

# OPA1671 13-MHz, Low-Noise, Rail-to-Rail, Audio Operational Amplifier



## 1 Features

- Low noise:
  - 4 nV/ $\sqrt{\text{Hz}}$  at 10 kHz
  - 4.7 fA/ $\sqrt{\text{Hz}}$  at 1 kHz
- Low distortion: –109 dB (0.00035%)
- Wide gain bandwidth: 13 MHz
- Rail-to-rail input and output
- Low supply-voltage operation: 1.7 V to 5.5 V
- Low input capacitance
  - Differential: 6 pF
  - Common-mode: 2.5 pF
- Low input-bias current: 10 pA
- Low power supply current: 940  $\mu\text{A}$
- Industry-standard packages: SC-70 and SOT-23

## 2 Applications

- Microphone preamplifier
- Auxiliary line input and output
- Active filter circuit
- Transimpedance amplifier
- Voltage buffer

## 3 Description

The OPA1671 is a wide-bandwidth, low-noise, low-distortion, audio operational amplifier that provides rail-to-rail input and output operation. This device offers an excellent combination of low voltage noise, current noise, and input capacitance, allowing the device to deliver high performance in a wide array of audio and industrial applications. The unique internal topology of the OPA1671 delivers very low distortion (–109 dB), while only consuming 940  $\mu\text{A}$  of power supply current. The wide bandwidth (13 MHz) and high slew rate (5 V/ $\mu\text{s}$ ) of OPA1671 makes this device an excellent choice for high gain audio and industrial signal conditioning.

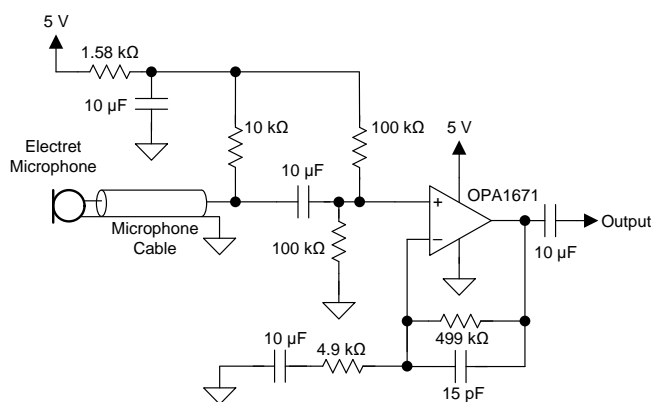
The OPA1671 is available in the SC-70 and SOT-23 packages and is specified over the industrial temperature range (–40°C to +125°C).

### Device Information<sup>(1)</sup>

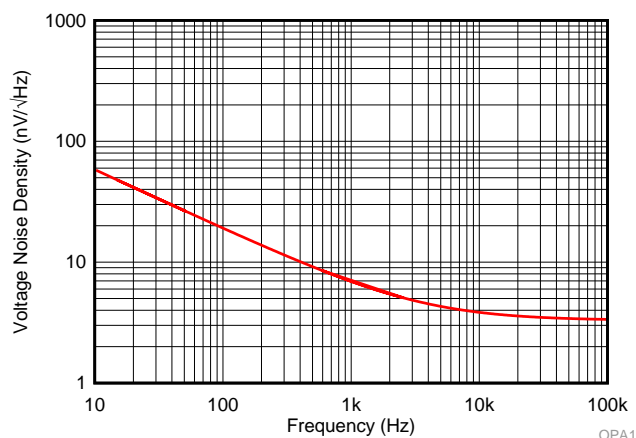
PART NUMBER	PACKAGE	BODY SIZE (NOM)
OPA1671	SC-70 (5)	2.00 mm x 1.25 mm
	SOT-23 (5)	2.90 mm x 1.60 mm

(1) For all available packages, see the package option addendum at the end of the data sheet.

### Electret Microphone Preamplifier



### OPA1671 Voltage Noise Density



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## 4 Revision History

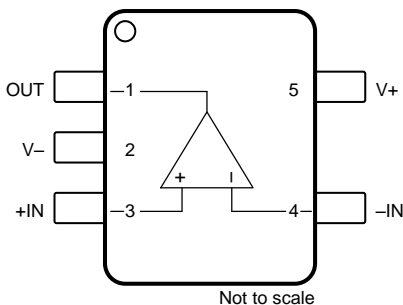
NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

<b>Changes from Revision A (January 2019) to Revision B</b>	<b>Page</b>
• Added SOT-23 (DBV) package and associated content to data sheet .....	1
• Added input offset voltage specification for $V_{CM} = (V+), (V-)$ .....	5

<b>Changes from Original (November 2018) to Revision A</b>	<b>Page</b>
• Changed from advanced information (preview) to production data (active).....	1

## 5 Pin Configuration and Functions

**DBV and DCK Packages  
5-Pin SOT-23 and SC-70  
Top View**



**Pin Functions**

PIN		I/O	DESCRIPTION
NAME	NO.		
-IN	4	I	Inverting input
+IN	3	I	Noninverting input
OUT	1	O	Output
V-	2	—	Negative (lowest) power supply
V+	5	—	Positive (highest) power supply

## 6 Specifications

### 6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

	MIN	MAX	UNIT
Supply voltage, $V_S = (V+) - (V-)$		6	V
Input voltage	(V-) -0.3	(V+) +0.3	V
Output short-circuit <sup>(2)</sup>	Continuous		
Operating temperature, $T_A$	-55	150	°C
Storage temperature, $T_{stg}$	-65	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) Short-circuit to ground, one amplifier per package.

### 6.2 ESD Ratings

			VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	2000	V
		Charged-device model (CDM), per JEDEC specification JESD22-C101 <sup>(2)</sup>	500	

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

	MIN	NOM	MAX	UNIT
Supply voltage, $V_S = (V+) - (V-)$	1.7 ( $\pm 0.85$ )		5.5 ( $\pm 2.75$ )	V
Specified temperature, $T_A$	-40		125	°C

### 6.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		OPA1671		UNIT
		DBV (SOT-23)	DCK (SC-70)	
		5 PINS	5 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	187.1	214.7	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	107.4	127.1	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	57.5	60.0	°C/W
$\Psi_{JT}$	Junction-to-top characterization parameter	33.5	33.4	°C/W
$\Psi_{JB}$	Junction-to-board characterization parameter	57.1	59.8	°C/W
$R_{\theta JC(bot)}$	Junction-to-case (bottom) thermal resistance	n/a	n/a	°C/W

- (1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.

## 6.5 Electrical Characteristics

at  $V_S = \pm 0.85\text{ V}$  to  $\pm 2.75\text{ V}$  ( $V_S = 1.7\text{ V}$  to  $5.5\text{ V}$ ),  $T_A = 25^\circ\text{C}$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = V_S / 2$ , and  $V_{OUT} = V_S / 2$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
<b>AUDIO PERFORMANCE</b>							
THD+N	Total harmonic distortion + noise	$G = 1$ , $f = 1\text{ kHz}$ , $V_O = 1\text{ V}_{RMS}$ , $V_S = 5.5\text{ V}$		0.00035%			
					-109		dB
IMD	Intermodulation distortion	$G = 1$ , $V_O = 1\text{ V}_{RMS}$ , $V_S = 5.5\text{ V}$	SMPTE/DIN Two-Tone, 4:1, (60 Hz and 7 kHz)	0.00158%			
					-96		dB
				0.0005%			
			CCIF Two-Tone (19 kHz and 20 kHz)		-106		dB
<b>FREQUENCY RESPONSE</b>							
GBW	Gain-bandwidth product			13			MHz
SR	Slew rate	4-V step, $G = 1$		5			V/ $\mu\text{s}$
$t_S$	Settling time	$T_O$ 0.1%, 2-V step, $G = 1$		0.75			$\mu\text{s}$
		$T_O$ 0.01%, 2-V step, $G = 1$		1			
	Overload recovery time	$V_{IN} \times \text{gain} > V_S$		0.35			$\mu\text{s}$
<b>NOISE</b>							
	Input voltage noise	$f = 0.1\text{ Hz}$ to $10\text{ Hz}$		2.4			$\mu\text{V}_{PP}$
$e_N$	Input voltage noise density	$f = 10\text{ Hz}$		45			$\text{nV}/\sqrt{\text{Hz}}$
		$f = 1\text{ kHz}$		7			
		$f = 10\text{ kHz}$		4.0			
$i_N$	Input current noise	$f = 1\text{ kHz}$		4.7			$\text{fA}/\sqrt{\text{Hz}}$
<b>OFFSET VOLTAGE</b>							
$V_{OS}$	Input offset voltage	$V_{CM} = (V_+)$				$\pm 1.6$	mV
		$V_{CM} = (V_-)$				$\pm 1.6$	
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$				$\pm 0.25$	
$dV_{OS}/dT$	Input offset voltage drift	$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$				$\pm 0.3$	$\pm 2.2$
PSRR	Input offset voltage versus power supply	$V_{CM} = (V_-)$				$\pm 30$	$\pm 130$
<b>INPUT BIAS CURRENT</b>							
$I_B$	Input bias current					$\pm 10$	pA
$I_{OS}$	Input offset current					$\pm 10$	
<b>INPUT VOLTAGE RANGE</b>							
$V_{CM}$	Common-mode voltage range			$V_-$		$V_+$	V
CMRR	Common-mode rejection ratio	$V_S = 1.7\text{ V}$ , $(V_-) < V_{CM} < (V_+) - 1.25\text{ V}$		74	91		dB
		$V_S = 5.5\text{ V}$ , $(V_-) < V_{CM} < (V_+) - 1.25\text{ V}$		80	96		
		$V_S = 1.7\text{ V}$ , $V_{CM} = 0\text{ V}$ to $1.7\text{ V}$		60	88		
		$V_S = 5.5\text{ V}$ , $V_{CM} = 0\text{ V}$ to $5.5\text{ V}$		68	102		
<b>INPUT CAPACITANCE</b>							
$Z_{ID}$	Differential			$10^{13} \parallel 6$			$\text{M}\Omega \parallel \text{pF}$
$Z_{ICM}$	Common-mode			$10^{13} \parallel 2.5$			$\text{G}\Omega \parallel \text{pF}$
<b>OPEN-LOOP GAIN</b>							
$A_{OL}$	Open-loop voltage gain	$(V_-) + 50\text{ mV} < V_O < (V_+) - 50\text{ mV}$ , $R_L = 10\text{ k}\Omega$			97	113	dB
			$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		106		
		$(V_-) + 200\text{ mV} < V_O < (V_+) - 200\text{ mV}$ , $R_L = 2\text{ k}\Omega$			97	112	
			$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$		105		

