

# LMC6024 Low Power CMOS Quad Operational Amplifier

Check for Samples: LMC6024

#### **FEATURES**

- Specified for 100 k $\Omega$  and 5 k $\Omega$  Loads
- High Voltage Gain 120 dB
- Low Offset Voltage Drift 2.5 μV/°C
- Ultra Low Input Bias Vurrent 40 fA
- Input Common-mode Range Includes V
- Operating Range from +5V to +15V Supply
- Low Distortion 0.01% at 1 kHz
- Slew Rate 0.11 V/µs
- Micropower Operation 1 mW

#### **APPLICATIONS**

- High-impedance Buffer or Preamplifier
- **Current-to-voltage Converter**
- Long-term Integrator
- Sample-and-hold Circuit
- **Peak Detector**
- Medical Instrumentation
- **Industrial Controls**

#### DESCRIPTION

The LMC6024 is a CMOS quad operational amplifier which can operate from either a single supply or dual supplies. Its performance features include an input common-mode range that reaches V-, low input bias current and voltage gain (into 100 k $\Omega$  and 5 k $\Omega$  loads) that is equal to or better than widely accepted bipolar equivalents, while the power supply requirement is less than 1 mW.

This chip is built with Texas Instrument's advanced Double-Poly Silicon-Gate CMOS process.

See the LMC6022 datasheet for a CMOS dual operational amplifier with these same features.

#### **Connection Diagram**

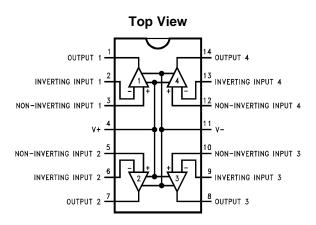


Figure 1. 14-Pin DIP and SOIC Package See Package Number D0014A



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

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# **Absolute Maximum Ratings** (1)(2)

Differential Input Voltage		±Supply Voltage			
Supply Voltage (V <sup>+</sup> - V <sup>-</sup> )		16\			
Lead Temperature	Soldering, 10 sec.	260°C			
Storage Temperature Range		-65°C to +150°C			
Voltage at Output/Input Pin		$(V^{+}) + 0.3V, (V^{-}) - 0.3V$			
Current at Input Pin		±5 mA			
Current at Output Pin		±18 mA			
Current at Power Supply Pin		35 mA			
Output Short Circuit to V+		See <sup>(3)</sup>			
Output Short Circuit to V		See <sup>(4)</sup>			
Junction Temperature		150°C			
ESD Tolerance <sup>(5)</sup>		1000V			
Power Dissipation		See <sup>(6)</sup>			

- (1) Absolute Maximum Ratings indicate limits beyond which damage to the component may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but do not guarantee specific performance limits. For guaranteed specifications and test conditions, see the Electrical Characteristics. The guaranteed specifications apply only for the test conditions listed.
- (2) If Military/Aerospace specified devices are required, please contact the Texas Instruments Sales Office/ Distributors for availability and specifications.
- (3) Do not connect output to V<sup>+</sup> when V<sup>+</sup> is greater than 13V or reliability may be adversely affected.
- (4) Applies to both single-supply and split-supply operation. Continuous short circuit operation at elevated ambient temperature and/or multiple Op Amp shorts can result in exceeding the maximum allowed junction temperature of 150°C. Output currents in excess of ±30 mA over long term may adversly affect reliability.
- (5) Human body model, 100 pF discharge through a 1.5 kΩ resistor.
- The maximum power dissipation is a function of  $T_{J(max)}$ ,  $\theta_{JA}$ , and  $T_A$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(max)} T_A)/\theta_{JA}$ .

## **Operating Ratings**

Temperature Range	-40°C ≤ T <sub>J</sub> ≤ +85°C				
Supply Voltage Range	4.75V to 15.5V				
Power Dissipation	Power Dissipation				
Thermal Resistance (θ <sub>JA</sub> ) <sup>(2)</sup>	Thermal Resistance (θ <sub>JA</sub> ) <sup>(2)</sup> 14-Pin DIP				
	14-Pin SOIC	115°C/W			

(1) For operating at elevated temperatures the device must be derated based on the thermal resistance  $\theta_{JA}$  with  $P_D = (T_J - T_A)/\theta_{JA}$ .

(2) All numbers apply for packages soldered directly into a PC board.



