



SBAS040B - DECEMBER 1995 - REVISED FEBRUARY 2005

# 10-Bit, 40MHz Sampling **ANALOG-TO-DIGITAL CONVERTER**

### **FEATURES**

NO MISSING CODES

INTERNAL REFERENCE

LOW POWER: 380mW

HIGH SNR: 58dB

INTERNAL TRACK-AND-HOLD

### APPLICATIONS

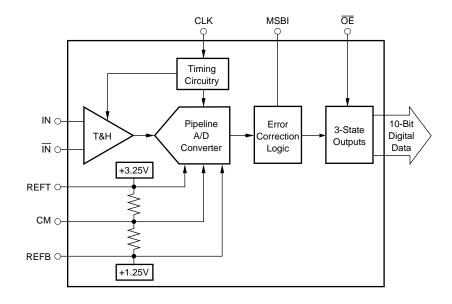
- VIDEO DIGITIZING
- ULTRASOUND IMAGING
- GAMMA CAMERAS
- SET-TOP BOXES
- CABLE MODEMS
- CCD IMAGING **Color Copiers Scanners** Camcorders **Security Cameras Fax Machines**
- IF AND BASEBAND DIGITIZATION
- TEST INSTRUMENTATION

### DESCRIPTION

The ADS821 is a low-power, monolithic 10-bit, 40MHz Analog-to-Digital (A/D) converter utilizing a small geometry CMOS process. This complete converter includes a 10-bit quantizer with internal track-and-hold, reference, and a power-down feature. It operates from a single +5V power supply and can be configured to accept either differential or single-ended input signals.

The ADS821 employs digital error correction to provide excellent Nyquist differential linearity performance for demanding imaging applications. Its low distortion, high SNR, and high oversampling capability give it the extra margin needed for telecommunications and video applications.

This high-performance converter is specified for AC and DCperformance at a 40MHz sampling rate. The ADS821 is available in an SO-28 package.





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#### **ABSOLUTE MAXIMUM RATINGS(1)**

+V <sub>S</sub> +6V
Analog Input 0V to (+V <sub>S</sub> + 300mV)
Logic Input
Case Temperature+100°C
Junction Temperature+150°C
Storage Temperature+125°C
External Top Reference Voltage (REFT)+3.4V max
External Bottom Reference Voltage (REFB)+1.1V min

NOTES: (1) Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability.

# ELECTROSTATIC DISCHARGE SENSITIVITY

This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

#### PACKAGE/ORDERING INFORMATION(1)

PRODUCT	PACKAGE-LEAD	PACKAGE DESIGNATOR	SPECIFIED TEMPERATURE RANGE	PACKAGE MARKING	ORDERING NUMBER	TRANSPORT MEDIA, QUANTITY
ADS821	SO-8	DW	-40°C to +85°C	ADS821U	ADS821U	Rails, 28
"	"	II .	"	"	ADS821U/1K	Tape and Reel, 1000

NOTE: (1) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at www.ti.com.

### **ELECTRICAL CHARACTERISTICS**

At T<sub>A</sub> = +25°C, V<sub>S</sub> = +5V, Sampling Rate = 40MHz, and with a 50% duty cycle clock having a 2ns rise-and-fall time, unless otherwise noted.

				ADS821U		
PARAMETER	CONDITIONS	TEMP	MIN	TYP	MAX	UNITS
RESOLUTION					10	Bits
Specified Temperature Range	T <sub>AMBIENT</sub>		-40		+85	°C
ANALOG INPUT						
Differential Full-Scale Input Range			+1.25		+3.25	V
Common-Mode Voltage					+2.25	V
Analog Input Bandwidth (–3dB)	00 (050)	0.500		400		
Small-Signal Full-Power	-20dBFS <sup>(1)</sup> Input	+25°C		400		MHz MHz
	0dBFS Input	+25°C		65		
Input Impedance				1.25    4		MΩ    pF
DIGITAL INPUT						
Logic Family			'''	HCT Compatible	CMOS	
Convert Command	Start Conversion			Falling Edge	т	_
ACCURACY <sup>(2)</sup>						
Gain Error		+25°C		±0.6	±1.5	%
		Full		±1.1	±2.5	%
Gain Drift		0500		±85	0.45	ppm/°C
Power-Supply Rejection of Gain	$\Delta$ +V <sub>S</sub> = ±5%	+25°C Full		0.01 +2.1	0.15	%FSR/% %
Input Offset Error Power-Supply Rejection of Offset	$\Delta + V_S = \pm 5\%$	+25°C		0.02	±3.5 0.15	% %FSR/%
****	$\Delta + V_S = \pm 3\%$	+25 C		0.02	0.15	70F3R/70
CONVERSION CHARACTERISTICS			4.01		4014	
Sample Rate			10k	0.5	40M	Sample/s
Data Latency				6.5		Convert Cycle
DYNAMIC CHARACTERISTICS						
Differential Linearity Error	$t_{H} = 13ns^{(3)}$					
f = 500kHz		+25°C		±0.5	±1.0	LSB
f = 12MHz		0°C to +70°C +25°C		±0.6 ±0.5	±1.0 +1.0	LSB LSB
T = 12IVIHZ		+25°C 0°C to +70°C		±0.5 ±0.6	±1.0 ±1.0	LSB
No Missing Codes		0°C to +70°C		±0.6 Tested	±1.0	LOD
Integral Linearity Error at f = 500kHz		0°C to +70°C		±0.5	+2.0	LSB
Spurious-Free Dynamic Range (SFDR)						
f = 500kHz (-1dBFS input)		+25°C	60	70		dBFS
, 1 - A		Full	54	67		dBFS
f = 12MHz (-1dBFS input)		+25°C	58	63		dBFS
		Full	54	62		dBFS

NOTES: (1) dBFS refers to dB below Full-Scale. (2) Percentage accuracies are referred to the internal A/D converter Full-Scale Range of 4Vp-p. (3) Refer to Timing Diagram footnotes for the differential linearity performance conditions for the SO and SSOP packages. (4) IMD is referred to the larger of the two input signals. If referred to the peak envelope signal ( $\approx$  0dB), the intermodulation products will be 7dB lower. (5) Based on (SINAD - 1.76)/6.02. (6) No "rollover" of bits.



