



LPV521



JAJSS82E - AUGUST 2009 - REVISED JULY 2024

LPV521 ナノパワー、1.8V、RRIO、CMOS 入力オペアンプ

1 特長

V_S = 5V (特に記載のない限り標準値):

- 電源電流 (V_S = 0.3V 時):400nA (最大値)

- 動作電圧範囲:1.6V~5.5V

- 低い TCV_{OS}:3.5µV/°C (最大値)

- Vos:1mV (最大値)

- 入力バイアス電流:40fA

- PSRR:109dB - CMRR:102dB

開ループ ゲイン:132dB

- ゲイン帯域幅積:6.2kHz

- スルーレート: 2.4V/ms

- 入力電圧ノイズ (f = 100Hz 時): 255nV/√Hz

- 温度範囲:-40℃~+125℃

2 アプリケーション

- ワイヤレス環境センサ
- グリッド アセット監視
- 雷気メータ
- 煙探知器と熱探知器
- ガス検出器
- ポータブル エレクトロニクス
- サーモスタット
- フィールドトランスミッタとセンサ

3 概要

LPV521 は、非常に長いバッテリ寿命を必要とするアプリ ケーション向けに設計されたシングル ナノパワー 552nW アンプです。1.6V~5.5V の動作電圧範囲と標準 351nA の消費電流の組み合わせにより、RFID リーダーやリモー トセンサなどのナノパワーアプリケーションに最適です。 入力同相モード電圧はレール全体にわたって 0.1V であ り、TCVos が保証され、レールツーレールの電圧出力性 能を備えています。LPV521 の CMOS 入力段は注意深 く設計され、標準で 40fA という低い I_{BIAS} 電流によって競 合製品に差を付けています。この低い入力電流により、メ グオーム抵抗や高インピーダンスのフォトダイオード、充電 センスなどの状況で生じる、I_{BIAS} や I_{OS} の誤差が大きく減 少します。LPV521 は PowerWise® ファミリの製品であ り、電力対性能比が非常に優れています。

広い入力同相モード電圧範囲、保証された 1mV の Vos および 3.5µV/℃の TCVos により、ハイサイドとローサイド 両方の電流センシングで正確で安定した測定を実現しま す。

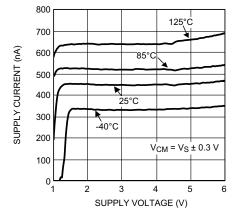
また、EMI 保護が組み込まれ、携帯電話や他の RFID リ ーダーからの不要な RF 信号による影響を低減していま す。

LPV521 は、5 ピン SC70 および 8 ピン PDIP パッケー ジで供給されます。

パッケージ情報

部品番号	パッケージ ⁽¹⁾	パッケージ サイズ ⁽²⁾	
I PV521	DCK (SC70, 5)	2mm × 2.1mm	
LI VSZ I	P (PDIP、8)	9.81mm × 9.43mm	

- 詳細については、セクション 10 を参照してください。
- パッケージ サイズ (長さ×幅) は公称値であり、該当する場合はピ ンも含まれます。



NanoPower の消費電流



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4 Pin Configuration and Functions

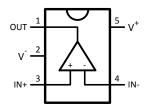


図 4-1. DCK Package, 5-Pin SC70 (Top View)

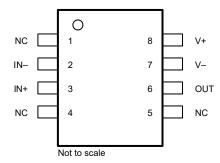


図 4-2. P Package, 8-Pin PDIP (Top View)

表 4-1. Pin Functions

PIN				
NAME	NO) .	TYPE	DESCRIPTION
INAIVIE	DCK (SC70)	P (PDIP)		
IN+	3	3	Input	Noninverting input
IN-	4	2	Input	Inverting input
OUT	1	6	Output	Output
NC	_	1, 4, 5	_	Do not connect
V+	5	8	Power	Positive power supply
V-	2	7	Power	Negative power supply



5 Specifications

5.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)(1)

			MIN	MAX	UNIT
	Any pin relative to V ⁻		-0.3	6	V
	Input voltage, IN+, IN-, C	OUT pins	V ⁻ - 0.3	V ⁺ + 0.3	V
	Input current, V+, V-, OU	T pins		40	mA
	Differential input voltage	Differential input voltage (V _{IN+} – V _{IN-})		300	mV
TJ	Junction temperature ⁽²⁾		-40	150	°C
	Mounting temperature	Infrared or convection (30s)		260	°C
	Woulding temperature	Wave soldering lead temperature (4s)		260	°C
T _{stg}	Storage temperature		-65	150	°C

- (1) Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.
- (2) The maximum power dissipation is a function of TJ(MAX), θJA. The maximum allowable power dissipation at any ambient temperature is PD = (TJ(MAX) TA) / θJA. All numbers apply for packages soldered directly onto a printed circuit board (PCB).

5.2 ESD Ratings

			VALUE	UNIT
DCK (S	C70) PACKAGE			
		Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	±2000	
V _(ESD)	Electrostatic discharge	Charged device model (CDM) per JEDEC specification JESD22-C101 ⁽²⁾	±1000	V
		Machine model	±200	
P (PDIP	PACKAGE			
		Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	±2000	
V _(ESD)	Electrostatic discharge	Charged device model (CDM) per ANSI/ESDA/JEDEC JS-002 ⁽²⁾	±1000	V
		Machine model	±200	

- (1) JEDEC document JEP155 states that 500V HBM allows safe manufacturing with a standard ESD control process.
- (2) JEDEC document JEP157 states that 250V CDM allows safe manufacturing with a standard ESD control process.

5.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)(1)

		MIN	NOM	MAX	UNIT
Vs	Supply voltage, $V_S = (V+) - (V-)$	1.6		5.5	V
T _A	Temperature ⁽²⁾	-40		125	°C

- (1) Absolute Maximum Ratings indicate limits beyond which damage may occur. Recommended Operating Conditions indicate conditions for which the device is intended to be functional, but specific performance is not tested. For tested specifications and test conditions, see Electrical Characteristics.
- (2) The maximum power dissipation is a function of TJ(MAX), θJA. The maximum allowable power dissipation at any ambient temperature is PD = (TJ(MAX) TA) / θJA. All numbers apply for packages soldered directly onto a PCB.



5.4 Thermal Information

		LPV	/521	
	THERMAL METRIC ⁽¹⁾	DCK (SC70)	P (PDIP)	UNIT
		5 PINS	8 PINS	
R _{θJA}	Junction-to-ambient thermal resistance ⁽²⁾	456	102.3	°C/W
R _{0JC(top)}	Junction-to-case(top) thermal resistance	53.9	81.2	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	48.9	64.9	°C/W
Ψлт	Junction-to-top characterization parameter	6.6	47.6	°C/W
ΨЈВ	Junction-to-board characterization parameter	48.3	64.1	°C/W
R _{θJC(bot)}	Junction-to-case(bottom) thermal resistance	N/A	N/A	°C/W

⁽¹⁾ For information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.

5.5 Electrical Characteristics

at T_A = 25°C, V^+ = 1.8V, 3.3V, and 5V, V^- = 0V, V_{CM} = V_O = V_S / 2, and R_L > 1 $M\Omega$ (unless otherwise noted)⁽¹⁾