## **DC Electrical Characteristics**

The following specifications apply for  $V^+ = 5V$ ,  $V^- = 0V$ ,  $V_{CM} = 1.5V$ ,  $V_O = 2.5V$ , and  $R_L = 1M$  unless otherwise noted. **Boldface** limits apply at the temperature extremes; all other limits  $T_J = 25^{\circ}C$ .

	Parameter	Test	Conditions	Typical <sup>(1)</sup>	LMC6024I Limit <sup>(2)</sup>	Units
Vos	Input Offset Voltage			1	9	mV
					11	Max
ΔV <sub>OS</sub> /ΔT	Input Offset Voltage Average Drift			2.5		μV/°C
I <sub>B</sub>	Input Bias Current			0.04		pA
					200	Max
los	Input Offset Current			0.01	100	pA Max
R <sub>IN</sub>	Input Resistance			>1		TeraΩ
CMRR	Common Mode Rejection	$0V \le V_{CM} \le 12V$		83	63	dB
	Ratio	V <sup>+</sup> = 15V			61	Min
+PSRR	Positive Power Supply	5V ≤ V <sup>+</sup> ≤ 15V		83	63	dB
	Rejection Ratio				61	Min
-PSRR	Negative Power Supply	0V ≤ V <sup>-</sup> ≤ −10V		94	74	dB
	Rejection Ratio				73	Min
$V_{CM}$	Input Common-Mode Voltage	$V^{+} = 5V \text{ and } 15V$		-0.4	-0.1	V
	Range	For CMRR ≥ 50 DB			0	Max
				V <sup>+</sup> - 1.9	V <sup>+</sup> - 2.3	V
					V+ - 2.5	Min
$A_V$	Large Signal Voltage Gain	$R_L = 100 \text{ k}\Omega^{(3)}$	Sourcing	1000	200	V/mV
					100	Min
			Sinking	500	90	V/mV Min
					40	
		$R_L = 5 k\Omega^{(3)}$	Sourcing	1000 100 <b>75</b> 250 50		V/mV Min
			Sinking			V/mV Min
					20	
Vo	Output Voltage Swing	$V^{+} = 5V$ $R_{L} = 100 \text{ k}\Omega \text{ to } 2.5V$		4.987	4.40	V Min
		N_ = 100 K22 to 2.5V			4.43	
					0.06	V Max
					0.09	
		$V^{+} = 5V$ $R_{L} = 5 \text{ k}\Omega \text{ to } 2.5V$		4.940	4.20	V Min
		N_ = 3 K22 to 2.3 V			4.00	
				0.040	0.25	V Max
		) /t			0.35	
		$V^{+} = 15V$ $R_{L} = 100 \text{ k}\Omega \text{ to } 7.5V$		14.970	14.00	V Min
				0.007	13.90	
				0.007	0.06	V Max
		\/t 45\/		44.040	0.09	V Min
		$V^{+} = 15V$ $R_{L} = 5 k\Omega \text{ to } 7.5V$		14.840	13.70	
				0.110	13.50	
					0.32	V Max
					0.40	

<sup>(1)</sup> Typical values represent the most likely parametric norm.

<sup>(2)</sup> All limits are guaranteed by testing or correlation.

<sup>(3)</sup>  $V^+ = 15V$ ,  $V_{CM} = 7.5V$ , and  $R_L$  connected to 7.5V. For Sourcing tests,  $7.5V \le V_O \le 11.5V$ . For Sinking tests,  $2.5V \le V_O \le 7.5V$ .



## **DC Electrical Characteristics (continued)**

The following specifications apply for  $V^+$  = 5V,  $V^-$  = 0V,  $V_{CM}$  = 1.5V,  $V_O$  = 2.5V, and  $R_L$  = 1M unless otherwise noted. **Boldface** limits apply at the temperature extremes; all other limits  $T_J$  = 25°C.

	Parameter	Test Conditions	Typical <sup>(1)</sup>	LMC6024I Limit <sup>(2)</sup>	Units	
lo	Output Current	V <sup>+</sup> = 5V	22	13	mA	
		Sourcing, $V_O = 0V$ Sinking $V_O = 5V$		9	Min	
		Oliking VO = 5V	21	13	mA	
				9	Min	
		V <sup>+</sup> = 15V	40	23	mA	
		Sourcing, $V_O = 0V$ Sinking, $V_O = 13V$ <sup>(5)</sup>		15	Min	
		Oliking, VO = 10V	39	23	mA	
				15	Min	
I <sub>S</sub>	Supply Current	All Four Amplifiers	160	240	μΑ	
		$V_O = 1.5V$		280	Max	

Applies to both single-supply and split-supply operation. Continuous short circuit operation at elevated ambient temperature and/or multiple Op Amp shorts can result in exceeding the maximum allowed junction temperature of 150°C. Output currents in excess of ±30 mA over long term may adversly affect reliability.

