











TPS62242-Q1

SLVSB38C - MARCH 2011 - REVISED AUGUST 2016

# TPS62242-Q1 2.25-MHz 300-mA Buck Converter in DDC (SOT) Package

### **Features**

- **Qualified for Automotive Applications**
- AEC-Q100 Qualified With the Following Results:
  - Device Temperature Grade 2
  - Device HBM ESD Classification Level H2
  - Device CDM ESD Classification Level C4B
- High Efficiency Up to 94%
- Output Current Up to 300 mA
- V<sub>IN</sub> Range From 2 V to 6 V
- 2.25-MHz Fixed-Frequency Operation
- Power-Save Mode at Light Load Currents
- Output Voltage Accuracy in PWM Mode ±1.5%
- 1.2-V Fixed Output Voltage
- 15-μA Typical Quiescent Current
- 100% Duty Cycle for Lowest Dropout
- Available in a SOT (5) 2.90-mm x 1.60-mm Package
- Allows < 1-mm Solution Height

## **Applications**

- **Automotive Applications**
- **Automotive Body Electronics** 
  - Body Control Module and Gateway
- Advanced Driver Assistance Systems (ADAS)
  - Front Camera, Surround View, and Park Assist
- Infotainment and Clusters

### 3 Description

The TPS62242-Q1 device is a highly efficient buck converter optimized for battery-powered portable applications. The device provides up to 300-mA output current from a single Li-Ion cell and is ideal for battery-powered portable applications, automotive applications, and other equipment like Advanced Driver Assistance Systems (ADAS).

With an input voltage range of 2 V to 6 V, the device supports applications powered by Li-Ion batteries with extended voltage range, two- and three-cell alkaline.

The TPS62242-Q1 operates at 2.25-MHz fixedswitching frequency and enters the power-save mode of operation at light load currents to maintain high efficiency over the entire load current range.

The power-save mode is optimized for low outputvoltage ripple. In shutdown mode, the current consumption is reduced to less than 1 µA. With 2.25-MHz fixed frequency and a 1.2-V fixed output voltage, the TPS62242-Q1 device allows the use of small inductors and capacitors to achieve a small solution size.

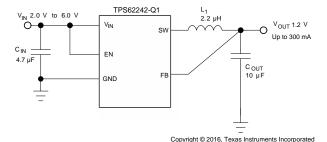
The TPS62242-Q1 operates over a temperature range of -40°C to 115°C. The device is available in a 5-pin SOT 2.90-mm × 1.60-mm package.

### Device Information<sup>(1)</sup>

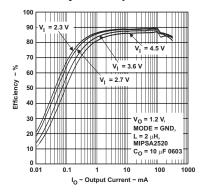
PART NUMBER	PACKAGE	BODY SIZE (NOM)	
TPS62242-Q1	SOT (5)	2.90 mm × 1.60 mm	

(1) For all available packages, see the orderable addendum at the end of the data sheet.

### **Typical Application Schematic**



#### **Efficiency vs Output Current**





# **Table of Contents**

1	Features 1		8.4 Device Functional Modes	. 10
2	Applications 1	9	Application and Implementation	12
3	Description 1		9.1 Application Information	. 12
4	Revision History2		9.2 Typical Application	. 12
5	Pin Configuration and Functions 4	10	Power Supply Recommendations	16
6	Specifications5	11	Layout	17
•	6.1 Absolute Maximum Ratings		11.1 Layout Guidelines	. 17
	6.2 ESD Ratings		11.2 Layout Example	. 17
	6.3 Recommended Operating Conditions	12	Device and Documentation Support	18
	6.4 Thermal Information5		12.1 Third-Party Products Disclaimer	. 18
	6.5 Electrical Characteristics		12.2 Receiving Notification of Documentation Updates	<b>18</b>
	6.6 Typical Characteristics		12.3 Community Resources	. 18
7	Parameter Measurement Information 8		12.4 Trademarks	. 18
8	Detailed Description 8		12.5 Electrostatic Discharge Caution	. 18
•	8.1 Overview		12.6 Glossary	. 18
	8.2 Functional Block Diagram9	13	Mechanical, Packaging, and Orderable Information	18
	8.3 Feature Description			10

# 4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

### Changes from Revision B (March 2013) to Revision C

**Page** 

•	Added ESD Ratings table, Thermal Information table, Feature Description section, Device Functional Modes, Application and Implementation section, Power Supply Recommendations section, Layout section, Device and Documentation Support section, and Mechanical, Packaging, and Orderable Information section
•	Deleted Ordering Information table; see POA at the end of the data sheet
•	Changed document title and description from "Step-Down" to "Buck Converter"
•	Changed from "Greater Than" to "Up to"
•	Changed Features and Applications bullets editorially
•	Changed description to automotive applications
•	Deleted duplicated information
•	Added 2.25-MHz fixed frequency and a 1.2-V fixed output voltage
•	Added PWM mode description
•	Added Free-air temperature range and reworded device package description.
•	Changed figure for $V_0 = 1.2 \text{ V}$ curves
•	Updated pinout image to new format
•	Deleted table note 3 about human body model and machine model
•	Deleted table row for adjustable voltage
•	Added table rows for inductance and output capacitance
•	Added PWM Mode
•	Deleted Dissipation Ratings section
•	Deleted in fixed output voltage versions from table note
•	Moved Figures 2, 6 through 9, and 11 through 13 to Application Curves
•	Changed Figures 6 through 9 and 11 through 13 for 1.2 V
•	Deleted Figures 1, 3 through 5, 10, 14, and 15
•	Deleted Mode transition row from table and corresponding figures 14 and 15
•	Moved Soft Start, Power Save Mode, and Short-Circuit Protection sections to Device Functional Modes section