	PARAMETER	TEST CONDITIONS		MIN	TYP	MAX	UNIT
OFFSET	VOLTAGE						
		\/ -\/=\0.2\/		-1	0.1	1	
.,	Innut offeet velters	$V_{CM} = V^- + 0.3V$	$T_A = -40^{\circ}\text{C to } +125^{\circ}\text{C}$	-1.23		1.23	mV
Vos	Input offset voltage	V _{CM} = V ⁺ – 0.3V		-1	0.1	1	mv
		V _{CM} = V - 0.3V	$T_A = -40^{\circ}\text{C to } +125^{\circ}\text{C}$	-1.23		1.23	
					±0.4		
TCVos	Input offset voltage drift ⁽²⁾	$T_A = -40^{\circ}\text{C to } +125^{\circ}\text{C}$	V ⁺ = 1.8V, 3.3V	-3		3	μV/°C
		1 _A = -40 C t0 +125 C	V ⁺ = 5V	-3.5		3.5	
PSRR	Power-supply rejection	1.6V ≤ V ⁺ ≤ 5.5V,		85	109		dB
PSKK	ratio	V _{CM} = 0.3V	T _A = -40°C to +125°C	76			ав
INPUT E	SIAS CURRENT	1	'	,		•	
		V ⁺ = 1.8V, 3.3V		-1	0.01	1	
I _{BIAS}	Input bias current	V ⁺ = 5V		-1	0.04	1	pA
		T _A = -40°C to +125°C		-50		+50	
		V ⁺ = 1.8V			10		
Ios	Input offset current	V ⁺ = 3.3V			20		fA
		V ⁺ = 5V			60		
NOISE				•		<u> </u>	
	Input-referred voltage	V ⁺ = 1.8V			24		.,
	noise	V ⁺ = 3.3V, 5V			22		μV_{PP}
			V ⁺ = 1.8V		265		
e _n	Input-referred voltage noise density	f = 100Hz	V ⁺ = 3.3V		259		nV/√ Hz
	Tiolog deligity		V ⁺ = 5V		255		
i _n	Input-referred current noise	f = 100Hz	'		100		fA/√ Hz

⁽²⁾ The maximum power dissipation is a function of TJ(MAX), θJA. The maximum allowable power dissipation at any ambient temperature is PD = (TJ(MAX) – TA) / θJA. All numbers apply for packages soldered directly onto a PCB.

5.5 Electrical Characteristics (続き)

at $T_A = 25^{\circ}C$, $V^+ = 1.8V$, 3.3V, and 5V, $V^- = 0V$, $V_{CM} = V_O = V_S / 2$, and $R_L > 1 M\Omega$ (unless otherwise noted)⁽¹⁾

	PARAMETER	TEST	CONDITIONS	MIN	TYP	MAX	UNIT
NPUT V	OLTAGE						
			V+ = 1.8V	66	92		
			V ⁺ = 1.8V, T _A = -40°C to +125°C	60			
		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	V+ = 3.3V	72	97		
		$V^- \le V_{CM} \le V^+$	V ⁺ = 3.3V, T _A = -40°C to +125°C	70			
			V+ = 5V	75	102		
			V ⁺ = 5V, T _A = -40°C to +125°C	74			
			V+ = 1.8V	75	101		
			V ⁺ = 1.8V, T _A = -40°C to +125°C	74			
	Common-mode rejection		V+ = 3.3V	78	106		
CMRR	ratio	$V^{-} \le V_{CM} \le V^{+} - 1.1V$	V+ = 3.3V, T _A = -40°C to +125°C	75			dB
			V+ = 5V	84	108		
			V ⁺ = 5V, T _A = -40°C to +125°C	80			
			V ⁺ = 1.8V	75	120		
			V ⁺ = 1.8V, T _A = -40°C to +125°C	53			
			V ⁺ = 3.3V	77	121		
		$V^{+} - 0.6V \le V_{CM} \le V^{+}$	V ⁺ = 3.3V, T _A = -40°C to +125°C	76	.=.		
			V ⁺ = 5V	77	115		
			$V^+ = 5V$, $T_A = -40^{\circ}C$ to $+125^{\circ}C$	76			
		V ⁺ = 1.8V, CMRR ≥ 67dB, V ⁺ = 3.3V, CMRR ≥ 72dB, V ⁺ = 5V, CMRR ≥ 75dB	0 00, 14 10 0 10 120 0	(V ⁻) - 0.1		(V ⁺) + 0.1	V
CMVR Common-mode voltage range		$T_A = -40^{\circ}\text{C to } +125^{\circ}\text{C},$ $V^+ = 1.8V, \text{ CMRR} \ge 60\text{dB},$ $V^+ = 3.3V, \text{ CMRR} \ge 70\text{dB},$ $V^+ = 5V, \text{ CMRR} \ge 74\text{dB}$		(V-)		(V ⁺)	V
PEN-L	OOP GAIN						
			V+ = 1.8V	74	125		
		$V^- + 0.5V \le V_0 \le V^+ - 0.5V$, $R_L = 100k\Omega \text{ to } V^+/2$	V ⁺ = 1.8V, T _A = -40°C to +125°C	73			
			V+ = 3.3V	82	120		dB
A _{VOL}	Large-signal voltage gain		V ⁺ = 3.3V, T _A = -40°C to +125°C	76			
			V+ = 5V	84	132		
			V+ = 5V, T _A = -40°C to +125°C	76			
REQUE	ENCY RESPONSE						
			V+ = 1.8V		6.1		
SBW	Gain bandwidth product	$C_L = 20 pF, R_L = 100 k\Omega$	V+ = 3.3V, 5V		6.2		kHz
			V ⁺ = 1.8V		2.9		
		Falling edge, A _V = +1,	V+ = 3.3V		2.9		
		V _{IN} = V ⁺ to V ⁻	V+ = 5V	1.1	2.7		
			V ⁺ = 5V, T _A = -40°C to +125°C	1.2			
SR	Slew rate		V ⁺ = 1.8V		2.3		V/ms
		Rising edge, A _V = +1,	V ⁺ = 3.3V		2.5		
		Kising edge, $A_V = +1$, $V_{IN} = V^-$ to V^+	V ⁺ = 5V	1.1	2.4		
			$V^{+} = 5V$, $T_{A} = -40^{\circ}$ C to +125°C	1.2			
			V+ = 1.8V	1.2	72		
) _m	Phase margin	$C_L = 20 pF, R_L = 100 k\Omega$	V+ = 3.3V, 5V		73		deg
			V = 3.3V, 3V V+ = 1.8V, 3.3V		19		
G _m	Gain margin	$C_L = 20pF, R_L = 100k\Omega$					dB
			V+ = 5V		20		



5.5 Electrical Characteristics (続き)

at $T_A = 25^{\circ}$ C, $V^+ = 1.8$ V, 3.3V, and 5V, $V^- = 0$ V, $V_{CM} = V_O = V_S / 2$, and $R_L > 1$ M Ω (unless otherwise noted)⁽¹⁾

	PARAMETER	TES"	T CONDITIONS	MIN	TYP	MAX	UNIT
OUTPUT	-		'				
			V ⁺ = 1.8V		2	50	
			V ⁺ = 1.8V, T _A = -40°C to +125°C			50	
		Swing from positive rail,	V+ = 3.3V		3	50	
		$R_L = 100k\Omega \text{ to V}^+/2,$ $V_{IN}(\text{diff}) = 100\text{mV}$	$V^+ = 3.3V$, $T_A = -40$ °C to $+125$ °C			50	
			V+ = 5V		3	50	
.,	Output valtage		V ⁺ = 5V, T _A = -40°C to +125°C			50	mV
Vo	Output voltage		V+ = 1.8V		2	50	IIIV
			V ⁺ = 1.8V, T _A = -40°C to +125°C			50	
		Swing from negative rail, $R_L = 100k\Omega$ to $V^+/2$, $V_{IN}(diff) = -100mV$	V+ = 3.3V		2	50	
			$V^+ = 3.3V$, $T_A = -40$ °C to $+125$ °C			50	
			V+ = 5V		3	50	
			V ⁺ = 5V, T _A = -40°C to +125°C			50	
		Sourcing, V _O to V⁻,	V+ = 1.8V	1	3		
			V ⁺ = 1.8V, T _A = -40°C to +125°C	0.5			
			V+ = 3.3V	5	11		
		$V_{IN}(diff) = 100mV$	$V^+ = 3.3V$, $T_A = -40$ °C to $+125$ °C	4			
			V+ = 5V	15	23		
ı	Output oursent(3)		V ⁺ = 5V, T _A = -40°C to +125°C	8			A
lo	Output current ⁽³⁾		V+ = 1.8V	1	3		mA
			V ⁺ = 1.8V, T _A = -40°C to +125°C	0.5			
		Sinking, V _O to V ⁺ ,	V+ = 3.3V	5	12		
		$V_{IN}(diff) = -100mV$	V ⁺ = 3.3V, T _A = -40°C to +125°C	4			
			V+ = 5V	15	22		
			V ⁺ = 5V, T _A = -40°C to +125°C	8			

