









**OPA892, OPA2892** JAJSQK2A - NOVEMBER 2023 - REVISED JULY 2024

### OPAx892 2GHz、10V/V ゲイン安定、0.95nV/√Hz、超低 THD オペアンプ

#### 1 特長

- **0.95nV/√Hz** の非常に低い電圧ノイズ
- 高速度:
  - ゲイン帯域幅積:2GHz
  - スルー レート:700V/μs
  - 30ns のセトリング タイム (0.1%)
- **10V/V** 以上のゲインで安定
- 出力駆動、Io = 200mA (標準値)
- 非常に低い歪み:
  - THD = -78dBc (f = 1MHz,  $R_1$  = 150 $\Omega$ )
  - THD+N = -114dBc (f = 1kHz, BW = 80kHz)
- 広範な電源:
  - V<sub>CC</sub> =  $\pm 4.5$ V $\sim \pm 18$ V
- OPA892 のオフセット ヌルピン

#### 2 アプリケーション

- 超音波スキャナ
- ソース メジャー ユニット (SMU)
- 電力品質メータ
- 超音波スキャナ
- ベクトル信号トランシーバ (VST)
- 業務用オーディオミキサまたは制御卓
- 業務用マイク/ワイヤレスシステム
- 業務用スピーカ システム
- 業務用オーディオ アンプ
- サウンドバー
- ターンテーブル
- 業務用ビデオ カメラ
- ギターおよびその他楽器用アンプ
- データ アクイジション (DAQ)

# R- $R_{\text{G}}$ OPA892 低歪み圧電センサ アンプ

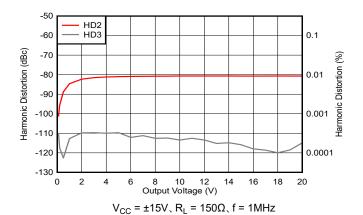
#### 3 概要

OPA892 および OPA2892 (OPAx892) は電圧ノイズが 非常に低い高速電圧帰還アンプで、通信やイメージング など低い電圧ノイズが要求されるアプリケーションに最適 です。シングルアンプの OPA892 とデュアルアンプの OPA2892 は AC 性能が非常に優れており、10V/V のゲ インで 290MHz の帯域幅、700V/μs のスルーレート、 30ns のセトリング タイム (0.1%) を実現します。 OPAx892 は、10 以上および -9 以下のゲインで安定しています。こ れらのアンプには、200mAの大きな駆動能力があり、アン プごとに 7.5mA の電流しか消費しません。f = 1MHz に おいて全高調波歪み (THD) が -68dBc である OPAx892 は、低歪みを必要とするアプリケーション用に設計されて います。広い出力電圧範囲にわたって低歪みを維持する ため、OPAx892 はイメージング、ソナー、オーディオなど の広いダイナミックレンジのアプリケーションに有用です。

#### 製品情報

部品番号	アンプ	パッケージ <sup>(1)</sup>	パッケージ サイズ (2)			
OPA892	1	D (SOIC, 8)	4.9mm × 6mm			
OPA2892	2	DGN (HVSSOP、 8)	3mm × 4.9mm			

- 詳細については、セクション 10 を参照してください。
- パッケージ サイズ (長さ×幅) は公称値であり、該当する場合はピ ンも含まれます。



高調波歪みと ピーク ツー ピークの出力電圧との関係



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### 4 Pin Configuration and Functions

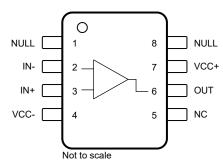


図 4-1. OPA892: D Package, 8-Pin SOIC (Top View)

表 4-1. Pin Functions: OPA892

PIN		TYPE	DESCRIPTION			
NAME	NO.	ITPE	DESCRIPTION			
IN-	2	Input	Inverting input			
IN+	3	Input	oninverting input			
NC	5	_	No connection			
NULL	1, 8	Input	oltage offset adjust			
OUT	6	Output	Output of amplifier			
VCC-	4	_	legative power supply			
VCC+	7	_	Positive power supply			

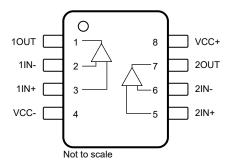


図 4-2. OPA2892: DGN Package, 8-pin HVSSOP (Top View)

表 4-2. Pin Functions: OPA2892

PIN		TYPE	DESCRIPTION	
NAME	NO.	ITPE	DESCRIPTION	
1IN-	2	Input	Channel 1 inverting input	
1IN+	3	Input	Channel 1 noninverting input	
10UT	1	Output	Channel 1 output	
2IN-	6	Input	Channel 2 inverting input	
2IN+	5	Input	Channel 2 noninverting input	
2OUT	7	Output	Channel 2 output	
VCC-	4	_	Negative power supply	
VCC+ 8		_	Positive power supply	
Thermal pad		_	Thermal pad. DGN (HVSSOP) package only. For best thermal performance, connect pad to large copper plane. Thermal pad can be connected to any pin on the device, or any other potential on the board if voltage on thermal pad remains between VCC+ and VCC	

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#### **5 Specifications**

#### 5.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)(1)

			MIN	MAX	UNIT
V <sub>CC</sub>	Supply voltage, V <sub>CC+</sub> – V <sub>CC-</sub>	Supply voltage, V <sub>CC+</sub> – V <sub>CC-</sub>			V
VI	Input voltage			±V <sub>CC</sub>	V
Io	Output current <sup>(2)</sup>			240	mA
V <sub>IO</sub>	Differential input voltage			±1.5	V
I <sub>IN</sub>	Continuous input current	Continuous input current		10	mA
		Any condition		150	
T <sub>J</sub>	Junction temperature	Continuous operation, long-term reliability <sup>(3)</sup>		125	°C
T <sub>stg</sub>	Storage temperature		-65	150	°C

- (1) Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.
- (2) When continuously operating at any output current, do not exceed the maximum junction temperature. Keep the output current less than the absolute maximum rating regardless of time interval.
- (3) The maximum junction temperature for continuous operation is limited by package constraints. Operation greater than this temperature can result in reduced reliability, lifetime of the device, or both.