# **ELECTRICAL CHARACTERISTICS (Cont.)**

At  $T_A = +25^{\circ}C$ ,  $V_S = +5V$ , Sampling Rate = 40MHz, and with a 50% duty cycle clock having a 2ns rise-and-fall time, unless otherwise noted.

PARAMETER	CONDITIONS	TEMP	MIN	TYP	MAX	UNITS
DYNAMIC CHARACTERISTICS (Cont.)						
2-Tone Intermodulation Distortion (IMD)(4)						
f = 4.4MHz and 4.5MHz (-7dBFS each tone)		+25°C		-61		dBc
		Full		-60		dBc
Signal-to-Noise Ratio (SNR)						
f = 500kHz (-1dBFS input)		+25°C	57	59		dB
		Full	55	59		dB
f = 12MHz (-1dBFS input)		+25°C	56	58		dB
		Full	54	58		dB
Signal-to-(Noise + Distortion) (SINAD)						
f = 500kHz (-1dBFS input)		+25°C	56	58.5		dB
		Full	52	58		dB
f = 12MHz (-1dBFS input)		+25°C	53	57		dB
		Full	50	56		dB
Differential Gain Error	NTSC or PAL	+25°C		0.5		%
Differential Phase Error		NTSC or PAL	+25°C		0.1	
Degrees						
Effective Bits <sup>(5)</sup>	$f_{IN} = 3.58MHz$	+25°C		9.3		Bits
Aperture Delay Time		+25°C	0=:0	2	_	ns
Aperture Jitter			+25°C		7	
ps rms	4 Ev. Evill Cools Issued	+25°C				
Over-Voltage Recovery Time <sup>(6)</sup>	1.5x Full-Scale Input	+25°C		2		ns
OUTPUTS						
Logic Family			TTL	HCT Compatible	CMOS	
Logic Coding	Logic Selectable			SOB or BTC		
Logic Levels	Logic LOW,	Full	0		0.4	V
	$C_L = 15pF max$					
	Logic HIGH,	Full	+2.5		+V <sub>S</sub>	V
	$C_L = 15pF max$					
3-State Enable Time				20	40	ns
3-State Disable Time		Full		2	10	ns
POWER-SUPPLY REQUIREMENTS						
Supply Voltage: +V <sub>S</sub>	Operating	Full	+4.75	+5	+5.25	V
Supply Current: +I <sub>S</sub>	Operating	+25°C		76	88	mA
-	Operating	Full		78	90	mA
Power Consumption	Operating	+25°C		380	440	mW
	Operating	Full		390	450	mW
Thermal Resistance, $\theta_{JA}$					75	°C/W

NOTES: (1) dBFS refers to dB below Full Scale. (2) Percentage accuracies are referred to the internal A/D converter Full-Scale Range of 4Vp-p. (3) Refer to Timing Diagram footnotes for the differential linearity performance conditions for the SO and SSOP packages. (4) IMD is referred to the larger of the two input signals. If referred to the peak envelope signal ( $\approx$  0dB), the intermodulation products will be 7dB lower. (5) Based on (SINAD - 1.76)/6.02. (6) No "rollover" of bits.

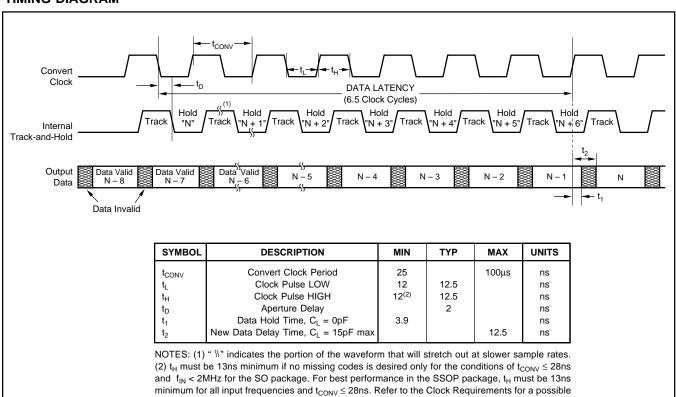
#### **PIN CONFIGURATION**

#### so **Top View** 0 GND 28 GND Bit 1 (MSB) 27 $\overline{\mathsf{IN}}$ 2 Bit 2 26 IN 3 Bit 3 4 25 **GND** 5 24 Bit 4 $+V_S$ 6 23 REFT Bit 5 7 22 Bit 6 CM ADS821 Bit 7 8 21 **REFB** Bit 8 9 20 +V<sub>S</sub> 10 19 Bit 9 MSBI ŌĒ Bit 10 (LSB) 11 18 DNC 12 17 $+V_S$ DNC 16 CLK GND 15 +V<sub>S</sub> DNC: Do Not Connect