**Electrical Characteristics (continued)**

at  $V_S = \pm 0.85\text{ V}$  to  $\pm 2.75\text{ V}$  ( $V_S = 1.7\text{ V}$  to  $5.5\text{ V}$ ),  $T_A = 25^\circ\text{C}$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = V_S / 2$ , and  $V_{OUT} = V_S / 2$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>OUTPUT</b>						
	Voltage output swing from rail	$V_S = 5.5\text{ V}$ , $R_L = 10\text{ k}\Omega$		10	20	mV
$I_{SC}$	Short-circuit current	Sinking, $V_S = 5.5\text{ V}$		-57		mA
		Sourcing, $V_S = 5.5\text{ V}$		66		
<b>POWER SUPPLY</b>						
$I_Q$	Quiescent current per amplifier	$I_O = 0\text{ mA}$		0.94	1.3	mA
		$I_O = 0\text{ mA}$ , $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$			1.4	

## 6.6 Typical Characteristics

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 2.5\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$  (unless otherwise noted)

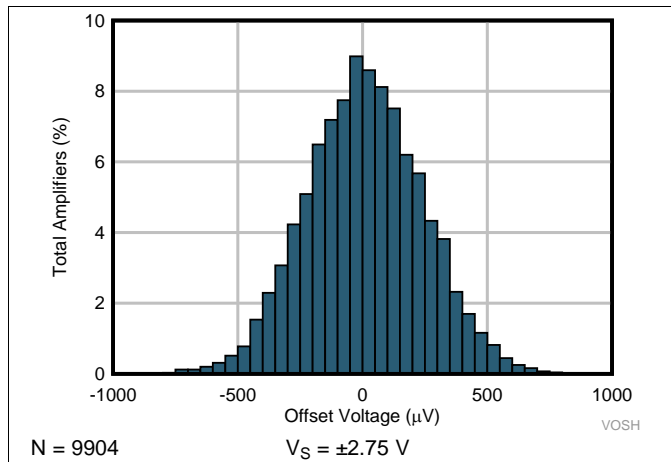


Figure 1. Offset Voltage Production Distribution

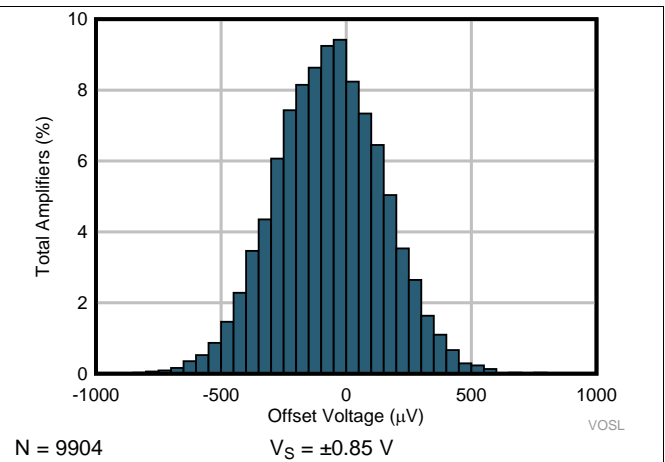


Figure 2. Offset Voltage Production Distribution

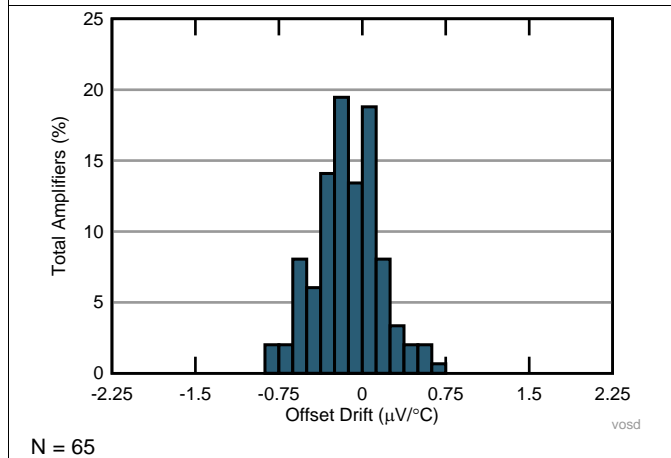


Figure 3. Offset Voltage Drift Distribution

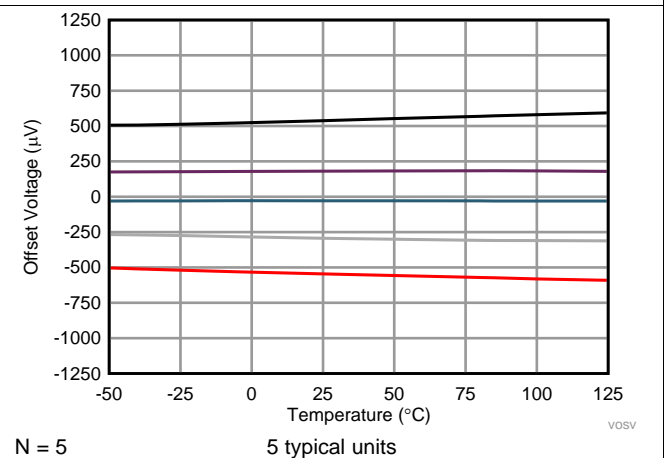


Figure 4. Offset Voltage vs Temperature

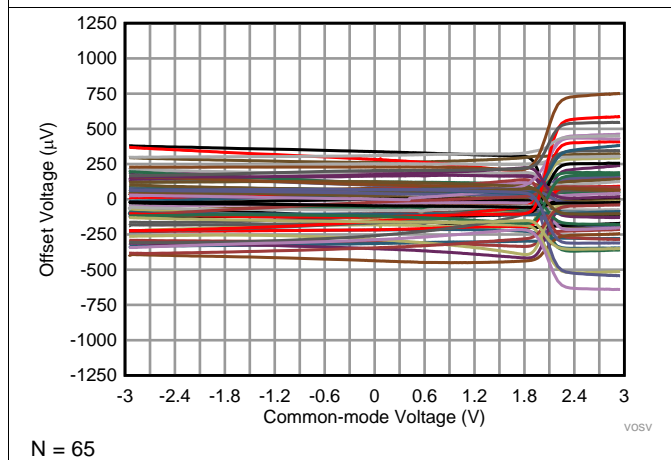


Figure 5. Offset Voltage vs Common Mode Voltage

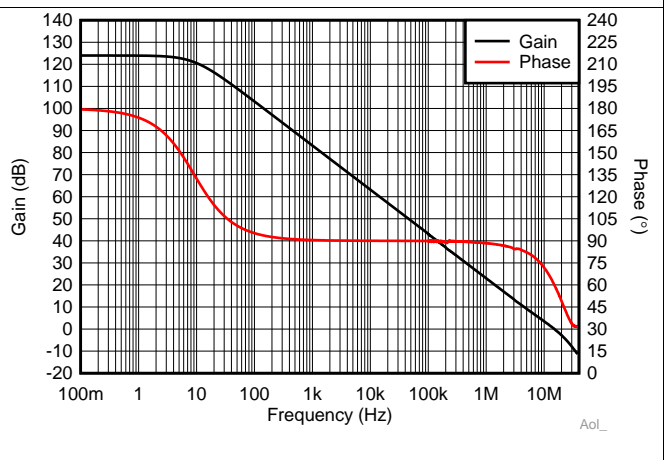


Figure 6. Open-Loop Gain and Phase vs Frequency

Typical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 2.5\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$  (unless otherwise noted)

