

www.ti.com

SNAS133D - FEBRUARY 2001 - REVISED MARCH 2013

LM4819 Boomer® Audio Power Amplifier Series 350mW Audio Power Amplifier with Shutdown Mode

Check for Samples: LM4819, LM4819MBD

FEATURES

- WSON, SOIC, and VSSOP Surface Mount Packaging
- Switch On/Off Click Suppression
- Unity-Gain Stable
- Minimum External Components

KEY SPECIFICATIONS

- THD+N at 1kHz, 350mW Continuous Average Output Power into 16Ω: 10% (max)
- THD+N at 1kHz, 300mW Continuous Average Output Power into 8Ω: 10% (max)
- Shutdown Current: 0.7µA (typ)

APPLICATIONS

- General Purpose Audio
- Portable Electronic Devices
- Information Appliances (IA)

Typical Application

DESCRIPTION

The LM4819 is a mono bridged power amplifier that is capable of delivering $350 \text{mW}_{\text{RMS}}$ output power into a 16Ω load or $300 \text{mW}_{\text{RMS}}$ output power into an 8Ω load with 10% THD+N from a 5V power supply.

The LM4819 Boomer audio power amplifier is designed specifically to provide high quality output power and minimize PCB area with surface mount packaging and a minimal amount of external components. Since the LM4819 does not require output coupling capacitors, bootstrap capacitors or snubber networks, it is optimally suited for low-power portable applications.

The closed loop response of the unity-gain stable LM4819 can be configured using external gain-setting resistors. The device is available in WSON, VSSOP, and SOIC package types to suit various applications.

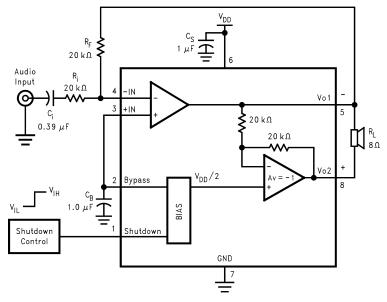


Figure 1. Typical Audio Amplifier Application Circuit

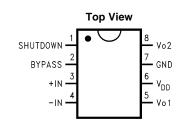
Connection Diagrams

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet. All trademarks are the property of their respective owners.



www.ti.com

SNAS133D-FEBRUARY 2001-REVISED MARCH 2013



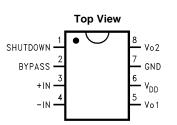
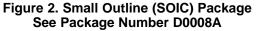
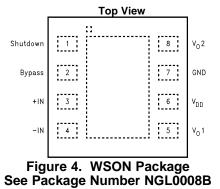


Figure 3. Mini Small Outline (VSSOP) Package

See Package Number DGK0008A





8

These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.



www.ti.com

Absolute Maximum Ratings⁽¹⁾⁽²⁾⁽³⁾

Supply Voltage		6.0V	
Storage Temperature			-65°C to +150°C
Input Voltage			-0.3V to V _{DD} +0.3V
Power Dissipation (P _D) ⁽⁴⁾			Internally Limited
ESD Susceptibility ⁽⁵⁾			3.5kV
ESD Susceptibility ⁽⁶⁾			250V
Junction Temperature (T _J)			150°C
Soldering Information	Small Outline Package	Vapor Phase (60 seconds)	215°C
		Infrared (15 seconds)	220°C
Thermal Resistance		θ _{JC} (VSSOP)	56°C/W
		θ _{JA} (VSSOP)	210°C/W
		θ_{JC} (SOIC)	35°C/W
		θ _{JA} (SOIC)	170°C/W
		θ _{JA} (WSON)	117°C/W ⁽⁷⁾
		θ _{JA} (WSON)	150°C/W ⁽⁸⁾

(1) All voltages are measured with respect to the ground pin, unless otherwise specified.

(2) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is functional, but do not ensure specific performance limits. Electrical Characteristics state DC and AC electrical specifications under particular test conditions which ensure specific performance limits. This assumes that the device is within the Operating Ratings. Specifications are not ensured for parameters where no limit is given. However, the typical value is a good indication of device's performance.

(3) If Military/Aerospace specified devices are required, please contact the TI Sales Office/ Distributors for availability and specifications.

(4) The maximum power dissipation must be derated at elevated temperatures and is dictated by T_{JMAX}, θ_{JA}, and the ambient temperature T_A. The maximum allowable power dissipation is P_{DMAX} = (T_{JMAX}-T_A)/θ_{JA}. For the LM4819, T_{JMAX} = 150°C and the typical junction-to-ambient thermal resistance (θ_{JA}) when board mounted is 210°C/W for the VSSOP package and 170°C/W for the SOIC package.

- (5) Human body model, 100pF discharged through a 1.5 k Ω resistor.
- (6) Machine Model, 220pF–240pF capacitor is discharged through all pins.

(7) The given θ_{JA} is for an LM4819 package in an NGL0008B with the Exposed-DAP soldered to a printed circuit board copper pad with an area equivalent to that of the Exposed-DAP itself. The Exposed-DAP of the NGL0008B package should be electrically connected to GND or an electrically isolated copper area.

(8) The given θ_{JA} is for an LM4819 package in an NGL0008B with the Exposed-DAP not soldered to any printed circuit board copper.

Operating Ratings⁽¹⁾⁽²⁾

Temperature Range $T_{MIN} \le T_A \le T_{MAX}$	−40°C ≤ T _A ≤ 85°C
Supply Voltage	$2.0V \le V_{CC} \le 5.5V$

(1) All voltages are measured with respect to the ground pin, unless otherwise specified.

(2) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is functional, but do not ensure specific performance limits. Electrical Characteristics state DC and AC electrical specifications under particular test conditions which ensure specific performance limits. This assumes that the device is within the Operating Ratings. Specifications are not ensured for parameters where no limit is given. However, the typical value is a good indication of device's performance.

www.ti.com

STRUMENTS

FXAS

Electrical Characteristics $V_{DD} = 5V^{(1)(2)}$

The following specifications apply for $V_{DD} = 5V$, $R_L = 16\Omega$ unless otherwise stated. Limits apply for $T_A = 25^{\circ}C$.

