

# LMZ31503 3A、4.5V~14.5V入力、QFNパッケージの パワー・モジュール

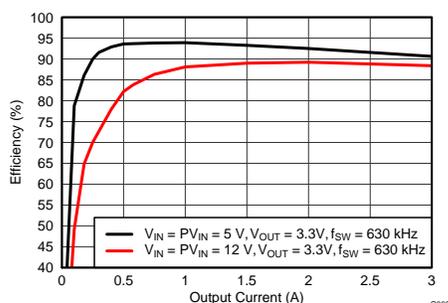
## 1 特長

- 小さな占有面積で低プロファイルの設計を可能にする完全な統合電源ソリューション
- 9mm×15mm×2.8mmのパッケージ
  - LMZ31506とピン互換
- 最大95%の効率
- 0.8V~5.5Vの広い範囲で出力電圧を設定可能、リファレンス精度1%
- オプションの分割電源レールにより最低1.6Vの入力電圧で動作
- 可変スイッチング周波数(330kHz~780kHz)
- 外部クロックに同期
- 調整可能なスロー・スタート
- 出力電圧シーケンシング/トラッキング
- パワー・グッド出力
- 低電圧誤動作防止(UVLO)をプログラム可能
- 過電流保護(ヒカップ・モード)
- 過熱保護機能
- プリバイアス出力によるスタートアップ
- 動作温度範囲: -40°C~+85°C
- 強化された熱特性: 13°C/W
- EN55022 Class Bの放射要件に準拠
  - シールド付きインダクタを内蔵
- **WEBENCH® Power Designer**により、LMZ31503を使用するカスタム設計を作成

## 2 アプリケーション

- ブロードバンドおよび通信インフラストラクチャ
- 自動試験機器/医療用機器
- Compact PCI、PCI Express、PXI Express
- DSPおよびFPGAのポイント・オブ・ロード・アプリケーション
- 高密度分散電源システム

効率



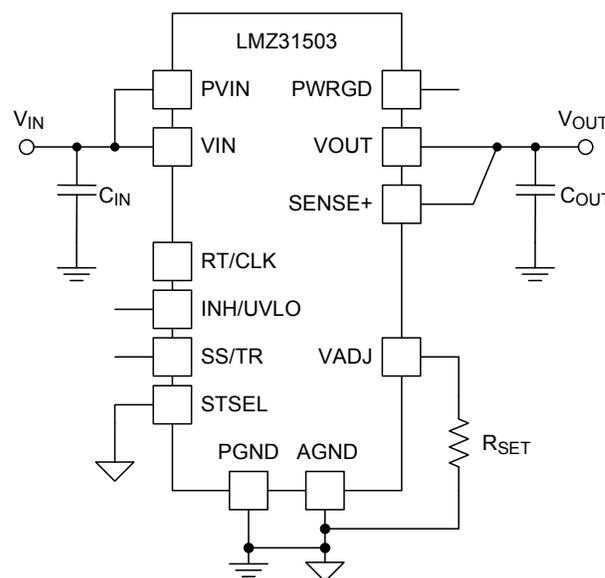
## 3 概要

LMZ31503パワー・モジュールは、3AのDC/DCコンバータをパワー-MOSFET、シールド付きインダクタ、およびパッシブ部品とともに低プロファイルのQFNパッケージに実装した、使いやすい集積電源ソリューションです。外部部品は3個しか使用せず、ループ補償や磁気部品の選択プロセスも不要になります。

9mm×15mm×2.8mmのQFNパッケージはプリント基板にハンダ付けしやすく、小型のポイント・オブ・ロード設計で、95%を超える効率、優れた消費電力、接合部から周囲へ13°C/Wの熱インピーダンスを実現できます。このデバイスは、周囲温度85°Cにおいて無気流でも、3Aの定格出力電流を完全に供給できます。

LMZ31503は、ディスクリートPOL設計と同等の柔軟性および機能セットを備え、高性能DSPおよびFPGAへの電力供給に最適です。先進のパッケージング技術により、標準のQFN実装/試験手法に対応した、堅牢で信頼性の高い電源ソリューションを実現できます。

概略回路図



## 4 Specifications

### 4.1 Absolute Maximum Ratings<sup>(1)</sup>

over operating temperature range (unless otherwise noted)