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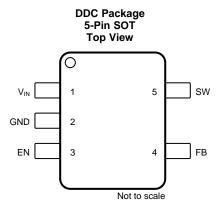


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# **5 Pin Configuration and Functions**



#### **Pin Functions**

PIN		1/0	DESCRIPTION		
NAME	NO.	1,0	DESCRIPTION		
EN	3	I	This is the enable pin of the device. Pulling this pin to low forces the device into shutdown mode. Pulling this pin to high enables the device. This pin must be terminated.		
FB	4	I	Feedback Pin for the internal regulation loop. Connect the external resistor divider to this pin. In case of fixed output voltage option, connect this pin directly to the output capacitor.		
GND	2	PWR	GND supply pin.		
SW	5	0	This is the switch pin and is connected to the internal MOSFET switches. Connect the inductor to this terminal.		
V <sub>IN</sub>	1	PWR	V <sub>IN</sub> power supply pin.		

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### 6 Specifications

### 6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	MAX	UNIT
$V_{I}$	Input voltage <sup>(2)</sup>	-0.3	7	V
	Voltage at EN	-0.3	V <sub>IN</sub> + 0.3, ≤7	V
	Voltage on SW	-0.3	7	V
	Peak output current	Interna	lly limited	Α
$T_{J}$	Maximum operating junction temperature	-40	150	ů
T <sub>stg</sub>	Storage temperature	-65	150	ů

<sup>(1)</sup> Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

### 6.2 ESD Ratings

			VALUE	UNIT
.,	Electrostatic	Human-body model (HBM), per AEC Q100-002 <sup>(1)</sup>	±2000	
V <sub>(ESD)</sub>	discharge	Charged-device model (CDM), per AEC Q100-011	±750	V

<sup>(1)</sup> AEC Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specification.

### 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	MAX	UNIT
$V_{I}$	Supply voltage, VIN	2	6	V
L	Inductance	1.5	4.7	μH
$C_OUT$	Output capacitance	4.7	10	μF
$T_A$	Operating ambient temperature	-40	115	°C
$T_J$	Operating junction temperature	-40	125	°C

### 6.4 Thermal Information

		TPS62242-Q1	
	THERMAL METRIC <sup>(1)</sup>	DDC (SOT)	UNIT
		5 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	193.7	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	40.7	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	35	°C/W
ΨЈТ	Junction-to-top characterization parameter	0.9	°C/W
ΨЈВ	Junction-to-board characterization parameter	34.7	°C/W
$R_{\theta JC(bot)}$	Junction-to-case (bottom) thermal resistance	N/A	°C/W

For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.

<sup>(2)</sup> All voltage values are with respect to network ground terminal.



### 6.5 Electrical Characteristics

Over full operating ambient temperature range, typical values are at  $T_A$  = 25°C. Unless otherwise noted, specifications apply for condition  $V_{IN}$  = EN = 3.6 V. External components  $C_{IN}$  = 4.7  $\mu$ F 0603,  $C_{OUT}$  = 10  $\mu$ F 0603, L = 2.2  $\mu$ H, refer to parameter measurement information.