5.5 Electrical Characteristics (続き)

at $T_A = 25^{\circ}$ C, $V^+ = 1.8$ V, 3.3V, and 5V, $V^- = 0$ V, $V_{CM} = V_O = V_S / 2$, and $R_L > 1$ M Ω (unless otherwise noted)⁽¹⁾

	PARAMETER	TEST CONDITIONS		MIN	TYP	MAX	UNIT
POWER SUPPLY							
			V ⁺ = 1.8V		345	400	nA
			V ⁺ = 1.8V, T _A = -40°C to +125°C			580	nA
		$V_{CM} = V^- + 0.3 V$	V+ = 3.3V		346	400	nA
		V _{CM} = V + 0.3 V	V ⁺ = 3.3V, T _A = -40°C to +125°C			600	nA
			V+ = 5V		351	400	nA
	Cumply surrent		V ⁺ = 5V, T _A = -40°C to +125°C			620	nA
I _S Su _l	Supply current	V _{CM} = V* - 0.3 V	V ⁺ = 1.8V		472	600	nA
			V ⁺ = 1.8V, T _A = -40°C to +125°C			850	nA
			V+ = 3.3V		471	600	nA
			V ⁺ = 3.3V, T _A = -40°C to +125°C			860	nA
			V+ = 5V		475	600	nA
			V ⁺ = 5V, T _A = -40°C to +125°C			870	nA
NOISE II	MMUNITY						
			f = 400MHz		121		
MIDD	EMI rejection ratio,	· and IN– ⁽⁴⁾ $V_{RF_PEAK} = 100 \text{mV}_P (-20 \text{dB}_P)$	f = 900MHz		121		٩D
MIRR	IN+ and IN- (4)		f = 1800MHz		124		dB
			f = 2400MHz		142		

⁽¹⁾ Electrical Characteristics values apply only for factory testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device such that T_J = T_A. No min and max specifications of parametric performance are indicated in the electrical tables under conditions of internal self-heating where T_J > T_A. Absolute Maximum Ratings indicate junction temperature limits beyond which the device may be permanently degraded, either mechanically or electrically.

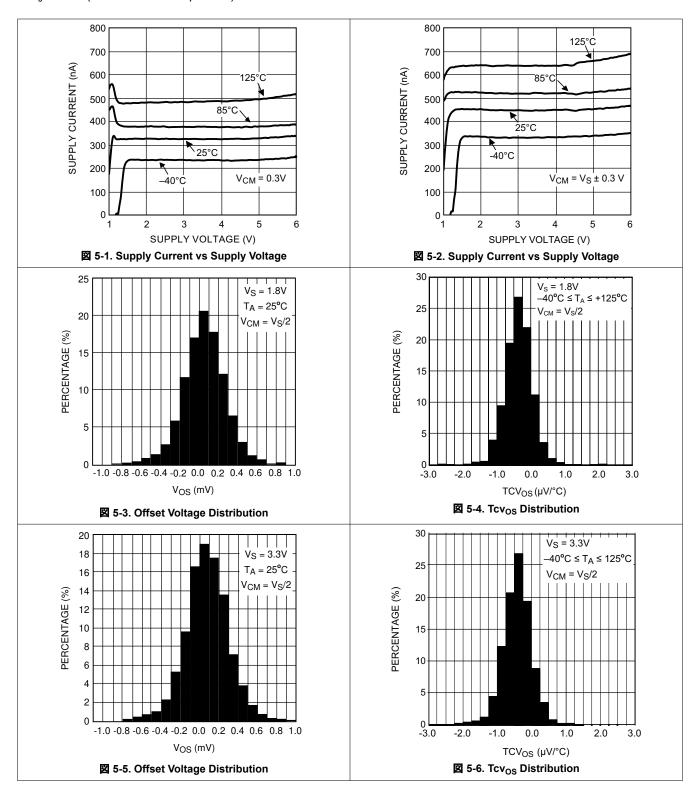
⁽²⁾ The offset voltage average drift is determined by dividing the change in V_{OS} at the temperature extremes by the total temperature change.

⁽³⁾ The short circuit test is a momentary open-loop test.

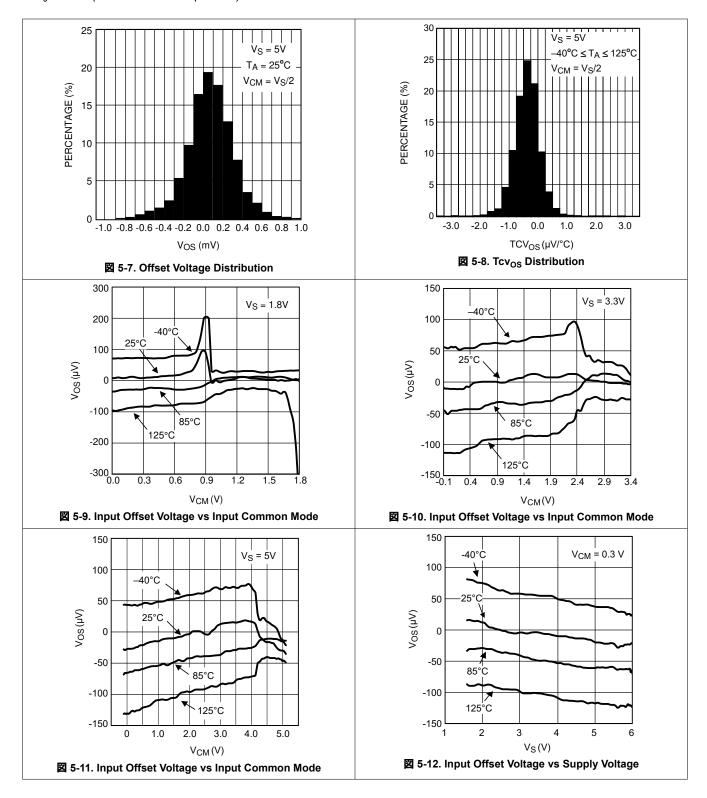
⁽⁴⁾ The EMI rejection ratio is defined as EMIRR = $20\log (V_{RF_PEAK}/\Delta V_{OS})$.