		VALUE	UNIT
Input Voltage	VIN	–0.3 to 16	V
	PVIN	–0.3 to 16	V
	INH/UVLO	–0.3 to 6	V
	VADJ	–0.3 to 3	V
	PWRGD	–0.3 to 6	V
	SS/TR	–0.3 to 3	V
	STSEL	–0.3 to 3	V
	RT/CLK	–0.3 to 6	V
Output Voltage	PH	–1 to 20	V
	PH 10ns Transient	–3 to 20	V
V <sub>DIFF</sub> (GND to exposed thermal pad)		–0.2 to 0.2	V
Source Current	RT/CLK	±100	µA
	PH	Current Limit	A
Sink Current	PH	Current Limit	A
	PVIN	Current Limit	A
	PWRGD	–0.1 to 5	mA
Operating Junction Temperature		–40 to 125 <sup>(2)</sup>	°C
Storage Temperature		–65 to 150	°C
Peak Reflow Case Temperature <sup>(3)</sup>		245 <sup>(4)</sup>	°C
Maximum Number of Reflows Allowed <sup>(3)</sup>		3 <sup>(4)</sup>	
Mechanical Shock	Mil-STD-883D, Method 2002.3, 1 msec, 1/2 sine, mounted	1500	G
Mechanical Vibration	Mil-STD-883D, Method 2007.2, 20-2000Hz	20	

- (1) Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) See the temperature derating curves in the Typical Characteristics section for thermal information.
- (3) For soldering specifications, refer to the [Soldering Requirements for BQFN Packages](#) application note.
- (4) Devices with a date code prior to week 14 2018 (1814) have a peak reflow case temperature of 240°C with a maximum of one reflow

## 4.2 Thermal Information

THERMAL METRIC <sup>(1)</sup>		LMZ31503	UNIT
		RUQ47	
		47 PINS	
$\theta_{JA}$	Junction-to-ambient thermal resistance <sup>(2)</sup>	13	°C/W
$\Psi_{JT}$	Junction-to-top characterization parameter <sup>(3)</sup>	2.5	°C/W
$\Psi_{JB}$	Junction-to-board characterization parameter <sup>(4)</sup>	5	°C/W

- (1) For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report.
- (2) The junction-to-ambient thermal resistance,  $\theta_{JA}$ , applies to devices soldered directly to a 100 mm x 100 mm double-sided PCB with 1 oz. copper and natural convection cooling. Additional airflow reduces  $\theta_{JA}$ .
- (3) The junction-to-top characterization parameter,  $\Psi_{JT}$ , estimates the junction temperature,  $T_J$ , of a device in a real system, using a procedure described in JESD51-2A (sections 6 and 7).  $T_J = \Psi_{JT} * P_{dis} + T_T$ ; where  $P_{dis}$  is the power dissipated in the device and  $T_T$  is the temperature of the top of the device.
- (4) The junction-to-board characterization parameter,  $\Psi_{JB}$ , estimates the junction temperature,  $T_J$ , of a device in a real system, using a procedure described in JESD51-2A (sections 6 and 7).  $T_J = \Psi_{JB} * P_{dis} + T_B$ ; where  $P_{dis}$  is the power dissipated in the device and  $T_B$  is the temperature of the board 1mm from the device.

## 4.3 Package Specifications

LMZ31503		UNIT
Weight		1.26 grams
Flammability	Meets UL 94 V-O	
MTBF Calculated reliability	Per Bellcore TR-332, 50% stress, $T_A = 40^\circ\text{C}$ , ground benign	40.1 Mhrs

## 4.4 Electrical Characteristics

Over  $-40^\circ\text{C}$  to  $85^\circ\text{C}$  free-air temperature,  $P_{VIN} = V_{IN} = 12\text{ V}$ ,  $V_{OUT} = 1.8\text{ V}$ ,  $I_{OUT} = 3\text{ A}$ ,