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY						
V <sub>IN</sub>	Input voltage range		2		6	V
	1 5 5	2.3 V ≤ V <sub>IN</sub> ≤ 6 V			300	
I <sub>OUT</sub>	Output current	2 V ≤ V <sub>IN</sub> ≤ 2.3 V			150	mA
		I <sub>OUT</sub> = 0 mA. Pulse frequency modulation (PFM) mode enabled, device not switching		15		
l <sub>Q</sub>	Operating quiescent current	$I_{OUT}$ = 0 mA. PFM mode enabled, device switching, $V_{OUT}$ = 1.2 V $^{(1)}$		18.5		μА
		$I_{OUT}$ = 0 mA, switching with no load, PWM operation, $V_{OUT}$ = 1.2 V, $V_{IN}$ = 3 V		3.8		mA
	Chutdown ourrent	EN = GND, T <sub>A</sub> = 25°C		0.1	1	μΑ
I <sub>SD</sub>	Shutdown current	EN = GND, $T_A = -40$ °C to 115°C			5	μA
	Hadamakan ladan kabula	Falling		1.85		
UVLO	Undervoltage lockout threshold	Rising		1.95		V
ENABLE,	MODE				'	
V <sub>IH</sub>	High-level input voltage, EN	2 V ≤ V <sub>IN</sub> ≤ 6 V	1		$V_{IN}$	V
		2 V ≤ V <sub>IN</sub> ≤ 6 V, T <sub>A</sub> = 25°C	0		0.4	V
$V_{IL}$	Low-level input voltage, EN	$2 \text{ V} \le \text{V}_{\text{IN}} \le 6 \text{ V}$ , $\text{T}_{\text{A}} = -40^{\circ}\text{C}$ to 115°C			0.35	V
I <sub>IN</sub>	Input bias current, EN	EN, MODE = GND or V <sub>IN</sub>		0.01	1	μА
POWER S	WITCH	11				•
_	High-side MOSFET ON-resistance			240	480	
R <sub>DS(on)</sub>	Low-side MOSFET ON-resistance	$V_{IN} = V_{GS} = 3.6 \text{ V}, T_A = 25^{\circ}\text{C}$		180	380	mΩ
	Forward current limit MOSFET high- side and low-side	$V_{IN} = V_{GS} = 3.6 \text{ V}, T_{A} = 25^{\circ}\text{C}$	0.56	0.7	0.84	
I <sub>LIMF</sub>		$V_{IN} = V_{GS} = 3.6 \text{ V}, T_A = -40^{\circ}\text{C} \text{ to } 115^{\circ}\text{C}$	0.54		0.95	Α
TSD	Thermal shutdown	Increasing junction temperature	135	150	165	°C
	Thermal shutdown hysteresis	Decreasing junction temperature	12	14	16	°C
OSCILLAT	·	,	<u> </u>			
$f_{\sf SW}$	Oscillator frequency	2 V ≤ V <sub>IN</sub> ≤ 6 V	2	2.25	2.5	MHz
OUTPUT						
V <sub>OUT</sub>	Output voltage			1.2		V
V <sub>REF</sub>	Reference voltage	T <sub>A</sub> = 25°C	594	600	606	mV
	,	PWM operation, 2 V $\leq$ V <sub>IN</sub> $\leq$ 6 V, in fixed output voltage versions V <sub>FB</sub> = V <sub>OUT</sub> , See <sup>(2)</sup> , T <sub>A</sub> = 25°C	-1.5%	0%	1.5%	
$V_{FB}$	Feedback voltage	PWM operation, 2 V $\leq$ V <sub>IN</sub> $\leq$ 6 V, in fixed output voltage versions V <sub>FB</sub> = V <sub>OUT</sub> , See $^{(2)}$ ,T <sub>A</sub> = $-40^{\circ}$ C to 115°C	-1.5%		2.5%	
	Feedback voltage PFM mode	Device in PFM mode		0%		
	Load regulation	PWM mode		-0.5		%/A
t <sub>Start up</sub>	Start-up time	Time from active EN to reach 95% of V <sub>OUT</sub> nominal		500		μS
t <sub>Ramp</sub>	V <sub>OUT</sub> ramp UP time	Time to ramp from 5% to 95% of V <sub>OUT</sub>		250		μS
		$V_{IN} = 3.6 \text{ V}, V_{IN} = V_{OUT} = V_{SW}, \text{ EN} = \text{GND},^{(3)}, T_A = 25^{\circ}\text{C}$		0.1	1	
l <sub>lkg</sub>	Leakage current into SW pin	$V_{IN} = 3.6 \text{ V}, V_{IN} = V_{OUT} = V_{SW}, \text{ EN = GND, } ^{(3)}, \\ T_A = -40^{\circ}\text{C to } 115^{\circ}\text{C}$			10	μА

<sup>(1)</sup> See the parameter measurement information.

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<sup>(2)</sup> For  $V_{IN} = V_{O} + 0.6$ 

<sup>(3)</sup> The internal resistor divider network is disconnected from FB pin.



### 6.6 Typical Characteristics

### **Table 1. Table of Graphs**

		FIGURE
Shutdown Current into VIN	vs Input Voltage, $(T_A = 85^{\circ}C, T_A = 25^{\circ}C, T_A = -40^{\circ}C)$	Figure 1
Quiescent Current	vs Input Voltage, $(T_A = 85^{\circ}C, T_A = 25^{\circ}C, T_A = -40^{\circ}C)$	Figure 2
Static Prain Source On State Resistance	vs Input Voltage, $(T_{\Delta} = 85^{\circ}C, T_{\Delta} = 25^{\circ}C, T_{\Delta} = -40^{\circ}C)$	Figure 3
Static Drain-Source On-State Resistance		Figure 4

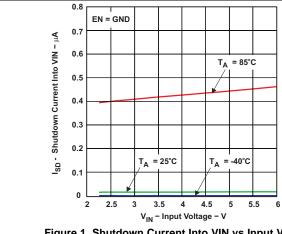


Figure 1. Shutdown Current Into VIN vs Input Voltage

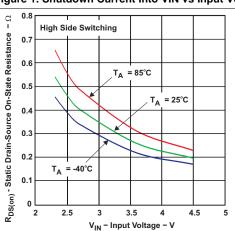


Figure 3. Static Drain-Source On-State Resistance vs Input Voltage

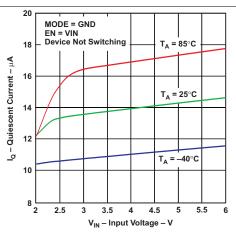


Figure 2. Quiescent Current vs Input Voltage

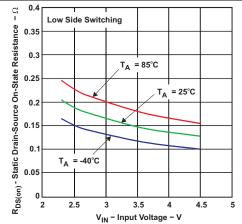
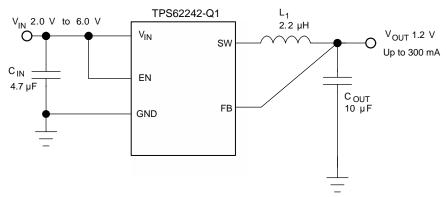


Figure 4. Static Drain-Source On-State Resistance vs Input Voltage

### 7 Parameter Measurement Information



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Figure 5. Typical Application Parameters

### 8 Detailed Description

#### 8.1 Overview

The TPS62242-Q1 step-down converter typically operates with 2.25-MHz fixed-frequency pulse width modulation (PWM) at moderate to heavy load currents. At light load currents, the converter can automatically enter power save mode and then operates in PFM mode.