#### **AC Electrical Characteristics**

The following specifications apply for  $V^+ = 5V$ ,  $V^- = 0V$ ,  $V_{CM} = 1.5V$ ,  $V_O = 2.5V$ , and  $R_L = 1M$  unless otherwise noted. **Boldface** limits apply at the temperature extremes; all other limits  $T_J = 25$ °C.

	Parameter	Test Conditions	Typical <sup>(1)</sup>	LMC6024I Limit <sup>(2)</sup>	Units
SR	Slew Rate	See <sup>(3)</sup>	0.11	0.05	V/µs
				0.03	Min
GBW	Gain-Bandwidth Product		0.35		MHz
$\theta_{M}$	Phase Margin		50		Deg
G <sub>M</sub>	Gain Margin		17		dB
	Amp-to-Amp Isolation	See <sup>(4)</sup>	130		dB
e <sub>n</sub>	Input-Referred Voltage Noise	F = 1 kHz	42		nV/√ <del>Hz</del>
i <sub>n</sub>	Input-Referred Current Noise	F = 1 kHz	0.0002		pA/√ <del>Hz</del>

- Typical values represent the most likely parametric norm.
- All limits are guaranteed by testing or correlation.
- $V^+$  = 15V. Connected as Voltage Follower with 10V step input. Number specified is the slower of the positive and negative slew rates. Input referred,  $V^+$  = 15V and R<sub>L</sub> = 100 k $\Omega$  connected to 7.5V. Each amp excited in turn with 1 kHz to produce V<sub>O</sub> = 13 V<sub>PP</sub>.

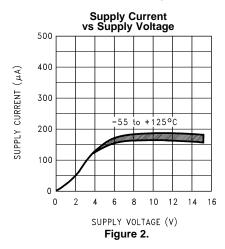
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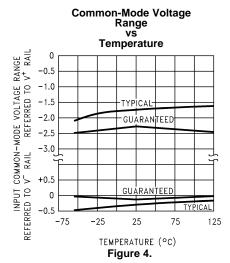
Do not connect output to V+ when V+ is greater than 13V or reliability may be adversely affected.

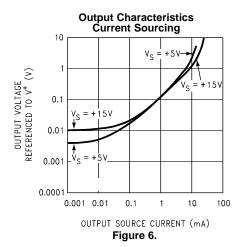


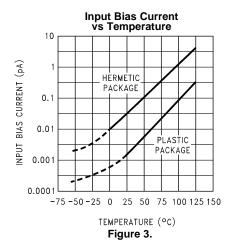
## **Typical Performance Characteristics**

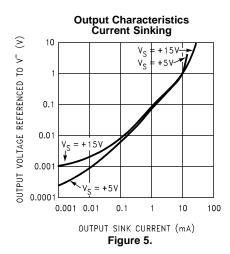
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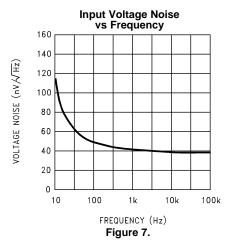








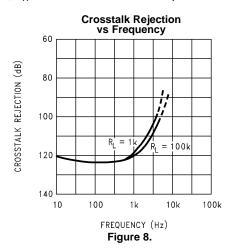


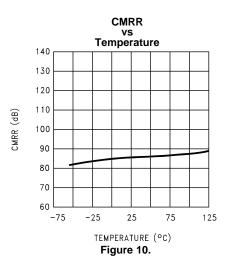


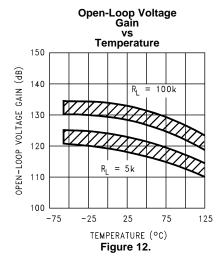


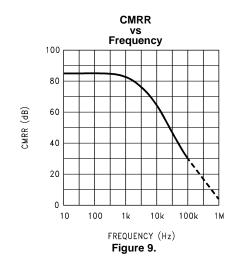
# **Typical Performance Characteristics (continued)**