	Descusion		LM4819		Units (Limits)
Parameter		Test Conditions	Typical ⁽³⁾	Limit ⁽⁴⁾⁽⁵⁾	
I _{DD}	Quiescent Power Supply Current	$V_{IN} = 0V, I_0 = 0A$	1.5	3.0	mA (max)
I _{SD}	Shutdown Current	$V_{PIN1} = V_{DD}{}^{(6)}$	1.0	5.0	μA (max)
V _{SDIH}	Shutdown Voltage Input High			4.0	V (min)
V _{SDIL}	Shutdown Voltage Input Low			1.0	V (max)
V _{OS}	Output Offset Voltage	$V_{IN} = 0V$	5	50	mV (max)
D	Output Dower	$THD = 10\%, f_{IN} = 1kHz$	350		mW
Po	Output Power	THD = 10%, f_{IN} = 1kHz, R_L = 8 Ω	300		mW
THD+N	Total Harmonic Distortion + Noise	$P_O = 270 \text{mW}_{\text{RMS}}, A_{\text{VD}} = 2, f_{\text{IN}} = 1 \text{kHz}$	1		%

(1) All voltages are measured with respect to the ground pin, unless otherwise specified.

(2) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is functional, but do not ensure specific performance limits. Electrical Characteristics state DC and AC electrical specifications under particular test conditions which ensure specific performance limits. This assumes that the device is within the Operating Ratings. Specifications are not ensured for parameters where no limit is given. However, the typical value is a good indication of device's performance.

(3) Typical specifications are specified at 25°C and represent the parametric norm.

(4) Tested limits are specified to TI's AOQL (Average Outgoing Quality Level).

- (5) Datasheet min/max specification limits are specified by designs, test, or statistical analysis.
- (6) The shutdown pin (pin1) should be driven as close as possible to V_{DD} for minimum current in Shutdown Mode.

Electrical Characteristics $V_{DD} = 3V^{(1)(2)}$

The following specifications apply for V_{DD} = 3V and R_L = 16 Ω load unless otherwise stated. Limits apply to T_A = 25°C.

	Descusion	Test Osmilitisms	LM4819		Units
Parameter		Test Conditions	Typical ⁽³⁾	Limit ⁽⁴⁾⁽⁵⁾	(Limits)
I _{DD}	Quiescent Power Supply Current	$V_{IN} = 0V, I_0 = 0A$	1.0	3.0	mA (max)
I _{SD}	Shutdown Current	$V_{PIN1} = V_{DD}{}^{(6)}$	0.7	5.0	μA (max)
V _{SDIH}	Shutdown Voltage Input High			2.4	V (min)
V _{SDIL}	Shutdown Voltage Input Low			0.6	V (max)
V _{OS}	Output Offset Voltage	$V_{IN} = 0V$	5	50	mV
D	Output Dower	$THD = 10\%, f_{IN} = 1kHz$	110		mW
Po	Output Power	$THD = 10\%, f_{IN} = 1 kHz, R_L = 8\Omega$	90		mW
THD+N	Total Harmonic Distortion + Noise	$P_O=80mW_RMS,A_VD=2,f_IN=1kHz$	1		%

(1) All voltages are measured with respect to the ground pin, unless otherwise specified.

(2) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is functional, but do not ensure specific performance limits. Electrical Characteristics state DC and AC electrical specifications under particular test conditions which ensure specific performance limits. This assumes that the device is within the Operating Ratings. Specifications are not ensured for parameters where no limit is given. However, the typical value is a good indication of device's performance.

(3) Typical specifications are specified at 25°C and represent the parametric norm.

(4) Tested limits are specified to TI's AOQL (Average Outgoing Quality Level).

(5) Datasheet min/max specification limits are specified by designs, test, or statistical analysis.

(6) The shutdown pin (pin1) should be driven as close as possible to V_{DD} for minimum current in Shutdown Mode.



LM4819, LM4819MBD

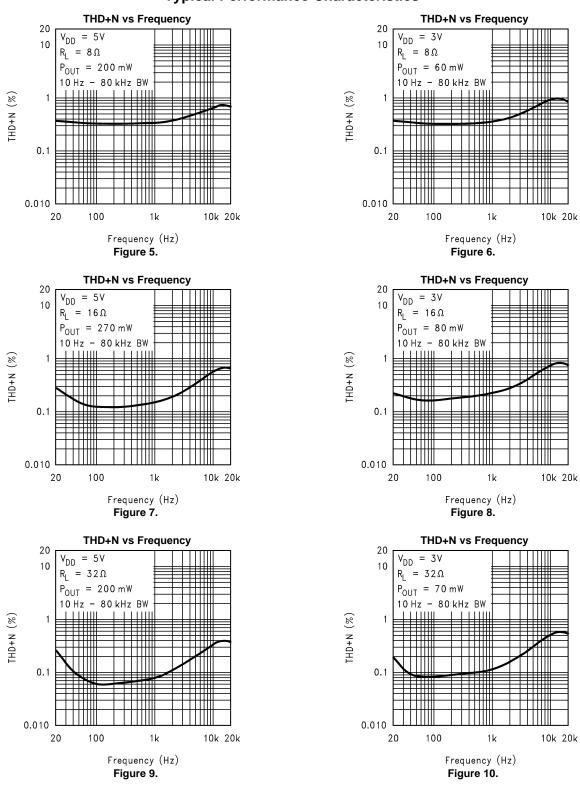
www.ti.com

SNAS133D – FEBRUARY 2001 – REVISED MARCH 2013 External Components Description

(See Figure 1)

Components		Functional Description			
1.	R _i	Combined with R_f , this inverting input resistor sets the closed-loop gain. R_i also forms a high pass filter with C_i at $f_c = 1/(2\pi R_i C_i)$.			
2.	C _i	This input coupling capacitor blocks DC voltage at the amplifier's terminals. Combined with R _i , it creates a high pass filter with R _i at $f_c = 1/(2\pi R_i C_i)$. Refer to the section, Proper Selection of External Components for an explanation of how to determine the value of C _i .			
3.	R _f	Combined with R_i , this is the feedback resistor that sets the closed-loop gain: $A_v = 2(R_F/R_i)$.			
4.	Cs	This is the power supply bypass capacitor that filters the voltage applied to the power supply pin. Refer to the Application Information section for proper placement and selection of C_s .			
5.	C _B	This is the bypass pin capacitor that filters the voltage at the BYPASS pin. Refer to the section, Proper Selection of External Components, for information concerning proper placement and selection of C_{B} .			