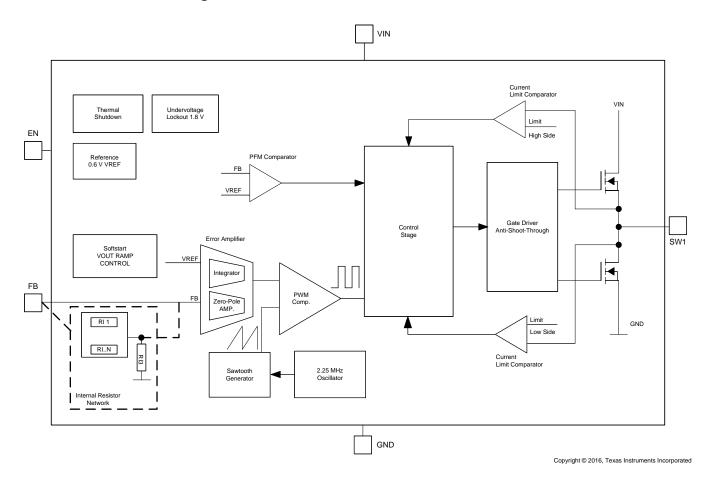
During PWM operation, the converter uses a unique fast-response voltage-mode control scheme with input voltage feed-forward to achieve good line and load regulation, allowing the use of small ceramic input and output capacitors. At the beginning of each clock cycle initiated by the clock signal, the high-side MOSFET switch is turned on. The current then flows from the input capacitor through the high-side MOSFET switch through the inductor to the output capacitor and load. During this phase, the current ramps up until the PWM comparator trips and the control logic turns off the switch. The current limit comparator also turns off the switch if the current limit of the high-side MOSFET switch is exceeded. After a dead time preventing shoot-through current, the low-side MOSFET rectifier is turned on and the inductor current ramps down. The current then flows from the inductor to the output capacitor and to the load. It returns back to the inductor through the low-side MOSFET rectifier.

The next cycle is initiated by the clock signal again turning off the low-side MOSFET rectifier and turning on the high-side MOSFET switch.

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### 8.2 Functional Block Diagram



### 8.3 Feature Description

### 8.3.1 Undervoltage Lockout

The undervoltage lockout circuit prevents the device from malfunctioning at low input voltages and from excessive discharge of the battery and disables the output stage of the converter. The undervoltage lockout threshold is typically 1.85 V with falling V<sub>IN</sub>.

#### 8.3.2 **Enable**

The device is enabled by setting the EN pin to high. During the start-up time (t<sub>Start up</sub>), the internal circuits are settled and the soft-start circuit is activated. The EN input can be used to control power sequencing in a system with various DC-DC converters. The EN pin can be connected to the output of another converter, to drive the EN pin high and sequence supply rails. With EN pin = GND, the device enters shutdown mode in which all circuits are disabled. In fixed-output voltage versions, the internal resistor divider network is then disconnected from FB pin.

### 8.3.3 Thermal Shutdown

As soon as the junction temperature, T<sub>J</sub>, exceeds 150°C (typical) the device goes into thermal shutdown. In this mode, the high-side and low-side MOSFETs are turned off. The device continues its operation when the junction temperature falls below the thermal shutdown hysteresis.

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#### 8.4 Device Functional Modes

#### 8.4.1 Soft Start

The TPS62242-Q1 device has an internal soft-start circuit that controls the ramp up of the output voltage. The output voltage ramps up from 5% to 95% of its nominal value within typical 250 μs. This limits the inrush current in the converter during ramp up and prevents possible input voltage drops when using a battery or high impedance power source. The soft-start circuit is enabled within the start-up time, t<sub>Start-up</sub>.

#### 8.4.2 Power Save Mode

The power save mode is enabled. If the load current decreases, the converter enters power save mode operation automatically. During power save mode, the converter skips switching and operates with reduced frequency in PFM mode with a minimum-quiescent current to maintain high efficiency.

The transition from PWM mode to PFM mode occurs once the inductor current in the low-side MOSFET switch becomes zero, which indicates discontinuous conduction mode.

During the power save mode, a PFM comparator monitors the output voltage. As the output voltage falls below the PFM comparator threshold of  $V_{OUT}$  nominal, the device starts a PFM current pulse. The high-side MOSFET switch turns on, and the inductor current ramps up. After the on-time expires, the switch turns off and the low-side MOSFET switch turns on until the inductor current becomes zero.

The converter effectively delivers a current to the output capacitor and the load. If the load is below the delivered current, the output voltage rises. If the output voltage is equal to or greater than the PFM comparator threshold, the device stops switching and enters a sleep mode with typical 15-µA current consumption.

If the output voltage is still below the PFM comparator threshold, a sequence of further PFM current pulses are generated until the PFM comparator threshold is reached. The converter starts switching again once the output voltage drops below the PFM comparator threshold.

With a fast single-threshold comparator, the output-voltage ripple during PFM mode operation can be kept to a minimum. The PFM pulse is time controlled, allowing the user to modify the charge transferred to the output capacitor by the value of the inductor. The resulting PFM output voltage ripple and PFM frequency both depend on the size of the output capacitor and the inductor value. Increasing output capacitor values and inductor values minimize the output ripple. The PFM frequency decreases with smaller inductor values and increases with larger values.