#### 5.2 ESD Ratings

			VALUE	UNIT
V	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001, all pins <sup>(1)</sup>	±4000	\/
V <sub>(ESD)</sub>	Liectiostatic discriarge	Charged device model (CDM), per ANSI/ESDA/JEDEC JS-002, all pins <sup>(2)</sup>	±1500	v

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

#### 5.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

			MIN	NOM	MAX	UNIT
V	Supply voltage	Dual-supply	±4.5	±15	±18	V
V <sub>CC</sub>		Single-supply	9	30	36	V
T <sub>A</sub>	Operating free-air temperature		-40	25	85	°C

#### 5.4 Thermal Information

		OPA892	OPA2892	
	THERMAL METRIC <sup>(1)</sup>	D (SOIC)	DGN (HVSSOP)	UNIT
		8 PINS	8 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	124.5	52	°C/W
R <sub>0JC(top)</sub>	Junction-to-case (top) thermal resistance	65.0	75.2	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	72.2	24.5	°C/W
$\Psi_{JT}$	Junction-to-top characterization parameter	13.6	4	°C/W
$\Psi_{JB}$	Junction-to-board characterization parameter	71.4	24.5	°C/W
R <sub>0JC(bot)</sub>	Junction-to-case (bottom) thermal resistance	N/A	9.1	°C/W

(1) For information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.

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#### 5.5 Electrical Characteristics

at  $T_A = 25$ °C,  $V_{CC} = \pm 15$  V, and  $R_L = 150$   $\Omega$  (unless otherwise noted)

	PARAMETER	TEST CO	ONDITIONS	MIN TYP I	MAX UNIT
DYNAMI	C PERFORMANCE				
		0 : 40	V <sub>CC</sub> = ±15 V	290	
	Small-signal bandwidth	Gain = 10	V <sub>CC</sub> = ±5 V	250	
	(–3 dB)	O a ira	V <sub>CC</sub> = ±15 V	110	
DIM		Gain = 20	V <sub>CC</sub> = ±5 V	100	
BW		Onitro 40	V <sub>CC</sub> = ±15 V	17	—— MHz
	Bandwidth for 0.1-dB flatness	Gain = 10	V <sub>CC</sub> = ±5 V	17	
	Full manual banduidth(1)	V <sub>O(PP)</sub> = 20 V, V <sub>CC</sub> = ±15 V	1	11.1	
	Full power bandwidth <sup>(1)</sup>	V <sub>O(PP)</sub> = 5 V, V <sub>CC</sub> = ±5 V		31.8	
CD	Slew rate <sup>(2)</sup>	Cain - 40	V <sub>CC</sub> = ±15 V, 20-V step	700	1//
SR	Siew rate (=)	Gain = 10	V <sub>CC</sub> = ±5 V, 5-V step	500	V/μs
	Sottling time to 0.19/	Coin = 10	V <sub>CC</sub> = ±15 V, 5-V step	22	
+	Settling time to 0.1%	Gain = –10	V <sub>CC</sub> = ±5 V, 2-V step	22	nc
t <sub>s</sub>	Cattling time to 0.040/	Coin = 10	V <sub>CC</sub> = ±15 V, 5-V step	160	ns
	Settling time to 0.01%	Gain = –10	V <sub>CC</sub> = ±5 V, 2-V step	160	
AUDIO F	PERFORMANCE				<u>'</u>
	N Total harmonic distortion + noise	Gain = 10, f = 1 kHz, BW = 80 kHz	$V_{CC}$ = ±15 V, $R_{L}$ = 600 $\Omega$ , $V_{O}$ = 3 $V_{RMS}$	-114	dB
				0.0002	%
			$V_{CC} = \pm 15 \text{ V}, R_L = 2 \text{ k}\Omega,$ $V_O = 3 \text{ V}_{RMS}$	-114	dB
THD+N				0.0002	%
I UD+IN			$V_{CC} = \pm 5 \text{ V, R}_{L} = 600 \Omega,$ $V_{O} = 1 \text{ V}_{RMS}$	-106	dB
				0.0005	%
			$V_{CC}$ = ±5 V, $R_L$ = 2 k $\Omega$ , $V_O$ = 1 $V_{RMS}$	-106	dB
				0.0005	%
		Gain = 10, SMPTE/DIN two-tone,	$V_{CC} = \pm 15 \text{ V},$ $V_{O} = 3 \text{ V}_{RMS}, \text{ R}_{L} = 600 \Omega$ $V_{CC} = \pm 15 \text{ V},$ $V_{O} = 3 \text{ V}_{RMS}, \text{ R}_{L} = 2 \text{ k}\Omega$ $V_{CC} = \pm 5 \text{ V},$ $V_{O} = 1 \text{ V}_{RMS}, \text{ R}_{L} = 600 \Omega$	-109	dB
				0.00036	%
				-109	dB
IMD	Intermodulation distortion			0.00036	%
טואוו	intermodulation distortion	4:1 (60 Hz and 7 kHz)		-105	dB
				0.00056	%
			V <sub>CC</sub> = ±5 V,	-105	dB
			$V_O = 1 V_{RMS}, R_L = 2 k\Omega$	0.00056	%
NOISE A	ND DISTORTION PERFORMA	NCE			'
		$V_{O(pp)} = 2 \text{ V, f} = 1 \text{ MHz,}$		-78	
TUD	Tatal la amerania diatantian	gain = 10, V <sub>CC</sub> = ±15 V	R <sub>L</sub> = 1 kΩ	-86	dD.
THD	Total harmonic distortion	V <sub>O(pp)</sub> = 2 V, f = 1 MHz,		-77	dBc
		gain = 10, V <sub>CC</sub> = ±5 V	R <sub>L</sub> = 1 kΩ	-85	
V <sub>n</sub>	Input voltage noise	V <sub>CC</sub> = ±5 V or ±15 V, f > 10	) kHz	0.95	nV/√H:
In	Input current noise	V <sub>CC</sub> = ±5 V or ±15 V, f > 10	) kHz	2.3	pA/√H:
X <sub>T</sub>	Channel-to-channel crosstalk (OPA2892 only)	V <sub>CC</sub> = ±5 V or ±15 V, f = 1	MHz	-54	dBc



#### 5.5 Electrical Characteristics (続き)

at T<sub>A</sub> = 25°C, V<sub>CC</sub> = ±15 V, and R<sub>L</sub> = 150  $\Omega$  (unless otherwise noted)