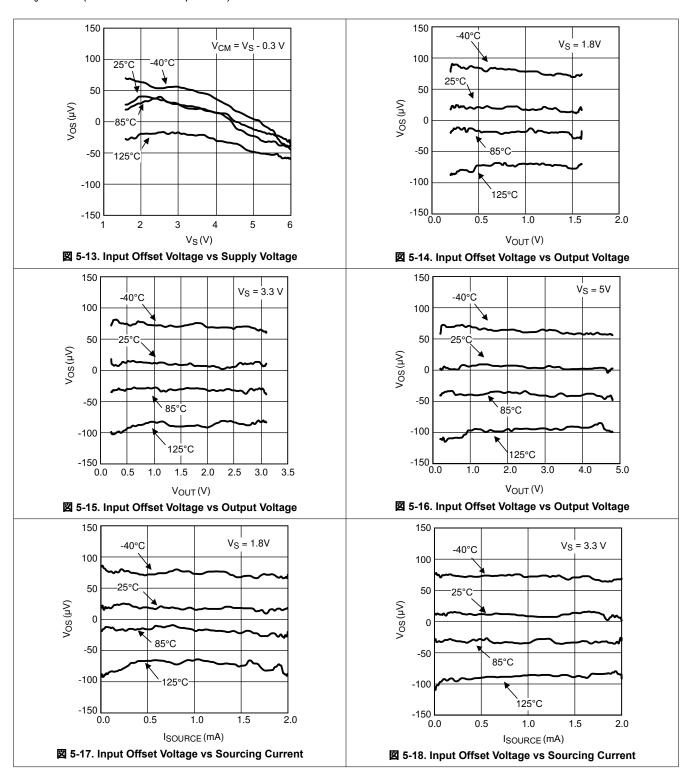
5.6 Typical Characteristics

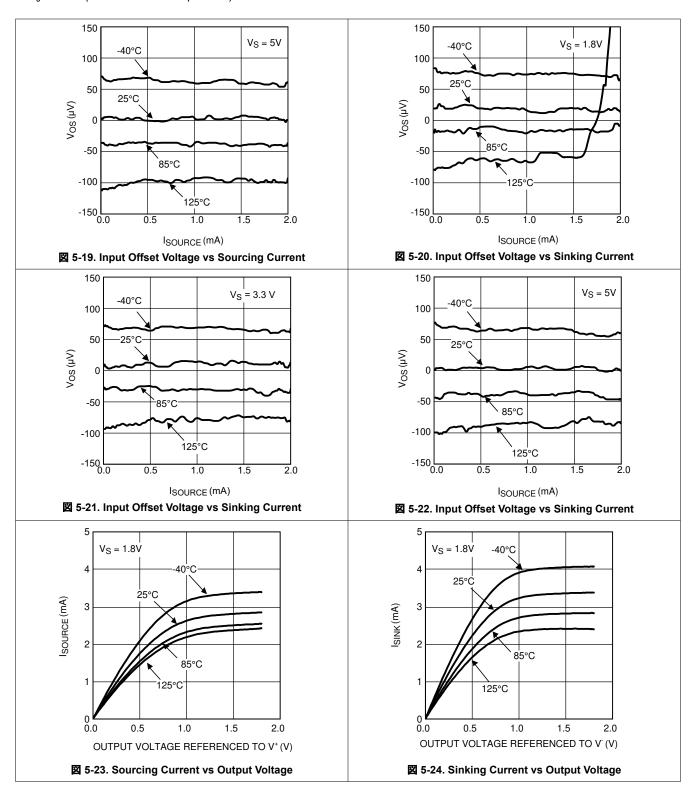




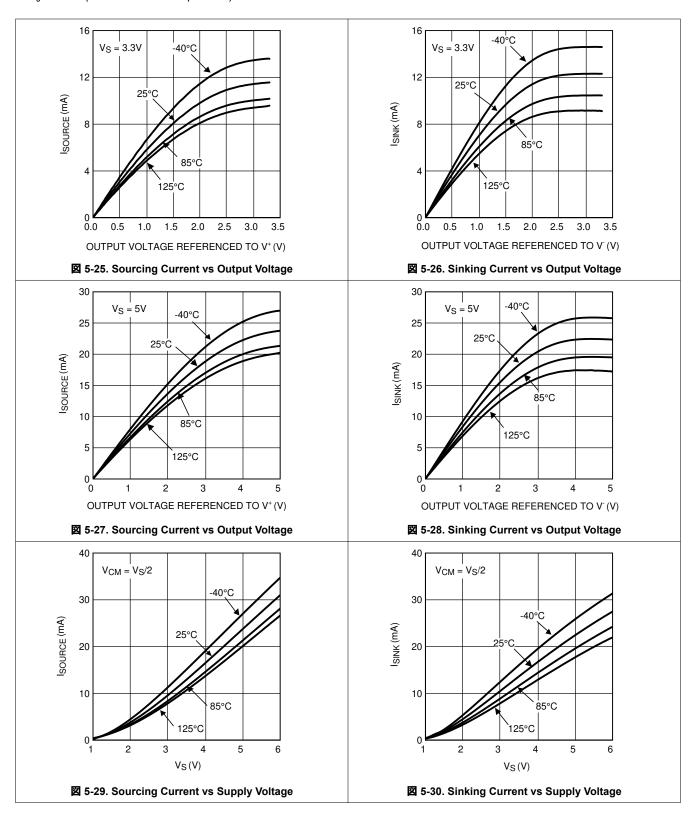


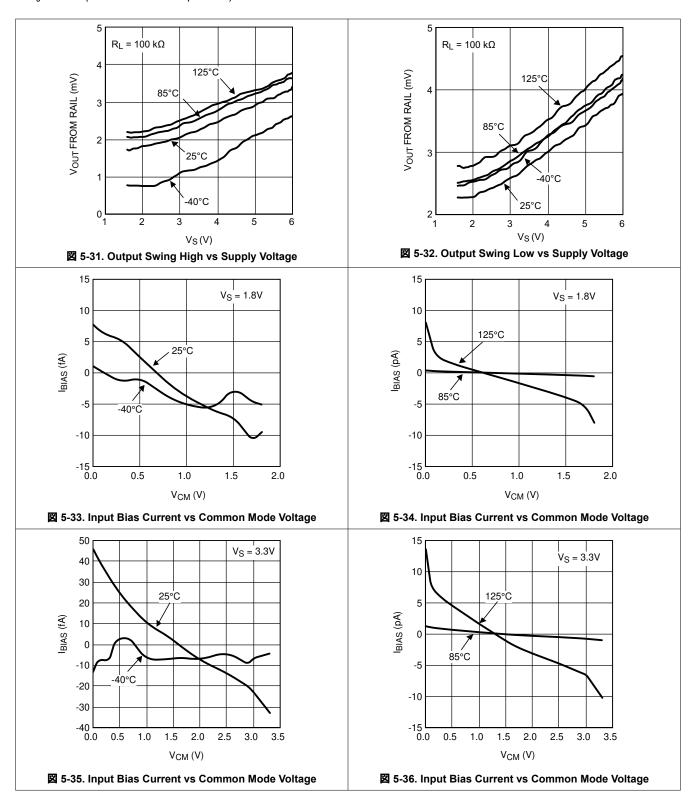




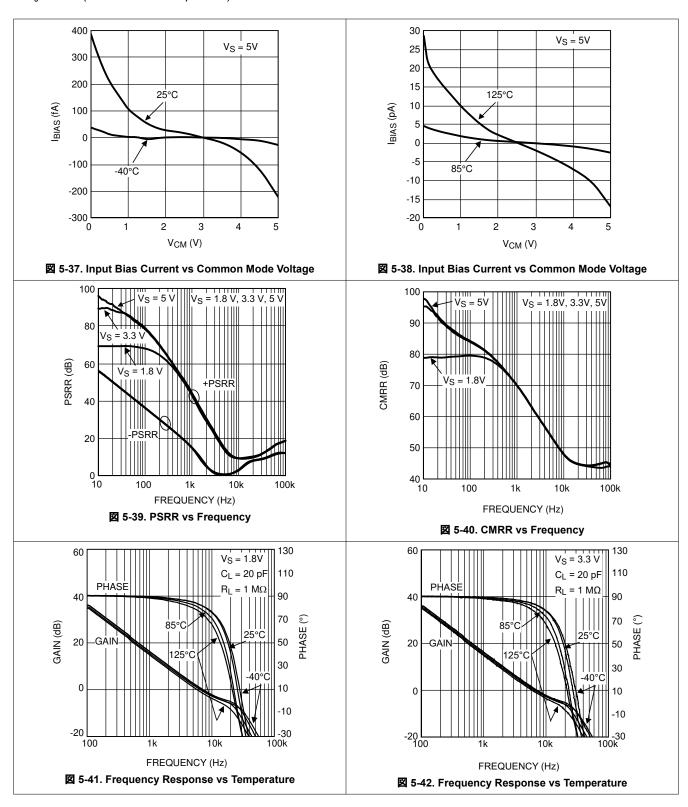




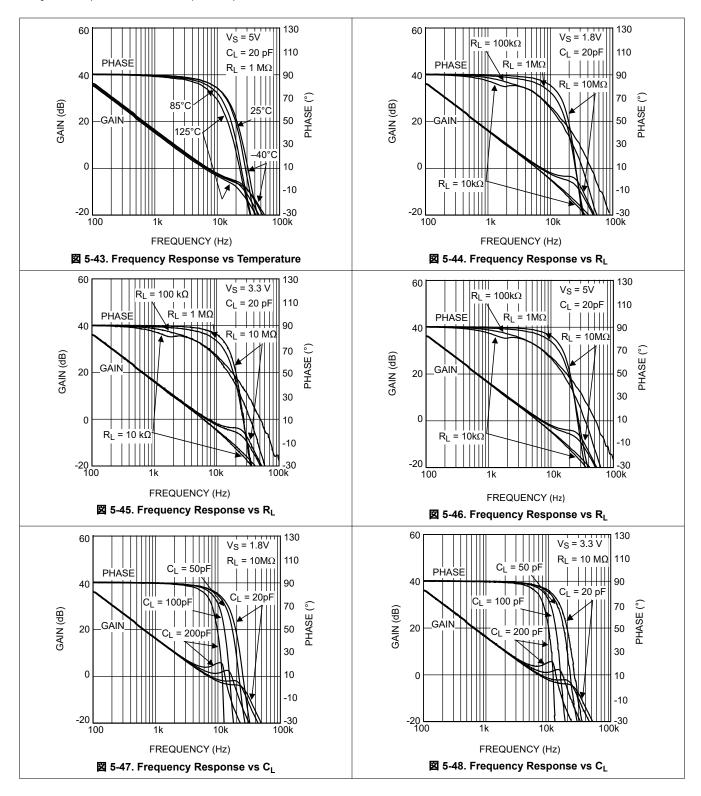




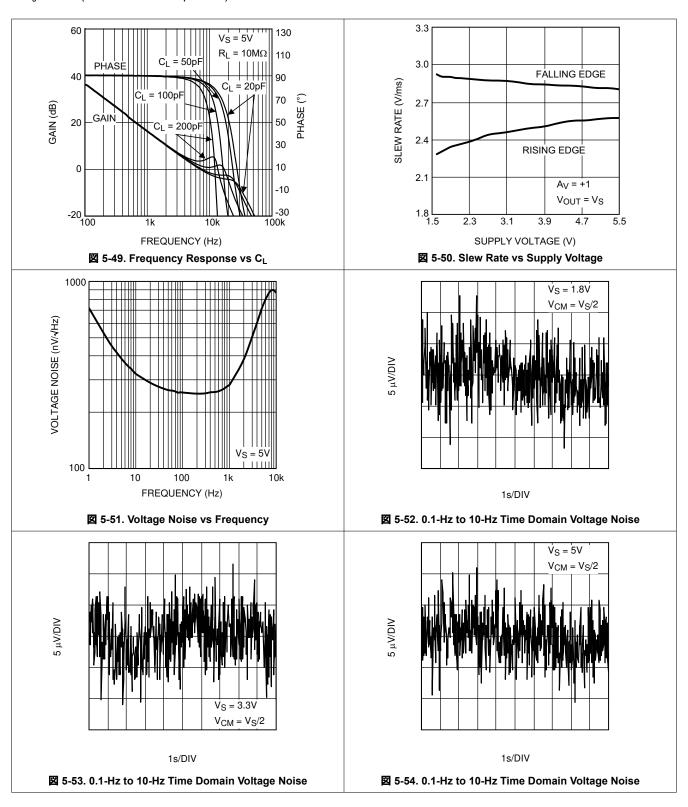


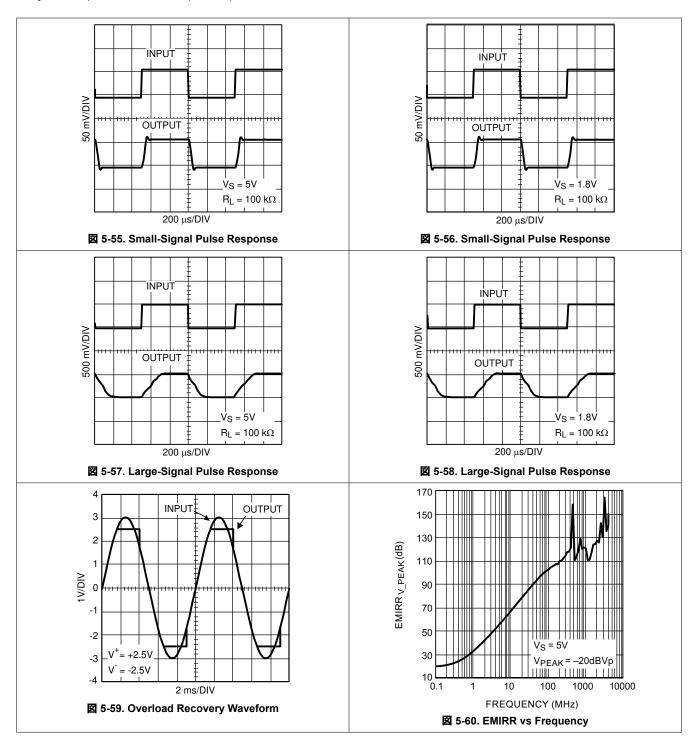












6 Detailed Description

6.1 Overview

The LPV521 is fabricated with Texas Instruments' state-of-the-art VIP50 process. This proprietary process dramatically improves the performance of Texas Instruments' low-power and low-voltage operational amplifiers. The following sections showcase the advantages of the VIP50 process and highlight circuits that enable ultra-low power consumption.

6.2 Functional Block Diagram

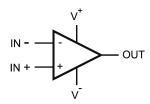


図 6-1. Block Diagram

6.3 Feature Description

The amplifier differential inputs consist of a noninverting input (+IN) and an inverting input (-IN). The amplifier amplifies only the difference in voltage between the two inputs, which is called the differential input voltage. The output voltage of the op-amp V_{OUT} is given by \pm 1:

$$V_{OUT} = A_{OL} (IN^+ - IN^-)$$
 (1)

where A_{OI} is the open-loop gain of the amplifier, typically around 132dB (4,000,000 ×, or 0.25 μ V/V).

6.4 Device Functional Modes

6.4.1 Input Stage

The LPV521 has a rail-to-rail input that provides more flexibility for the system designer. Rail-to-rail input is achieved by using in parallel, one PMOS differential pair and one NMOS differential pair. When the common mode input voltage (V_{CM}) is near V^+ , the NMOS pair is on and the PMOS pair is off. When V_{CM} is near V^- , the NMOS pair is off and the PMOS pair is on. When V_{CM} is between V^+ and V^- , internal logic decides how much current each differential pair get. This special logic maintains stable and low-distortion amplifier operation within the entire common-mode voltage range.

Both input stages have an offset voltage (V_{OS}) characteristic; therefore, the offset voltage of the LPV521 becomes a function of V_{CM} . V_{OS} has a crossover point at 1.0V less than V^+ . See the *Input Offset Voltage vs Input Common Mode* curves in the *Typical Characteristics*. Take care in situations where the input signal amplitude is comparable to the V_{OS} value or the design requires high accuracy. In these situations, the input signal must avoid the crossover point. In addition, parameters such as PSRR and CMRR that involve the input offset voltage are also affected by changes in V_{CM} across the differential-pair transition region.