#### **PIN DESCRIPTIONS**

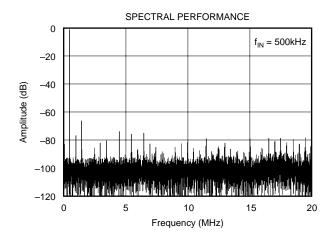
	DEGIGNATOR	DECORIDEION
PIN	DESIGNATOR	DESCRIPTION
1	GND	Ground
2	B1	Bit 1, Most Significant Bit (MSB)
3	B2	Bit 2
4	B3	Bit 3
5	B4	Bit 4
6	B5	Bit 5
7	B6	Bit 6
8	B7	Bit 7
9	B8	Bit 8
10	B9	Bit 9
11	B10	Bit 10, Least Significant Bit (LSB)
12	DNC	Do Not Connect
13	DNC	Do Not Connect
14	GND	Ground
15	+V <sub>S</sub>	+5V Power Supply
16	CLK	Convert Clock Input, 50% Duty Cycle
17	+V <sub>S</sub>	+5V Power Supply
18	ŌĒ	HIGH: High-Impedance State. LOW or Floating:
		Normal Operation. Internal pull-down resistor.
19	MSBI	Most Significant Bit Inversion, HIGH: MSB in-
		verted for complementary output. LOW or Float-
		ing: Straight output. Internal pull-down resistor.
20	+V <sub>S</sub>	+5V Power Supply
21	REFB	Bottom Reference Bypass. For external bypass-
		ing of internal +1.25V reference.
22	CM	Common-Mode Voltage. It is derived by (REFT +
		REFB)/2.
23	REFT	Top Reference Bypass. For external bypassing
		of internal +3.25V reference.
24	+V <sub>S</sub>	+5V Power Supply
25	GND	Ground
26	<u>IN</u>	Input
27	ΙΝ	Complementary Input
28	GND	Ground

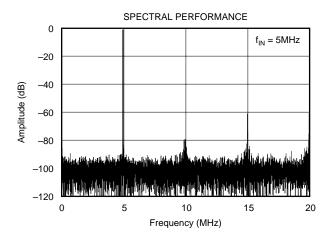
#### **TIMING DIAGRAM**

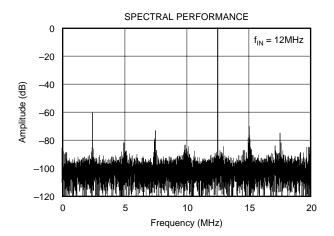


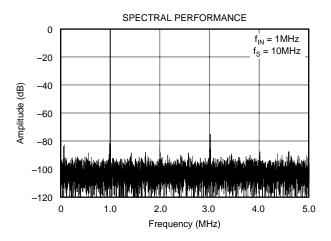
clock skew circuit for this condition.

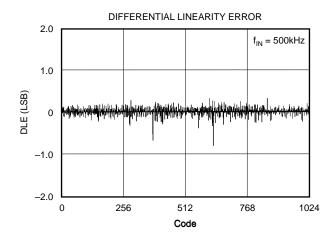
# TYPICAL CHARACTERISTICS

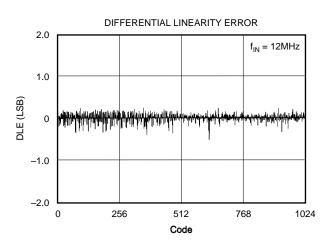








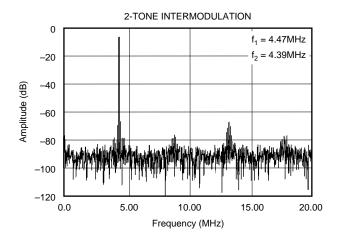


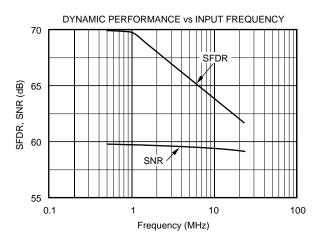


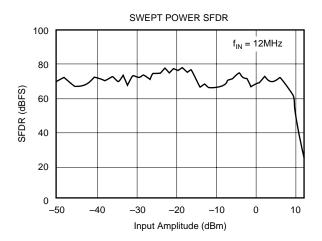


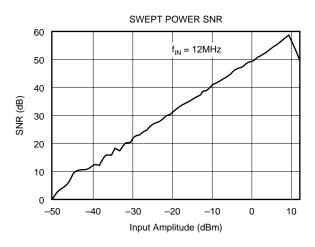


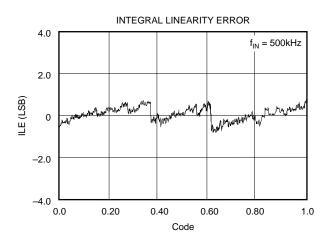
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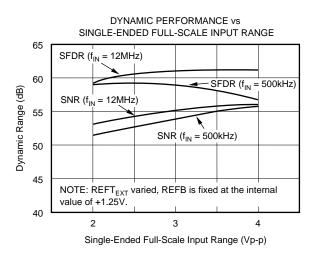