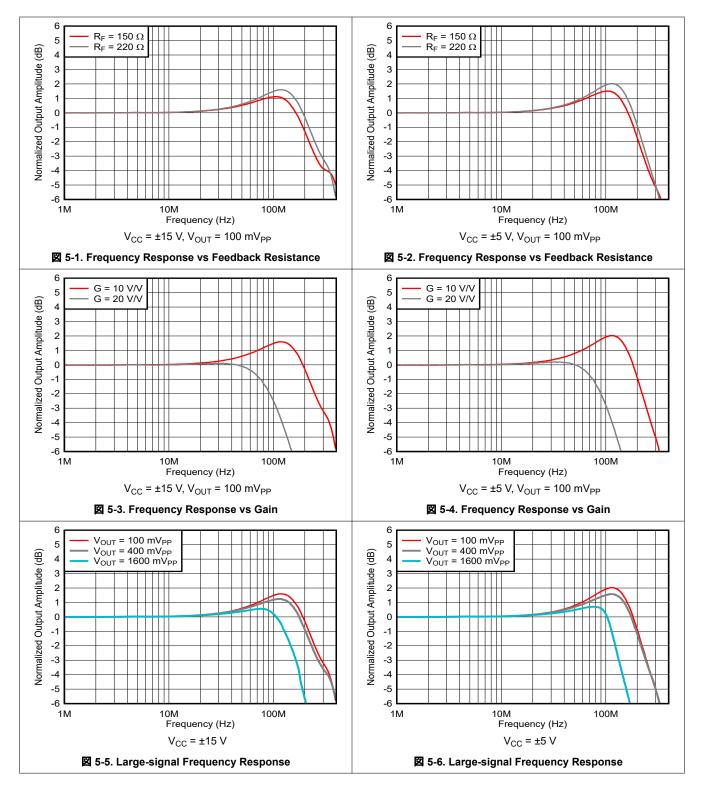
	PARAMETER	TEST CO	NDITIONS	MIN	TYP	MAX	UNIT
DC PER	RFORMANCE						
		V <sub>CC</sub> = ±15 V, V <sub>O</sub> = ±10 V,	T <sub>A</sub> = 25°C	93	100		dB
		R <sub>L</sub> = 1 kΩ	T <sub>A</sub> = full range	92			dB
	Open-loop gain	V <sub>CC</sub> = ±5 V, V <sub>O</sub> = ±2.5 V,	T <sub>A</sub> = 25°C	92	98		dB
		$R_L = 1 k\Omega$	T <sub>A</sub> = full range	91			dB
V <sub>OS</sub>	Input offset voltage	V <sub>CC</sub> = ±5 V or ±15 V, T <sub>A</sub> = 2	5°C		0.2	1	mV
	Offset voltage drift	$V_{CC}$ = ±5 V or ±15 V, $T_A$ = for	ıll range		1		μV/°C
1	Input bias current	V <sub>CC</sub> = ±5 V or ±15 V	T <sub>A</sub> = 25°C		9	20	μA
I <sub>IB</sub>	input bias current	V <sub>CC</sub> - ±3 v 0l ±13 v	T <sub>A</sub> = full range			33	μA
	Input offeet ourrent	V .5V .45V	T <sub>A</sub> = 25°C		30	250	nA
I <sub>OS</sub>	Input offset current	V <sub>CC</sub> = ±5 V or ±15 V	T <sub>A</sub> = full range			400	nA
	Input offset current drift	$V_{CC} = \pm 5 \text{ V or } \pm 15 \text{ V, } T_A = \text{fi}$	ıll range		0.2		nA/°C
INPUT (	CHARACTERISTICS			•			
V	Common-mode input voltage	V <sub>CC</sub> = ±15 V		±13.8	±14.3		V
$V_{ICR}$		V <sub>CC</sub> = ±5 V		±3.8	±4.3		\ \ \
	Common-mode rejection ratio	$V_{CC} = \pm 15 \text{ V}, V_{ICR} = \pm 12 \text{ V}$	T <sub>A</sub> = 25 °C	85	104		- dB
CMRR			T <sub>A</sub> = full range	80			
Civilat		$V_{CC} = \pm 5 \text{ V}, V_{ICR} = \pm 2.5 \text{ V}$	T <sub>A</sub> = 25 °C	90	106		ub ub
		V <sub>CC</sub> - ±3 v, v <sub>ICR</sub> - ±2.3 v	T <sub>A</sub> = full range	85			
	Input impedance	Common-mode			10    1.2		MΩ    pF
	input impedance	Differential-mode			6   1.8		kΩ    pF
OUTPU	T CHARACTERISTICS						
		$V_{CC}$ = ±15 V, $R_L$ = 250 $\Omega$		±12	±12.9		
Vo	Output voltage swing	$V_{CC}$ = ±5 V, $R_L$ = 150 $\Omega$		±3	±3.5		V
<b>v</b> 0	Output voltage swiling	$V_{CC} = \pm 15 \text{ V}, R_L = 1 \text{ k}\Omega$		±13	±13.6		
		$V_{CC}$ = ±5 V, $R_L$ = 1 k $\Omega$	_	±3.4	±3.8		
I <sub>o</sub>	Output current	R <sub>L</sub> = 10 Ω	V <sub>CC</sub> = ±15 V	160	200		mA
-0	Output ourrorn	10 12	V <sub>CC</sub> = ±5 V	120	160		1117 (
R <sub>O</sub>	Output resistance <sup>(3)</sup>	Open-loop			8		Ω
POWER	RSUPPLY						
		V <sub>00</sub> = +15 V	T <sub>A</sub> = 25°C		7.5	10	
loo	Supply current (per amplifier)	V <sub>CC</sub> = ±15 V	T <sub>A</sub> = full range			11	mA
I <sub>CC</sub>	Supply current (per amplifier)	V <sub>CC</sub> = ±5 V	T <sub>A</sub> = 25°C			9	'''
			T <sub>A</sub> = full range		6.5	10	1
PSRR	Power-supply rejection ratio	Voc = +5 V or +15 V	T <sub>A</sub> = 25 °C	90	105		dB
FORK	Power-supply rejection ratio	$V_{CC}$ = ±5 V or ±15 V	T <sub>A</sub> = full range	85			uБ

<sup>(1)</sup> Full-power bandwidth = slew rate /  $[\pi V_{O(P-P)}]$ .

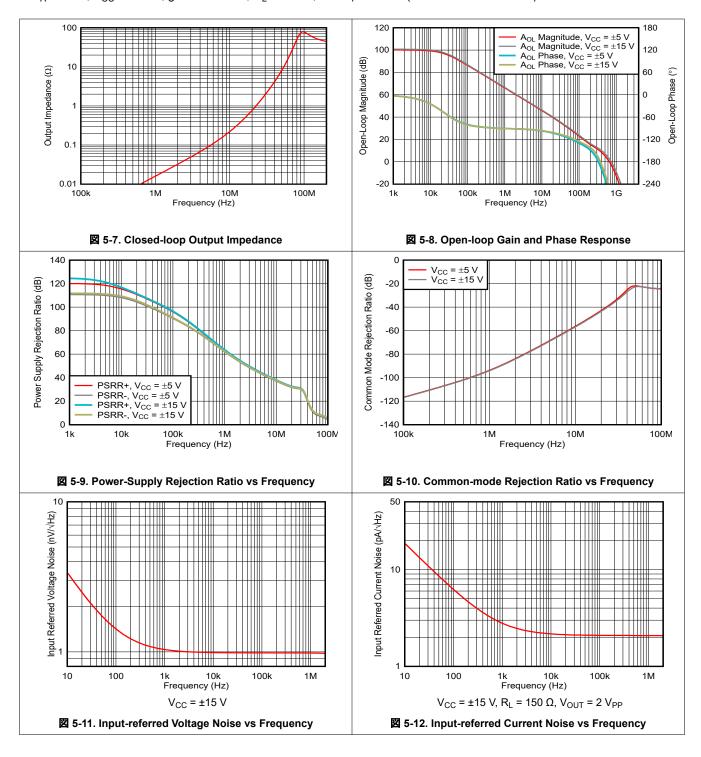
<sup>(2)</sup> Slew rate is measured from an output level range of 25% to 75%.