If the output current cannot be supported in PFM mode, the device exits PFM mode and enters PWM mode.

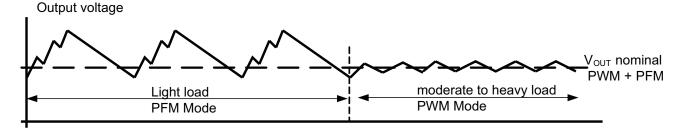


Figure 6. Power Save Mode

#### 8.4.2.1 100% Duty Cycle Low Dropout Operation

The device starts to enter 100% duty-cycle mode once the input voltage comes close to the nominal output voltage. To maintain the output voltage, the high-side MOSFET switch is turned on 100% for one or more cycles.

With further decreasing  $V_{\text{IN}}$  the high-side MOSFET switch is turned on completely. In this case, the converter offers a low input-to-output voltage difference. This is particularly useful in battery-powered applications to achieve longest operation time by taking full advantage of the entire battery voltage range.



### **Device Functional Modes (continued)**

The minimum input voltage to maintain regulation depends on the load current and output voltage, and can be calculated as:

 $V_{IN}min = V_{O}max + I_{O}max (R_{DS(on)}max + R_{L})$ 

#### where

- I<sub>O</sub>max = maximum output current plus inductor ripple current
- R<sub>DS(on)</sub>max = maximum P-channel switch R<sub>DS(on)</sub>
- R<sub>I</sub> = DC resistance of the inductor
- V<sub>O</sub>max = nominal output voltage plus maximum output voltage tolerance

### (1)

### 8.4.3 Short-Circuit Protection

The high-side and low-side MOSFET switches are short-circuit protected with maximum switch current equal to  $I_{LIMF}$ . The current in the switches is monitored by current limit comparators. Once the current in the high-side MOSFET switch exceeds the threshold of its current limit comparator, it turns off and the low-side MOSFET switch is activated to ramp down the current in the inductor and high-side MOSFET switch. The high-side MOSFET switch can only turn on again once the current in the low-side MOSFET switch has decreased below the threshold of its current limit comparator.



### 9 Application and Implementation

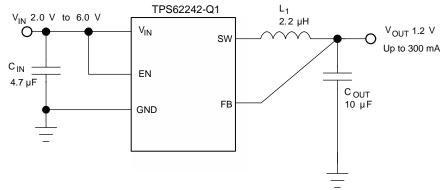
#### NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 9.1 Application Information

The TPS62242-Q1 device is a high-efficiency synchronous step-down DC-DC converter featuring power save mode.

### 9.2 Typical Application



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Figure 7. Fixed 1.2 V

### 9.2.1 Design Requirements

The device operates over an input voltage range from 2 V to 6 V.

#### 9.2.2 Detailed Design Procedure

Table 2 shows the list of components for the *Application Curves*. Users must verify and validate these components for suitability with their application before using the components.

**Table 2. List of Components** 

VALUE	COMPONENT REFERENCE	PART NUMBER	MANUFACTURER
4.7 μF, 6.3 V. X5R Ceramic	C <sub>IN</sub>	GRM188R60J475K	Murata
10 μF, 6.3 V. X5R Ceramic	C <sub>OUT</sub>	GRM188R60J106M	Murata
22 pF, COG Ceramic	C <sub>1</sub>		Murata
2.2 μH, 110 mΩ	L <sub>1</sub>	LPS3015	Coilcraft

### 9.2.2.1 Output Filter Design (Inductor and Output Capacitor)

The TPS62242-Q1 device is designed to operate with inductors in the range of 1.5  $\mu$ H to 4.7  $\mu$ H and with output capacitors in the range of 4.7  $\mu$ F to 22  $\mu$ F. The device is optimized for operation with a 2.2- $\mu$ H inductor and 10- $\mu$ F output capacitor.

Larger or smaller inductor values can be used to optimize the performance of the device for specific operation conditions. For stable operation, the L and C values of the output filter may not fall below 1- $\mu$ H effective Inductance and 3.5- $\mu$ F effective capacitance. Selecting larger capacitors is less critical, because the corner frequency of the L-C filter moves to lower frequencies with fewer stability problems.



#### 9.2.2.1.1 Inductor Selection

The inductor value has a direct effect on the ripple current. The selected inductor must be rated for its DC resistance and saturation current (Table 3). The inductor ripple current ( $\Delta I_L$ ) decreases with higher inductance and increases with higher  $V_L$  or  $V_C$ .

The inductor selection also has an impact on the output voltage ripple in the PFM mode. Higher inductor values lead to lower-output voltage ripple and higher PFM frequency, and lower inductor values lead to a higher-output voltage ripple with lower PFM frequency.

Equation 2 calculates the maximum inductor current in PWM mode under static load conditions. The saturation current of the inductor should be rated higher than the maximum inductor current as calculated with Equation 3. This is the recommendation because during heavy-load transients the inductor current rises above the calculated value.

$$\Delta I_{L} = V_{OUT} \times \frac{1 - \frac{V_{OUT}}{V_{IN}}}{L \times f}$$

$$I_{Lmax} = I_{OUTmax} + \frac{\Delta I_{L}}{2}$$
(2)

where

- f =Switching frequency (2.25-MHz typical)
- L = Inductor value
- ΔI<sub>L</sub> = Peak-to-Peak inductor ripple current

A more conservative approach is to select the inductor current rating just for the maximum switch current limit  $I_{\text{I-IMF}}$  of the converter.