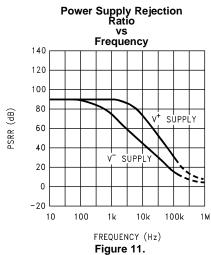
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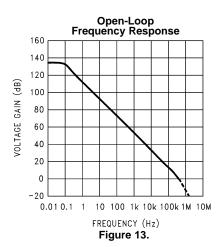










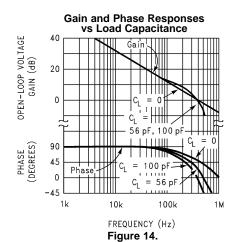


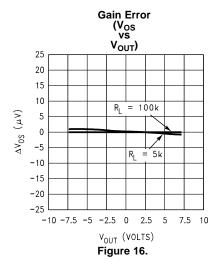
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## **Typical Performance Characteristics (continued)**

 $V_S = \pm 7.5V$ ,  $T_A = 25$ °C unless otherwise specified





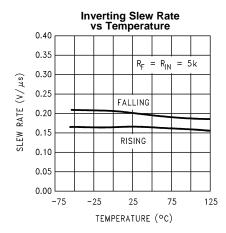
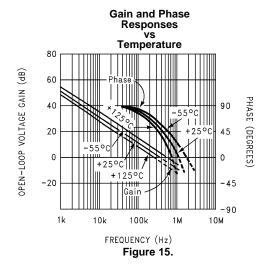
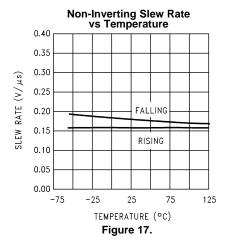
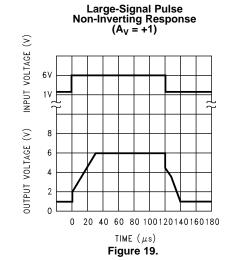


Figure 18.



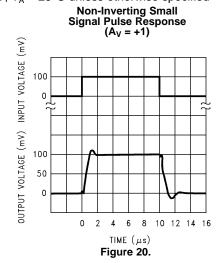






## **Typical Performance Characteristics (continued)**

 $V_S = \pm 7.5 V$ ,  $T_A = 25$ °C unless otherwise specified





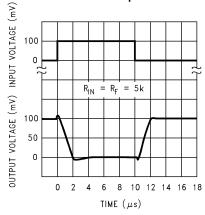


Figure 22.

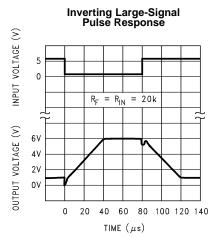
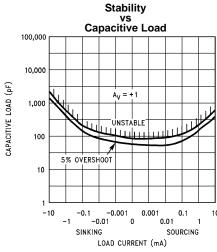


Figure 21.



Avoid resistive loads of less than  $500\Omega$ , as they may cause instability. Figure 23.

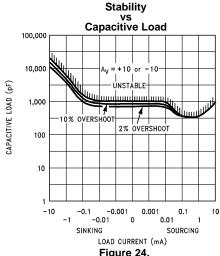


Figure 24.

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#### APPLICATION HINTS

#### **AMPLIFIER TOPOLOGY**

The topology chosen for the LMC6024 is unconventional (compared to general-purpose op amps) in that the traditional unity-gain buffer output stage is not used; instead, the output is taken directly from the output of the integrator, to allow rail-to-rail output swing. Since the buffer traditionally delivers the power to the load, while maintaining high op amp gain and stability, and must withstand shorts to either rail, these tasks now fall to the integrator.

As a result of these demands, the integrator is a compound affair with an embedded gain stage that is doubly fed forward (via  $C_f$  and  $C_{ff}$ ) by a dedicated unity-gain compensation driver. In addition, the output portion of the integrator is a push-pull configuration for delivering heavy loads. While sinking current the whole amplifier path consists of three gain stages with one stage fed forward, whereas while sourcing the path contains four gain stages with two fed forward.

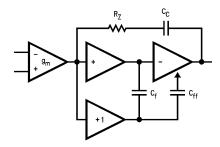


Figure 25. LMC6024 Circuit Topology (Each Amplifier)

The large signal voltage gain while sourcing is comparable to traditional bipolar op amps, for load resistance of at least 5 k $\Omega$ . The gain while sinking is higher than most CMOS op amps, due to the additional gain stage; however, when driving load resistance of 5 k $\Omega$  or less, the gain will be reduced as indicated in the Electrical Characterisitics. The op amp can drive load resistance as low as 500 $\Omega$  without instability.