<sup>(3)</sup> Keep junction temperature less than the absolute maximum rating when the output is heavily loaded or shorted; see also セクション 5.1.

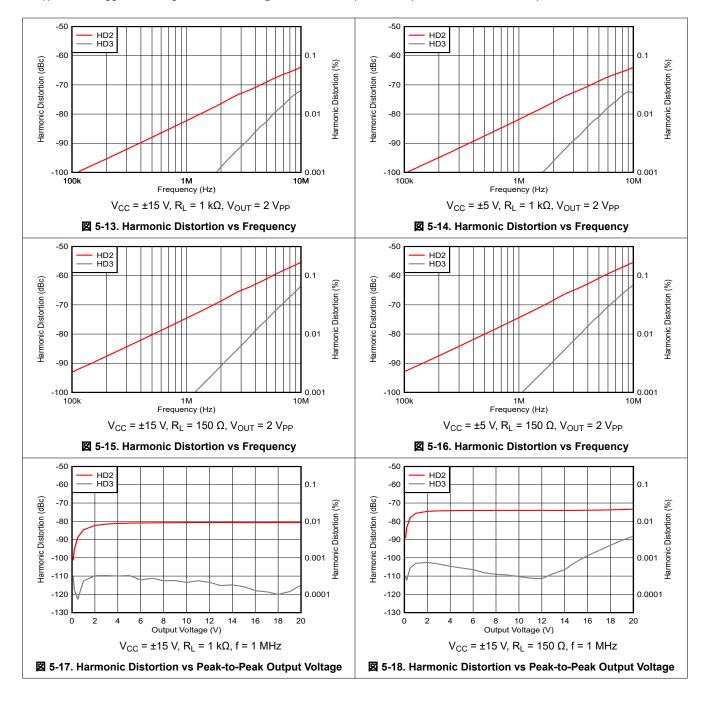
#### 5.6 Typical Characteristics



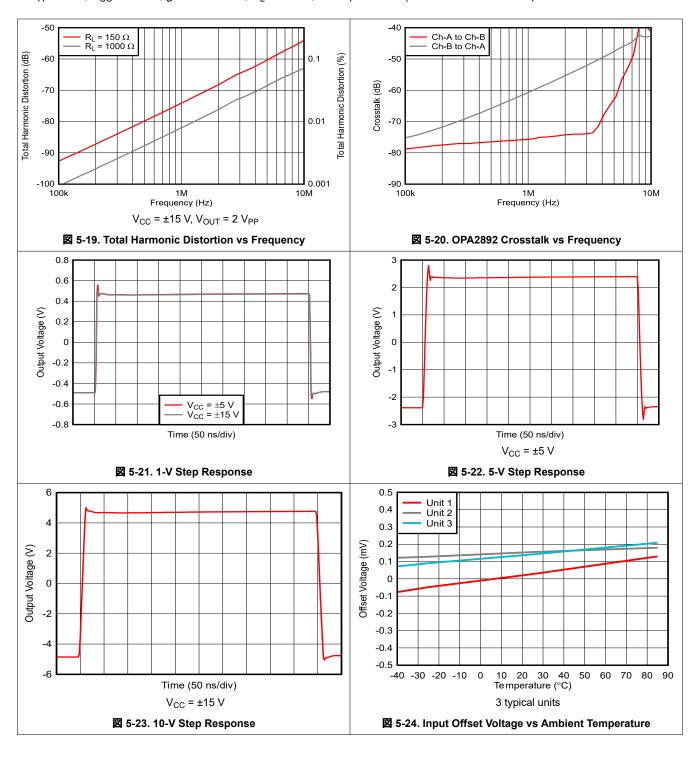




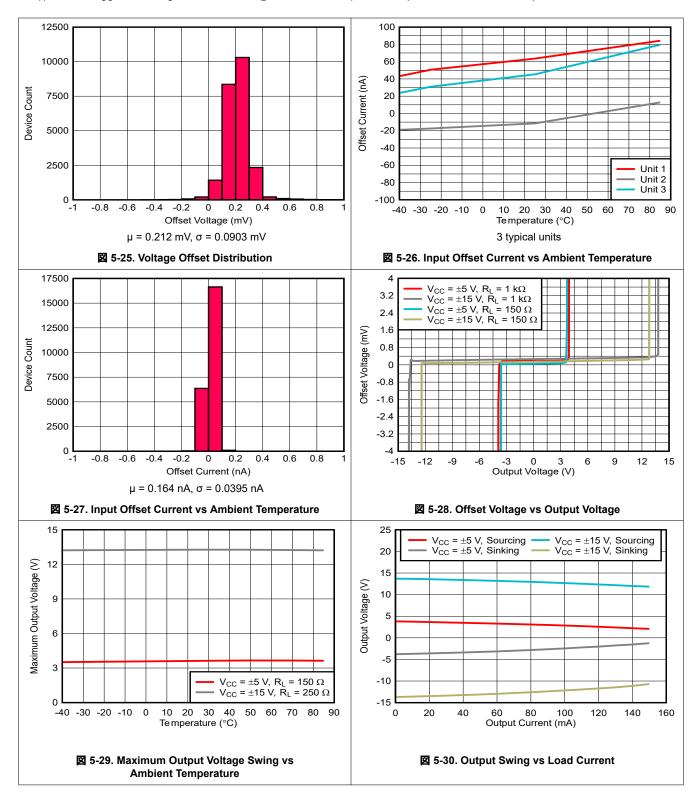




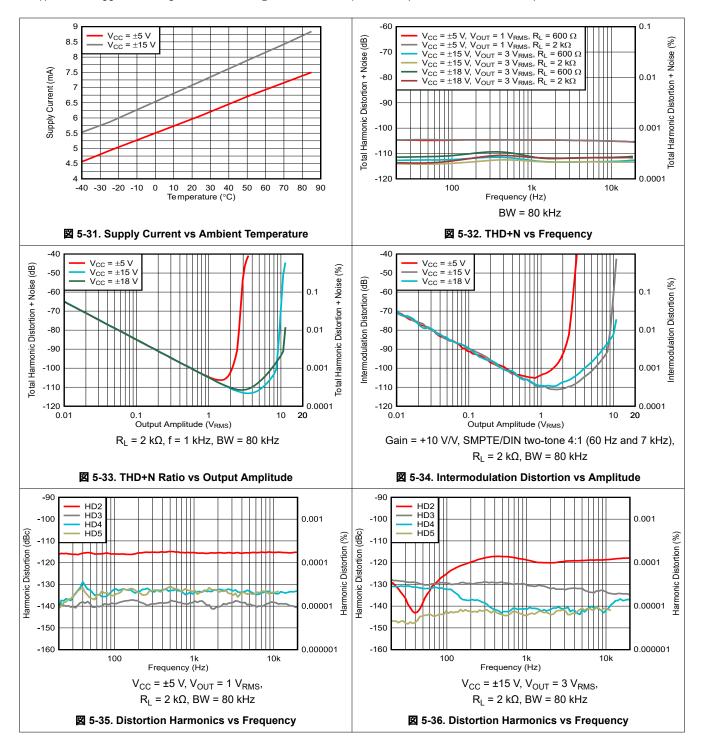




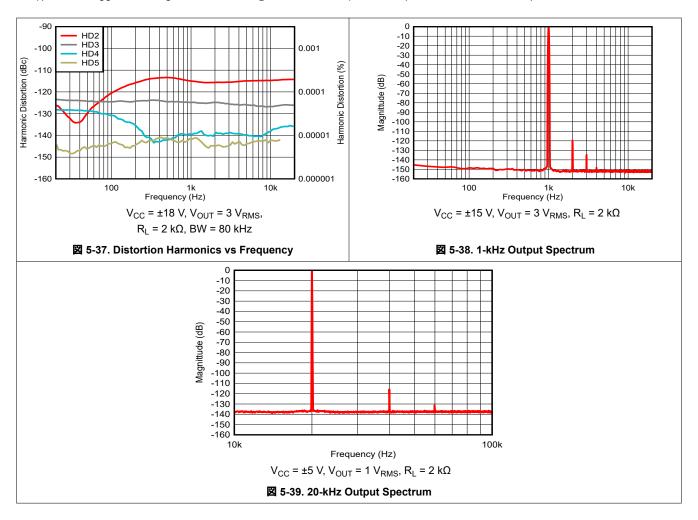














#### **6 Detailed Description**

#### 6.1 Overview

The OPAx892 are high-speed operational amplifiers configured in a decompensated voltage-feedback architecture. The OPAx892 are stable with gain configurations of 10 V/V or greater. These amplifiers are built using a greater than 30-V, complementary, bipolar process with NPN and PNP transistors possessing an  $f_T$  of several GHz. This configuration results in exceptionally high-performance amplifiers with wide bandwidth, high slew rate, fast settling time, and low distortion.

#### **6.2 Functional Block Diagram**

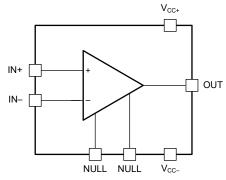


図 6-1. OPA892: Single Channel

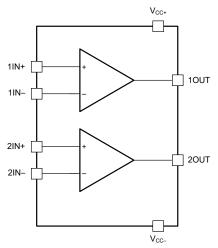


図 6-2. OPA2892: Dual Channel

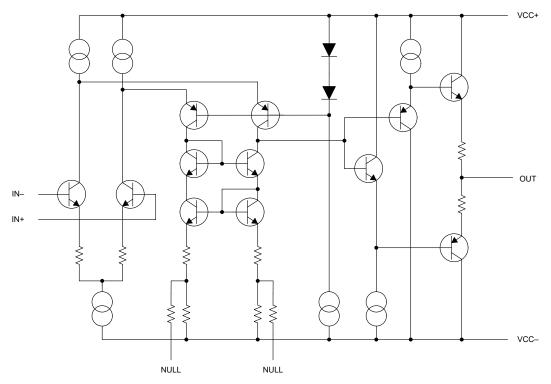


図 6-3. OPA892 Simplified Schematic

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#### **6.3 Feature Description**

#### 6.3.1 Offset Nulling

The OPAx892 have a very low input offset voltage for high-speed amplifiers. However, if additional correction is required, an offset nulling function is provided on the OPA892. To adjust the input offset voltage, place a potentiometer between pin 1 and pin 8 of the device, and tie the wiper to the negative supply. ☒ 6-4 shows this feature.

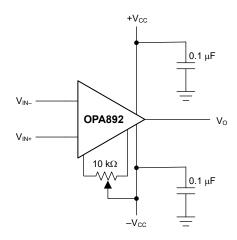