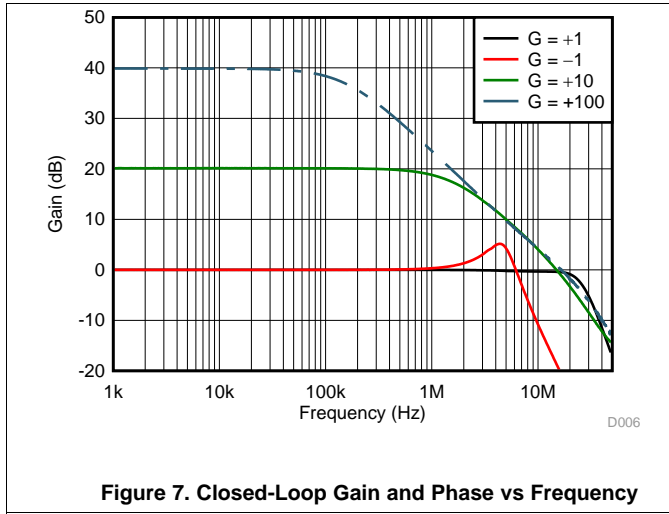


Figure 7. Closed-Loop Gain and Phase vs Frequency

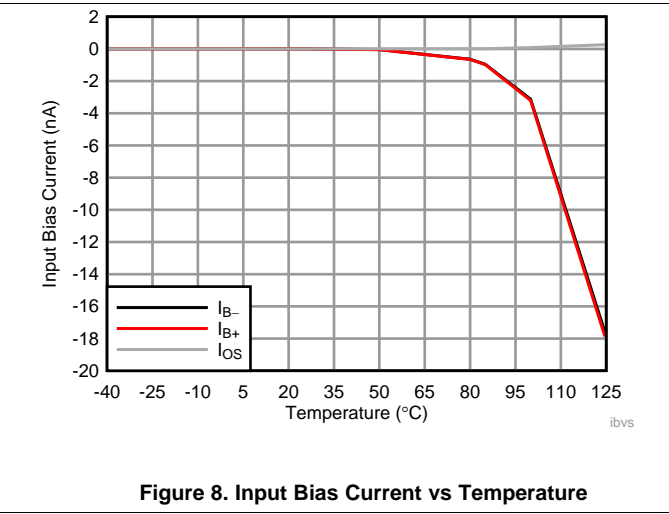


Figure 8. Input Bias Current vs Temperature

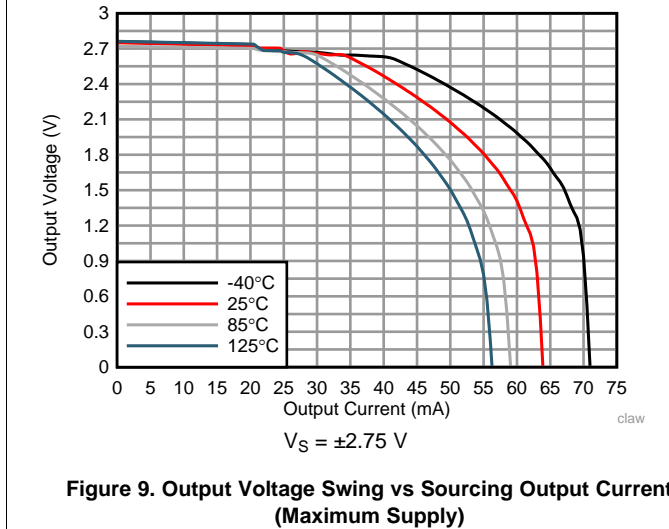


Figure 9. Output Voltage Swing vs Sourcing Output Current (Maximum Supply)

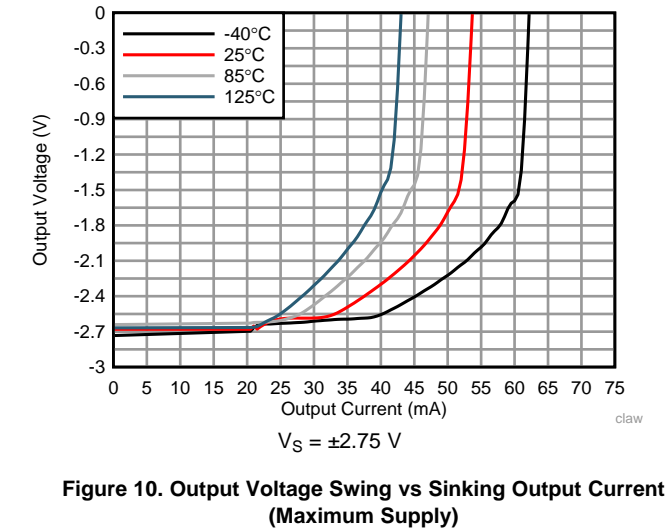


Figure 10. Output Voltage Swing vs Sinking Output Current (Maximum Supply)

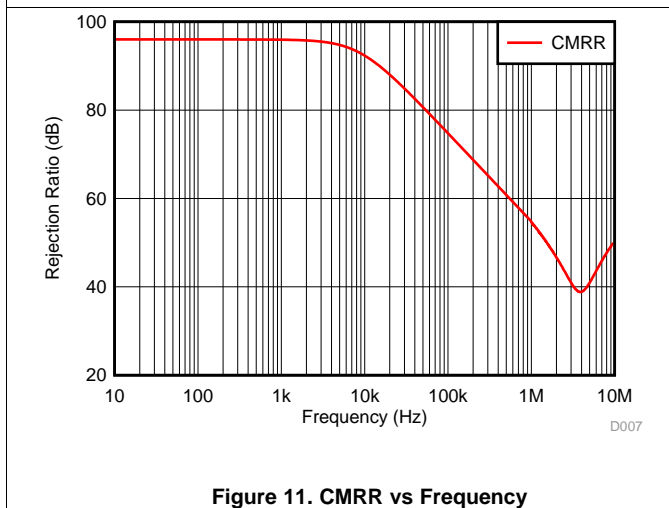


Figure 11. CMRR vs Frequency

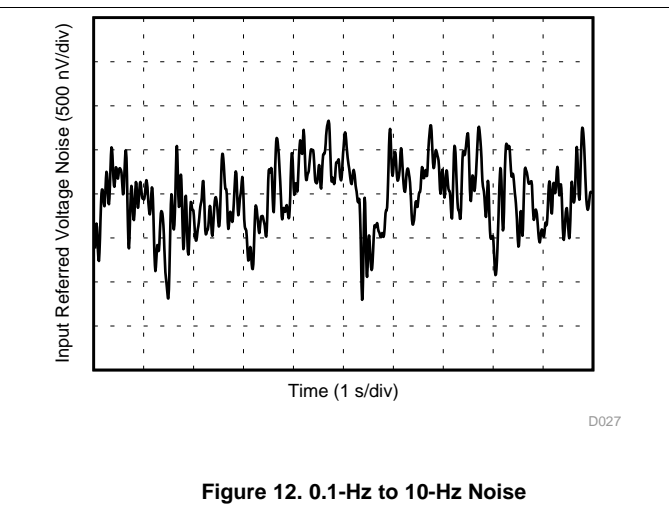
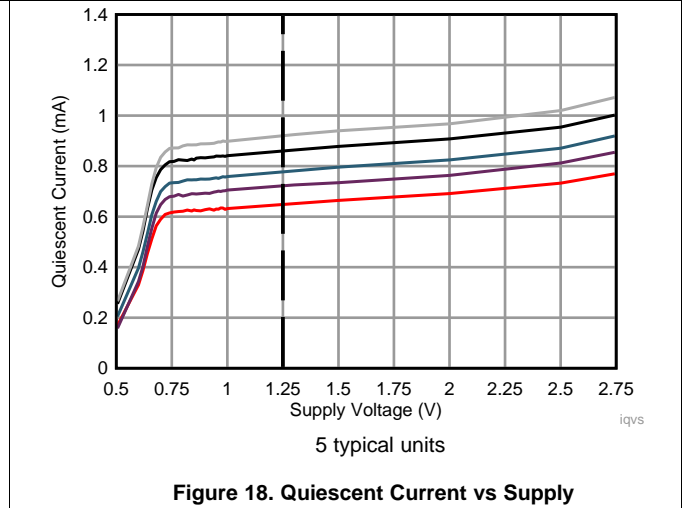
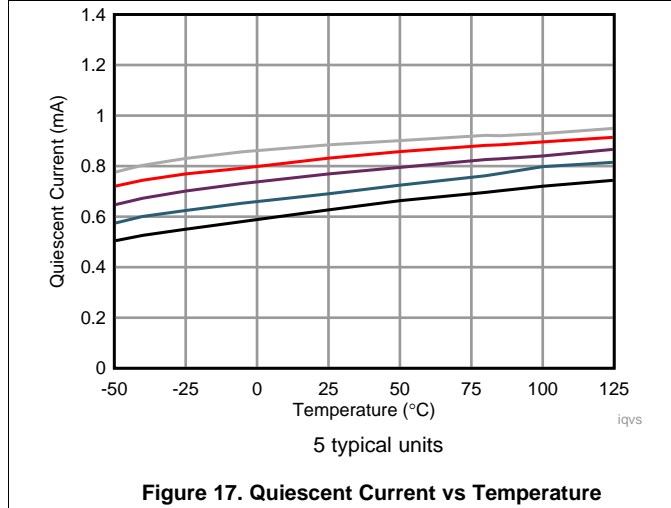
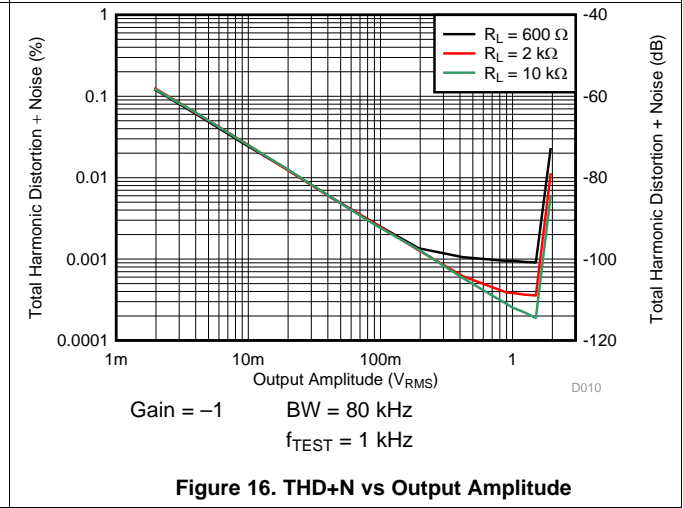
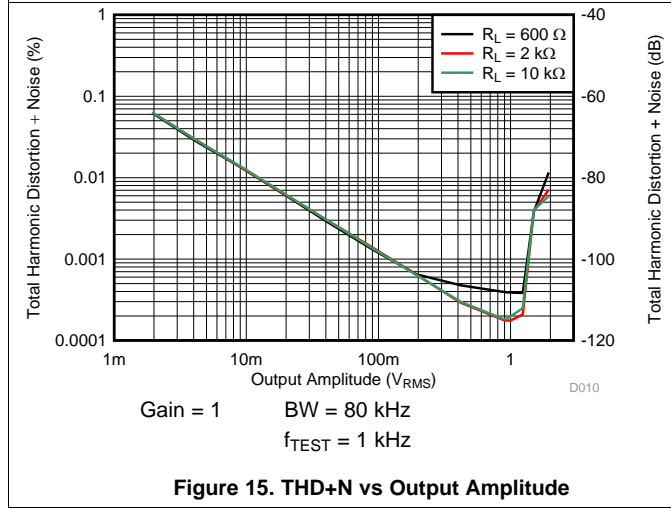
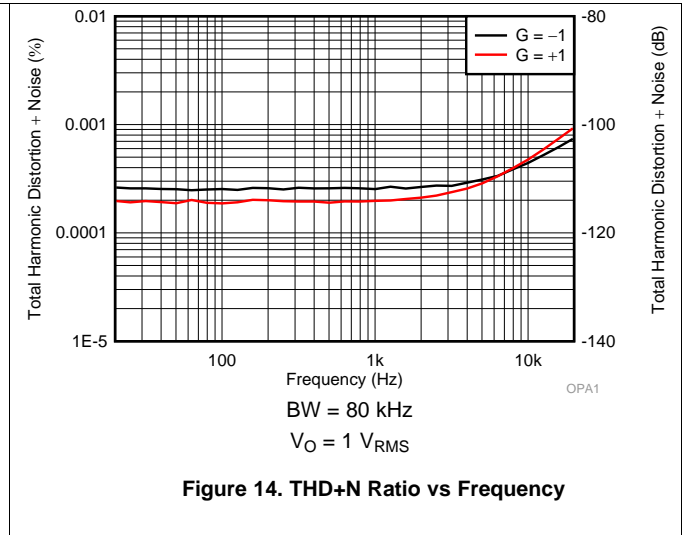
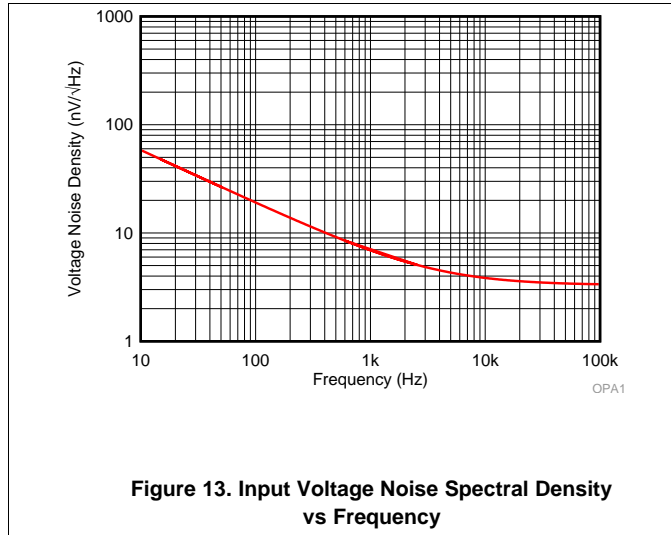