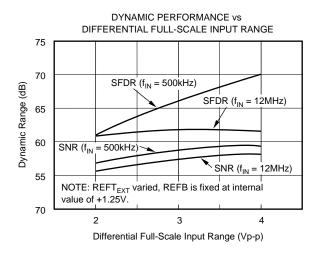


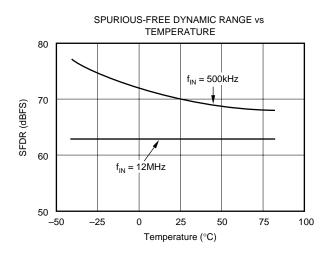


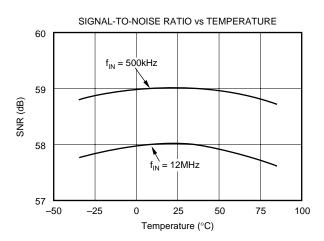


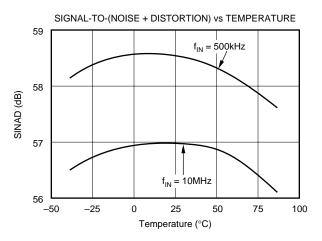


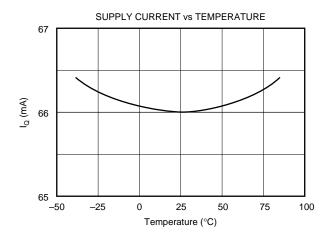
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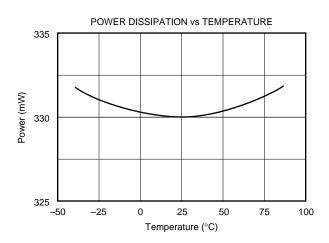




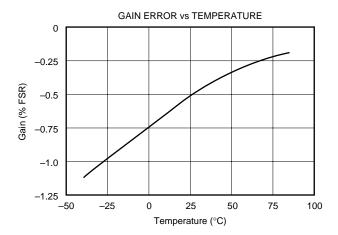


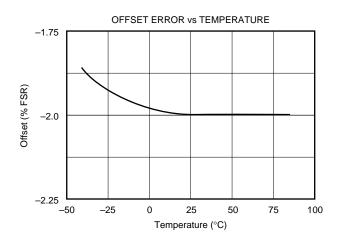


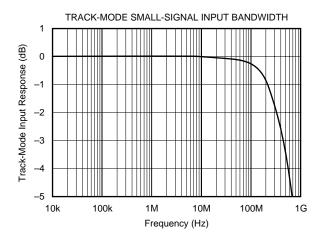


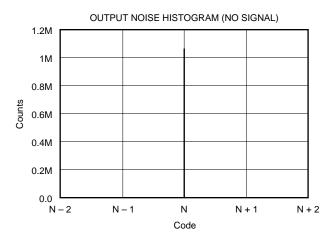


# **TYPICAL CHARACTERISTICS (Cont.)**









### THEORY OF OPERATION

The ADS821 is a high-speed, sampling A/D converter with pipelining. It uses a fully differential architecture and digital error correction to ensure 10-bit resolution. The differential track-and-hold circuit is shown in Figure 1. The switches are controlled by an internal clock that has a non-overlapping 2-phase signal,  $\phi 1$  and  $\phi 2$ . At the sampling time, the input signal is sampled on the bottom plates of the input capacitors. In the next clock phase,  $\phi 2$ , the bottom plates of the input capacitors are connected together and the feedback capacitors are switched to the op amp output. At this time, the charge redistributes between  $C_1$  and  $C_H$ , completing one track-and-hold cycle. The differential output is a held DC representation of the analog input at the sample time. The track-and-hold circuit can also convert a single-ended input signal into a fully differential signal for the quantizer.

The pipelined quantizer architecture has 9 stages with each stage containing a 2-bit quantizer and a 2-bit Digital-to-Analog Converter (DAC), as shown in Figure 2. Each 2-bit quantizer stage converts on the edge of the sub-clock, which is twice the frequency of the externally applied clock. The output of each quantizer is fed into its own delay line to

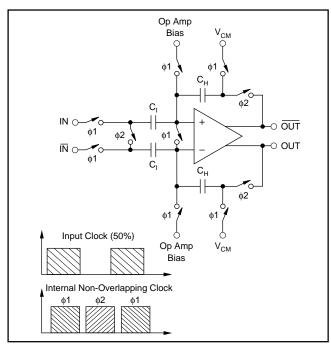


FIGURE 1. Input Track-and-Hold Configuration with Timing Signals.

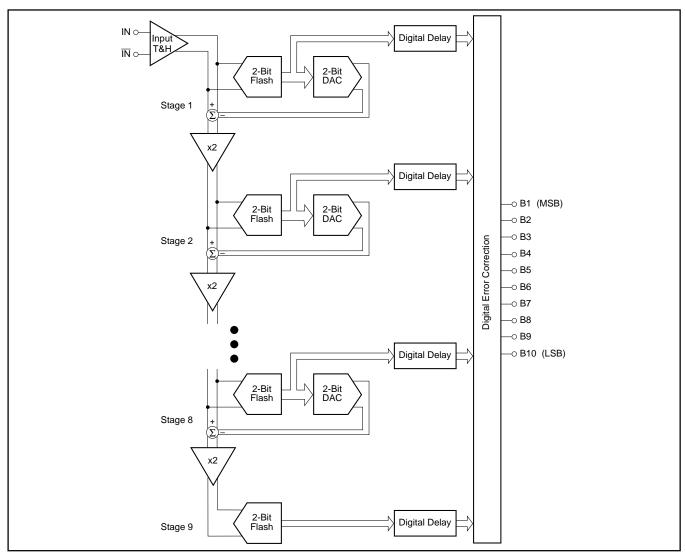


FIGURE 2. Pipeline A/D Converter Architecture.



time-align it with the data created from the following quantizer stages. This aligned data is fed into a digital error correction circuit that can adjust the output data based on the information found on the redundant bits. This technique gives the ADS821 excellent differential linearity and ensures no missing-codes at the 10-bit level.