図 6-4. Offset Nulling Schematic

#### **6.4 Device Functional Modes**

The OPAx892 family has a single functional mode and can be used with both single-supply or split power-supply configurations. The power-supply voltage must be greater than  $9 \text{ V} (\pm 4.5 \text{ V})$  and less than  $36 \text{ V} (\pm 18 \text{ V})$ .

#### 7 Application and Implementation

注

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

#### 7.1 Application Information

#### 7.1.1 Driving a Capacitive Load

The OPAx892 are internally compensated to maximize bandwidth and slew-rate performance. To maintain stability, take additional precautions when driving capacitive loads with a high-performance amplifier. As a result of the internal compensation, significant capacitive loading directly on the output node decreases the device phase margin, and potentially lead to high-frequency ringing or oscillations. Therefore, for capacitive loads greater than 10 pF, place an isolation resistor in series with the output of the amplifier.  $\boxtimes$  7-1 shows this configuration. For most applications, a minimum resistance of 20  $\Omega$  is recommended. In 75- $\Omega$  transmission systems, setting the series resistor value to 75  $\Omega$  is a beneficial choice because this value isolates any capacitance loading and provides source impedance matching.

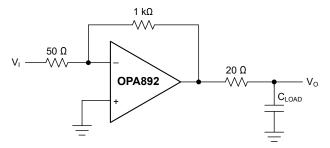


図 7-1. Driving a Capacitive Load

#### 7.1.2 General Configuration

When receiving low-level signals, limiting the bandwidth of the incoming signals into the system is often required. Z 7-2 shows how the simplest way to accomplish this limiting is to place an RC filter at the noninverting pin of the amplifier.