Figure 12. 0.1-Hz to 10-Hz Noise



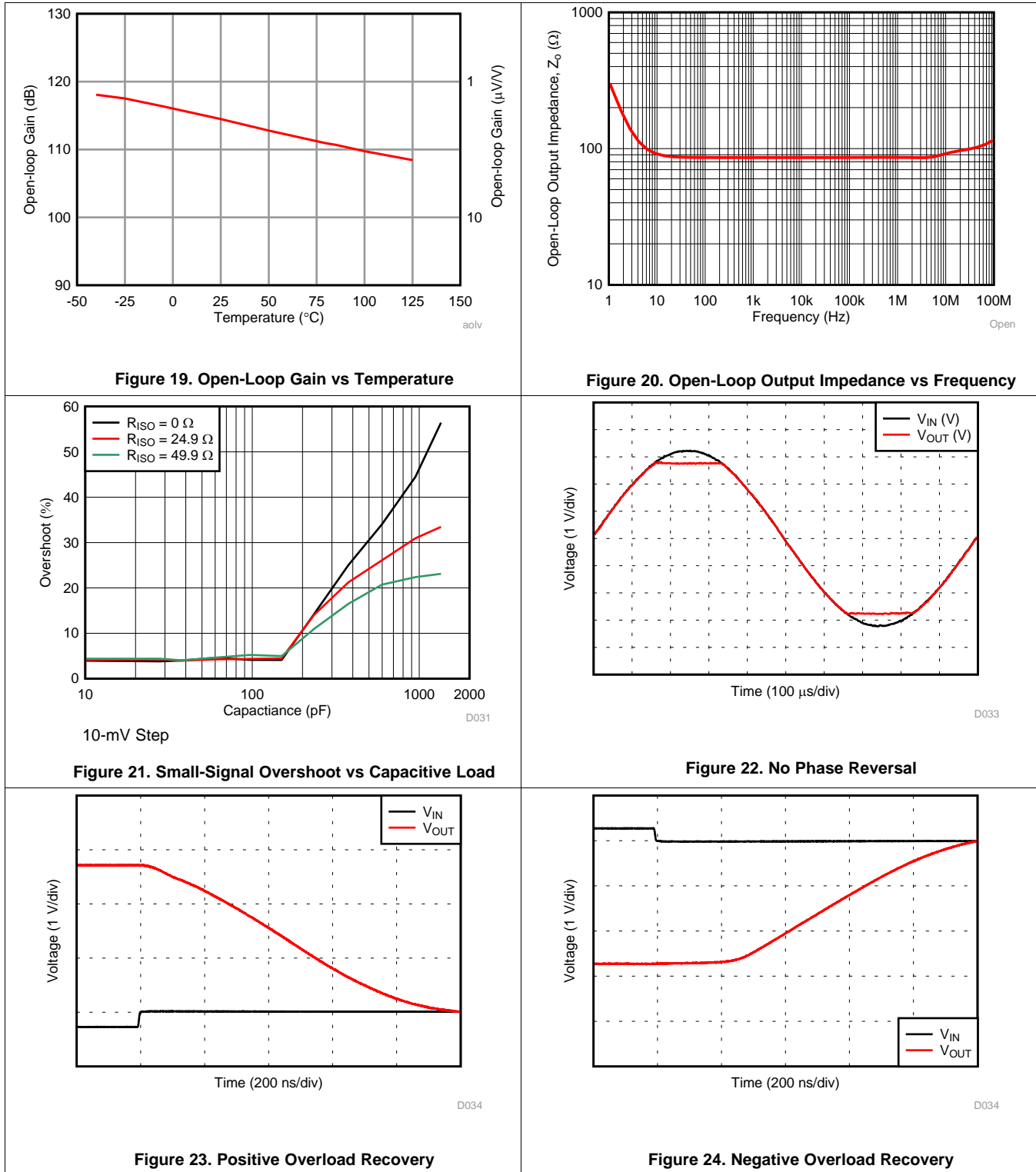
Typical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 2.5\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$  (unless otherwise noted)



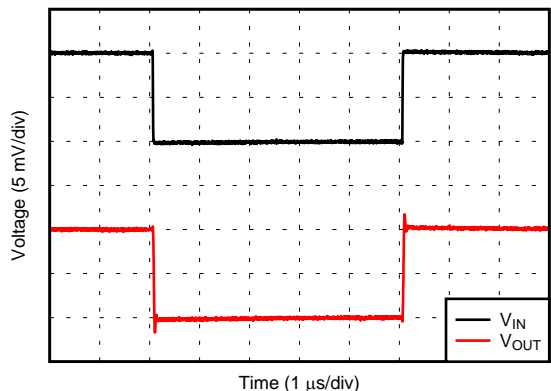
### Typical Characteristics (continued)

at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 2.5\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$  (unless otherwise noted)



Typical Characteristics (continued)

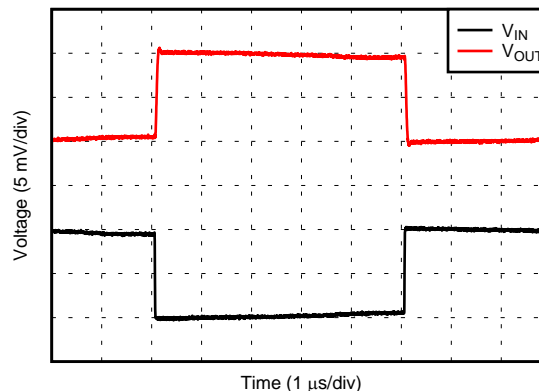
at  $T_A = 25^\circ\text{C}$ ,  $V_S = \pm 2.5\text{ V}$ ,  $V_{CM} = V_S / 2$ ,  $R_L = 10\text{ k}\Omega$  connected to  $V_S / 2$  (unless otherwise noted)