Copyright © 2001–2013, Texas Instruments Incorporated



Typical Performance Characteristics

www.ti.com

INSTRUMENTS

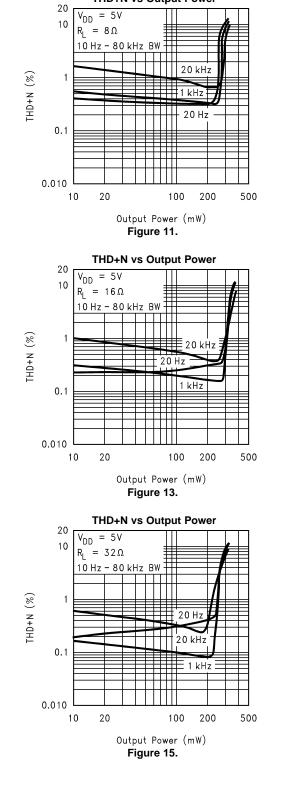
Texas

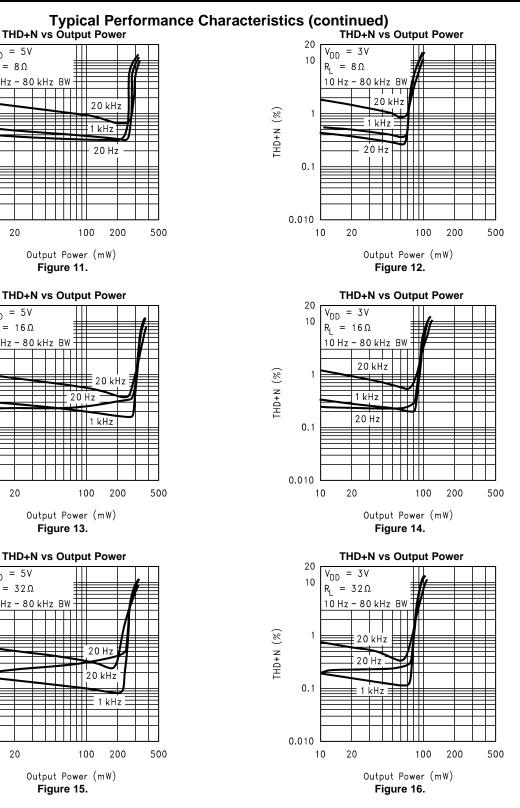
Copyright © 2001–2013, Texas Instruments Incorporated

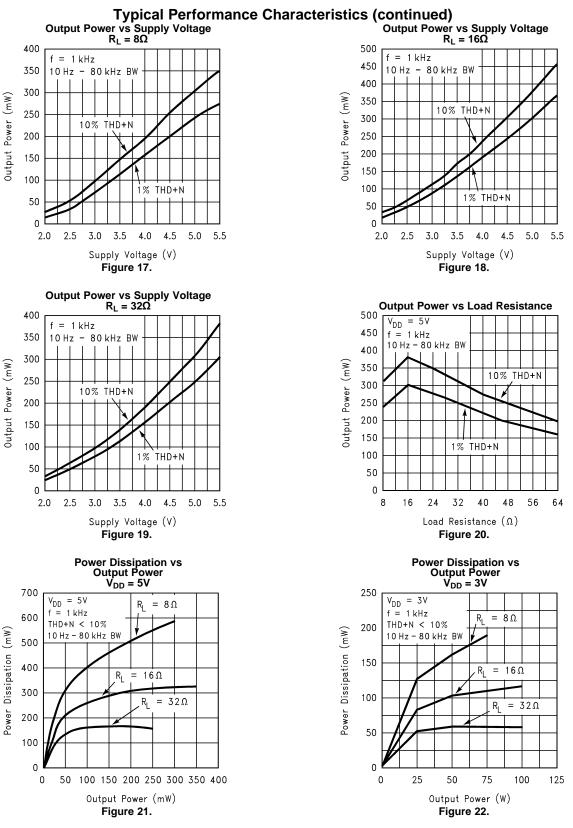
EXAS INSTRUMENTS

www.ti.com

SNAS133D-FEBRUARY 2001-REVISED MARCH 2013





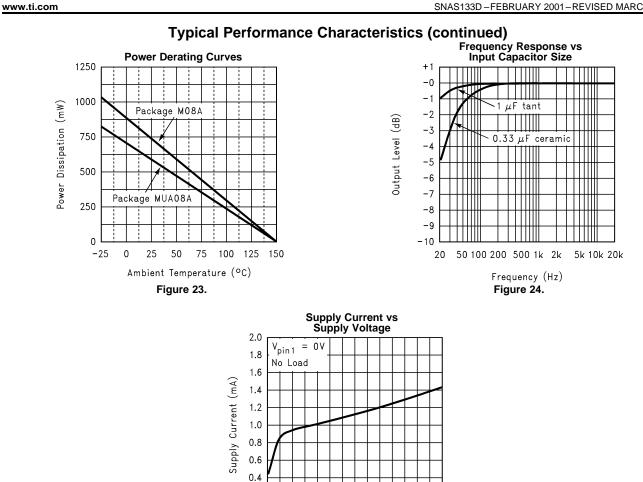


8

NSTRUMENTS

Texas





0.2 0.0

2.0 2.5

3.0 3.5 4.0 4.5 5.0 5.5

Supply Voltage (V) Figure 25.

,

(2)

(3)

(4)

APPLICATION INFORMATION

BRIDGE CONFIGURATION EXPLANATION

As shown in Figure 1, the LM4819 consists of two operational amplifiers. External resistors, R_i and R_F set the closed-loop gain of the first amplifier (and the amplifier overall), whereas two internal $20k\Omega$ resistors set the second amplifier's gain at -1. The LM4819 is typically used to drive a speaker connected between the two amplifier outputs.