Accepting larger values of ripple current allows the use of low inductance values, but results in higher output voltage ripple, greater core losses, and lower output current capability.

The total losses of the coil strongly impact the efficiency of the DC-DC conversion and consist of both the losses in the DC resistance  $(R_{(DC)})$  and the following frequency-dependent components:

- The losses in the core material (magnetic hysteresis loss, especially at high switching frequencies)
- Additional losses in the conductor from the skin effect (current displacement at high frequencies)
- Magnetic field losses of the neighboring windings (proximity effect)
- Radiation losses

**Table 3. List of Inductors** 

INDUCTANCE (μH)	DIMENSIONS (mm)	PART NUMBER	MANUFACTURER		
2	2.5 × 2 × 1	MIPS2520D2R2	FDK		
2	2.5 × 2 × 1.2	MIPSA2520D2R2	FDK		
2.2	2.5 × 2 × 1	KSLI-252010AG2R2	Hitachi Metals		
2.2	2.5 × 2 × 1.2	LQM2HPN2R2MJ0L	Murata		
2.2	3 × 3 × 1.4	LPS3015	Coilcraft		

### 9.2.2.1.2 Output Capacitor Selection

The advanced fast-response voltage-mode control scheme of the TPS62242-Q1 device allows the use of tiny ceramic capacitors. Ceramic capacitors with low-ESR values have the lowest-output voltage ripple and are recommended. The output capacitor requires either an X7R or X5R dielectric. Y5V and Z5U dielectric capacitors, aside from their wide variation in capacitance over temperature, become resistive at high frequencies.

At nominal load current, the device operates in PWM mode and the RMS ripple current is calculated as in Equation 4:

$$I_{RMSC_{OUT}} = V_{OUT} \times \frac{1 - \frac{V_{OUT}}{V_{IN}}}{L \times f} \times \frac{1}{2 \times \sqrt{3}}$$
(4)

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At nominal load current, the device operates in PWM mode and the overall output voltage ripple is the sum of the voltage spike caused by the output capacitor ESR plus the voltage ripple caused by charging and discharging the output capacitor as in Equation 5:

$$\Delta V_{OUT} = V_{OUT} \times \frac{1 - \frac{V_{OUT}}{V_{IN}}}{L \times f} \times \left(\frac{1}{8 \times C_{OUT} \times f} + ESR\right)$$
(5)

At light load currents, the converter operates in power save mode and the output voltage ripple depends on the output capacitor and inductor value. Larger output capacitor and inductor values minimize the voltage ripple in PFM mode and tighten DC output accuracy in PFM mode.

### 9.2.2.1.3 Input Capacitor Selection

The buck converter has a natural pulsating input current; therefore, a low-ESR input capacitor is required for best input voltage filtering and minimizing the interference with other circuits caused by high-input voltage spikes. For most applications, a 4.7- $\mu$ F to 10- $\mu$ F ceramic capacitor is recommended (Table 4). Because ceramic capacitors lose up to 80% of their initial capacitance at 5 V, TI recommends using a 10- $\mu$ F input capacitor for input voltages greater than 4.5 V. The input capacitor can be increased without any limit for better input voltage filtering.

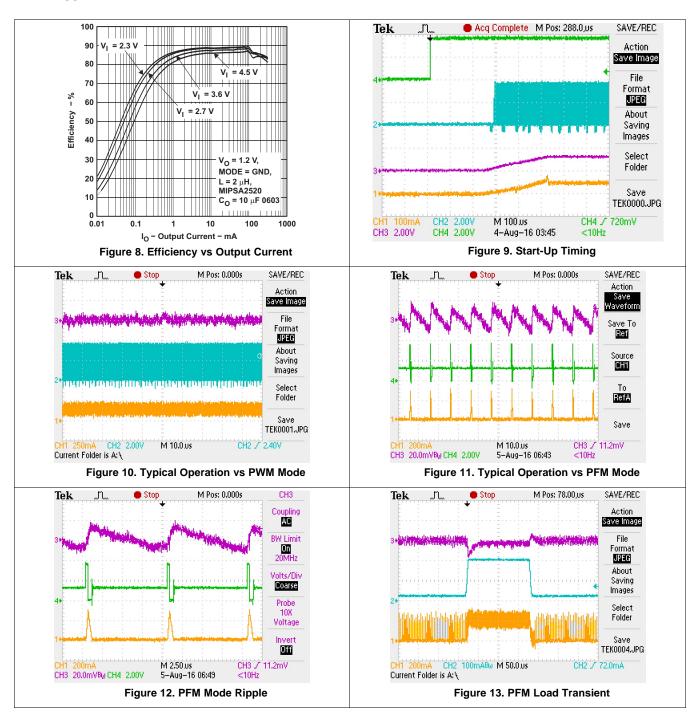
Take care when using only small ceramic input capacitors. When a ceramic capacitor is used at the input, and the power is being supplied through long wires, such as from a wall adapter, a load step at the output, or  $V_{IN}$  step on the input, can induce ringing at the VIN pin. The ringing can couple to the output and be mistaken as loop instability, or could even damage the part by exceeding the maximum ratings.