10-mV step  $G = +1$

D035

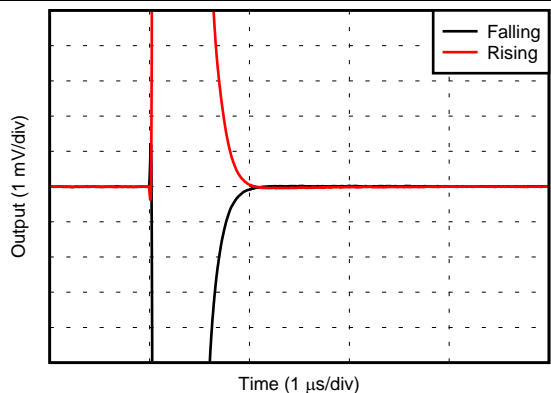
Figure 25. Small-Signal Step Response



10-mV step  $G = -1$

D035

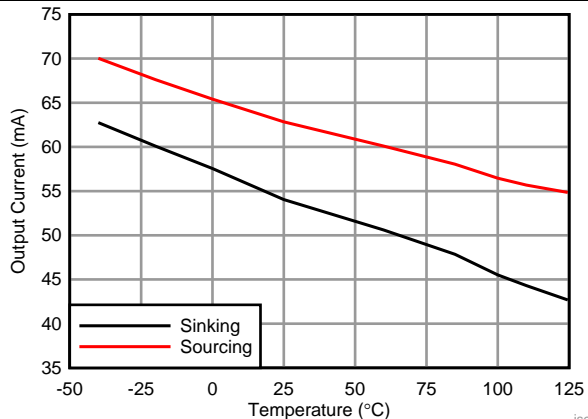
Figure 26. Small-Signal Step Response



2-V Step

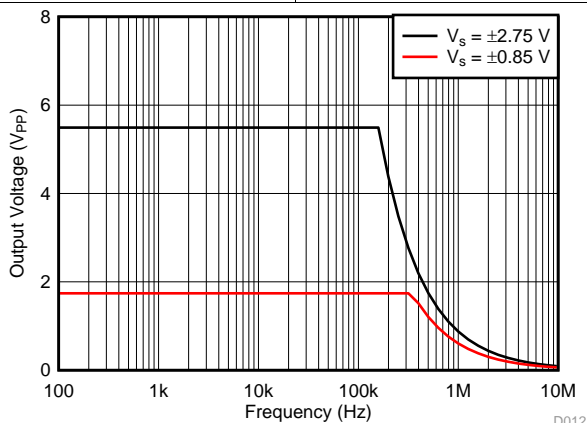
D037

Figure 27. Settling Time



iscv

Figure 28. Short-Circuit Current vs Temperature



D012

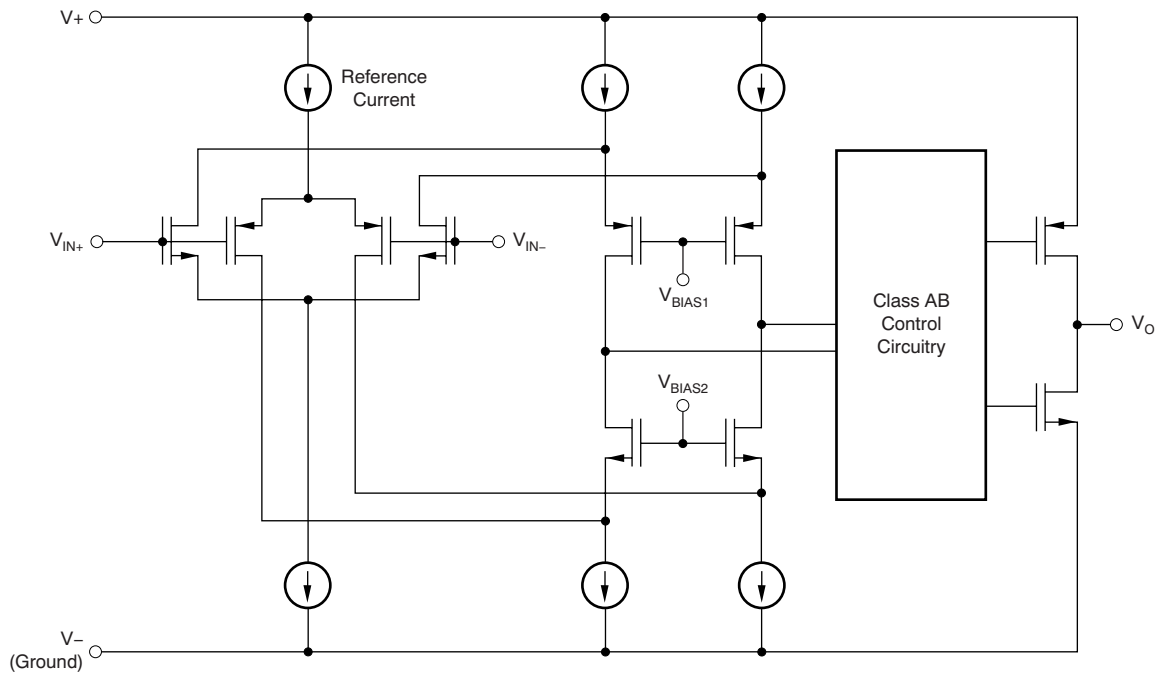
Figure 29. Maximum Output Voltage vs Frequency

## 7 Detailed Description

### 7.1 Overview

The OPA1671 is a rail-to-rail input, very low noise operational amplifier (op amp). The OPA1671 operates from 1.7 V to 5.5 V, is unity-gain stable, and is designed for a wide range of audio and general-purpose applications. The OPA1671 strengths also include 13-MHz bandwidth and 4.0-nV/ $\sqrt{\text{Hz}}$  noise spectral density, with very low input bias current (10 pA). These strengths make the OPA1671 a great choice for a preamplifier in microphone circuits, sensor modules and buffering high-fidelity, digital-to-analog converters (DACs).

### 7.2 Functional Block Diagram



## 7.3 Feature Description

### 7.3.1 Operating Voltage

The OPA1671 op amp can be used with single or dual supplies from an operating range of  $V_S = 1.7\text{ V}$  ( $\pm 0.85\text{ V}$ ) up to  $5.5\text{ V}$  ( $\pm 2.75\text{ V}$ ).

#### CAUTION

Supply voltages greater than  $6\text{ V}$  can permanently damage the device (see [Absolute Maximum Ratings](#))

Key parameters that vary over the supply voltage or temperature range are shown in the [Typical Characteristics](#) section.

### 7.3.2 Input Bias Current

Typically, input bias current is approximately  $\pm 10\text{ pA}$ . Input voltages exceeding the power supplies, however, can cause excessive current to flow into or out of the input pins. Momentary voltages greater than the power supply can be tolerated if the input current is limited to  $10\text{ mA}$ . This limitation is easily accomplished with an input resistor, as shown in [Figure 30](#).

Unlike many operational amplifiers, there are no diodes connected between the positive and negative input terminals. As a result, differential voltages up to the full supply voltage do not cause any significantly higher current flow into the inputs.

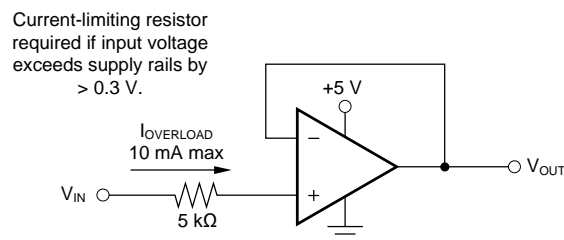


Figure 30. Input Current Protection

### 7.3.3 Common-Mode Voltage Range

The OPA1671 features true rail-to-rail inputs, allowing full common mode operation from the negative supply voltage to the positive supply voltage. This full common mode operation is achieved with complimentary N-channel and P-channel differential input pairs. The N-channel pair is active for input voltages close to the positive rail, typically  $(V+) - 1.25\text{ V}$  to  $(V+)$ . The P-channel is active for common-mode inputs from  $(V-)$  to  $(V+) - 1.25\text{ V}$ . There is a small transition region, typically from  $(V+) - 1.25\text{ V}$  to  $(V+) - 1\text{ V}$ . In this region, the offset voltage transitions between the P-channel and N-channel offset values. [Figure 5](#) shows the difference between offset in the P and N regions.

## Feature Description (continued)

### 7.3.4 EMI Susceptibility and Input Filtering

Operational amplifiers vary in susceptibility to EMI. If conducted EMI enters the operational amplifier, the dc offset at the amplifier output can shift from its nominal value when EMI is present. This shift is a result of signal rectification associated with the internal semiconductor junctions. Although all operational amplifier pin functions can be affected by EMI, the input pins are likely to be the most susceptible. The OPA1671 operational amplifier incorporates an internal input low-pass filter that reduces the amplifier response to EMI. Both common-mode and differential-mode filtering are provided by the input filter. The filter is designed for a cutoff frequency of approximately 20 MHz (–3 dB), with a rolloff of 20 dB per decade.

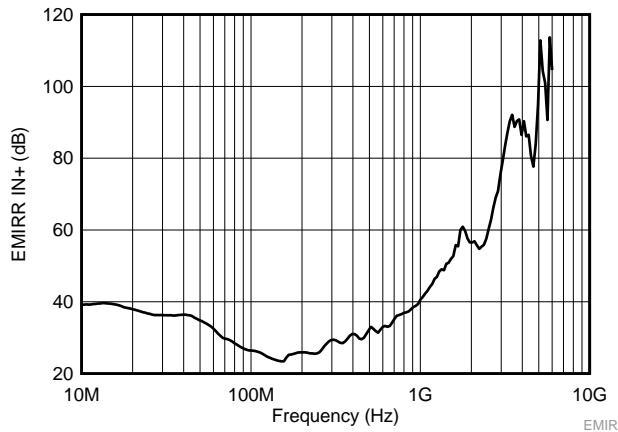


Figure 31. OPA1671 EMIRR vs Frequency

Table 1. OPA1671 EMIRR IN+ for Frequencies of Interest

FREQUENCY	APPLICATION OR ALLOCATION	EMIRR IN+
400 MHz	Mobile radio, mobile satellite, space operation, weather, radar, ultra-high frequency (UHF) applications	30 dB
900 MHz	Global system for mobile communications (GSM) applications, radio communication, navigation, GPS (to 1.6 GHz), GSM, aeronautical mobile, UHF applications	38 dB
1.8 GHz	GSM applications, mobile personal communications, broadband, satellite, L-band (1 GHz to 2 GHz)	60 dB
2.4 GHz	802.11b, 802.11g, 802.11n, Bluetooth®, mobile personal communications, industrial, scientific and medical (ISM) radio band, amateur radio and satellite, S-band (2 GHz to 4 GHz)	59 dB
3.6 GHz	Radiolocation, aero communication and navigation, satellite, mobile, S-band	90 dB
5 GHz	802.11a, 802.11n, aero communication and navigation, mobile communication, space and satellite operation, C-band (4 GHz to 8 GHz)	100 dB

### 7.4 Device Functional Modes

The OPA1671 has a single functional mode and is operational when the power-supply voltage is greater than 1.7 V ( $\pm 0.85$  V). The maximum specified power-supply voltage for the OPA1671 is 5.5 V ( $\pm 2.75$  V).

## 8 Application and Implementation

### NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 8.1 Application Information

The OPA1671 is a low-noise, rail-to-rail input and output operational amplifier specifically designed for portable applications. The device operates from 1.7 V to 5.5 V, is unity-gain stable, and suitable for a wide range of audio and general-purpose applications. The class AB output stage is capable of driving  $\leq 10\text{-k}\Omega$  loads connected to any point between  $V+$  and ground. The input common-mode voltage range includes both rails, and allows the OPA1671 device to be used in virtually any single-supply application. Rail-to-rail input and output swing significantly increases dynamic range, especially in low-supply applications, and makes the device a great choice for driving sampling analog-to-digital converters (ADCs).