$C_{IN1} = 2 \times 22\ \mu\text{F}$  ceramic,  $C_{IN2} = 68\ \mu\text{F}$  poly-tantalum,  $C_{OUT1} = 4 \times 47\ \mu\text{F}$  ceramic (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
$I_{OUT}$	Output current	$T_A = 85^\circ\text{C}$ , natural convection	0		3	A
$V_{IN}$	Input bias voltage range	Over $I_{OUT}$ range	4.5		14.5	V
$P_{VIN}$	Input switching voltage range	Over $I_{OUT}$ range	1.6 <sup>(1)</sup>		14.5	V
$UVLO$	$V_{IN}$ Undervoltage lockout	$V_{IN}$ = increasing		4.0	4.5	V
		$V_{IN}$ = decreasing	3.5	3.85		
$V_{OUT(adj)}$	Output voltage adjust range	Over $I_{OUT}$ range	0.8		5.5	V
$V_{OUT}$	Set-point voltage tolerance	$T_A = 25^\circ\text{C}$ , $I_{OUT} = 0\text{ A}$			$\pm 1.0\%$ <sup>(2)</sup>	
	Temperature variation	$-40^\circ\text{C} \leq T_A \leq +85^\circ\text{C}$ , $I_{OUT} = 0\text{ A}$			$\pm 0.3\%$	
	Line regulation	Over $P_{VIN}$ range, $T_A = 25^\circ\text{C}$ , $I_{OUT} = 0\text{ A}$			$\pm 0.1\%$	
	Load regulation	Over $I_{OUT}$ range, $T_A = 25^\circ\text{C}$			$\pm 0.1\%$	
	Total output voltage variation	Includes set-point, line, load, and temperature variation				$\pm 1.5\%$ <sup>(2)</sup>
$\eta$	Efficiency	$P_{VIN} = V_{IN} = 12\text{ V}$ $I_O = 1.5\text{ A}$	$V_{OUT} = 5\text{ V}$ , $f_{SW} = 780\text{ kHz}$		91.5 %	
			$V_{OUT} = 3.3\text{ V}$ , $f_{SW} = 630\text{ kHz}$		89.0 %	
			$V_{OUT} = 2.5\text{ V}$ , $f_{SW} = 480\text{ kHz}$		86.9 %	
			$V_{OUT} = 1.8\text{ V}$ , $f_{SW} = 480\text{ kHz}$		85.2 %	
			$V_{OUT} = 1.2\text{ V}$ , $f_{SW} = 480\text{ kHz}$		82.1 %	
			$V_{OUT} = 0.8\text{ V}$ , $f_{SW} = 330\text{ kHz}$		78.7 %	
		$P_{VIN} = V_{IN} = 5\text{ V}$ $I_O = 1.5\text{ A}$	$V_{OUT} = 3.3\text{ V}$ , $f_{SW} = 630\text{ kHz}$		93.3 %	
			$V_{OUT} = 2.5\text{ V}$ , $f_{SW} = 480\text{ kHz}$		91.4 %	
			$V_{OUT} = 1.8\text{ V}$ , $f_{SW} = 480\text{ kHz}$		88.8 %	
			$V_{OUT} = 1.2\text{ V}$ , $f_{SW} = 480\text{ kHz}$		85.2 %	
	$V_{OUT} = 0.8\text{ V}$ , $f_{SW} = 330\text{ kHz}$		81.8 %			
	Output voltage ripple	20 MHz bandwidth		35		mV <sub>PP</sub>
$I_{LIM}$	Overcurrent threshold			5.8		A

- (1) The minimum  $P_{VIN}$  voltage is 1.6V or ( $V_{OUT} + 0.7\text{ V}$ ), whichever is greater.  $V_{IN}$  must be greater than 4.5V.
- (2) The stated limit of the set-point voltage tolerance includes the tolerance of both the internal voltage reference and the internal adjustment resistor. The overall output voltage tolerance will be affected by the tolerance of the external  $R_{SET}$  resistor.

## Electrical Characteristics (continued)

Over -40°C to 85°C free-air temperature,  $P_{VIN} = V_{IN} = 12\text{ V}$ ,  $V_{OUT} = 1.8\text{ V}$ ,  $I_{OUT} = 3\text{ A}$ ,