6.4.2 Output Stage

The LPV521 output voltage swings 3mV from rails at a 3.3V supply, which provides the maximum possible dynamic range at the output. This feature is particularly important when operating on low supply voltages.

The LPV521 maximum output voltage swing defines the maximum swing possible under a particular output load. The LPV521 output swings 50mV from the rail at a 5V supply with an output load of $100k\Omega$.

7 Applications and Implementation

注

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7.1 Application Information

The LPV521 is specified for operation from 1.6V to 5.5V (± 0.8 V to ± 2.25 V). Many of the specifications apply from -40° C to $\pm 125^{\circ}$ C. The LMV521 features rail-to-rail input and rail-to-rail output swings while consuming only nanowatts of power. Parameters that exhibit significant variance with regard to operating voltage or temperature are presented in $\pm 790 \times 10^{\circ}$ 5.6.

7.1.1 Driving Capacitive Load

The LPV521 is internally compensated for stable unity gain operation, with a 6.2kHz, typical gain bandwidth. However, the unity gain follower is the most sensitive configuration to capacitive load. The combination of a capacitive load placed at the output of an amplifier along with the amplifier output impedance creates a phase lag, which reduces the phase margin of the amplifier. If the phase margin is significantly reduced, the response is underdamped, and causes peaking in the transfer. When there is too much peaking, the op amp can start oscillating.

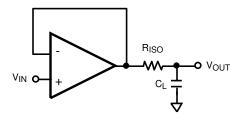


図 7-1. Resistive Isolation of Capacitive Load

To drive heavy capacitive loads, use an isolation resistor, $R_{\rm ISO}$, as in \boxtimes 7-1. By using this isolation resistor, the capacitive load is isolated from the amplifier output. The larger the value of $R_{\rm ISO}$, the more stable the amplifier. If the value of $R_{\rm ISO}$ is sufficiently large, the feedback loop is stable, independent of the value of $C_{\rm L}$. However, larger values of $R_{\rm ISO}$ result in reduced output swing and reduced output current drive.