#### 8.1.1 Capacitive Loads

The dynamic characteristics of the OPA1671 amplifiers are optimized for commonly encountered gains, loads, and operating conditions. The combination of low closed-loop gain and high capacitive loads decreases the phase margin of the amplifier and can lead to gain peaking or oscillations. As a result, heavier capacitive loads must be isolated from the output. Add a small resistor (for example,  $R_S = 50\ \Omega$ ) in series with the output to isolate heavier capacitive loads.

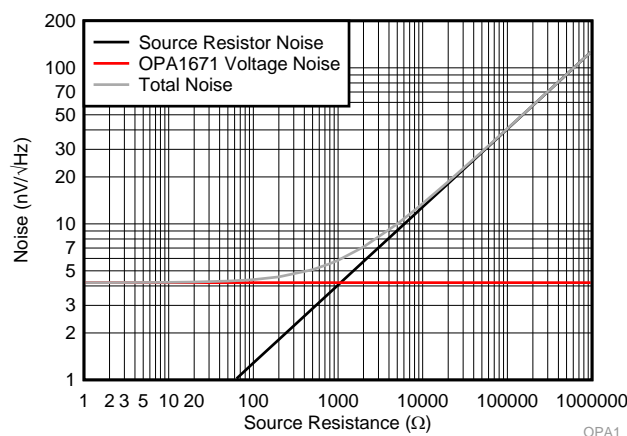
#### 8.1.2 Noise Performance

Figure 31 shows the total circuit noise for varying source impedances with the operational amplifier in a unity-gain configuration (with no feedback resistor network and therefore no additional noise contributions). The op amp itself contributes a voltage noise component and a current noise component. The voltage noise is commonly modeled as a time-varying component of the offset voltage. The current noise is modeled as the time-varying component of the input bias current and reacts with the source resistance to create a voltage component of noise. For a CMOS-input device, the noise resulting from the input current is negligible; therefore, the total noise is dominated by the voltage noise of the OPA1671 at low source resistance, and the resistor noise  $> 1\ \text{k}\Omega$ .

Figure 31 shows the calculation of the total circuit noise, with these parameters:

- $e_n$  = voltage noise
- $R_S$  = source impedance
- $k$  = Boltzmann's constant =  $1.38 \times 10^{-23}\ \text{J/K}$
- $T$  = temperature in kelvins (K)

For more details on calculating noise, see [Basic Noise Calculations](#).



**Figure 32. Noise Performance of the OPA1671 in a Unity-Gain Buffer Configuration**

## Application Information (continued)

### 8.1.3 Basic Noise Calculations

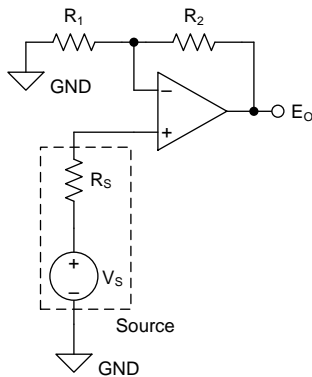
Low-noise circuit design requires careful analysis of all noise sources. External noise sources can dominate in many cases; consider the effect of source resistance on overall op amp noise performance. Total noise of the circuit is the root-sum-square combination of all noise components.

The resistive portion of the source impedance produces thermal noise proportional to the square root of the resistance. This function is plotted in [Figure 31](#). The source impedance is typically fixed; consequently, select the op amp and the feedback resistors to minimize the respective contributions to the total noise.

[Figure 33](#) shows noninverting (A) and inverting (B) op amp circuit configurations with gain. In circuit configurations with gain, the feedback network resistors contribute noise. In general, the current noise of the op amp reacts with the feedback resistors to create additional noise components.

The selected feedback resistor values make these noise sources negligible. Low impedance feedback resistors load the output of the amplifier. The equations for total noise are shown for both configurations.

#### (A) Noise in Noninverting Gain Configuration



Noise at the output is given as  $E_O$ , where

$$(1) \quad E_O = \left(1 + \frac{R_2}{R_1}\right) \cdot \sqrt{(e_S)^2 + (e_N)^2 + (e_{R_1 \parallel R_2})^2 + (i_N \cdot R_S)^2 + \left(i_N \cdot \left[\frac{R_1 \cdot R_2}{R_1 + R_2}\right]\right)^2} \quad [V_{RMS}]$$

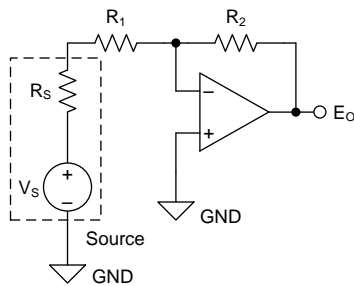
$$(2) \quad e_S = \sqrt{4 \cdot k_B \cdot T(K) \cdot R_S} \quad \left[\frac{V}{\sqrt{Hz}}\right] \quad \text{Thermal noise of } R_S$$

$$(3) \quad e_{R_1 \parallel R_2} = \sqrt{4 \cdot k_B \cdot T(K) \cdot \left[\frac{R_1 \cdot R_2}{R_1 + R_2}\right]} \quad \left[\frac{V}{\sqrt{Hz}}\right] \quad \text{Thermal noise of } R_1 \parallel R_2$$

$$(4) \quad k_B = 1.38065 \cdot 10^{-23} \quad \left[\frac{J}{K}\right] \quad \text{Boltzmann Constant}$$

$$(5) \quad T(K) = 237.15 + T(^{\circ}C) \quad [K] \quad \text{Temperature in kelvins}$$

#### (B) Noise in Inverting Gain Configuration



Noise at the output is given as  $E_O$ , where

$$(6) \quad E_O = \left(1 + \frac{R_2}{R_S + R_1}\right) \cdot \sqrt{(e_N)^2 + (e_{R_1 + R_S \parallel R_2})^2 + \left(i_N \cdot \left[\frac{(R_S + R_1) \cdot R_2}{R_S + R_1 + R_2}\right]\right)^2} \quad [V_{RMS}]$$

$$(7) \quad e_{R_1 + R_S \parallel R_2} = \sqrt{4 \cdot k_B \cdot T(K) \cdot \left[\frac{(R_S + R_1) \cdot R_2}{R_S + R_1 + R_2}\right]} \quad \left[\frac{V}{\sqrt{Hz}}\right] \quad \text{Thermal noise of } (R_1 + R_S) \parallel R_2$$

$$(8) \quad k_B = 1.38065 \cdot 10^{-23} \quad \left[\frac{J}{K}\right] \quad \text{Boltzmann Constant}$$

$$(9) \quad T(K) = 237.15 + T(^{\circ}C) \quad [K] \quad \text{Temperature in kelvins}$$

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- (1)  $e_N$  is the voltage noise of the amplifier. For the OPA1671 series of operational amplifiers,  $e_N = 4.0 \text{ nV}/\sqrt{\text{Hz}}$  at 10 kHz.
- (2)  $i_N$  is the current noise of the amplifier. For the OPA1671 series of operational amplifiers,  $i_N = 4.5 \text{ fA}/\sqrt{\text{Hz}}$  at 1 kHz.
- (3) For additional resources on noise calculations, see [TI's Precision Labs Series](#).

**Figure 33. Noise Calculation in Gain Configurations**



## 8.2 Typical Application

This design uses an OPA1671 as a preamplifier for an electret microphone. Electret microphone types are common in many audio applications of varying performance levels. The OPA1671 offers very low noise in a tiny package, and is designed for use in electret preamplifier circuits.

Figure 34 shows the solution.

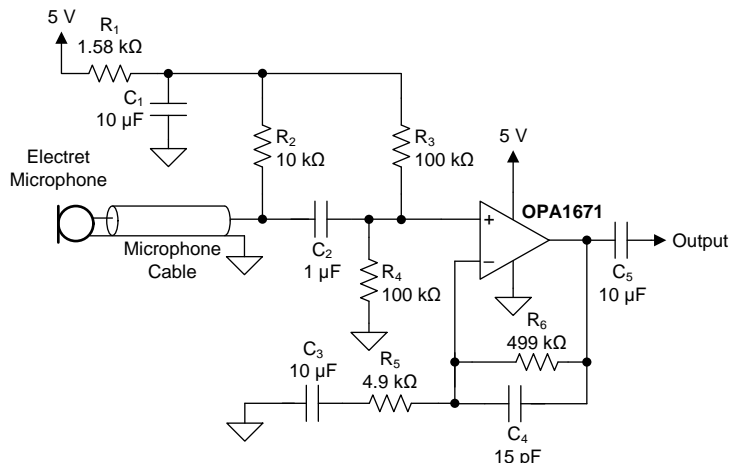


Figure 34. Electret Preamplifier Schematic

### 8.2.1 Design Requirements

This solution has the following requirements:

- Supply voltage: 5 V
- Gain: 100 V/V
- Frequency response: 3 dB from 20 Hz to 20 kHz
- Output: 2.5 V  $\pm$ 1 V
- Output noise density: < 1  $\mu$ V/ $\sqrt{\text{Hz}}$  at 10 kHz

## Typical Application (continued)

### 8.2.2 Detailed Design Procedure

The preamplifier circuit uses a noninverting gain configuration to allow for high input impedance, with independent gain-setting resistor values. DC bypass is accomplished with  $C_2$  and  $C_3$ , with the low frequency poles set by  $C_2$ ,  $R_4$ ,  $C_3$  and  $R_5$ ; see [Equation 1](#) and [Equation 2](#).

$$p_{L1} = \frac{1}{2\pi \cdot (R_3 \parallel R_4) \cdot C_2} = 3.18 \text{ Hz} \tag{1}$$

$$p_{L2} = \frac{1}{2\pi \cdot R_5 \cdot C_2} = 3.23 \text{ Hz} \tag{2}$$

The filter cutoff frequency is determined by a higher frequency pole, set by  $R_5$  and  $C_4$ .