**Table 4. List of Capacitors** 

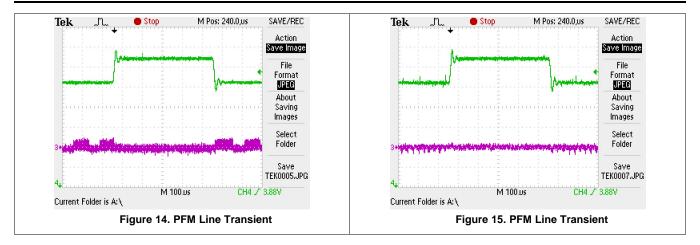
CAPACITANCE (μF)	CAPACITANCE (µF) DIMENSIONS (mm)		MANUFACTURER		
4.7	4.7 $0603: 1.6 \times 0.8 \times 0.8$		Murata		
10	0603: 1.6 × 0.8 × 0.8	GRM188R60J106M69D	Murata		



### 9.2.3 Application Curves







# 10 Power Supply Recommendations

The TPS62242-Q1 device has no special requirements for its input power supply. The input power supply output current must be rated according to the supply voltage, output voltage, and output current of the TPS62242-Q1.

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### 11 Layout

### 11.1 Layout Guidelines

As for all switching power supplies, the layout is an important step in the design. Proper function of the device demands careful attention to PCB layout. To get the specified performance, the board layout must be carefully done. If not carefully done, the regulator could show poor line or load regulation, and additional stability issues as well as EMI problems. Figure 16 shows an example of layout design with the TLV62242-Q1 device.

- Providing a low-inductance, low-impedance ground path is critical. Therefore, use wide and short traces for the main current paths. The input capacitor as well as the inductor and output capacitor must be placed as close as possible to the IC pins.
- The FB line must be connected directly to the output capacitor and the FB line must be routed away from noisy components and traces (for example, the SW line).
- Because of the small package of this converter and the overall small solution size, the thermal performance of the PCB layout is important. For good thermal performance, PCB design of at least four layers is recommended.

### 11.2 Layout Example

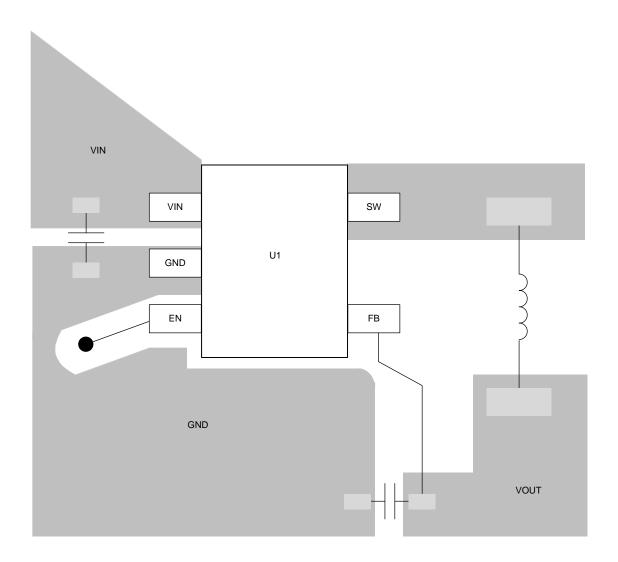


Figure 16. Suggested Layout for Fixed Output Voltage

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### 12 Device and Documentation Support

### 12.1 Third-Party Products Disclaimer

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### 12.5 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### 12.6 Glossary

SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.

### 13 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

www.ti.com 23-May-2025

#### PACKAGING INFORMATION

Orderable part number	Status	Material type	Package   Pins	Package qty   Carrier	RoHS	Lead finish/ Ball material	MSL rating/ Peak reflow	Op temp (°C)	Part marking (6)
						(4)	(5)		
TPS62242QDDCRQ1	Active	Production	SOT-23- THIN (DDC)   5	3000   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 115	SAW
TPS62242QDDCRQ1.B	Active	Production	SOT-23- THIN (DDC)   5	3000   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 115	SAW

<sup>(1)</sup> Status: For more details on status, see our product life cycle.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

#### OTHER QUALIFIED VERSIONS OF TPS62242-Q1:

<sup>(2)</sup> Material type: When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

<sup>(3)</sup> RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

<sup>(4)</sup> Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

<sup>(5)</sup> MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

<sup>(6)</sup> Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

# **PACKAGE OPTION ADDENDUM**

www.ti.com 23-May-2025

• Catalog : TPS62242

NOTE: Qualified Version Definitions:

• Catalog - TI's standard catalog product

# **PACKAGE MATERIALS INFORMATION**

www.ti.com 26-Dec-2020

### TAPE AND REEL INFORMATION





Α0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



### \*All dimensions are nominal

Device	Package Type	Package Drawing			Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS62242QDDCRQ1	SOT- 23-THIN	DDC	5	3000	179.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3