 \gtrsim 7-1 shows the recommended minimum R_{ISO} values for a 5V supply. \boxtimes 7-2 shows the typical response obtained with the C_L = 50pF and R_{ISO} = 154kΩ. The other values of R_{ISO} in Table 7-1 are chosen to achieve similar dampening at the respective capacitive loads. Notice that for the LPV521 with larger a C_L, a smaller R_{ISO} can be used for stability. However, for a given C_L, a larger R_{ISO} provides a more damped response. For capacitive loads of 20pF and less, no isolation resistor is needed.

表 7-1. Recommended Minimum R_{ISO} Values for a 5V Supply

CL	R _{ISO}
0pF to 20pF	Not needed
50pF	154kΩ
100pF	118kΩ
500pF	52.3kΩ
1nF	33.2kΩ
5nF	17.4kΩ
10nF	13.3kΩ

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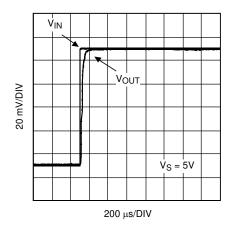


図 7-2. Step Response

7.1.2 EMI Suppression

The near-ubiquity of cellular, Bluetooth®, and Wi-Fi® signals and the rapid rise of sensing systems incorporating wireless radios make electromagnetic interference (EMI) an evermore important design consideration for precision signal paths. Though RF signals lie outside the op-amp band, RF carrier switching can modulate the dc offset of the op amp. Also some common RF modulation schemes can induce down-converted components. The added dc offset and the induced signals are amplified with the signal of interest and thus corrupt the measurement. The LPV521 uses on-chip filters to reject these unwanted RF signals at the inputs and power supply pins, thereby preserving the integrity of the precision signal path.

Twisted pair cabling and the active front-end common-mode rejection provide immunity against low-frequency noise (for example, 60Hz or 50Hz mains) but are ineffective against RF interference. Even a few centimeters of printed circuit board (PCB) trace and wiring for sensors located close to the amplifier can pick up significant 1GHz RF. The integrated EMI filters of the LPV521 reduce or eliminate external shielding and filtering requirements, thus increasing system robustness. A larger EMIRR means more rejection of the RF interference. For more information on EMIRR, see the *AN-1698 A Specification for EMI Hardened Operational Amplifiers* application report.

7.2 Typical Applications

7.2.1 60Hz Twin T-Notch Filter

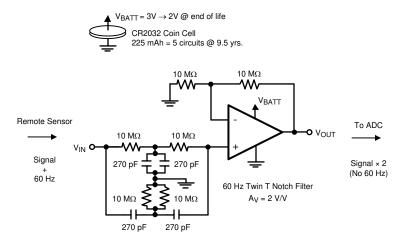


図 7-3. 60Hz Notch Filter

7.2.1.1 Design Requirements

Small signals from transducers in remote and distributed sensing applications commonly suffer strong 60Hz interference from ac power lines. The circuit of \boxtimes 7-3 notches out the 60Hz and provides a gain A_V = 2 for the sensor signal represented by a 1kHz sine wave. Similar stages can be cascaded to remove 2nd and 3rd harmonics of 60Hz. Thanks to the nA power consumption of the LPV521, even five such circuits can run for 9.5 years from a small CR2032 lithium cell. These batteries have a nominal voltage of 3V and an end of life voltage of 2V. With an operating voltage from 1.6V to 5.5V, the LPV521 can function over this voltage range.

7.2.1.2 Detailed Design Procedure

The notch frequency is set by $F_0 = 1 / 2\pi RC$. To achieve a 60Hz notch, use $R = 10M\Omega$ and C = 270pF. If eliminating 50Hz noise, which is common in European systems, use $R = 11.8M\Omega$ and C = 270pF.

The twin T notch filter works by having two separate paths from V_{IN} to the amplifier input. A low-frequency path through resistors R-R and another separate high-frequency path through capacitors C-C. However, at frequencies around the notch frequency, the two paths have opposing phase angles and the two signals tend to cancel at the amplifier input.

To ensure that the target center frequency is achieved, and to maximize the notch depth (Q factor), balance the filter as much as possible. To obtain circuit balance, while overcoming limitations of available standard resistor and capacitor values, use passives in parallel to achieve the 2C and R/2 circuit requirements for the filter components that connect to ground.

To ensure that passive component values stay as expected, clean the board with alcohol, rinse with deionized water, and air dry. Ensure that the board remains in a relatively low humidity environment to minimize moisture that can increase the conductivity of board components. Also large resistors come with considerable parasitic stray capacitance; the effects can be reduced by cutting out the ground plane below components of concern.

Use Large resistors in the feedback network to minimize battery drain. When designing with large resistors, consider the resistor thermal noise, op-amp current noise, as well as op-amp voltage noise in the noise analysis of the circuit. The noise analysis for the circuit in $\boxed{2}$ 7-3 can be done over a bandwidth of 5kHz, which takes the conservative approach of overestimating the bandwidth (LPV521 typical GBW/A_V is less). The total noise at the output is approximately $800\mu V_{PP}$, which is excellent considering the total consumption of the circuit is only 540nA. The dominant noise terms are op-amp voltage noise ($550\mu V_{PP}$), current noise through the feedback network ($430\mu V_{PP}$), and current noise through the notch filter network ($280\mu V_{PP}$). Thus, the total circuit noise is less than ½ LSB of a 10-bit system with a 2V reference, which is 1mV.



7.2.1.3 Application Curve

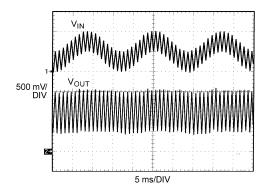


図 7-4. 60Hz Notch Filter Waveform

7.2.2 Portable Gas Detection Sensor

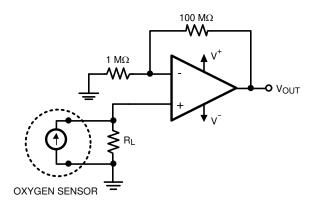


図 7-5. Precision Oxygen Sensor

7.2.2.1 Design Requirements

Gas sensors are used in many different industrial and medical applications. Gas sensors generate a current that is proportional to the percentage of a particular gas sensed in an air sample. This current goes through a load resistor and the resulting voltage drop is measured. The LPV521 is an excellent choice for this application because the device draws only 345nA of current and operates on supply voltages down to 1.6V. Depending on the sensed gas and sensitivity of the sensor, the output current can be in the order of tens of microamperes to a few milliamperes. Gas sensor data sheets often specify a recommended load resistor value or suggest a range of load resistors from which to choose.

Oxygen sensors are used when air quality or oxygen delivered to a patient needs to be monitored. Fresh air contains 20.9% oxygen. Air samples containing less than 18% oxygen are considered dangerous. This application detects oxygen in air. Oxygen sensors are also used in industrial applications where the environment must lack oxygen. An example is when food is vacuum packed. There are two main categories: oxygen sensors that sense oxygen when oxygen is abundantly present (for example, in air or near an oxygen tank), and oxygen sensors that detect traces of oxygen in ppm.

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7.2.2.2 Detailed Design Procedure

7.2.2.3 Application Curve

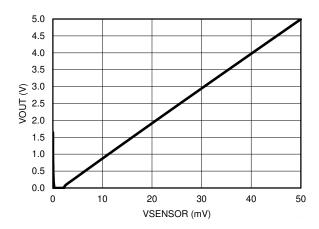


図 7-6. Calculated Oxygen Sensor Circuit Output (Single 5V Supply)

7.2.3 High-Side Battery Current Sensing

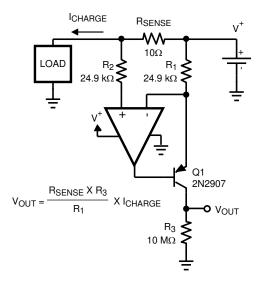


図 7-7. High-Side Current Sensing

7.2.3.1 Design Requirements

The rail-to-rail common-mode input range and the very low quiescent current make the LPV521 an excellent choice for use in high-side and low-side battery current-sensing applications. The high-side current-sensing

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circuit in 🗵 7-7 is commonly used in a battery charger to monitor the charging current to prevent overcharging. A sense resistor R_{SENSE} is connected in series with the battery.