The output data is available in Straight Offset Binary (SOB) or Binary Two's Complement (BTC) format.

#### THE ANALOG INPUT AND INTERNAL REFERENCE

The analog input of the ADS821 can be configured in various ways and driven with different circuits, depending on the nature of the signal and the level of performance desired. The ADS821 has an internal reference that sets the full-scale input range of the A/D converter. The differential input range has each input centered around the common-mode of +2.25V, with each of the two inputs having a full-scale range of +1.25V to +3.25V. Since each input is 2Vp-p and 180° out-of-phase with the other, a 4V differential input signal to the quantizer results. As shown in Figure 3, the positive full-scale reference (REFT) and the negative full-scale reference (REFB) are brought out for external bypassing. In addition, the commonmode (CM) voltage may be used as a reference to provide the appropriate offset for the driving circuitry. However, care must be taken not to appreciably load this reference node. For more information regarding external references, single-ended inputs, and ADS821 drive circuits, refer to the applications section.

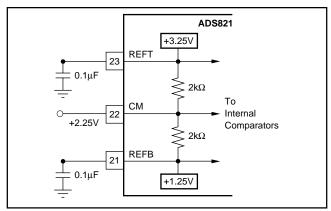


FIGURE 3. Internal Reference Structure.

#### **CLOCK REQUIREMENTS**

The CLK pin accepts a CMOS level clock input. Both the rising and falling edges of the externally applied clock controls the various interstage conversions in the pipeline. Therefore, the clock signal's jitter, rise-and-fall times and duty cycle can affect conversion performance.

- Low clock jitter is critical to SNR performance in frequency-domain signal environments.
- Clock rise and fall times should be as short as possible (< 2ns for best performance).</li>

For most applications, the clock duty should be set to 50%. For applications requiring no missing codes, however, a slight skew in the duty cycle will improve DNL performance for conversion rates > 35MHz and input frequencies < 2MHz (see Timing Diagram) in the SO package. For the best performance in the SSOP package, the clock should be skewed under all input frequencies with conversion rates > 35MHz. A possible method for skewing the 50% duty cycle source is shown in Figure 4.

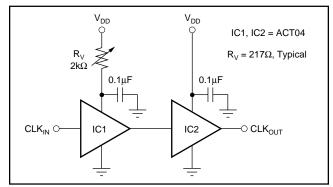


FIGURE 4. Clock Skew Circuit.

#### **DIGITAL OUTPUT DATA**

The 10-bit output data is provided at CMOS logic levels. There is a 6.5 clock cycle data latency from the start convert signal to the valid output data. The standard output coding is Straight Offset Binary where a full-scale input signal corresponds to all "1's" at the output. This condition is met with pin 19 LOW or Floating due to an internal pull-down resistor. By applying a high voltage to this pin, a BTC output will be provided where the most significant bit is inverted. The digital outputs of the ADS821 can be set to a high impedance state by driving  $\overline{\text{OE}}$  (pin 18) with a logic HIGH. Normal operation is achieved with pin 18 LOW or Floating due to internal pull-down resistors. This function is provided for testability purposes and is not meant to drive digital buses directly or be dynamically changed during the conversion process.

	OUTPUT CODE				
DIFFERENTIAL INPUT <sup>(1)</sup>	SOB PIN 19 FLOATING or LOW	BTC PIN 19 HIGH			
+FS (IN = +3.25V, $\overline{\text{IN}}$ = +1.25V) +FS - 1LSB +FS - 2LSB +3/4 Full-Scale +1/2 Full-Scale +1/4 Full-Scale +1LSB Bipolar Zero (IN = $\overline{\text{IN}}$ = +2.25V) -1LSB -1/4 Full-Scale -1/2 Full-Scale -3/4 Full-Scale -FS + 1LSB	111111111 111111111 111111110 1110000000 1100000000	011111111 011111111 0111111110 011000000			
-FS (IN = +1.25V, $\overline{\text{IN}}$ = +3.25V) NOTE: (1) In the single-ended input	000000000	1000000000			

TABLE I. Coding Table for the ADS821.



### **APPLICATIONS**

#### **DRIVING THE ADS821**

The ADS821 has a differential input with a common-mode of +2.25V. For AC-coupled applications, the simplest way to create this differential input is to drive the primary winding of a transformer with a single-ended input. A differential output is created on the secondary if the center tap is tied to the common-mode (CM) voltage of +2.25V, as per Figure 5. This transformer-coupled input arrangement provides good highfrequency AC performance. It is important to select a transformer that gives low distortion and does not exhibit core saturation at full-scale voltage levels. Since the transformer does not appreciably load the ladder, there is no need to buffer the CM output in this instance. In general, it is advisable to keep the current draw from the CM output pin below 0.5µA to avoid nonlinearity in the internal reference ladder. A FET input operational amplifier such as the OPA130 can provide a buffered reference for driving external circuitry. The analog IN and IN inputs should be bypassed with 22pF capacitors to minimize track-and-hold glitches and to improve high-input frequency performance.

