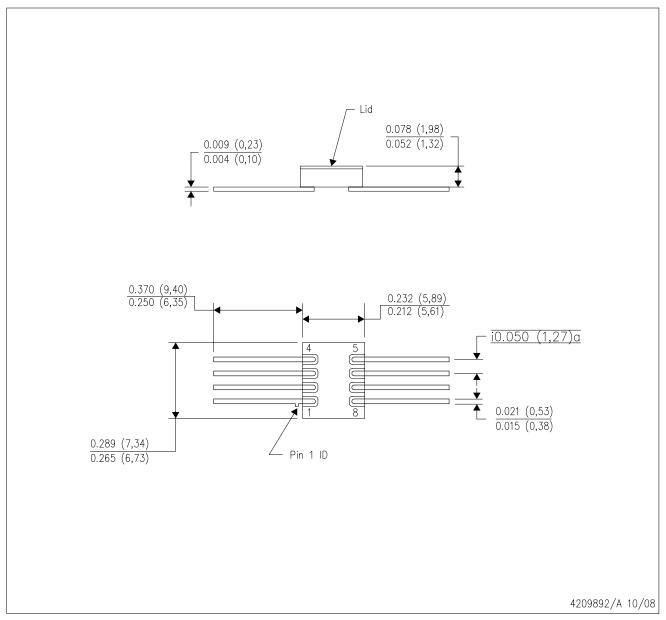


#### \*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	T (µm)	B (mm)
OPA211SHKJ	HKJ	CFP	8	25	506.98	26.16	6220	NA
OPA211SHKQ	HKQ	CFP	8	25	506.98	26.16	6220	NA

## HKJ (R-CDFP-F8)

## CERAMIC DUAL FLATPACK



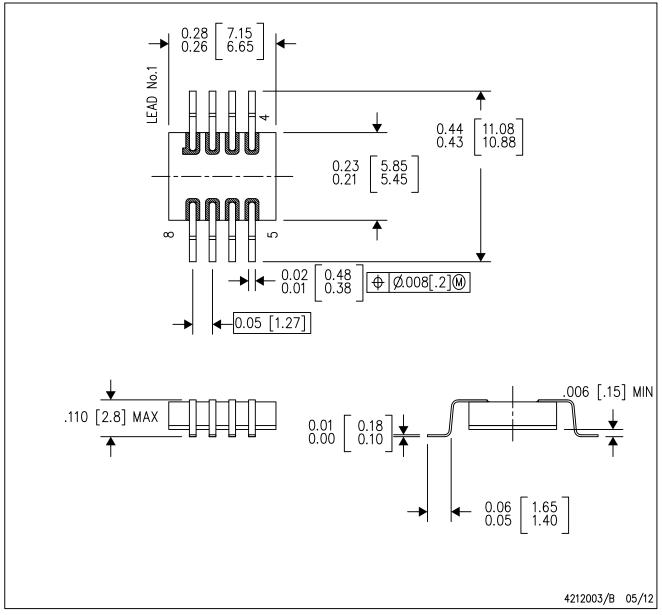
NOTES:

- A. All linear dimensions are in inches (millimeters).
- B. This drawing is subject to change without notice.
- C. This package can be hermetically sealed with a metal lid.
- D. The terminals will be gold plated.



HKQ (R-CDFP-G8)

CERAMIC GULL WING



NOTES:

- All linear dimensions are in inches (millimeters).
- This drawing is subject to change without notice.
- This package can be hermetically sealed with a metal lid.
- D. The terminals will be gold plated.E. Lid is not connected to any lead.



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