7.2.3.2 Detailed Design Procedure

The theoretical output voltage of the circuit is V_{OUT} = [($R_{SENSE} \times R_3$) / R_1] × I_{CHARGE} . In reality, however, as a result of the finite current gain of the transistor (β), the current that travels through R_3 is not I_{CHARGE} . Instead, R_3 is $\alpha \times I_{CHARGE}$ or β / (β +1) × I_{CHARGE} . A Darlington pair can be used to increase the β and performance of the measuring circuit.

Using the components shown in \boxtimes 7-7 results in $V_{OUT} \approx 4000\Omega \times I_{CHARGE}$. This result is needed to amplify a 1mA I_{CHARGE} to near full-scale of an analog-to-digital converter (ADC) with V_{REF} at 4.1V. A resistor, R_2 is used at the noninverting input of the amplifier, with the same value as R_1 to minimize offset voltage.

Selecting values per \boxtimes 7-7 limits the current traveling through the R₁ – Q1 – R₃ leg of the circuit to under 1µA, which is on the same order as the LPV521 supply current. Increasing resistors R₁, R₂, and R₃ decreases the measuring circuit supply current and extends battery life.

Decreasing R_{SENSE} minimizes error due to resistor tolerance; however, this decrease also decreases $V_{SENSE} = I_{CHARGE} \times R_{SENSE}$, and in turn, the amplifier offset voltage has a more significant contribution to the total error of the circuit. With the components shown in \boxtimes 7-7, the measurement circuit supply current can be kept below 1.5µA and measure 100µA to 1mA.

7.2.3.3 Application Curve

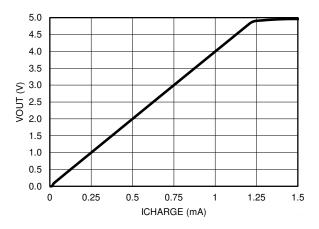


図 7-8. Calculated High-Side Current Sense Circuit Output

7.3 Power Supply Recommendations

The LPV521 is specified for operation from 1.6V to 5.5V (± 0.8 V to ± 2.75 V) over a -40°C to ± 125 °C temperature range. Parameters that can exhibit significant variance with regard to operating voltage or temperature are presented in the ± 79 3 \times 5.6.

注意

Supply voltages greater than 6 V can permanently damage the device.

Low bandwidth nanopower devices do not have good high frequency (> 1kHz) ac PSRR rejection against high-frequency switching supplies and other kHz and greater noise sources; therefore, extra supply filtering is recommended if kHz-range noise is expected on the power-supply lines.

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7.4 Layout

7.4.1 Layout Guidelines

For best operational performance of the device, use good printed circuit board (PCB) layout practices, including:

- Noise can propagate into analog circuitry through the power pins of the circuit as a whole and the op amp.
 Use bypass capacitors to reduce the coupled noise by providing low-impedance power sources local to the analog circuitry.
- Connect low-ESR, 0.1µF ceramic bypass capacitors between each supply pin and ground, placed as close to the device as possible. A single bypass capacitor from V+ to ground is applicable for single-supply applications.
- Separate grounding for analog and digital portions of circuitry is one of the simplest and most-effective methods of noise suppression. One or more layers on multilayer PCBs are usually devoted to ground planes. A ground plane helps distribute heat and reduces EMI noise pickup. Physically separate digital and analog grounds paying attention to the flow of the ground current.
- To reduce parasitic coupling, run the input traces as far away from the supply or output traces as possible. If not possible, cross the sensitive trace perpendicular as opposed to in parallel with the noisy trace.
- Place the external components as close to the device as possible. セクション 7.4.2 shows how keeping RF and RG close to the inverting input minimizes parasitic capacitance.
- Keep the length of input traces as short as possible. Always remember that the input traces are the most sensitive part of the circuit.
- Consider a driven, low-impedance guard ring around the critical traces. A guard ring can significantly reduce leakage currents from nearby traces that are at different potentials.

7.4.2 Layout Example

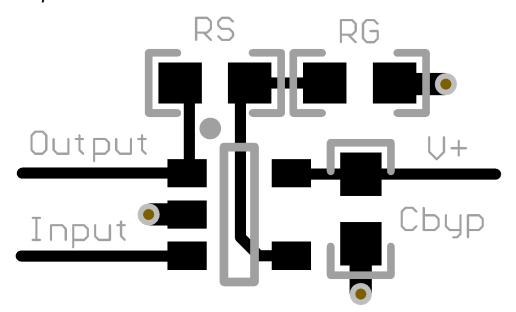


図 7-9. Noninverting Layout Example

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8 Device and Documentation Support

8.1 Device Support

8.1.1 Development Support

- LPV521 PSPICE Model
- TINA-TI SPICE-Based Analog Simulation Program, http://www.ti.com/tool/tina-ti
- Capacitive Load Drive Solution Using an Isolation Resistor reference design
- DIP Adapter Evaluation Module, http://www.ti.com/tool/dip-adapter-evm
- Evaluation board for 5-pin, north-facing amplifiers in the SC70 package, SNOA487.
- Manual for LMH730268 Evaluation board 551012922-001

8.2 Documentation Support

8.2.1 Related Documentation

For related documentation, see the following:

- Texas Instruments, Feedback Plots Define Op Amp AC Performance application bulletin
- Texas Instruments, AN-1698 A Specification for EMI Hardened Operational Amplifiers application report
- Texas Instruments, EMI Rejection Ratio of Operational Amplifiers application report
- Texas Instruments, Handbook of Operational Amplifier Applications application report

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English Data Sheet: SNOSB14



9 Revision History

資料番号末尾の英字は改訂を表しています。その改訂履歴は英語版に準じています。

Changes from Revision D (December 2014) to Revision E (July 2024)	Page
ドキュメント全体にわたって表、図、相互参照の採番方法を更新	1
• P (PDIP、8) パッケージと関連する内容をドキュメントに追加	1
「アプリケーション」を更新	1
「パッケージ情報」表を更新	1
Added missing thermal information for DCK (SC70) package	4
Moved all Electrical Characteristics tables into one table	
Updated Electrical Characteristics note 1	4
Added missing CMRR test condition for V+ = 5V	4
Updated common mode voltage range to fix the incorrect conditions	4
• Updated Figure 5-4 and Figure 5-6, TcvOS Distribution, to fix test condition typos	8
 Changed A_{OI} typical value from "100 dB (100,000 ×, or 10 μV/V)" to "132dB (4000,000 ×). 	
Feature Description	18
Changes from Revision C (February 2013) to Revision D (December 2014)	Page
・ 「ピン構成および機能」セクション、「ESD 定格」表、「機能説明」セクション、「デバイスの機能	
リケーションと実装」セクション、「電源に関する推奨事項」セクション、「レイアウト」セクション、	=
ントのサポート」ヤクション「メカニカル パッケージ および注文情報」ヤクションを追加	1

10 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

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PACKAGING INFORMATION

Orderable part number	Status	Material type	Package Pins	Package qty Carrier	RoHS	Lead finish/	MSL rating/	Op temp (°C)	Part marking
	(1)	(2)			(3)	Ball material	Peak reflow		(6)
						(4)	(5)		
LPV521MG/NOPB	Active	Production	SC70 (DCK) 5	1000 SMALL T&R	Yes	Call TI Sn	Level-1-260C-UNLIM	-40 to 125	AHA
LPV521MG/NOPB.A	Active	Production	SC70 (DCK) 5	1000 SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	AHA
LPV521MGE/NOPB	Active	Production	SC70 (DCK) 5	250 SMALL T&R	Yes	Call TI Sn	Level-1-260C-UNLIM	-40 to 125	AHA
LPV521MGE/NOPB.A	Active	Production	SC70 (DCK) 5	250 SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	AHA
LPV521MGX/NOPB	Active	Production	SC70 (DCK) 5	3000 LARGE T&R	Yes	Call TI Sn	Level-1-260C-UNLIM	-40 to 125	AHA
LPV521MGX/NOPB.A	Active	Production	SC70 (DCK) 5	3000 LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	AHA
LPV521P	Active	Production	PDIP (P) 8	50 TUBE	Yes	NIPDAU	N/A for Pkg Type	-40 to 125	LPV521
LPV521P.A	Active	Production	PDIP (P) 8	50 TUBE	Yes	NIPDAU	N/A for Pkg Type	-40 to 125	LPV521

⁽¹⁾ Status: For more details on status, see our product life cycle.