Figure 1 shows that the output of Amp1 servers as the input to Amp2, which results in both amplifiers producing signals identical in magnitude but 180° out of phase. Taking advantage of this phase difference, a load is placed between V_{01} and V_{02} and driven differentially (commonly referred to as "bridge mode"). This results in a differential gain of

 $A_{VD} = 2 * (R_f/R_i)$

Bridge mode is different from single-ended amplifiers that drive loads connected between a single amplifier's output and ground. For a given supply voltage, bridge mode has a distinct advantage over the single-ended configuration: its differential output doubles the voltage swing across the load. This results in four times the output power when compared to a single-ended amplifier under the same conditions. This increase in attainable output assumes that the amplifier is not current limited or the output signal is not clipped. To ensure minimum output signal clipping when choosing an amplifier's closed-loop gain, refer to the Audio Power Amplifier Design Example section.

Another advantage of the differential bridge output is no net DC voltage across the load. This results from biasing V_{01} and V_{02} at half-supply. This eliminates the coupling capacitor that single supply, single-ended amplifiers require. Eliminating an output coupling capacitor in a single-ended configuration forces a single supply amplifier's half-supply bias voltage across the load. The current flow created by the half-supply bias voltage increases internal IC power dissipation and may permanently damage loads such as speakers.

POWER DISSIPATION

Power dissipation is a major concern when designing a successful bridged or single-ended amplifier. Equation 2 states the maximum power dissipation point for a single-ended amplifier operating at a given supply voltage and driving a specified load.

$$P_{DMAX} = (V_{DD})^2 / (2\pi^2 R_L)$$
 (W) Single-ended

However, a direct consequence of the increased power delivered to the load by a bridged amplifier is an increase in the internal power dissipation point for a bridge amplifier operating at the same given conditions. Equation 3 states the maximum power dissipation point for a bridged amplifier operating at a given supply voltage and driving a specified load.

 $P_{DMAX} = 4(V_{DD})^2/(2\pi^2 R_L)$ (W) Bridge Mode

The LM4819 has two operational amplifiers in one package and the maximum internal power dissipation is four times that of a single-ended amplifier. However, even with this substantial increase in power dissipation, the Lm4819 does not require heatsinking. From Equation 3, assuming a 5V power supply and an 8Ω load, the maximum power dissipation point is 633mW. The maximum power dissipation point obtained from Equation 3 must not exceed the power dissipation predicted by Equation 4:

$$P_{DMAX} = (T_{JMAX} - T_A)/\theta_{JA} (W)$$

For the micro DGK0008A package, $\theta_{JA} = 210^{\circ}$ C/W, for the D0008A package, $\theta_{JA} = 170^{\circ}$ C/W, and $T_{JMAX} = 150^{\circ}$ C for the LM4819. For a given ambient temperature, T_A , Equation 4 can be used to find the maximum internal power dissipation supported by the IC packaging. If the result of Equation 3 is greater than the result of Equation 4, then decrease the supply voltage, increase the load impedance, or reduce the ambient temperature. For a typical application using the D0008A packaged LM4819 with a 5V power supply and an 8 Ω load, the maximum ambient temperature that does not violate the maximum junction temperature is approximately 42°C. If a DGK0008A packaged part is used instead with the same supply voltage and load, the maximum ambient temperature is 17°C. In both cases, it is assumed that a device is a surface mount part operating around the maximum power dissipation point. The assumption that the device is operating around the maximum power dissipation point is incorrect for an 8 Ω load. The maximum power dissipation point occurs when the output power is equal to the maximum power dissipation or 50% efficiency. The LM4819 is not capable of the output power level (633mW) required to operate at the maximum power dissipation point for an 8 Ω load. To find the maximum power dissipation, the graph Figure 22 must be used. From the graph, the maximum power dissipation for an 8 Ω



(1)



load and a 5V supply is approximately 575mW. Substituting this value back into Equation 4 for P_{DMAX} and using $\theta_{JA} = 210^{\circ}$ C/W for the DGK0008A package, the maximum ambient temperature is calculated to be 29°C. Using $\theta_{JA} = 170^{\circ}$ C/W for the D0008A package, the maximum ambient temperature is 52°C. Refer to the Typical Performance Characteristics curves for power dissipation information for lower output powers and maximum power dissipation for each package at a given ambient temperature.

POWER SUPPLY BYPASSING

As with any power amplifier, proper supply bypassing is critical for low noise performance and high power supply rejection. The capacitors connected to the bypass and power supply pins should be placed as close to the LM4819 as possible. The capacitor connected between the bypass pin and ground improves the internal bias voltage's stability, producing improved PSRR. The improvements to PSRR increase as the bypass pin capacitor value increases. Typical applications employ a 5V regulator with 10μ F and 0.1μ F filter capacitors that aid in supply stability. Their presence, however, does not eliminate the need for bypassing the supply nodes of the LM4819. The selection of bypass capacitor values, especially C_B, depends on desired PSRR requirements, click and pop performance as explained in the section, Proper Selection of External Components, as well as system cost and size constraints.

SHUTDOWN FUNCTION

The voltage applied to the LM4819's SHUTDOWN pin controls the shutdown function. Activate micro-power shutdown by applying V_{DD} to the SHUTDOWN pin. When active, the LM4819's micro-power shutdown feature turns off the amplifier's bias circuitry, reducing the supply current. The logic threshold is typically $1/2V_{DD}$. The low 0.7µA typical shutdown current is achieved by applying a voltage that is as near as V_{DD} as possible to the SHUTDOWN pin. A voltage that is less than V_{DD} may increase the shutdown current. Avoid intermittent or unexpected micro-power shutdown by ensuring that the SHUTDOWN pin is not left floating but connected to either V_{DD} or GND.