Figure 6 shows an AC-coupled single-ended input interface circuit using the low-cost, current feedback OPA694 as the active gain stage. When testing this configuration in gains of +4, +5.8, and +8.2, it was noted that reducing the feedback

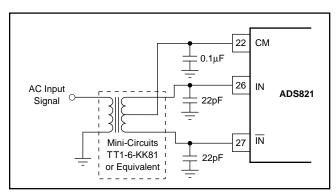


FIGURE 5. AC-Coupled, Single-Ended to Differential Drive Circuit Using a Transformer.

resistor of the OPA694 from the typical  $402\Omega$  to  $360\Omega$  resulted in a wider bandwidth, thus improving distortion at higher gains. The gain resistor was scaled to  $120\Omega$ ,  $75\Omega$ , and  $50\Omega$  for each of the three gain settings. The two  $330\Omega$  resistors set the RC time constant and the values can be varied, although higher values will have the effect of moving the corner frequency of the created high-pass filter down. In Figure 6, the -3dB point is set at 4.2kHz.

Figure 7 illustrates another possible low-cost interface circuit that utilizes resistors and capacitors in place of a transformer. Depending on the signal bandwidth, the component values should be carefully selected in order to maintain the performance outlined in the data sheet. The input capacitors, C<sub>IN</sub>, and the input resistors, R<sub>IN</sub>, create a high-pass filter with the lower corner frequency at  $f_C = 1/(2\pi R_{IN}C_{IN})$ . The corner frequency can be reduced by either increasing the value of  $R_{IN}$  or  $C_{IN}$ . If the circuit operates with a  $50\Omega$  or  $75\Omega$  impedance level, the resistors are fixed and only the value of the capacitor can be increased. Usually AC-coupling capacitors are electrolytic or tantalum capacitors with values of 1mF or higher. It should be noted that these large capacitors become inductive with increased input frequency, which could lead to signal amplitude errors or oscillation. To maintain a low ACcoupling impedance throughout the signal band, a small value (e.g. 1µF) ceramic capacitor could be added in parallel with the polarized capacitor.

Capacitors  $C_{SH1}$  and  $C_{SH2}$  are used to minimize current glitches resulting from the switching in the input track-and-hold stage and to improve signal-to-noise performance. These capacitors can also be used to establish a low-pass filter and effectively reduce the noise bandwidth. In order to create a real pole, resistors  $R_{SER1}$  and  $R_{SER2}$  were added in series with each input. The cut off frequency of the filter is determined by  $f_C = 1/(2\pi R_{SER} \bullet (C_{SH} + C_{ADC}))$  where  $R_{SER}$  is the resistor in series with the input,  $C_{SH}$  is the external capacitor from the input to ground, and  $C_{ADC}$  is the internal input capacitance of the A/D converter (typically 4pF).

Resistors  $R_1$  and  $R_2$  are used to derive the necessary common-mode voltage from the buffered top and bottom references. The total load of the resistor string should be selected

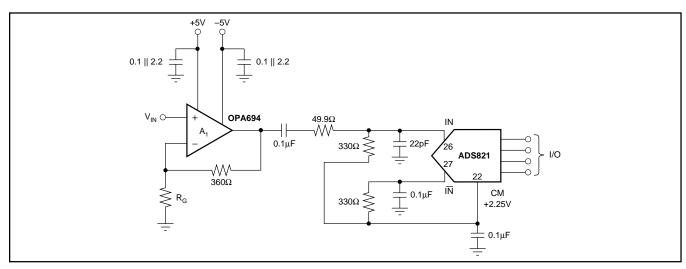


FIGURE 6. Low-Cost, AC-Coupled, Single-Ended Input Circuit.



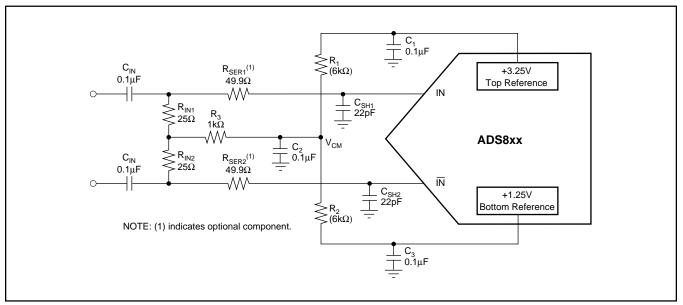


FIGURE 7. AC-Coupled Differential Input Circuit.

so that the current does not exceed 1mA. Although the circuit in Figure 7 uses two resistors of equal value so that the common-mode voltage is centered between the top and bottom reference (+2.25V), it is not necessary to do so. In all cases the center point,  $V_{\text{CM}}$ , should be bypassed to ground in order to provide a low-impedance AC ground.

If the signal needs to be DC-coupled to the input of the ADS821, an operational amplifier input circuit is required. In the differential input mode, any single-ended signal must be modified to create a differential signal. This can be accomplished by using two operational amplifiers, one in the noninverting mode for the input and the other amplifier in the inverting mode for the complementary input. The low-distortion circuit in Figure 8 will provide the necessary input shifting required for signals centered around ground. It also employs a diode for output level shifting to ensure a low-distortion +3.25V output swing. See Figure 9 for another DC-coupled circuit. Other amplifiers can be used in place of the OPA860 if the lowest distortion is not necessary. If output level shifting circuits are not used, care must be taken to select operational amplifiers that give the necessary performance when swinging to +3.25V with a ±5V supply operational amplifier. The OPA620 and OPA621, or the lower power OPA650 or OPA820 can be used in place of the OPA860 in Figure 8. In that configuration, the OPA820 will typically swing to within 100mV of positive full scale.

The ADS821 can also be configured with a single-ended input full-scale range of +0.25V to +4.25V by tying the complementary input to the common-mode reference voltage, see Figure 10. This configuration will result in increased even-order harmonics, especially at higher input frequencies. This tradeoff, however, may be quite acceptable for time-domain applications. The driving amplifier must give adequate performance with a +0.25V to +4.25V output swing in this case.