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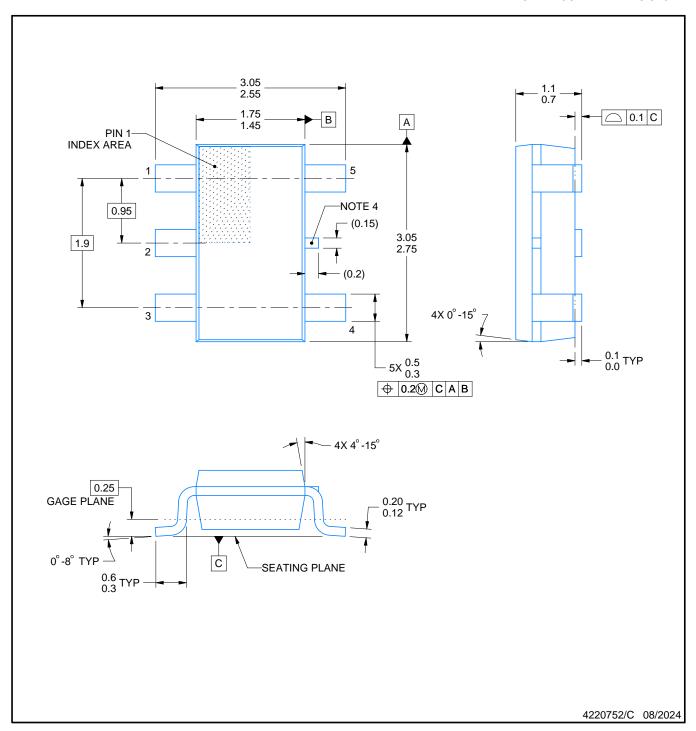


#### \*All dimensions are nominal

Device	Device Package Type		Pins	SPQ	Length (mm)	Width (mm)	Height (mm)	
TPS62242QDDCRQ1	SOT-23-THIN	DDC	5	3000	200.0	183.0	25.0	



SMALL OUTLINE TRANSISTOR



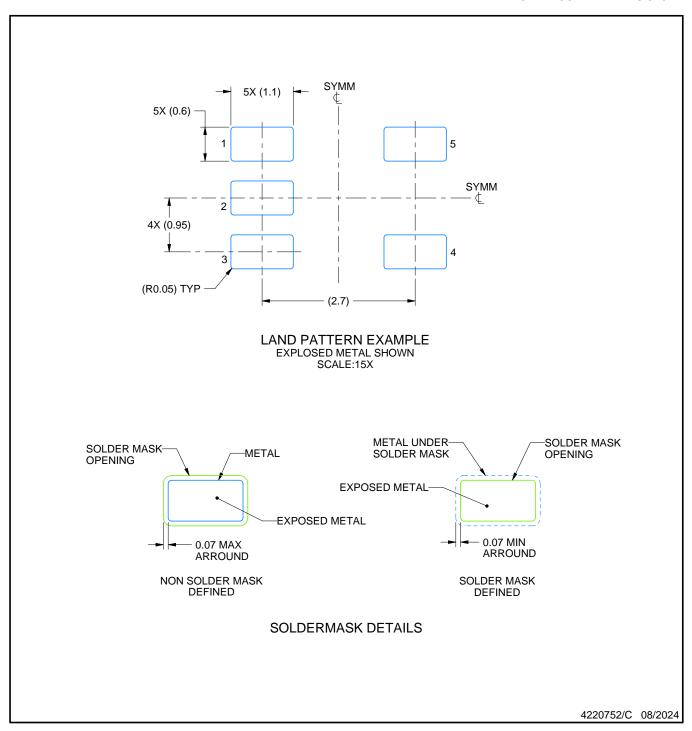
### NOTES:

- All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
   This drawing is subject to change without notice.
   Reference JEDEC MO-193.

- 4. Support pin may differ or may not be present.



SMALL OUTLINE TRANSISTOR

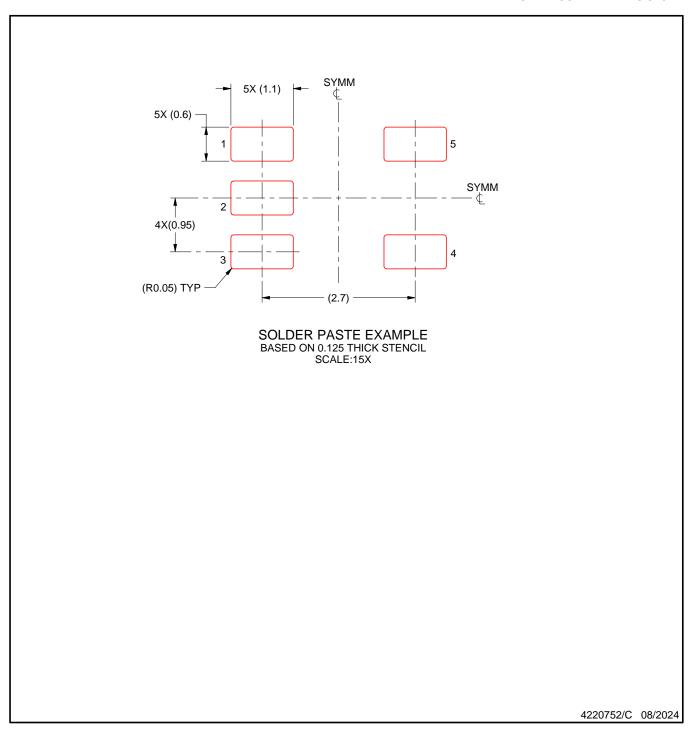


NOTES: (continued)

- 4. Publication IPC-7351 may have alternate designs.
- 5. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SMALL OUTLINE TRANSISTOR



NOTES: (continued)

- 6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

  7. Board assembly site may have different recommendations for stencil design.



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