$$p_H = \frac{1}{2\pi \cdot R_6 \cdot C_4} = 21.3 \text{ kHz} \tag{3}$$

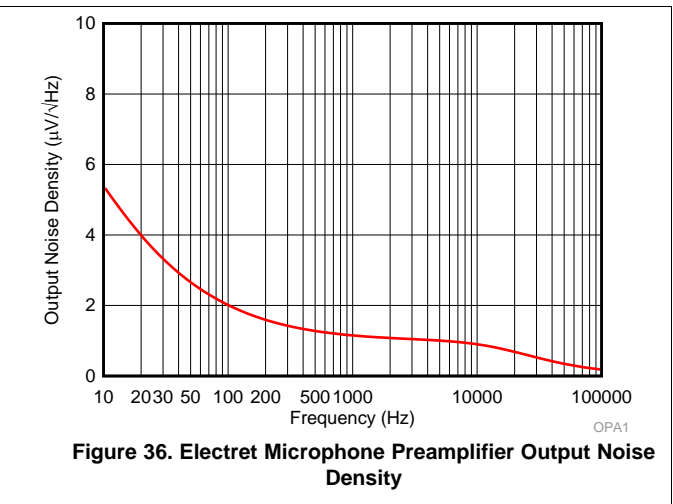
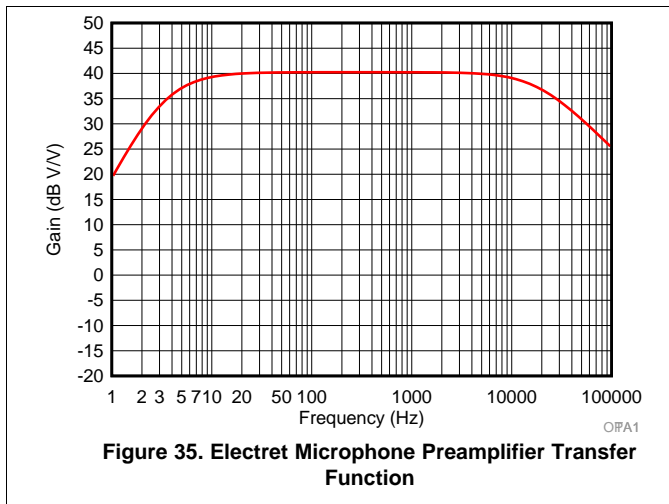
The gain of the circuit in the passband is set by  $R_5$  and  $R_6$ .

$$A(V/V) = \frac{R_6}{R_5} = 100 (40 \text{ dB}) \tag{4}$$

The output noise of the circuit (ignoring the electret microphone intrinsic noise and impedance) is the RSS average noise contribution from  $R_5$  and the input voltage noise of OPA1671.  $R_5$  was selected for minimal noise contribution without requiring a dc blocking cap. ( $C_3$ ) larger than  $10 \mu\text{F}$ . See [Equation 5](#) for the output noise density calculation at 10 kHz.

$$e_{N\_OUT} = \text{Input Referred Noise} \cdot \text{Gain} = \sqrt{(4kTR_5)^2 + V_{N\_10k}^2} \cdot 100 = 0.96 \mu\text{V}/\sqrt{\text{Hz}} \tag{5}$$

### 8.2.3 Application Curves



## 9 Power Supply Recommendations

The OPA1671 device is specified for operation from 1.7 V to 5.5 V ( $\pm 0.85$  V to  $\pm 2.75$  V).

## 10 Layout

### 10.1 Layout Guidelines

Paying attention to good layout practice is always recommended. Keep traces short and, when possible, use a printed-circuit board (PCB) ground plane with surface-mount components placed as close to the device pins as possible. Place a 0.1- $\mu$ F capacitor closely across the supply pins. These guidelines must be applied throughout the analog circuit to improve performance and provide benefits such as reducing the electromagnetic interference (EMI) susceptibility.

### 10.2 Layout Example

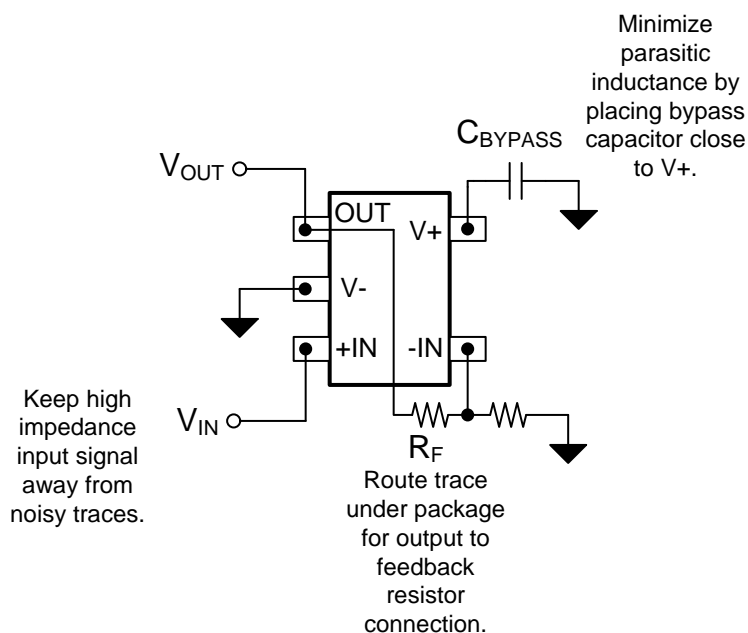


Figure 37. OPA1671 Layout Example

## 11 Device and Documentation Support

### 11.1 Device Support

#### 11.1.1 Development Support

##### 11.1.1.1 TINA-TI™ (Free Software Download)

TINA-TI™ is a simple, powerful, and easy-to-use circuit simulation program based on a SPICE engine. TINA-TI™ is a free, fully-functional version of the TINA™ software, preloaded with a library of macromodels in addition to a range of both passive and active models. TINA-TI™ provides all the conventional dc, transient, and frequency domain analysis of SPICE, as well as additional design capabilities.

Available as a [free download](#) from the Analog eLab Design Center, TINA-TI™ offers extensive post-processing capability that allows users to format results in a variety of ways. Virtual instruments offer the ability to select input waveforms and probe circuit nodes, voltages, and waveforms, creating a dynamic quick-start tool.

#### NOTE

These files require that either the TINA software (from DesignSoft™) or TINA-TI™ software be installed. Download the free TINA-TI™ software from the [TINA-TI™ folder](#).

### 11.2 Documentation Support

#### 11.2.1 Related Documentation

For related documentation see the following:

- Texas Instruments, [Circuit Board Layout Techniques](#)
- Texas Instruments, [Analog Engineer's Circuit Cookbook](#)

#### 11.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. In the upper right corner, click on *Alert me* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

#### 11.4 Community Resources

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

**TI E2E™ Online Community** *TI's Engineer-to-Engineer (E2E) Community*. Created to foster collaboration among engineers. At e2e.ti.com, you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.

**Design Support** *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

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## 11.6 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

## 11.7 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

## 12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical packaging and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

**PACKAGING INFORMATION**

Orderable part number	Status (1)	Material type (2)	Package   Pins	Package qty   Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
<a href="#">OPA1671IDBVR</a>	Active	Production	SOT-23 (DBV)   5	3000   LARGE T&R	Yes	NIPDAU   SN	Level-2-260C-1 YEAR	-40 to 125	1X6T
OPA1671IDBVR.A	Active	Production	SOT-23 (DBV)   5	3000   LARGE T&R	Yes	SN	Level-2-260C-1 YEAR	-40 to 125	1X6T
<a href="#">OPA1671IDBVT</a>	Active	Production	SOT-23 (DBV)   5	250   SMALL T&R	Yes	NIPDAU   SN	Level-2-260C-1 YEAR	-40 to 125	1X6T
OPA1671IDBVT.A	Active	Production	SOT-23 (DBV)   5	250   SMALL T&R	Yes	SN	Level-2-260C-1 YEAR	-40 to 125	1X6T
OPA1671IDBVTG4.A	Active	Production	SOT-23 (DBV)   5	250   SMALL T&R	-	Call TI	Call TI	-40 to 125	1X6T
<a href="#">OPA1671IDCKR</a>	Active	Production	SC70 (DCK)   5	3000   LARGE T&R	Yes	NIPDAU   SN	Level-2-260C-1 YEAR	-40 to 125	1D3
OPA1671IDCKR.A	Active	Production	SC70 (DCK)   5	3000   LARGE T&R	Yes	SN	Level-2-260C-1 YEAR	-40 to 125	1D3
<a href="#">OPA1671IDCKT</a>	Active	Production	SC70 (DCK)   5	250   SMALL T&R	Yes	NIPDAU   SN	Level-2-260C-1 YEAR	-40 to 125	1D3
OPA1671IDCKT.A	Active	Production	SC70 (DCK)   5	250   SMALL T&R	Yes	SN	Level-2-260C-1 YEAR	-40 to 125	1D3
<a href="#">OPA1671IDCKTG4</a>	Active	Production	SC70 (DCK)   5	250   SMALL T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	1D3
OPA1671IDCKTG4.A	Active	Production	SC70 (DCK)   5	250   SMALL T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	1D3

(1) **Status:** For more details on status, see our [product life cycle](#).