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⁽³⁾ RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

⁽⁴⁾ Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

⁽⁵⁾ MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

⁽⁶⁾ Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

PACKAGE OPTION ADDENDUM

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In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

PACKAGE MATERIALS INFORMATION

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TAPE AND REEL INFORMATION



TAPE DIMENSIONS KO P1 BO W Cavity A0

A0	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LPV521MG/NOPB	SC70	DCK	5	1000	178.0	8.4	2.25	2.45	1.2	4.0	8.0	Q3
LPV521MGE/NOPB	SC70	DCK	5	250	178.0	8.4	2.25	2.45	1.2	4.0	8.0	Q3
LPV521MGX/NOPB	SC70	DCK	5	3000	178.0	8.4	2.25	2.45	1.2	4.0	8.0	Q3



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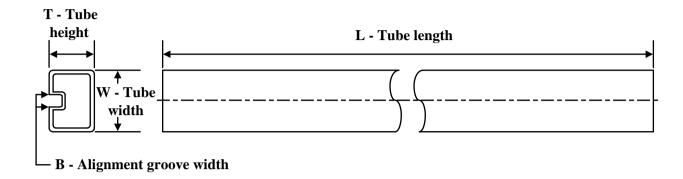
*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LPV521MG/NOPB	SC70	DCK	5	1000	208.0	191.0	35.0
LPV521MGE/NOPB	SC70	DCK	5	250	208.0	191.0	35.0
LPV521MGX/NOPB	SC70	DCK	5	3000	208.0	191.0	35.0

PACKAGE MATERIALS INFORMATION

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TUBE



*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	T (µm)	B (mm)
LPV521P	Р	PDIP	8	50	506	13.97	11230	4.32
LPV521P.A	Р	PDIP	8	50	506	13.97	11230	4.32

P (R-PDIP-T8)

PLASTIC DUAL-IN-LINE PACKAGE



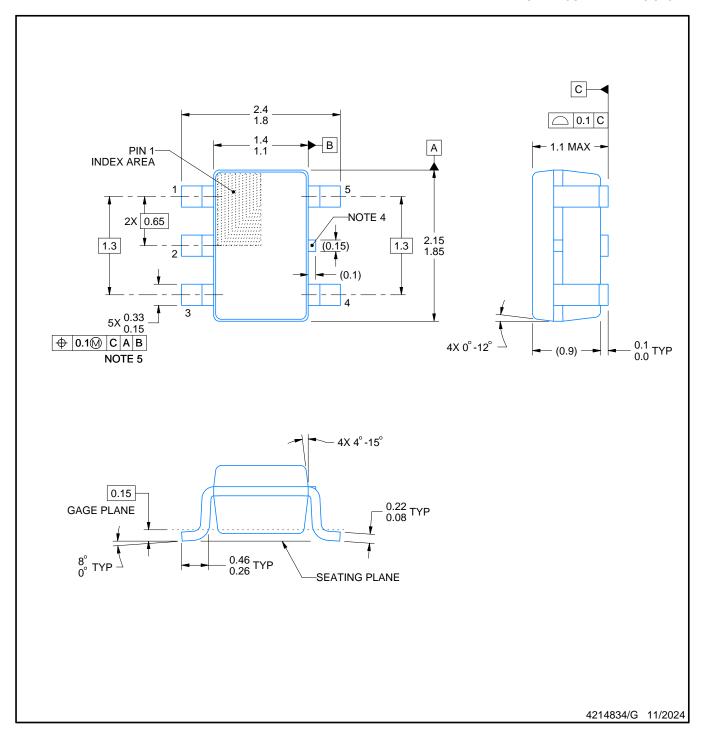
NOTES:

- A. All linear dimensions are in inches (millimeters).
- B. This drawing is subject to change without notice.
- C. Falls within JEDEC MS-001 variation BA.





SMALL OUTLINE TRANSISTOR



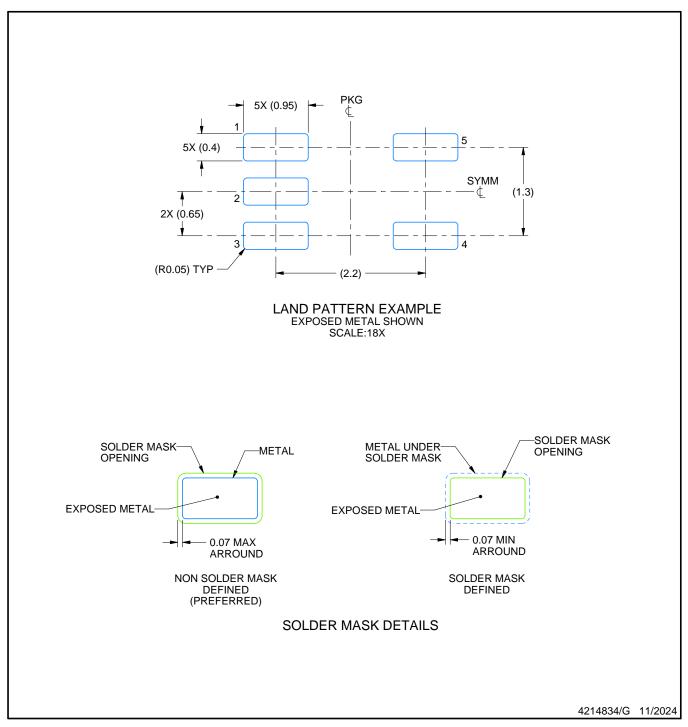
NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
 2. This drawing is subject to change without notice.
 3. Reference JEDEC MO-203.

- 4. Support pin may differ or may not be present.5. Lead width does not comply with JEDEC.
- 6. Body dimensions do not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.25mm per side



SMALL OUTLINE TRANSISTOR

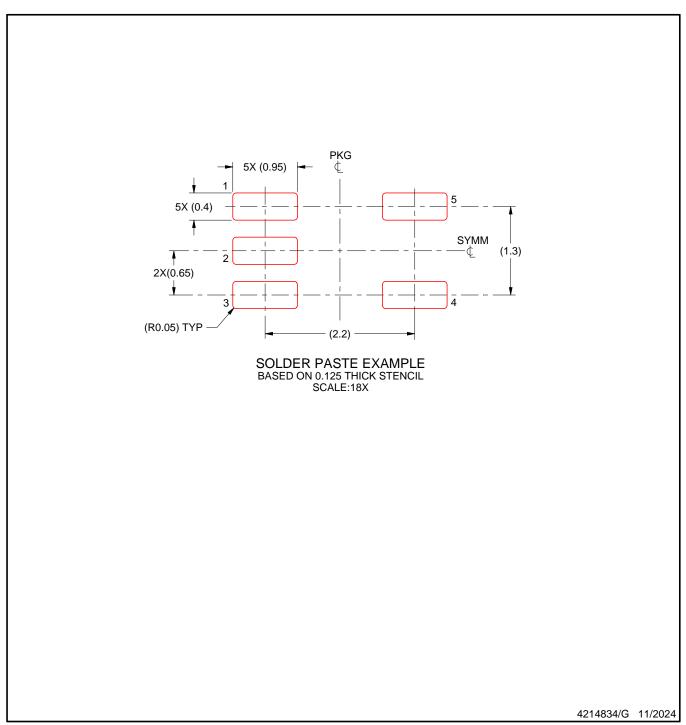


NOTES: (continued)

7. Publication IPC-7351 may have alternate designs.8. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SMALL OUTLINE TRANSISTOR



NOTES: (continued)

- 9. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 10. Board assembly site may have different recommendations for stencil design.



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