There are a few ways to activate micro-power shutdown. These included using a single-pole, single-throw switch, a microcontroller, or a microprocessor. When using a switch, connect an external $10k\Omega$ to $100k\Omega$ pull-up resistor between the SHUTDOWN pin and V_{DD}. Connect the switch between the SHUTDOWN pin and ground. Select normal amplifier operation by closing the switch. Opening the switch connects the shutdown pin to V_{DD} through the pull-up resistor, activating micro-power shutdown. The switch and resistor ensure that the SHUTDOWN pin will not float. This prevents unwanted state changes. In a system with a microprocessor or a microcontroller, use a digital output to apply the control voltage to the SHUTDOWN pin. Driving the SHUTDOWN pin with active circuitry eliminates the pull-up resistor

PROPER SELECTION OF EXTERNAL COMPONENTS

Optimizing the LM4819's performance requires properly selecting external components. Though the LM4819 operates well when using external components with wide tolerances, best performance is achieved by optimizing component values.

The LM4819 is unity gain stable, giving the designer maximum design flexibility. The gain should be set to no more than a given application requires. This allows the amplifier to achieve minimum THD+N and maximum signal-to-noise ratio. These parameters are compromised as the closed-loop gain increases. However, low gain demands input signals with greater voltage swings to achieve maximum output power. Fortunately, many signal sources such as audio CODECs have outputs of $1V_{RMS}$ (2.83V_{P-P}). Please refer to the Audio Power Amplifier Design section for more information on selecting the proper gain.

Another important consideration is the amplifier's close-loop bandwidth. To a large extent, the bandwidth is dictated by the choice of external components shown in Figure 1. The input coupling capacitor, C_i, forms a first order high pass filter that limits low frequency response. This value should be chosen based on needed frequency response for a few distinct reasons discussed below

Input Capacitor Value Selection

Amplifying the lowest audio frequencies requires a high value input coupling capacitor (C_i in Figure 1). A high value capacitor can be expensive and may compromise space efficiency in portable designs. In many cases the speakers used in portable systems, whether internal or external, have little ability to reproduce signals below 150Hz. Applications using speakers with limited frequency response reap little improvement by using a large input capacitor.

Copyright © 2001–2013, Texas Instruments Incorporated

Besides affecting system cost and size, C_i has an effect on the LM4819's click and pop performance. When the supply voltage is first applied, a transient (pop) is created as the charge on the input capacitor changes from zero to a quiescent state. The magnitude of the pop is directly proportional to the input capacitor's value. Higher value capacitors need more time to reach a quiescent DC voltage (usually 1/2 V_{DD}) when charged with a fixed current. The amplifier's output charges the input capacitor through the feedback resistor, R_F. Thus, selecting an input capacitor value that is no higher than necessary to meet the desired -3dB frequency can minimize pops.

As shown in Figure 1, the input resistor (R_i) and the input capacitor, C_i produce a -3dB high pass filter cutoff frequency that is found using Equation 5.

 $f_{-3dB} = 1/(2 \pi R_i C_i) (Hz)$

As an example when using a speaker with a low frequency limit of 150Hz, C_i, using Equation 5 is 0.063µF. The 0.39µF C_i shown in Figure 1 allows the LM4819 to drive a high efficiency, full range speaker whose response extends down to 20Hz.

Besides optimizing the input capacitor value, the bypass capacitor value, C_B requires careful consideration. The bypass capacitor's value is the most critical to minimizing turn-on pops because it determines how fast the LM4819 turns on. The slower the LM4819's outputs ramp to their quiescent DC voltage (nominally $1/2V_{DD}$), the smaller the turn-on pop. While the device will function properly (no oscillations or motorboating), with CB less than 1.0 μ F, the device will be much more susceptible to turn-on clicks and pops. Thus, a value of C_B equal to or greater than 1.0µF is recommended in all but the most cost sensitive designs.

Bypass Capacitor Value Selection

Besides minimizing the input capacitor size, careful consideration should be paid to the value of C_B, the capacitor connected to the BYPASS pin. Since C_B determines how fast the LM4819 settles to quiescent operation, its value is critical when minimizing turn-on pops. The slower the LM4819's outputs ramp to their quiescent DC voltage (nominally $1/2V_{DD}$), the smaller the turn-on pop. Choosing C_B equal to 1.0μ F along with a small value of C_i (in the range of 0.1µF to 0.39µF) produces a click-less and pop-less shutdown function. As discussed above, choosing C_i no larger than necessary for the desired bandwidth helps minimize clicks and pops.

Optimizing Click and Pop Reduction Performance

The LM4819 contains circuitry that minimizes turn-on and shutdown transients or "clicks and pops". For this discussion, turn on refers to either applying the power or supply voltage or when the shutdown mode is deactivated. While the power supply is ramping to it's final value, the LM4819's internal amplifiers are configured as unity gain buffers. An internal current source charges the voltage of the bypass capacitor, C_B, connected to the BYPASS pin in a controlled, linear manner. Ideally, the input and outputs track the voltage charging on the bypass capacitor. The gain of the internal amplifiers remains unity until the bypass capacitor is fully charged to $1/2V_{DD}$. As soon as the voltage on the bypass capacitor is stable, the device becomes fully operational. Although the BYPASS pin current cannot be modified, changing the size of the bypass capacitor, C_B, alters the device's turn-on time and magnitude of "clicks and pops". Increasing the value of C_B reduces the magnitude of turn-on pops. However, this presents a tradeoff: as the size of C_B increases, the turn-on time (Ton) increases. There is a linear relationship between the size of C_B and the turn on time. Below are some typical turn-on times for various values of C_B:

C _B	T _{ON}
0.01µF	20ms
0.1µF	200ms
0.22µF	440ms
0.47µF	940ms
1.0µF	2S



www.ti.com

(5)



www.ti.com

In order to eliminate "clicks and pops", all capacitors must be discharged before turn-on. Rapidly switching V_{DD} may not allow the capacitors to fully discharge, which may cause "clicks and pops".

AUDIO POWER AMPLIFIER DESIGN EXAMPLE

The following are the desired operational parameters:

Given:	
Power Output	100mW
Load Impedance	16Ω
Input Level	1Vrms (max)
Input Impedance	20kΩ
Bandwidth	100Hz–20kHz ± 0.25dB

The design begins by specifying the minimum supply voltage necessary to obtain the specified output power. To find this minimum supply voltage, use the Output Power vs. Supply Voltage graph in the Typical Performance Characteristics section. From the graph for a 16 Ω load, (graphs are for 8 Ω , 16 Ω , and 32 Ω loads) the supply voltage for 100mW of output power with 1% THD+N is approximately 3.15 volts.