(2) **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

(3) **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

(4) **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

(5) **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

(6) **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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**TAPE AND REEL INFORMATION**

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**


\*All dimensions are nominal

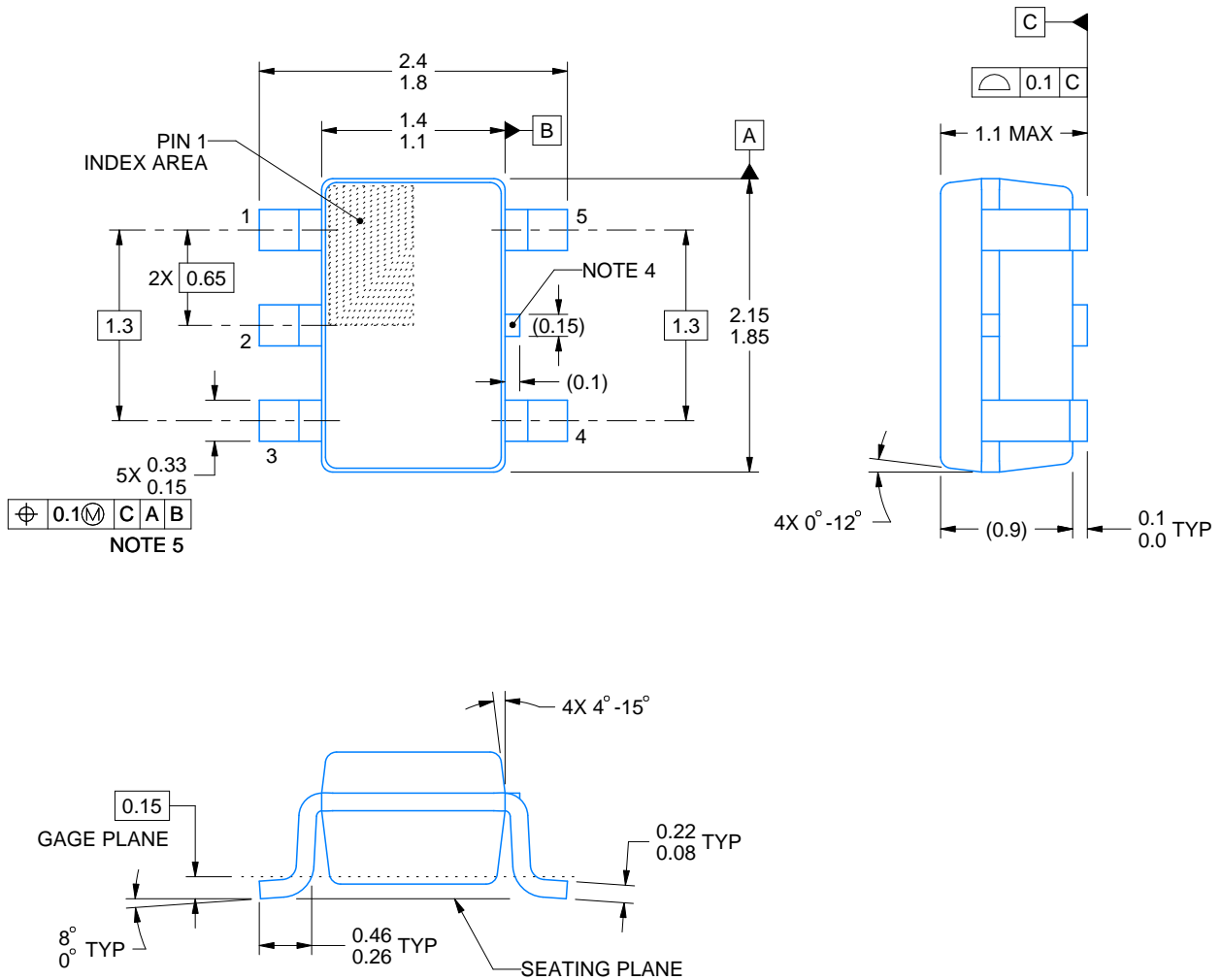
Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
OPA1671IDBVR	SOT-23	DBV	5	3000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
OPA1671IDBVT	SOT-23	DBV	5	250	180.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
OPA1671IDCKR	SC70	DCK	5	3000	180.0	8.4	2.3	2.5	1.2	4.0	8.0	Q3
OPA1671IDCKT	SC70	DCK	5	250	180.0	8.4	2.3	2.5	1.2	4.0	8.0	Q3
OPA1671IDCKTG4	SC70	DCK	5	250	178.0	9.0	2.4	2.5	1.2	4.0	8.0	Q3



**TAPE AND REEL BOX DIMENSIONS**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
OPA1671IDBVR	SOT-23	DBV	5	3000	208.0	191.0	35.0
OPA1671IDBVT	SOT-23	DBV	5	250	210.0	185.0	35.0
OPA1671IDCKR	SC70	DCK	5	3000	210.0	185.0	35.0
OPA1671IDCKT	SC70	DCK	5	250	210.0	185.0	35.0
OPA1671IDCKTG4	SC70	DCK	5	250	190.0	190.0	30.0



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NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. Reference JEDEC MO-203.
4. Support pin may differ or may not be present.
5. Lead width does not comply with JEDEC.
6. Body dimensions do not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.25mm per side

# EXAMPLE BOARD LAYOUT

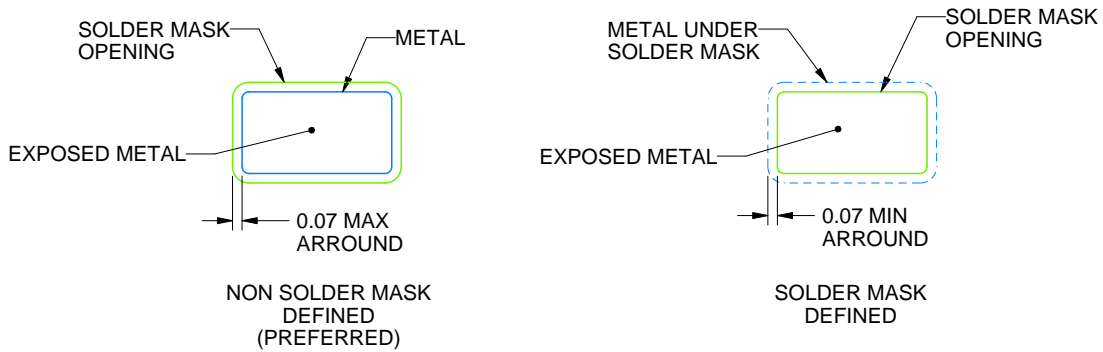
DCK0005A

SOT - 1.1 max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:18X



SOLDER MASK DETAILS

4214834/G 11/2024

NOTES: (continued)

- 7. Publication IPC-7351 may have alternate designs.
- 8. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

DCK0005A

SOT - 1.1 max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 THICK STENCIL  
SCALE:18X

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NOTES: (continued)

9. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
10. Board assembly site may have different recommendations for stencil design.

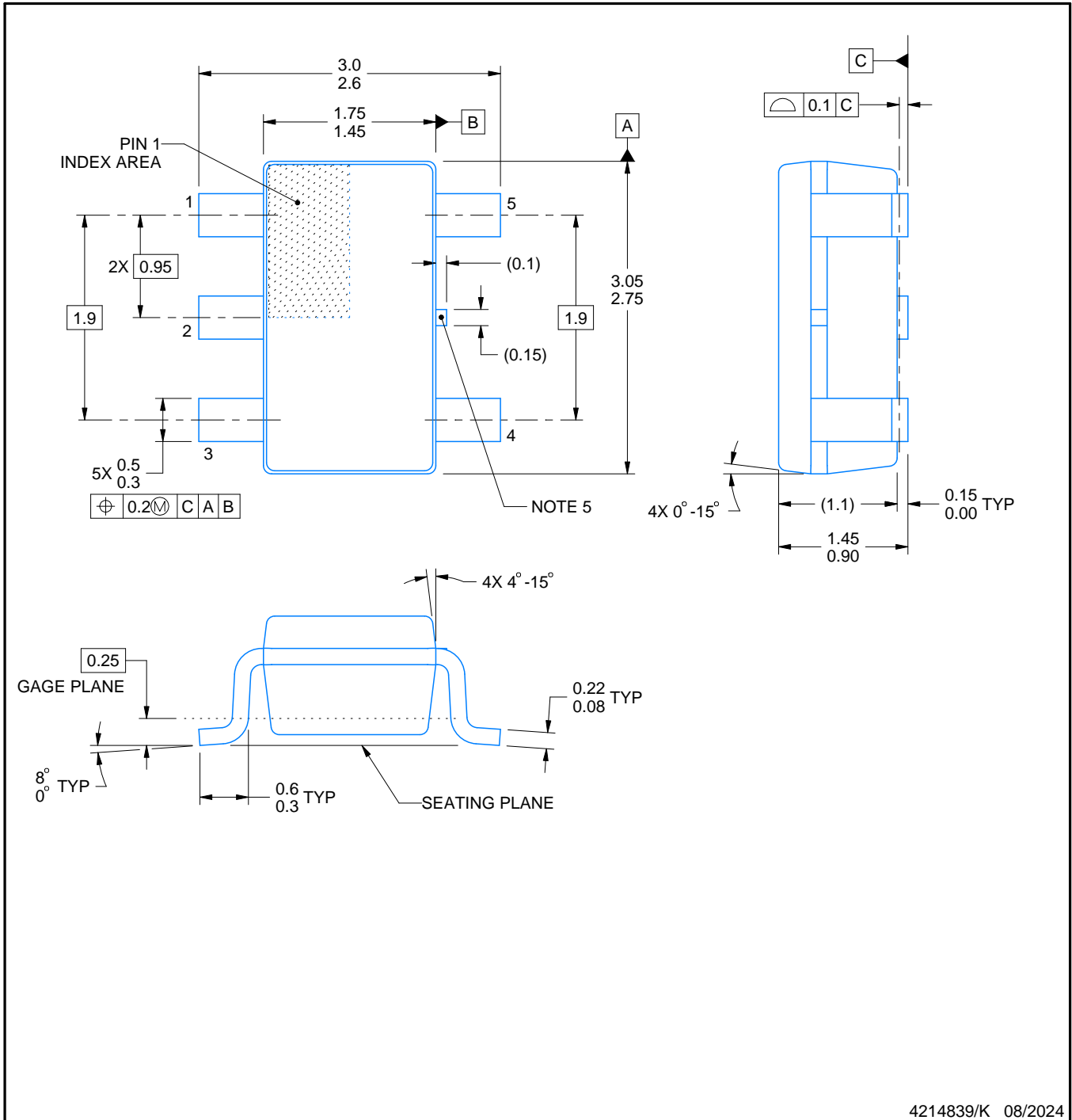


# PACKAGE OUTLINE

## DBV0005A

### SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



#### NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. Reference JEDEC MO-178.
4. Body dimensions do not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.25 mm per side.
5. Support pin may differ or may not be present.

# EXAMPLE BOARD LAYOUT

DBV0005A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:15X



SOLDER MASK DETAILS

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NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

DBV0005A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:15X

4214839/K 08/2024

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

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