# How to pick a linear regulator for noise-sensitive applications

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Noise-sensitive applications require a power supply that generates low internal noise and rejects noise from the power source. These applications include test and measurement applications, medical equipment, communication equipment, base stations, and many others. A lownoise power supply is used to power a signal chain that includes data converters, amplifiers, clocks, jitter cleaners, PLLs, analog front ends and many other devices. A lownoise power solution is essential to preserving signal accuracy and integrity. This article addresses criteria and parameters to consider in designing such a power solution, including important specifications for picking a linear regulator.

The terms "power supply ripple rejection" (PSRR) and "linear regulator" often are used together. The linear regulator's high ripple rejection makes it an integral part of a power solution. PSRR is a measure of how well the regulator filters a circuit by rejecting noise or ripple coming from the power-supply input at various frequencies. In both low-dropout regulators (LDOs) and linear regulators, PSRR is a measure of output ripple compared to the input ripple over a frequency range.

Since PSRR is calculated as ripple rejection, it is expected to be a negative number. However, it is represented as a positive number in the datasheet so that a higher number denotes higher noise rejection. Mathematically, it is expressed in decibels as

$$\mathrm{PSRR} = 20 \times \log \Biggl( \frac{\mathrm{V_{IN\_ripple}}}{\mathrm{V_{OUT\_ripple}}} \Biggr). \label{eq:PSRR}$$

The PSRR of a linear regulator can be divided into three frequency-range regions. The first region extends from DC to the roll-off frequency. The ripple rejection in this region is mostly dominated by open-loop gain and the bandgap reference. The second region extends from the roll-off frequency to the unity-gain frequency. The PSRR in this region is usually higher than in the first region and is mainly dominated by the open-loop gain of the regulator. The third region's frequency range is above that of the unity-gain frequency. The output capacitor, along with the linear regulator's parasitics (in the V<sub>IN</sub>-to-V<sub>OUT</sub> path), dominates this region. Therefore, the values of the selected output capacitor and its equivalent series resistance are quite important. This information can be found in any datasheet.

In addition to  $V_{IN}$ ,  $V_{OUT}$ , and system load requirements, an engineer needs to know the frequency range of ripple and noise in the system or power supply in order to select linear regulators with a good PSRR in that frequency range. For example, a switcher that switches at a frequency of 2 MHz may require a linear regulator that has a high PSRR at around 2 MHz. Figure 1 shows a linear regulator's high PSRR of about 55 dB at 2 MHz that helps to remove input noise. Also, when PSRR graphs in the regulator datasheets are evaluated, it is always good to note the dropout voltage at which the PSRR is measured. High dropout voltage leads to better PSRR but reduces the device's efficiency.



# Figure 1. Plot of linear regulator's widebandwidth, high PSRR

Figure 2 shows a switching regulator's spectral noise that is fed to a linear regulator. It can be seen that the switcher is operating at 500 kHz. Figure 3 shows the output spectrum of the Texas Instruments TPS7A4700 linear regulator. The spike caused by the switcher at 500 kHz has been attenuated. If the power solution is not designed for noise attenuation with high-PSRR linear regulators, the spike may show up at the output of the RF voltage-controlled oscillators, which after mixing affect the PA performance. The spike may also fold back into the audio band and create noise in an audio application.

Usually, noise and PSRR parameters are lumped together in a linear regulator's datasheet, which causes a lot of confusion because noise and PSRR are two very different characteristics. Noise is purely a physical phenomenon that occurs with transistors and resistors



#### Figure 3. Output noise spectrum of TPS7A4700 linear regulator with attenuated 500-kHz spike



inside the linear regulator on a very fundamental level. This type of noise may include thermal, flicker, and shot noise. Noise is usually indicated as a curve showing spectral noise density (in  $\mu V/\sqrt{Hz}$ ) versus frequency (Figure 4). Noise can also be indicated as integrated output noise (in  $\mu V_{RMS}$ ), listed under the electrical characteristics table in the datasheet (Figure 5). The output noise (in  $\mu VR_{MS}$ ) is the spectral noise density integrated over a certain frequency range and can be seen as the total noise in a specified frequency range.

The next obvious question is whether an engineer should look at spectral noise density or integrated output noise, or both. The answer depends purely on the engineer's application. For example, in RF applications where the signal does not have any dependency on the frequency, it makes more sense to look at the linear regulator's spectral noise density. However, in applications where the noise will be integrated by the system, such as powering DACs and ADCs, the engineer should look at the linear regulator's integrated output noise instead.

## Conclusion

This article has discussed the important specifications that design engineers need to consider when picking a linear regulator. It has also covered the criteria and parameters to consider in designing a power solution for low-noise applications. Given these guidelines, engineers should be able to preserve signal accuracy and integrity in their applications.

## Reference

1. Thomas Neu, "Power-supply design for high-speed ADCs," Analog Applications Journal (1Q 2010). Available www.ti.com/slyt366-aaj

## **Related Web sites**

Power Management: www.ti.com/power-aaj www.ti.com/ldo-aaj www.ti.com/tps7a4700-aaj Subscribe to the AAJ:

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#### Figure 5. Excerpt from TPS7A4700 datasheet showing integrated output noise voltage

PARAMETER		TEST CONDITIONS	TYP	UNIT
V <sub>NOISE</sub>			4.17	μV <sub>RMS</sub>
	Output noise voitage	$V_{IN} = 6 V, V_{OUT(NOM)} = 5 V, C_{OUT} = 50 \mu F, C_{NR} = 1 \mu F, BW = 10 Hz to 100 kHz$	4.67	$\mu V_{RMS}$

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