#### **COMPENSATING INPUT CAPACITANCE**

Refer to the LMC660 or LMC662 datasheets to determine whether or not a feedback capacitor will be necessary for compensation and what the value of that capacitor would be.

#### CAPACITIVE LOAD TOLERANCE

Like many other op amps, the LMC6024 may oscillate when its applied load appears capacitive. The threshold of oscillation varies both with load and circuit gain. The configuration most sensitive to oscillation is a unity-gain follower. See the Typical Performance Characteristics.

The load capacitance interacts with the op amp's output resistance to create an additional pole. If this pole frequency is sufficiently low, it will degrade the op amp's phase margin so that the amplifier is no longer stable at low gains. The addition of a small resistor ( $50\Omega$  to  $100\Omega$ ) in series with the op amp's output, and a capacitor (5 pF to 10 pF) from inverting input to output pins, returns the phase margin to a safe value without interfering with lower-frequency circuit operation. Thus, larger values of capacitance can be tolerated without oscillation. Note that in all cases, the output will ring heavily when the load capcitance is near the threshold for oscillation.

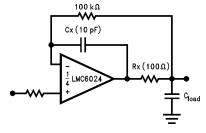


Figure 26. Rx, Cx Improve Capacitive Load Tolerance



Capacitive load driving capability is enhanced by using a pull up resistor to V<sup>+</sup> (Figure 27). Typically a pull up resistor conducting 50  $\mu$ A or more will significantly improve capacitive load responses. The value of the pull up resistor must be determined based on the current sinking capability of the amplifier with respect to the desired output swing. Open loop gain of the amplifier can also be affected by the pull up resistor (see DC Electrical Characteristics).

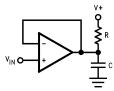


Figure 27. Compensating for Large Capacitive Loads with a Pull Up Resistor

# PRINTED-CIRCUIT-BOARD LAYOUT FOR HIGH-IMPEDANCE WORK

It is generally recognized that any circuit which must operate with less than 1000 pA of leakage current requires special layout of the PC board. When one wishes to take advantage of the ultra-low bias current of the LMC6024, typically less than 0.04 pA, it is essential to have an excellent layout. Fortunately, the techniques for obtaining low leakages are quite simple. First, the user must not ignore the surface leakage of the PC board, even though it may sometimes appear acceptably low, because under conditions of high humidity or dust or contamination, the surface leakage will be appreciable.

To minimize the effect of any surface leakage, lay out a ring of foil completely surrounding the LMC6024's inputs and the terminals of capacitors, diodes, conductors, resistors, relay terminals, etc. connected to the op-amp's inputs. See Figure 28. To have a significant effect, guard rings should be placed on both the top and bottom of the PC board. This PC foil must then be connected to a voltage which is at the same voltage as the amplifier inputs, since no leakage current can flow between two points at the same potential. For example, a PC board trace-to-pad resistance of 10<sup>12</sup> ohms, which is normally considered a very large resistance, could leak 5 pA if the trace were a 5V bus adjacent to the pad of an input. This would cause a 100 times degradation from the LMC6024's actual performance. However, if a guard ring is held within 5 mV of the inputs, then even a resistance of 10<sup>11</sup> ohms would cause only 0.05 pA of leakage current, or perhaps a minor (2:1) degradation of the amplifier's performance. See Figure 28, Figure 30, and Figure 31 for typical connections of guard rings for standard op-amp configurations. If both inputs are active and at high impedance, the guard can be tied to ground and still provide some protection; see Figure 32.

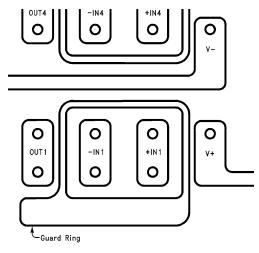


Figure 28. Example of Guard Ring in P.C. Board Layout (Using the LMC6024)

Product Folder Links: LMC6024

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#### **Guard Ring Connections**

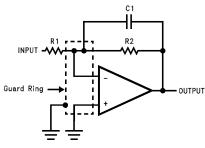
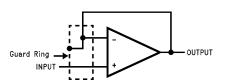