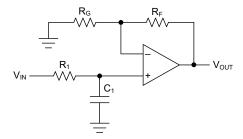


図 7-2. Single-Pole Low-Pass Filter

$$\frac{V_{OUT}}{V_{IN}} = \left(1 + \frac{R_F}{R_C}\right) \times \left(\frac{1}{1 + sR_1C_1}\right) \tag{1}$$

#### 7.2 Typical Application

One important characteristic of the OPAx892 amplifier is the decompensated architecture. By pushing out the dominate pole to a higher frequency using this common technique, the amplifier is no longer stable in lower gain configurations. The minimum stable gain for the OPAx892 is specified to be 10 V/V. When a lower gain is needed in a preamp or buffer application, a related product to be considered is the OPA891. Because the OPA891 is not decompensated, the gain-bandwidth product is approximately an order of magnitude lower than the OPAx892. Both of these amplifiers have similar noise performance, but the best bandwidth and distortion performance comes from using the correct amplifier depending on the gain needs of the application.

When applications require gain of 10 V/V or larger, choose the OPAx892 to obtain a low value of harmonic distortion and THD+N. Z 7-3 shows a where in the analog signal chain this type of amplification can be required. Often found in applications such as ultrasound, audio, and sonar, a preamp is used near the input sensor to boost the signal to a more practical level with an emphasis on keeping noise and distortion as small as possible. Later in the signal chain, significantly more gain can be required to provide for other required functions such analog filtering, mixing, splitting, or just the need to match the signal level to a following device. An amplifier such as the OPAx892 maintains the fidelity of the signal by providing the needed gain with significantly impacting distortion over a wide bandwidth and output swing. Z 7-4 shows the amplifier design example. The amplification stage provides an additional 10 V/V of gain to the analog signal chain.

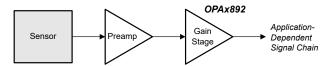


図 7-3. Gain Stage in an Analog-Front-End Block Diagram

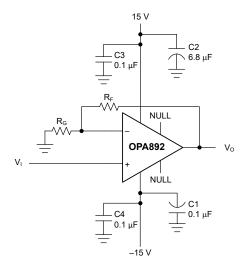


図 7-4. Noninverting Gain Configuration

#### 7.2.1 Design Requirements

The objective is to design a 10 V/V amplifier to be for a mid-stage amplifier that minimizes the THD of the signal over the output range shown in 表 7-1.

表 7-1. Design Parameters

<u> </u>				
PARAMETER	VALUE			
Supply voltage	±15 V			
Voltage gain	+10 V/V			
Small-signal peaking	< 2 dB			
Load resistance	1 kΩ			

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#### 7.2.2 Detailed Design Procedure

Set the gain to 10 V/V by the proper selection of the two resistors using equation  $\pm$  2. In this example, set the ratio of the resistance to 9 to obtain the design goal of a gain of 10. There exists a second degree of freedom that allows the absolute value to be somewhat arbitrary while maintaining the specified ratio of resistor values. Increasing feedback resistance leads to an increase in the amount of overshoot in the small-signal frequency response (see  $\pm$  5-1). In the time domain, the impact shows up as and increase in ringing and settling time for step-function input signals. If the resistances are very small, power dissipation effects increase.

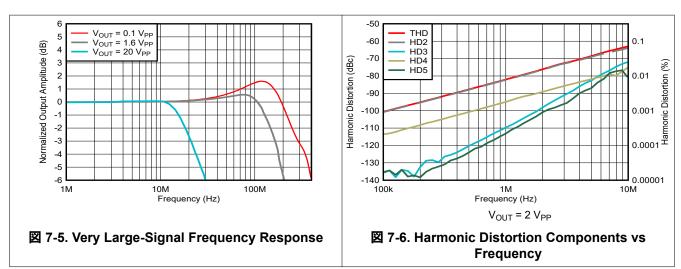
gain = 
$$\frac{V_0}{V_1} = 1 + \frac{R_F}{R_C}$$
 (2)

The best practice is to chose the resistors to be in of moderate values to avoid the detrimental effects at both extremes. Choosing  $R_F = 220~\Omega$  is a good compromise in between these two extremes. Using  $\stackrel{>}{\not\sim}$  2, the corresponding gain resistor is found to be 24  $\Omega$ . The amount of small-signal peaking is a modest 1.5 dB (see  $\boxtimes$  5-1), which meets the design goal.

A unique feature of this amplifier family is the output stage has been designed to drive a substantial amount of output current. This choice allows for the OPAx892 to maintain significant bandwidth even with very large input signals.  $\boxtimes$  7-5 shows the modest reduction of bandwidth, even for output signals as large as 20 V<sub>PP</sub>. The time domain impact of this feature is a more precise amplification (that is, lower distortion) even for large dynamic range input signals.

Using the amplifier designed in this section,  $\boxtimes$  7-6 shows the measured components of THD down to the 5th harmonic. The figure shows that the 2nd harmonic dictates the THD performance, with the 4th harmonic being the next highest component. Other amplifiers can produce low distortion at lower input levels but distortion rapidly rises as the output amplitude rises.  $\boxtimes$  5-17 shows the harmonic distortion stays approximately constant, even at large values of output amplitude, making the OPAx892 a solid choice for large amplitude applications where distortion and noise are critical considerations.

#### 7.2.3 Application Curves



#### 7.3 Power Supply Recommendations

The OPAx892 devices are designed to operate on power supplies ranging from  $\pm 4.5$  V to  $\pm 16$  V (single-ended supplies of 9 V to 32 V). Use a power-supply accuracy of 5% or better. When operated on a board with high-speed digital signals, provide isolation between digital signal noise and the analog input pins. The OPAx892 are connected to the positive power supply ( $V_{CC-}$ ) through pin 7 and pin 8, respectively. Both devices use pin 4 for the negative power supply ( $V_{CC-}$ ). Decouple each supply pin to GND as close to the device as possible.

#### 7.4 Layout

#### 7.4.1 Layout Guidelines

To achieve the levels of high-frequency performance of the OPAx892, follow proper printed-circuit board (PCB), high-frequency design techniques. The following is a general set of guidelines. In addition, a OPAx892 evaluation board is available to use as a guide for layout or for evaluating the device performance.