# EXTERNAL REFERENCES AND ADJUSTMENT OF FULL-SCALE RANGE

The internal-reference buffers are limited to approximately 1mA of output current. As a result, these internal +1.25V and +3.25V references may be overridden by external references that have at least 18mA (at room temperature) of output drive capability. In this instance, the common-mode voltage will be set halfway between the two references. This feature can be used to adjust the gain error, improve gain drift, or to change the full-scale input range of the ADS821. Changing the full-scale range to a lower value has the benefit of easing the swing requirements of external input amplifiers. The external references can vary as long as the value of the external top reference (REFT<sub>EXT</sub>) is less than or equal to +3.4V, the value of the external bottom reference (REFB<sub>EXT</sub>) is greater than or equal to +1.1V, and the difference between the external references are greater than or equal to 800mV.

For the differential configuration, the full-scale input range will be set to the external reference values that are selected. For the single-ended mode, the input range is  $2 \bullet (\text{REFT}_{\text{EXT}} - \text{REFB}_{\text{EXT}}),$  with the common-mode being centered at  $(\text{REFT}_{\text{EXT}} + \text{REFB}_{\text{EXT}})/2.$  Refer to the Typical Characteristics for expected performance versus full-scale input range.

The circuit in Figure 11 works completely on a single +5V supply. As a reference element, it uses the *micro*Power reference REF1004-2.5, which is set to a quiescent current of 0.1mA. Amplifier  $A_2$  is configured as a follower to buffer the +1.25V generated from the resistor divider. To provide the necessary current drive, a pull-down resistor ( $R_P$ ) is added.

Amplifier A<sub>1</sub> is configured as an adjustable gain stage, with a range of approximately 1 to 1.32. The pull-up resistor again relieves the op amp from providing the full current drive. The value of the pull-up, pull-down resistors is not critical and can be varied to optimize power consumption. The need for pull-up, pull-down resistors depends only on the drive capability of the selected drive amplifier and thus can be omitted.



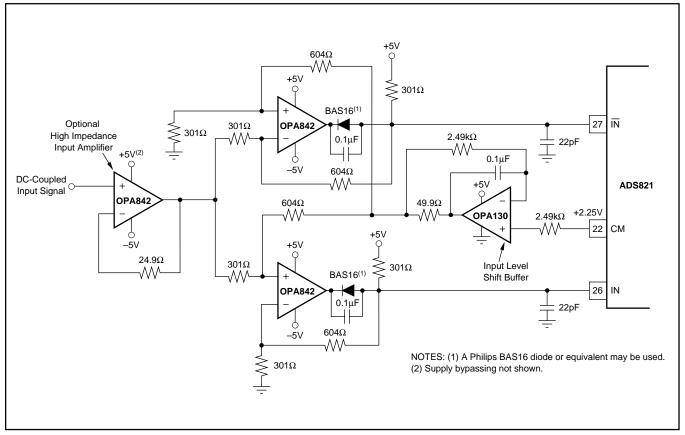


FIGURE 8. A Low-Distortion DC-Coupled, Single-Ended to Differential Input Driver Circuit.

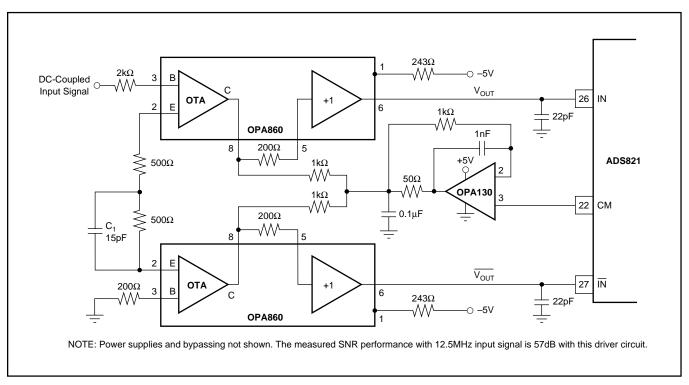


FIGURE 9. A Wideband DC-Coupled, Single-Ended to Differential Input Driver Circuit.

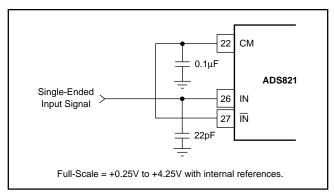


FIGURE 10. Single-Ended Input Connection.

#### PC-BOARD LAYOUT AND BYPASSING

A well-designed, clean PC-board layout will assure proper operation and clean spectral response. Proper grounding and bypassing, short lead lengths, and the use of ground planes are particularly important for high-frequency circuits. Multilayer PC-boards are recommended for best performance but if carefully designed, a two-sided PC-board with large, heavy ground planes can give excellent results. It is recommended that the analog and digital ground pins of the ADS821 be connected directly to the analog ground plane. In our experience, this gives the most consistent results. The A/D converter power-supply commons should be tied together at the analog ground plane. Power supplies should be bypassed with  $0.1\mu F$  ceramic capacitors as close to the pin as possible.

#### DYNAMIC PERFORMANCE TESTING

The ADS821 is a high-performance converter and careful attention to test techniques is necessary to achieve accurate

results. Highly accurate phase-locked signal sources allow high resolution FFT measurements to be made without using data windowing functions. A low jitter signal generator, such as the HP8644A for the test signal, phase-locked with a low jitter HP8022A pulse generator for the A/D converter clock, gives excellent results. Low-pass filtering (or bandpass filtering) of test signals is absolutely necessary to test the low distortion of the ADS821. Using a signal amplitude slightly lower than full scale will allow a small amount of "headroom" so that noise or DC offset voltage will not overrange the A/D converter and cause clipping on signal peaks.