$C_{IN1} = 2 \times 22\text{ }\mu\text{F}$  ceramic,  $C_{IN2} = 68\text{ }\mu\text{F}$  poly-tantalum,  $C_{OUT1} = 4 \times 47\text{ }\mu\text{F}$  ceramic (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
Transient response		1.0 A/ $\mu\text{s}$ load step from 50 to 100% $I_{OUT(max)}$	Recovery time	190		$\mu\text{s}$
			$V_{OUT}$ over/undershoot	35		mV
$V_{INH-H}$	Inhibit Control	Inhibit High Voltage	1.30		Open <sup>(3)</sup>	V
$V_{INH-L}$		Inhibit Low Voltage	-0.3		1.05	
	INH Input current	INH < 1.1 V		-1.15		$\mu\text{A}$
	INH Hysteresis current	INH > 1.26 V		-3.4		$\mu\text{A}$
$I_{I(stby)}$	Input standby current	INH pin to AGND		2	4	$\mu\text{A}$
Power Good	PWRGD Thresholds	$V_{OUT}$ rising	Good	94%		
			Fault	109%		
		$V_{OUT}$ falling	Fault	91%		
			Good	106%		
	PWRGD Low Voltage	$I(PWRGD) = 2\text{ mA}$			0.3	V
$f_{SW}$	Switching frequency	Over $V_{IN}$ and $I_{OUT}$ ranges, RT/CLK pin OPEN	270	330	390	kHz
$f_{CLK}$	Synchronization frequency	CLK Control	330		780	kHz
$V_{CLK-H}$	CLK High-Level Threshold		2.0		5.5	V
$V_{CLK-L}$	CLK Low-Level Threshold				0.8	V
$D_{CLK}$	CLK Duty cycle		20%		80%	
	Thermal Shutdown		Thermal shutdown	160	175	
		Thermal shutdown hysteresis		10		$^{\circ}\text{C}$
$C_{IN}$	External input capacitance	Ceramic	22 <sup>(4)</sup>			$\mu\text{F}$
		Non-ceramic	68 <sup>(4)</sup>			
$C_{OUT}$	External output capacitance	Ceramic	200 <sup>(5)</sup>		1500	$\mu\text{F}$
		Non-ceramic			5000	
			Equivalent series resistance (ESR)			

- (3) This control pin has an internal pullup. If this pin is left open circuit, the device operates when input power is applied. A small low-leakage (<300 nA) MOSFET is recommended for control. See the application section for further guidance.
- (4) A minimum of 68  $\mu\text{F}$  of polymer tantalum and/or ceramic external capacitance is required across the input ( $V_{IN}$  and PGND connected) for proper operation. Locate the capacitor close to the device. See [Table 5](#) for more details. When operating with split  $V_{IN}$  and  $P_{VIN}$  rails, place 4.7  $\mu\text{F}$  of ceramic capacitance directly at the  $V_{IN}$  pin to PGND.
- (5) The amount of required output capacitance varies depending on the output voltage (see [Table 3](#)). The amount of required capacitance must include ceramic capacitance. Locate the capacitance close to the device. Adding additional capacitance close to the load improves the response of the regulator to load transients. See [Table 3](#) and [Table 5](#) more details.