Figure 29. Inverting Amplifier Guard Ring Connections



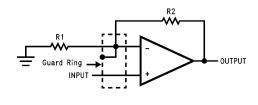


Figure 30. Non-Inverting Amplifier Guard Ring Connections

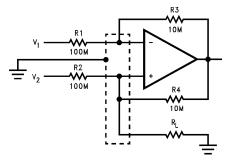
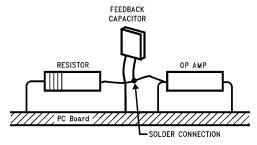


Figure 31. Follower Guard Ring Connections

Figure 32. Howland Current Pump Guard Ring Connections

The designer should be aware that when it is inappropriate to lay out a PC board for the sake of just a few circuits, there is another technique which is even better than a guard ring on a PC board: Don't insert the amplifier's input pin into the board at all, but bend it up in the air and use only air as an insulator. Air is an excellent insulator. In this case you may have to forego some of the advantages of PC board construction, but the advantages are sometimes well worth the effort of using point-to-point up-in-the-air wiring. See Figure 33.



(Input pins are lifted out of PC board and soldered directly to components. All other pins connected to PC board.)

Figure 33. Air Wiring



#### **BIAS CURRENT TESTING**

The test method of Figure 34 is appropriate for bench-testing bias current with reasonable accuracy. To understand its operation, first close switch S2 momentarily. When S2 is opened, then

$$I^{-} = \frac{dV_{OUT}}{dt} \times C2. \tag{1}$$

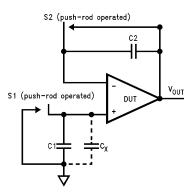


Figure 34. Simple Input Bias Current Test Circuit

A suitable capacitor for C2 would be a 5 pF or 10 pF silver mica, NPO ceramic, or air-dielectric. When determining the magnitude of I<sup>-</sup>, the leakage of the capacitor and socket must be taken into account. Switch S2 should be left shorted most of the time, or else the dielectric absorption of the capacitor C2 could cause errors.

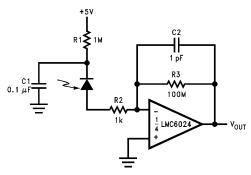
Similarly, if S1 is shorted momentarily (while leaving S2 shorted)

$$I^{+} = \frac{dV_{OUT}}{dt} \times (C1 + C_{\chi}) \tag{2}$$

where C<sub>x</sub> is the stray capacitance at the +input.

#### **Typical Single-Supply Applications**

$$(V^+ = 5.0 V_{DC})$$



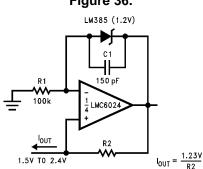
A 5V bias on the photodiode can cut its capacitance by a factor of 2 or 3, leading to improved response and lower noise. However, this bias on the photodiode will cause photodiode leakage (also known as its dark current).

Figure 35. Photodiode Current-to-Voltage Converter



 $(V^+ = 5.0 V_{DC})$ 

Figure 36.



(Upper limit of output range dictated by input common-mode range; lower limit dictated by minimum current requirement of LM385.)

Figure 37. Micropower Current Source

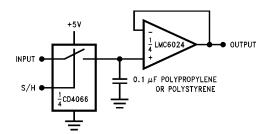
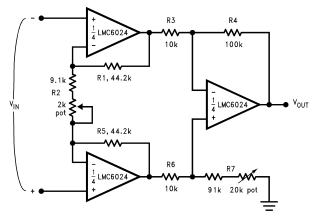


Figure 38. Low-Leakage Sample-and-Hold



If R1 = R5, R3 = R6, and R4 = R7;

Then

 $\frac{V_{OUT}}{V_{IN}} = \frac{R2 + 2R1}{R2} \times \frac{R4}{R3}.$ 

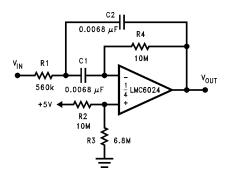
∴ $A_V$  ≈ 100 for circuit shown.

For good CMRR over temperature, low drift resistors should be used. Matching of R3 to R6 and R4 to R7 affects CMRR. Gain may be adjusted through R2. CMRR may be adjusted through R7.