Additional supply voltage creates the benefit of increased headroom that allows the LM4819 to reproduce peaks in excess of 100mW without output signal clipping or audible distortion. The choice of supply voltage must also not create a situation that violates maximum dissipation as explained above in the Power Dissipation section. For example, if a 3.3V supply is chosen for extra headroom then according to Equation 3 the maximum power dissipation point with a 16 Ω load is 138mW. Using Equation 4 the maximum ambient temperature is 121°C for the DGK0008A package and 126°C for the D0008A package.

After satisfying the LM4819's power dissipation requirements, the minimum differential gain is found using Equation 6.

$$A_{VD} \ge \sqrt{(P_0 R_L)} / (V_{IN}) = V_{orms} / V_{inrms}$$

Thus a minimum gain of 1.27 V/V allows the LM4819 to reach full output swing and maintain low noise and THD+N performance. For this example, let A_{VD} = 1.27. The amplifier's overall gain is set using the input (R_i) and feedback (R_F) resistors. With the desired input impedance set to 20k Ω , the feedback resistor is found using Equation 7.

$$R_F/R_i = A_{VD}/2 (V/V)$$

The value of R_F is 13k Ω .

The last step in this design example is setting the amplifier's -3dB frequency bandwidth. To achieve the desired ± 0.25 dB pass band magnitude variation limit, the low frequency response must extend to at least one-fifth the lower bandwidth limit and the high frequency response must extend to at least five times the upper bandwidth limit. The gain variation for both response limits is 0.17dB, well with in the ± 0.25 dB desired limit.

The results are:

 $f_L = 100Hz/5 = 20Hz$ $f_H = 20 \text{ kHz}*5 = 100\text{ kHz}$

As mentioned in the External Components section, R_i and C_i create a high pass filter that sets the amplifier's lower band pass frequency limit. Find the coupling capacitor's value using Equation 8.

 $C_i \ge 1/(2\pi R_i f_c) (F)$

(8)

(6)

(7)

 $C_i \ge 0.398\mu$ F, a standard value of 0.39μ F will be used. The product of the desired high frequency cutoff (100kHz in this example) and the differential gain, A_{VD} , determines the upper pass band response limit. With $A_{VD} = 1.27$ and $f_H = 100$ kHz, the closed-loop gain bandwidth product (GBWP) is 127kHz. This is less than the LM4819's 900kHz GBWP. With this margin the amplifier can be used in designs that require more differential gain while avoiding performance restricting bandwidth limitations.

Copyright © 2001–2013, Texas Instruments Incorporated

www.ti.com

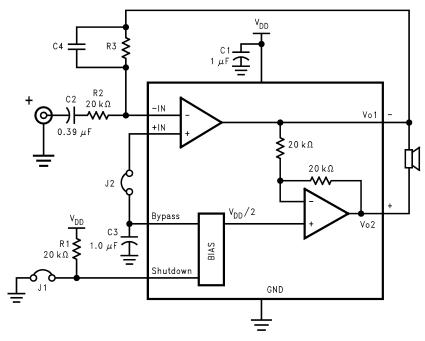


Figure 26. Higher Gain Audio Amplifier

The LM4819 is unity-gain stable and requires no external components besides gain-setting resistors, an input coupling capacitor, and proper supply bypassing in the typical application. However, if a closed-loop differential gain of greater than 10 is required, a feedback capacitor (C_4) may be needed as shown in Figure 26 to bandwidth limit the amplifier. This feedback capacitor creates a low pass filter that eliminates possible high frequency oscillations. Care should be taken when calculating the -3dB frequency in that an incorrect combination of R_3 and C_4 will cause rolloff before 20kHz. A typical combination of feedback resistor and capacitor that will not produce audio band high frequency rolloff is $R_3 = 20k\Omega$ and $C_4 = 25pF$. These components result in a -3dB point of approximately 320 kHz. It is not recommended that the feedback resistor and capacitor be used to implement a band limiting filter below 100kHz.

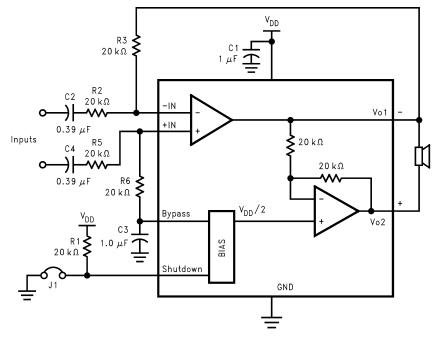
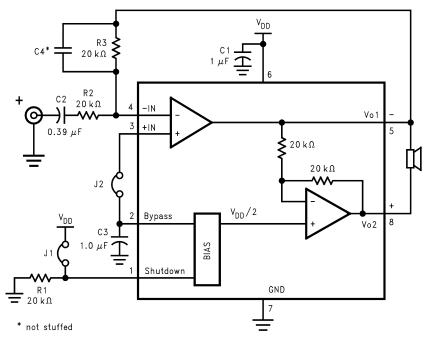


Figure 27. Differential Amplifier Configuration for LM4819



www.ti.com





LM4819 SOIC DEMO BOARD ARTWORK

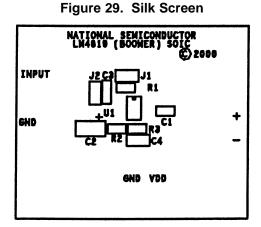
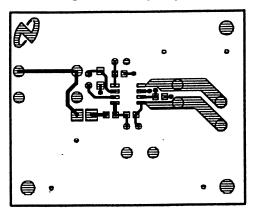