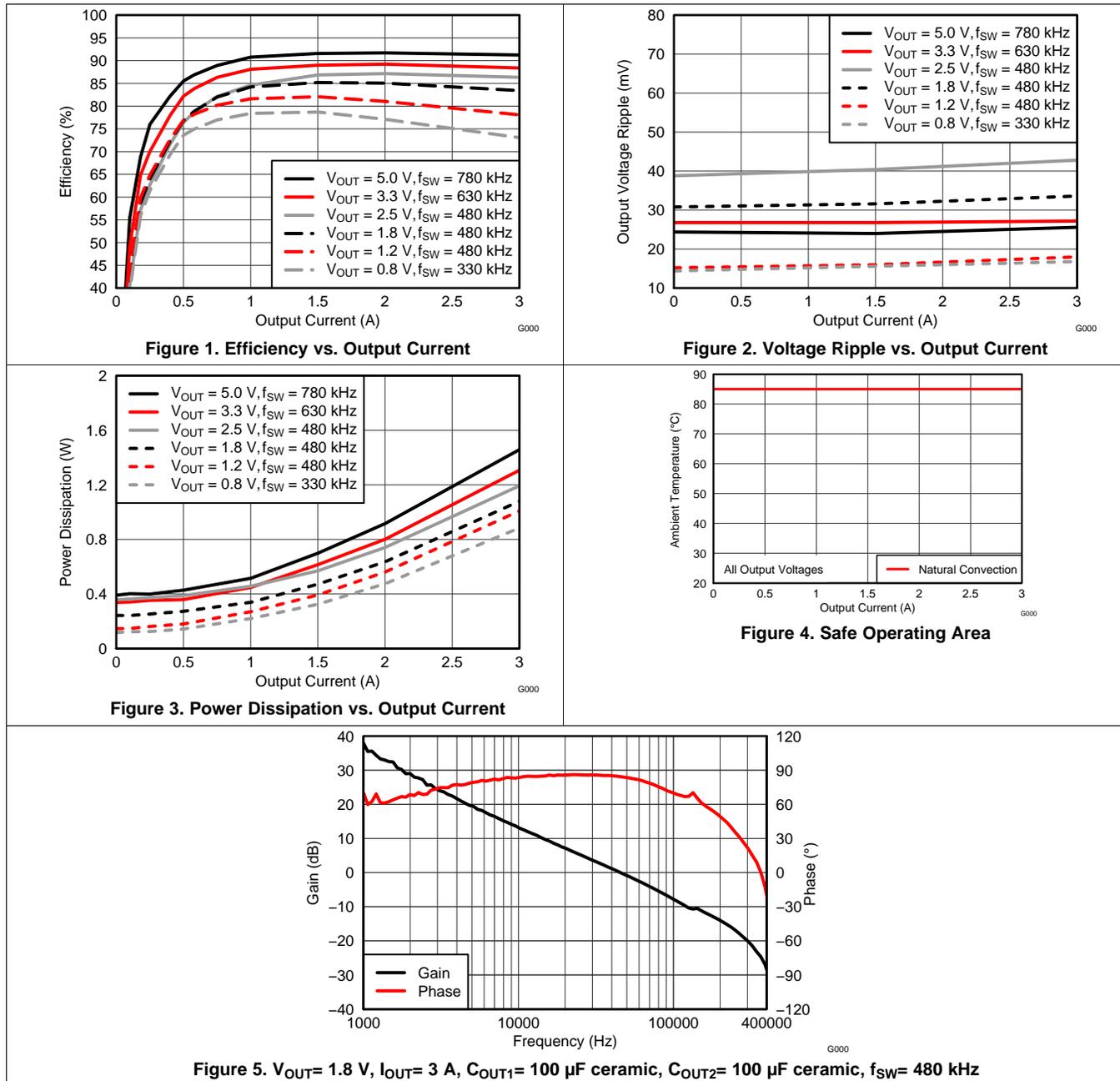


### Pin Descriptions

TERMINAL		DESCRIPTION
NAME	NO.	
AGND	1	Zero VDC reference for the analog control circuitry. Connect AGND to PGND at a single point. Connect near the output capacitors. See for a recommended layout.
	2	
	34	
	45	
INH/UVLO	8	Inhibit and UVLO adjust pin. Use an open drain or open collector output logic to control the INH function. A resistor divider between this pin, AGND and VIN adjusts the UVLO voltage. Tie both pins together when using this control.
	9	
DNC	3	Do Not Connect. Do not connect these pins to AGND, to another DNC pin, or to any other voltage. These pins are connected to internal circuitry. Each pin must be soldered to an isolated pad.
	4	
	5	
	15	
	16	
	18	
	19	
	20	
	22	
	23	
	30	
	31	
32		
PGND	36	Common ground connection for the PVIN, VIN, and VOUT power connections. See for a recommended layout.
	37	
	38	
PH	10	Phase switch node. These pins should be connected to a small copper island under the device for thermal relief. Do not place any external component on this pin or tie it to a pin of another function.
	11	
	12	
	13	
	14	
	17	
46		
PWRGD	33	Power good fault pin. Asserts low if the output voltage is low. A pull-up resistor is required.
PVIN	39	Input switching voltage. This pin supplies voltage to the power switches of the converter. See for a recommended layout.
	40	
	41	
RT/CLK	35	This pin automatically selects between RT mode and CLK mode. An external timing resistor adjusts the switching frequency of the device. In CLK mode, the device synchronizes to an external clock.
SENSE+	44	Remote sense connection. Connect this pin to VOUT at the load for improved regulation. This pin must be connected to VOUT at the load, or at the module pins.
SS/TR	6	Slow-start and tracking pin. Connecting an external capacitor to this pin adjusts the output voltage rise time. A voltage applied to this pin allows for tracking and sequencing control.
STSEL	7	Slow-start or track feature select. Connect this pin to AGND to enable the internal SS capacitor with a SS interval of approximately 1.1 ms. Leave this pin open to enable the TR feature.
VADJ	43	Connecting a resistor between this pin and AGND sets the output voltage.
VIN	42	Input bias voltage pin. Supplies the control circuitry of the power converter. See for a recommended layout.