Figure 39. Instrumentation Amplifier

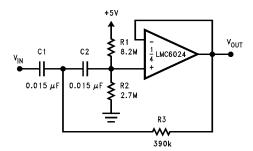


 $(V^+ = 5.0 V_{DC})$ 



 $f_O = 10 \text{ Hz}$  Q = 2.1Gain = -8.8

Figure 40. 10 Hz Bandpass Filter



 $f_c = 10 \text{ Hz}$  d = 0.895Gain = 1

Figure 41. 10 Hz High-Pass Filter (2 dB Dip)

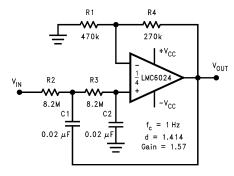
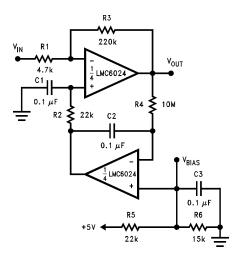


Figure 42. 1 Hz Low-Pass Filter (Maximally Flat, Dual Supply Only)



 $(V^+ = 5.0 V_{DC})$ 



$$\label{eq:Gain} \begin{split} \text{Gain} &= -46.8 \\ \text{Output offset voltage reduced to the level of the input offset voltage of the bottom amplifier (typically 1 mV), referred to $V_{BIAS}$. \end{split}$$

Figure 43. High Gain Amplifier with Offset Voltage Reduction

#### SNOS621D - AUGUST 2000 - REVISED MARCH 2013



# **REVISION HISTORY**

Cł	nanges from Revision C (March 2013) to Revision D	Pag	j€
•	Changed layout of National Data Sheet to TI format	1	Ę

www.ti.com 11-Nov-2025

#### PACKAGING INFORMATION

Orderable part number	Status	Material type	Package   Pins	Package qty   Carrier	RoHS	Lead finish/	MSL rating/	Op temp (°C)	Part marking
	(1)	(2)			(3)	Ball material	Peak reflow	Peak reflow	
						(4)	(5)		
LMC6024IM/NOPB	Active	Production	SOIC (D)   14	55   TUBE	Yes	SN	Level-1-260C-UNLIM	-40 to 85	LMC6024IM
LMC6024IM/NOPB.A	Active	Production	SOIC (D)   14	55   TUBE	Yes	SN	Level-1-260C-UNLIM	-40 to 85	LMC6024IM
LMC6024IM/NOPB.B	Active	Production	SOIC (D)   14	55   TUBE	Yes	SN	Level-1-260C-UNLIM	-40 to 85	LMC6024IM
LMC6024IMX/NOPB	Active	Production	SOIC (D)   14	2500   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	LMC6024IM
LMC6024IMX/NOPB.A	Active	Production	SOIC (D)   14	2500   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	LMC6024IM
LMC6024IMX/NOPB.B	Active	Production	SOIC (D)   14	2500   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	LMC6024IM

<sup>(1)</sup> Status: For more details on status, see our product life cycle.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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<sup>(3)</sup> RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

<sup>(4)</sup> Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

<sup>(5)</sup> MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

<sup>(6)</sup> Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.



# **PACKAGE OPTION ADDENDUM**

www.ti.com 11-Nov-2025

# **PACKAGE MATERIALS INFORMATION**

www.ti.com 23-May-2025

#### TAPE AND REEL INFORMATION





	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

#### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



#### \*All dimensions are nominal

Device		Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LMC6024IMX/NOPB	SOIC	D	14	2500	330.0	16.4	6.5	9.35	2.3	8.0	16.0	Q1

www.ti.com 23-May-2025



#### \*All dimensions are nominal

Ì	Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)	
ı	LMC6024IMX/NOPB	SOIC	D	14	2500	356.0	356.0	35.0	

# **PACKAGE MATERIALS INFORMATION**

www.ti.com 23-May-2025

#### **TUBE**



\*All dimensions are nominal

	Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	T (µm)	B (mm)
	LMC6024IM/NOPB	D	SOIC	14	55	495	8	4064	3.05
	LMC6024IM/NOPB.A	D	SOIC	14	55	495	8	4064	3.05
ĺ	LMC6024IM/NOPB.B	D	SOIC	14	55	495	8	4064	3.05



SMALL OUTLINE INTEGRATED CIRCUIT



#### NOTES:

- 1. All linear dimensions are in millimeters. Dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.

  2. This drawing is subject to change without notice.

  3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not
- exceed 0.15 mm, per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.43 mm, per side.
- 5. Reference JEDEC registration MS-012, variation AB.



SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.



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Last updated 10/2025