- **Ground planes**—ensure that the ground plane used on the board provides all components with a low-inductive ground connection. However, in the areas of the amplifier inputs and output, the ground plane can be removed to minimize stray capacitance.
- **Proper power-supply decoupling**—use a 6.8-µF tantalum capacitor in parallel with a 0.1-µF ceramic capacitor on each supply pin. Sharing the tantalum capacitor among several amplifiers is possible depending on the application, but always use a 0.1-µF ceramic capacitor on the supply pin of every amplifier. In addition, place the 0.1-µF capacitor as close as possible to the supply pin. As this distance increases, the inductance in the connecting trace makes the capacitor less effective. Strive for distances of less than 0.1 inch (2.54 mm) between the device power pins and the ceramic capacitors.
- Short trace runs or compact part placements—optimized high-frequency performance is achieved when
  stray series inductance has been minimized. To realize this, make the circuit layout as compact as possible,
  thereby minimizing the length of all trace runs. Pay particular attention to the inputs of the amplifier, keeping
  the trace lengths as short as possible. This layout helps to minimize stray capacitance at the input of the
  amplifier.

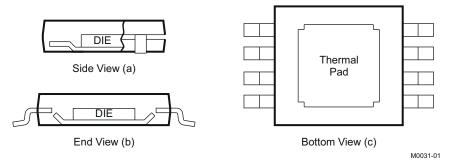
#### 7.4.1.1 General PowerPAD™ Integrated Circuit Package Design Considerations

The OPAx892 is available in a thermally-enhanced DGN package, which is a member of the PowerPAD integrated circuit package family.  $\boxtimes$  7-7 **a** and  $\boxtimes$  7-7 **b** show that this package is constructed using a downset leadframe upon which the die is mounted.  $\boxtimes$  7-7 **c** that this arrangement results in the leadframe being exposed as a thermal pad on the underside of the package. Because this thermal pad has direct thermal contact with the die, excellent thermal performance can be achieved by providing a good thermal path away from the thermal pad.

The PowerPAD integrated circuit package allows for both assembly and thermal management in one manufacturing operation. During the surface-mount solder operation (when the leads are being soldered), the thermal pad can also be soldered to a copper area underneath the package. Through the use of thermal paths within this copper area, heat can be conducted away from the package into either a ground plane or other heat dissipating device.

The PowerPAD integrated circuit package represents a breakthrough in combining the small area and ease of assembly of the surface mount with the previously awkward mechanical methods of heat sinking.

More complete details of the PowerPAD integrated circuit package installation process and thermal management techniques are found in *PowerPAD Thermally-Enhanced Package*. This document is found on the TI website (www.ti.com) by searching on the keyword PowerPAD. The document can also be ordered through your local TI sales office; refer to SLMA002 when ordering.

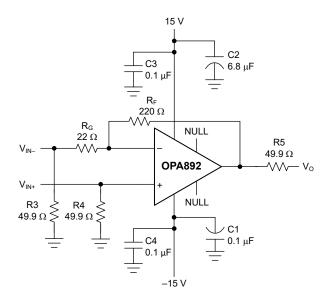


NOTE: The thermal pad (PowerPAD integrated circuit package) is electrically isolated from all other pins and can be connected to any potential from  $V_{CC-}$  to  $V_{CC+}$ . Typically, the thermal pad is connected to the ground plane because this plane tends to physically be the largest and is able to dissipate the most amount of heat.

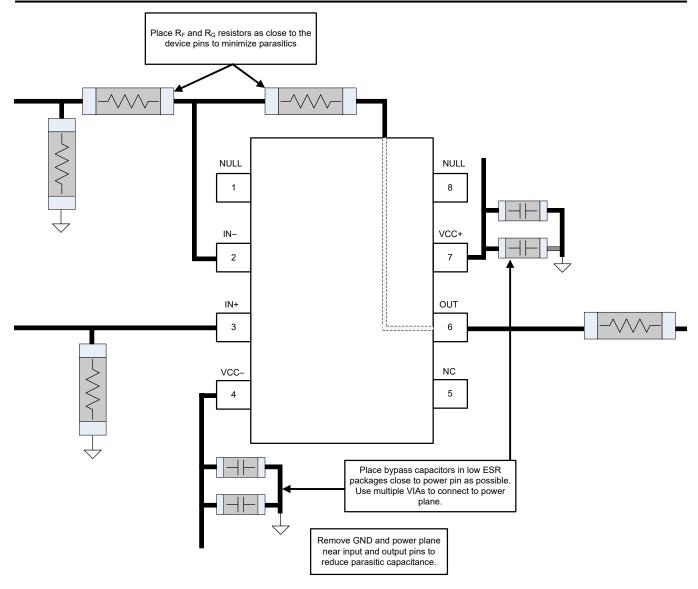
☑ 7-7. Views of Thermally-Enhanced DGN Package



#### 7.4.2 Layout Example







☑ 7-8. Layout Recommendations

#### 8 Device and Documentation Support

TI offers an extensive line of development tools. Tools and software to evaluate the performance of the device, generate code, and develop solutions are listed below.

#### 8.1 Documentation Support

#### 8.1.1 Related Documentation

For related documentation, see the following:

- Texas Instruments, Noise Analysis in Operational Amplifier Circuits application report
- Texas Instruments, PowerPAD Thermally Enhanced Package application report
- Texas Instruments, Single op-amp evaluation module for SO-8 packageusers guide
- Texas Instruments, Dual op-amp evaluation module for SO-8 package users guide
- Texas Instruments, Dual op amp evaluation module for MSOP-8 package users guide

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#### 8.6 用語集

テキサス・インスツルメンツ用語集 この用語集には、用語や略語の一覧および定義が記載されています。

### 9 Revision History

資料番号末尾の英字は改訂を表しています。その改訂履歴は英語版に準じています。

#### Changes from Revision \* (November 2023) to Revision A (July 2024) Page

Product Folder Links: OPA892 OPA2892

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#### 10 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

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Orderable part number	Status	Material type	Package   Pins	Package qty   Carrier	RoHS	Lead finish/	MSL rating/	Op temp (°C)	Part marking	
	(1)	(2)			(3)	Ball material	Peak reflow		(6)	
						(4)	(5)			
OPA2892DGNR	Active	Production	HVSSOP (DGN)   8	3000   LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 85	2892	
OPA2892DGNR.B	Active	Production	HVSSOP (DGN)   8	3000   LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 85	2892	
OPA892DR	Active	Production	SOIC (D)   8	3000   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	O892	
OPA892DR.B	Active	Production	SOIC (D)   8	3000   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	O892	

<sup>(1)</sup> Status: For more details on status, see our product life cycle.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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<sup>(5)</sup> MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

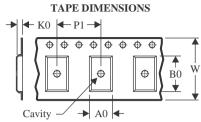
<sup>(6)</sup> Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

### **PACKAGE MATERIALS INFORMATION**

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#### TAPE AND REEL INFORMATION





A0	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

#### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



#### \*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
OPA2892DGNR	HVSSOP	DGN	8	3000	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
OPA892DR	SOIC	D	8	3000	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1