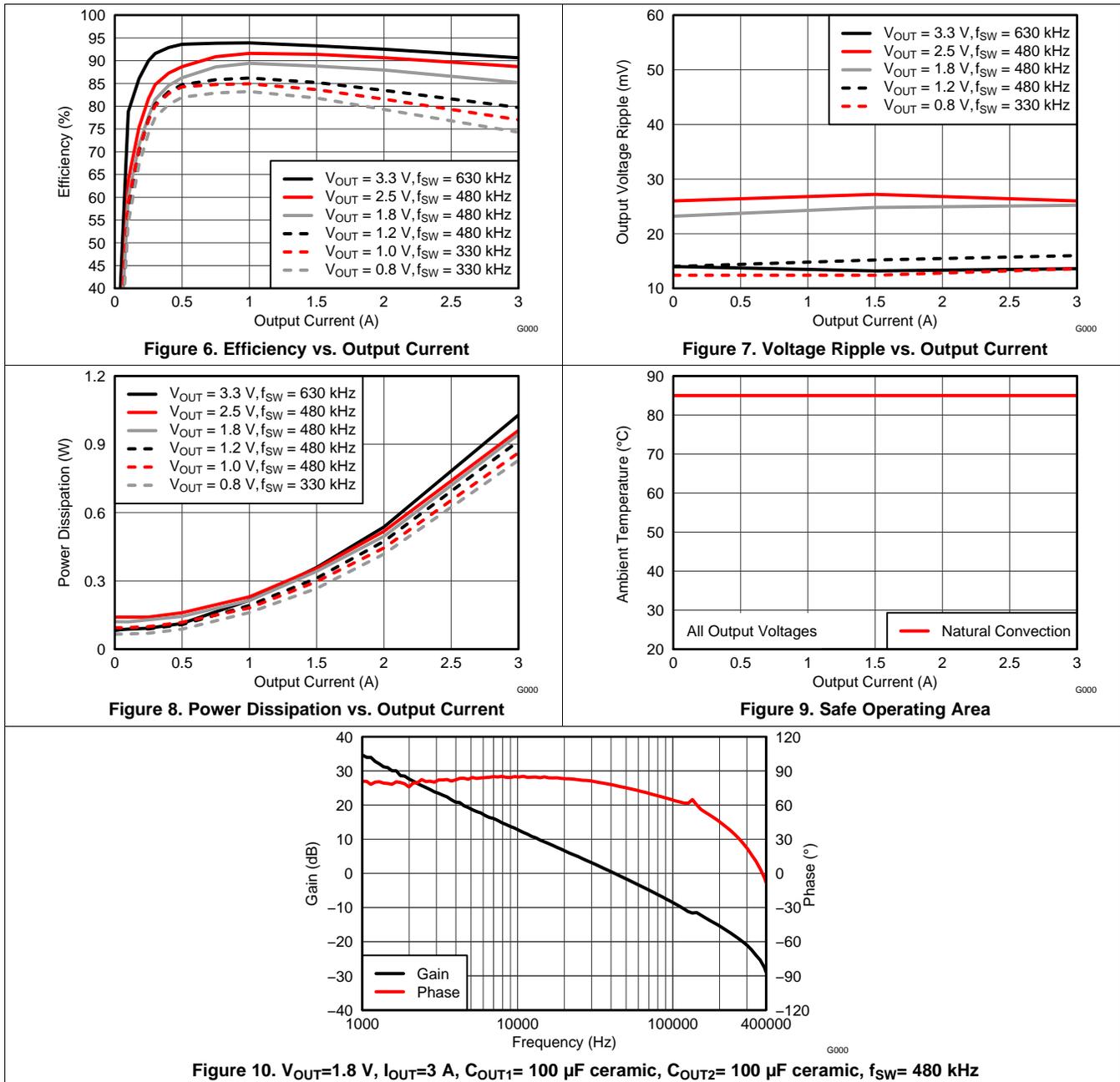


## 6 Typical Characteristics (PVIN = VIN = 12 V) <sup>(1)</sup> <sup>(2)</sup>



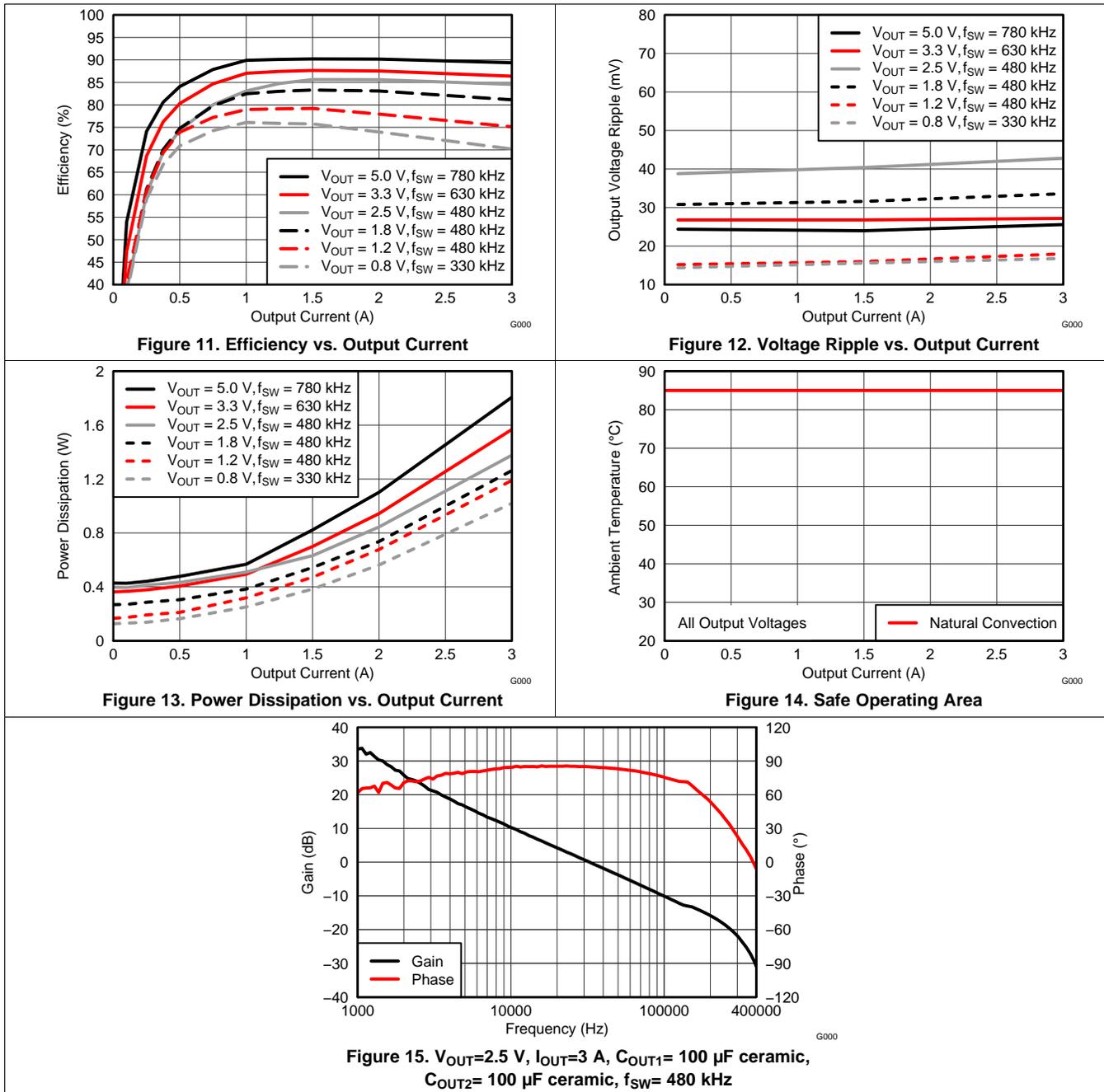
- (1) The electrical characteristic data has been developed from actual products tested at 25°C. This data is considered typical for the converter. Applies to [Figure 1](#), [Figure 2](#), and [Figure 3](#).
- (2) The temperature derating curves represent the conditions at which internal components are at or below the manufacturer's maximum operating temperatures. Derating limits apply to devices soldered directly to a 100 mm x 100 mm double-sided PCB with 1 oz. copper. Applies to [Figure 4](#).

7 Typical Characteristics (PVIN = VIN = 5 V) (1) (2)



- (1) The electrical characteristic data has been developed from actual products tested at 25°C. This data is considered typical for the converter. Applies to [Figure 6](#), [Figure 7](#), and [Figure 8](#).
- (2) The temperature derating curves represent the conditions at which internal components are at or below the manufacturer's maximum operating temperatures. Derating limits apply to devices soldered directly to a 100 mm x 100 mm double-sided PCB with 1 oz. copper. Applies to [Figure 9](#).

## 8 Typical Characteristics (P<sub>VIN</sub> = 12 V, V<sub>IN</sub> = 5 V) <sup>(1)</sup> <sup>(2)</sup>



- (1) The electrical characteristic data has been developed from actual products tested at 25°C. This data is considered typical for the converter. Applies to [Figure 11](#), [Figure 12](#), and [Figure 13](#).
- (2) The temperature derating curves represent the conditions at which internal components are at or below the manufacturer's maximum operating temperatures. Derating limits apply to devices soldered directly to a 100 mm x 100 mm double-sided PCB with 1 oz. copper. Applies to [Figure 14](#).