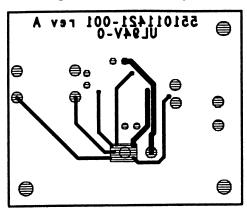
Figure 30. Top Layer





www.ti.com





LM4819 VSSOP DEMO BOARD ARTWORK

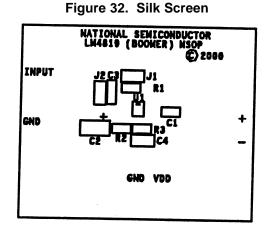
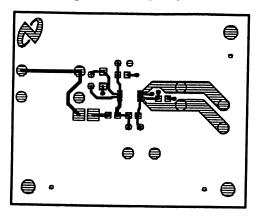


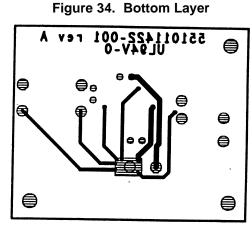
Figure 33. Top Layer







www.ti.com



LM4819 WSON DEMO BOARD ARTWORK

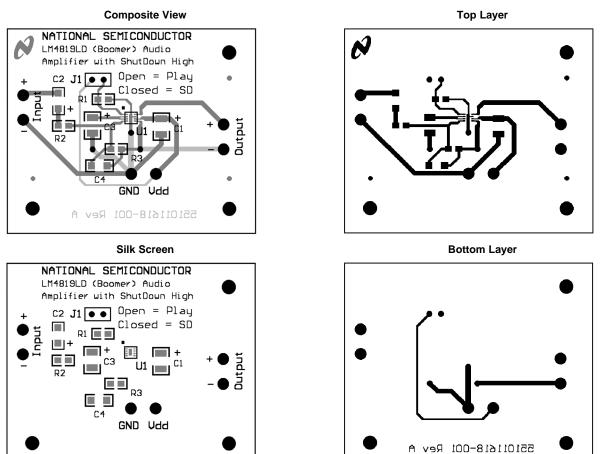


Table 1. Mono LM4819 Reference Design BoardsBill of Material for all Demo Boards

Item	Part Number	Part Description	Qty	Ref Designator
1	551011208-001	LM4819 Mono Reference Design Board	1	
10	482911183-001	LM4819 Audio AMP	1	U1
20	151911207-001	Tant Cap 1uF 16V 10	1	C1

Copyright © 2001–2013, Texas Instruments Incorporated

TEXAS INSTRUMENTS

www.ti.com

Table 1. Mono LM4819 Reference Design Boards Bill of Material for all Demo Boards (continued)

Item	Part Number	Part Description	Qty	Ref Designator
21	151911207-002	Cer Cap 0.39uF 50V Z5U 20% 1210	1	C2
25	152911207-001	Tant Cap 1uF 16V 10	1	C3
30	472911207-001	Res 20K Ohm 1/10W 5	3	R1, R2, R3
35	210007039-002	Jumper Header Vertical Mount 2X1 0.100	2	J1, J2

PCB LAYOUT GUIDELINES

This section provides practical guidelines for mixed signal PCB layout that involves various digital/analog power and ground traces. Designers should note that these are only "rule-of-thumb" recommendations and the actual results will depend heavily on the final layout.

General Mixed Signal Layout Recommendation

Power and Ground Circuits

For two layer mixed signal design, it is important to isolate the digital power and ground trace paths from the analog power and ground trace paths. Star trace routing techniques (bringing individual traces back to a central point rather than daisy chaining traces together in a serial manner) can have a major impact on low level signal performance. Star trace routing refers to using individual traces to feed power and ground to each circuit or even device. This technique will take require a greater amount of design time but will not increase the final price of the board. The only extra parts required will be some jumpers.

Single-Point Power / Ground Connections

The analog power traces should be connected to the digital traces through a single point (link). A "Pi-filter" can be helpful in minimizing high frequency noise coupling between the analog and digital sections. It is further recommended to put digital and analog power traces over the corresponding digital and analog ground traces to minimize noise coupling.

Placement of Digital and Analog Components

All digital components and high-speed digital signals traces should be located as far away as possible from analog components and circuit traces.

Avoiding Typical Design / Layout Problems

Avoid ground loops or running digital and analog traces parallel to each other (side-by-side) on the same PCB layer. When traces must cross over each other do it at 90 degrees. Running digital and analog traces at 90 degrees to each other from the top to the bottom side as much as possible will minimize capacitive noise coupling and cross talk.

Copyright © 2001–2013, Texas Instruments Incorporated

REVISION HISTORY

C	hanges from Revision C (March 2013) to Revision D	Page
•	Changed layout of National Data Sheet to TI format	18

Texas
INSTRUMENTS

www.ti.com

anges from Revision C (March 2013) to Revision D	Pa
Changed layout of National Data Sheet to TI format	



PACKAGING INFORMATION

Orderable part number	Status	Material type	Package Pins	Package qty Carrier	RoHS	Lead finish/	MSL rating/	Op temp (°C)	Part marking
	(1)	(2)			(3)	Ball material	Peak reflow		(6)
						(4)	(5)		
LM4819LD/NOPB	Active	Production	WSON (NGL) 8	1000 LARGE T&R	Yes	SN	Level-3-260C-168 HR	-40 to 85	G19
LM4819LD/NOPB.A	Active	Production	WSON (NGL) 8	1000 LARGE T&R	Yes	SN	Level-3-260C-168 HR	-40 to 85	G19
LM4819MM/NOPB	Active	Production	VSSOP (DGK) 8	1000 SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	G19
LM4819MM/NOPB.A	Active	Production	VSSOP (DGK) 8	1000 SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	G19
LM4819MMX/NOPB	Active	Production	VSSOP (DGK) 8	3500 LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	G19
LM4819MMX/NOPB.A	Active	Production	VSSOP (DGK) 8	3500 LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	G19
LM4819MX/NOPB	Active	Production	SOIC (D) 8	2500 LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	LM48
									19M
LM4819MX/NOPB.A	Active	Production	SOIC (D) 8	2500 LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	LM48
									19M

⁽¹⁾ **Status:** For more details on status, see our product life cycle.