### **PACKAGE MATERIALS INFORMATION**

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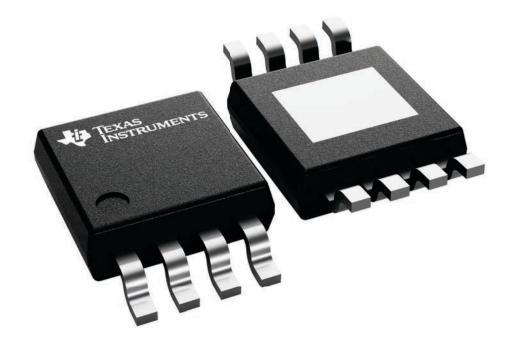
#### \*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)	
OPA2892DGNR	HVSSOP	DGN	8	3000	353.0	353.0	32.0	
OPA892DR	SOIC	D	8	3000	353.0	353.0	32.0	

3 x 3, 0.65 mm pitch

SMALL OUTLINE PACKAGE

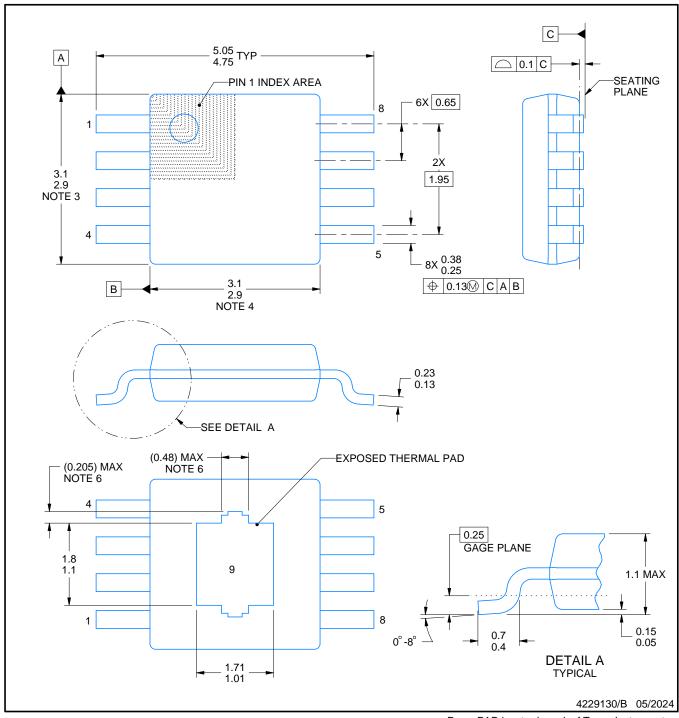
This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.



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## PowerPAD<sup>™</sup> VSSOP - 1.1 mm max height

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#### NOTES:

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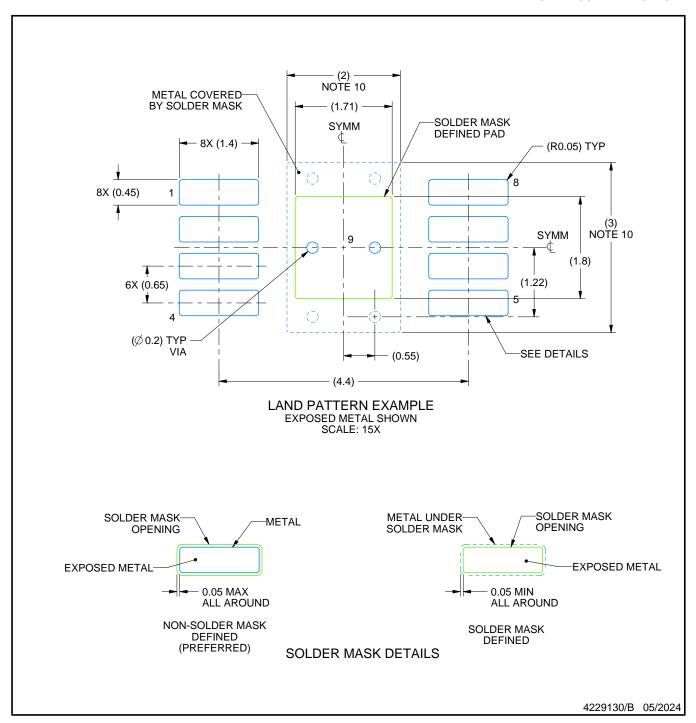
- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.

  2. This drawing is subject to change without notice.

  3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not
- exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- 5. Reference JEDEC registration MO-187.
- 6. Features may differ or may not be present.



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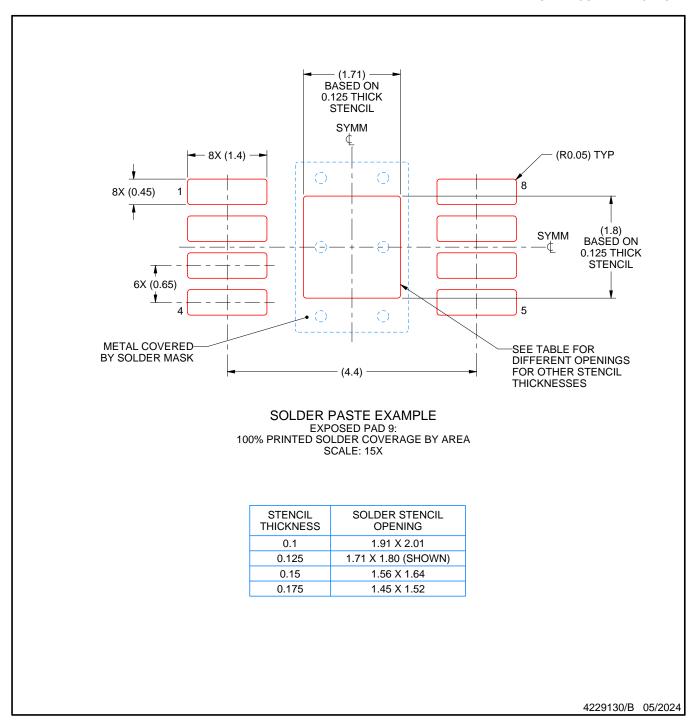


NOTES: (continued)

- 7. Publication IPC-7351 may have alternate designs.
- 8. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 9. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
- 10. Size of metal pad may vary due to creepage requirement.



SMALL OUTLINE PACKAGE



NOTES: (continued)

- 11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 12. Board assembly site may have different recommendations for stencil design.





SMALL OUTLINE INTEGRATED CIRCUIT



#### NOTES:

- 1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.



SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SMALL OUTLINE INTEGRATED CIRCUIT



NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.



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