#### DYNAMIC PERFORMANCE DEFINITIONS

1. Signal-to-Noise-and-Distortion Ratio (SINAD):

2. Signal-to-Noise Ratio (SNR):

3. Intermodulation Distortion (IMD):

IMD is referenced to the larger of the test signals  $f_1$  or  $f_2$ . Five "bins" either side of peak are used for calculation of fundamental and harmonic power. The "0" frequency bin (DC) is not included in these calculations as it is of little importance in dynamic signal processing applications.

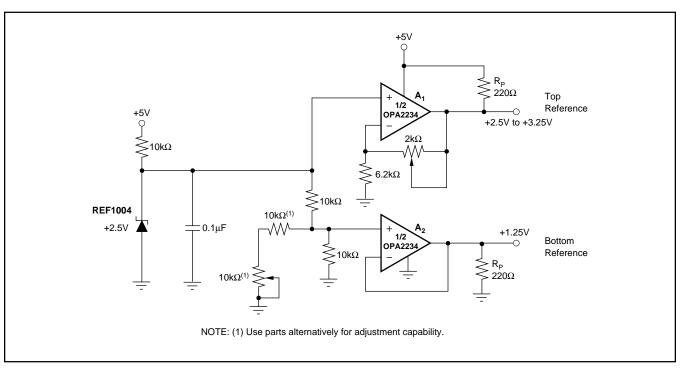


FIGURE 11. Optional External Reference to Set the Full-Scale Range Utilizing a Dual, Single-Supply Op Amp.



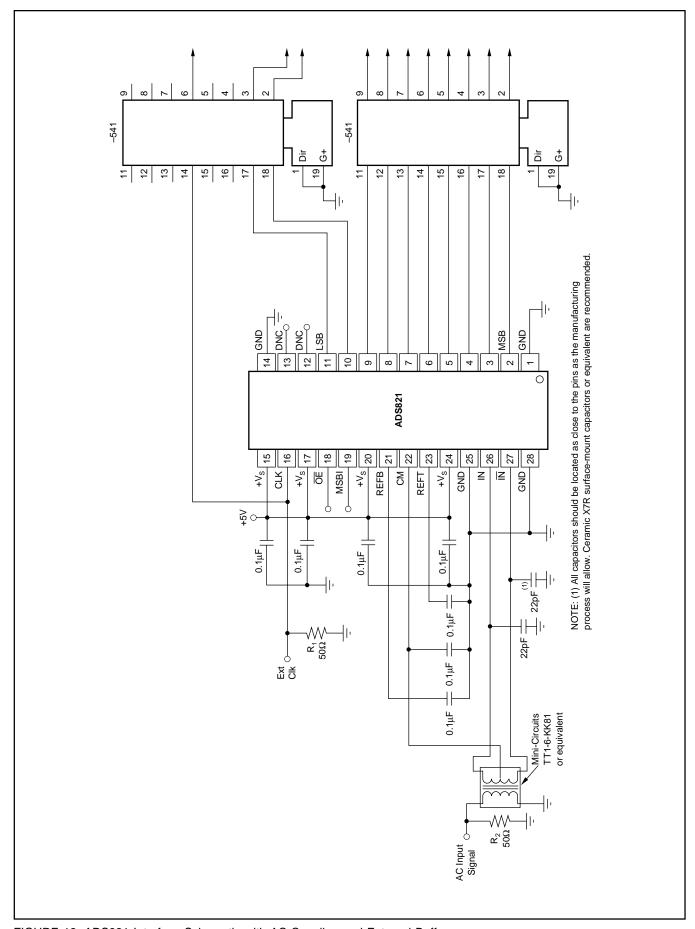


FIGURE 12. ADS821 Interface Schematic with AC-Coupling and External Buffers.

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#### PACKAGING INFORMATION

Orderable part number	Status	Material type	Package   Pins	Package qty   Carrier	<b>RoHS</b> (3)	Lead finish/ Ball material	MSL rating/ Peak reflow	Op temp (°C)	Part marking (6)
ADS821U	Active	Production	SOIC (DW)   28	20   TUBE	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 85	ADS821U
ADS821U.B	Active	Production	SOIC (DW)   28	20   TUBE	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 85	ADS821U

<sup>(1)</sup> Status: For more details on status, see our product life cycle.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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<sup>(3)</sup> RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

<sup>(4)</sup> Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

<sup>(5)</sup> MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

<sup>(6)</sup> Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

# **PACKAGE MATERIALS INFORMATION**

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#### **TUBE**



#### \*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	T (µm)	B (mm)
ADS821U	DW	SOIC	28	20	506.98	12.7	4826	6.6
ADS821U.B	DW	SOIC	28	20	506.98	12.7	4826	6.6

DW (R-PDSO-G28)

### PLASTIC SMALL OUTLINE



NOTES: A. All linear dimensions are in inches (millimeters). Dimensioning and tolerancing per ASME Y14.5M-1994.

- B. This drawing is subject to change without notice.
- C. Body dimensions do not include mold flash or protrusion not to exceed 0.006 (0,15).
- D. Falls within JEDEC MS-013 variation AE.



# DW (R-PDSO-G28)

## PLASTIC SMALL OUTLINE



NOTES:

- A. All linear dimensions are in millimeters.
- B. This drawing is subject to change without notice.
- C. Refer to IPC7351 for alternate board design.
- D. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525
- E. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.



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