⁽²⁾ Material type: When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

⁽³⁾ RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

⁽⁴⁾ Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

⁽⁵⁾ MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

⁽⁶⁾ Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

Important Information and Disclaimer: The information provided on this page represents TI's knowledge and belief as of the date that it is provided. TI bases its knowledge and belief on information provided by third parties, and makes no representation or warranty as to the accuracy of such information. Efforts are underway to better integrate information from third parties. TI has taken and continues to take reasonable steps to provide representative



www.ti.com

PACKAGE OPTION ADDENDUM

23-May-2025

and accurate information but may not have conducted destructive testing or chemical analysis on incoming materials and chemicals. TI and TI suppliers consider certain information to be proprietary, and thus CAS numbers and other limited information may not be available for release.

In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.



Texas

STRUMENTS

TAPE AND REEL INFORMATION





QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal	h							D		r.		t.
Device	-	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LM4819LD/NOPB	WSON	NGL	8	1000	178.0	12.4	2.8	2.8	1.0	8.0	12.0	Q1
LM4819MM/NOPB	VSSOP	DGK	8	1000	178.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
LM4819MMX/NOPB	VSSOP	DGK	8	3500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
LM4819MX/NOPB	SOIC	D	8	2500	330.0	12.4	6.5	5.4	2.0	8.0	12.0	Q1



www.ti.com

PACKAGE MATERIALS INFORMATION

9-Aug-2022

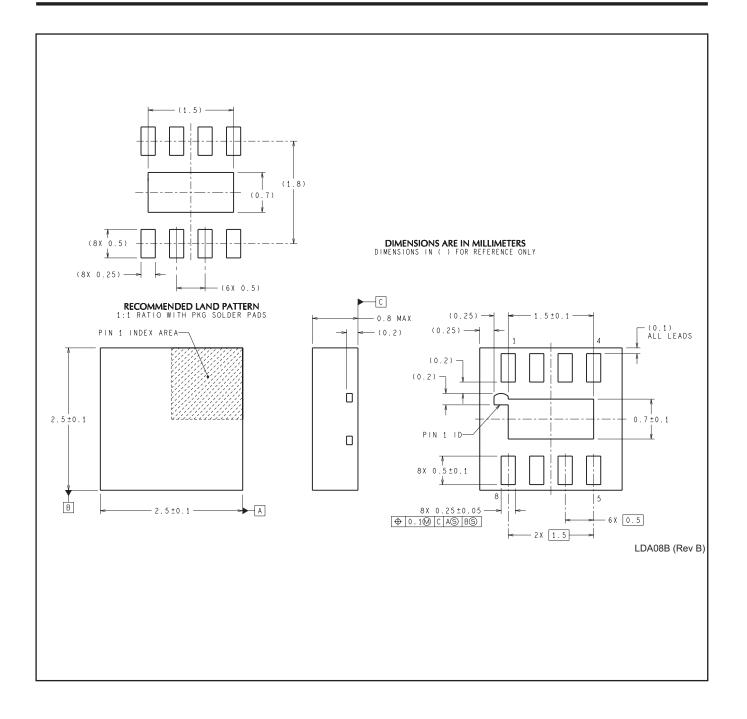


*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LM4819LD/NOPB	WSON	NGL	8	1000	208.0	191.0	35.0
LM4819MM/NOPB	VSSOP	DGK	8	1000	208.0	191.0	35.0
LM4819MMX/NOPB	VSSOP	DGK	8	3500	367.0	367.0	35.0
LM4819MX/NOPB	SOIC	D	8	2500	367.0	367.0	35.0

MECHANICAL DATA

NGL0008B





D0008A



PACKAGE OUTLINE

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



NOTES:

1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.

- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.



D0008A

EXAMPLE BOARD LAYOUT

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



D0008A

EXAMPLE STENCIL DESIGN

SOIC - 1.75 mm max height

SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

9. Board assembly site may have different recommendations for stencil design.



DGK0008A



PACKAGE OUTLINE

VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



NOTES:

PowerPAD is a trademark of Texas Instruments.

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M. 2. This drawing is subject to change without notice. 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not
- exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- 5. Reference JEDEC registration MO-187.



DGK0008A

EXAMPLE BOARD LAYOUT

[™] VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown

on this view. It is recommended that vias under paste be filled, plugged or tented.

9. Size of metal pad may vary due to creepage requirement.



DGK0008A

EXAMPLE STENCIL DESIGN

[™] VSSOP - 1.1 mm max height

SMALL OUTLINE PACKAGE



11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

12. Board assembly site may have different recommendations for stencil design.



IMPORTANT NOTICE AND DISCLAIMER

TI PROVIDES TECHNICAL AND RELIABILITY DATA (INCLUDING DATA SHEETS), DESIGN RESOURCES (INCLUDING REFERENCE DESIGNS), APPLICATION OR OTHER DESIGN ADVICE, WEB TOOLS, SAFETY INFORMATION, AND OTHER RESOURCES "AS IS" AND WITH ALL FAULTS, AND DISCLAIMS ALL WARRANTIES, EXPRESS AND IMPLIED, INCLUDING WITHOUT LIMITATION ANY IMPLIED WARRANTIES OF MERCHANTABILITY, FITNESS FOR A PARTICULAR PURPOSE OR NON-INFRINGEMENT OF THIRD PARTY INTELLECTUAL PROPERTY RIGHTS.

These resources are intended for skilled developers designing with TI products. You are solely responsible for (1) selecting the appropriate TI products for your application, (2) designing, validating and testing your application, and (3) ensuring your application meets applicable standards, and any other safety, security, regulatory or other requirements.

These resources are subject to change without notice. TI grants you permission to use these resources only for development of an application that uses the TI products described in the resource. Other reproduction and display of these resources is prohibited. No license is granted to any other TI intellectual property right or to any third party intellectual property right. TI disclaims responsibility for, and you will fully indemnify TI and its representatives against, any claims, damages, costs, losses, and liabilities arising out of your use of these resources.

TI's products are provided subject to TI's Terms of Sale or other applicable terms available either on ti.com or provided in conjunction with such TI products. TI's provision of these resources does not expand or otherwise alter TI's applicable warranties or warranty disclaimers for TI products.

TI objects to and rejects any additional or different terms you may have proposed.

Mailing Address: Texas Instruments, Post Office Box 655303, Dallas, Texas 75265 Copyright © 2025, Texas Instruments Incorporated