## 9 Application Information

### 9.1 Adjusting the Output Voltage

The VADJ control sets the output voltage of the LMZ31503. The output voltage adjustment range is from 0.8V to 5.5V. The adjustment method requires the addition of  $R_{SET}$ , which sets the output voltage, the connection of SENSE+ to VOUT, and in some cases  $R_{RT}$  which sets the switching frequency. The  $R_{SET}$  resistor must be connected directly between the VADJ (pin 43) and AGND (pin 45). The SENSE+ pin (pin 44) must be connected to VOUT either at the load for improved regulation or at VOUT of the module. The  $R_{RT}$  resistor must be connected directly between the RT/CLK (pin 35) and AGND (pin 34).

Table 1 gives the standard external  $R_{SET}$  resistor for a number of common bus voltages, along with the required  $R_{RT}$  resistor for that output voltage. For other output voltages, the value of the required resistor can either be calculated using Equation 1, or selected from the values given in Table 2.

**Table 1. Standard  $R_{SET}$  Resistor Values for Common Output Voltages**

RESISTORS	OUTPUT VOLTAGE $V_{OUT}$ (V)							
	0.8	1.0	1.2	1.5	1.8	2.5	3.3	5.0
$R_{SET}$ (k $\Omega$ )	open	5.76	2.87	1.62	1.13	0.665	0.453	0.267
$R_{RT}$ (k $\Omega$ )	open	open	324	324	324	324	158	105

$$R_{SET} = \frac{1.43}{\left(\left(\frac{V_{OUT}}{0.8}\right) - 1\right)} \text{ (k}\Omega\text{)} \quad (1)$$

**Table 2. Standard  $R_{SET}$  Resistor Values**

$V_{OUT}$ (V)	$R_{SET}$ (k $\Omega$ )	$R_{RT}$ (k $\Omega$ )	$f_{sw}$ (kHz)	$V_{OUT}$ (V)	$R_{SET}$ (k $\Omega$ )	$R_{RT}$ (k $\Omega$ )	$f_{sw}$ (kHz)
0.8	open	open	330	3.2	0.475	191	580
0.9	11.3	open	330	3.3	0.453	158	630
1.0	5.76	open	330	3.4	0.442	158	630
1.1	3.83	open	330	3.5	0.422	158	630
1.2	2.87	324	480	3.6	0.402	158	630
1.3	2.26	324	480	3.7	0.392	158	630
1.4	1.91	324	480	3.8	0.374	137	680
1.5	1.62	324	480	3.9	0.365	137	680
1.6	1.43	324	480	4.0	0.357	137	680
1.7	1.27	324	480	4.1	0.348	137	680
1.8	1.13	324	480	4.2	0.332	118	730
1.9	1.02	324	480	4.3	0.324	118	730
2.0	0.953	324	480	4.4	0.316	118	730
2.1	0.866	324	480	4.5	0.309	118	730
2.2	0.806	324	480	4.6	0.301	118	730
2.3	0.750	324	480	4.7	0.294	118	730
2.4	0.715	324	480	4.8	0.287	105	780
2.5	0.665	324	480	4.9	0.280	105	780
2.6	0.634	237	530	5.0	0.267	105	780
2.7	0.604	237	530	5.1	0.267	105	780
2.8	0.562	237	530	5.2	0.261	105	780
2.9	0.536	237	530	5.3	0.255	105	780
3.0	0.511	191	580	5.4	0.249	105	780
3.1	0.499	191	580	5.5	0.243	105	780

## 9.2 Capacitor Recommendations for the LMZ31503 Power Supply

### 9.2.1 Capacitor Technologies

#### 9.2.1.1 Electrolytic, Polymer-Electrolytic Capacitors

When using electrolytic capacitors, high-quality, computer-grade electrolytic capacitors are recommended. Polymer-electrolytic type capacitors are recommended for applications where the ambient operating temperature is less than 0°C. The Sanyo OS-CON capacitor series is suggested due to the lower ESR, higher rated surge, power dissipation, ripple current capability, and small package size. Aluminum electrolytic capacitors provide adequate decoupling over the frequency range of 2 kHz to 150 kHz, and are suitable when ambient temperatures are above 0°C.

#### 9.2.1.2 Ceramic Capacitors

The performance of aluminum electrolytic capacitors is less effective than ceramic capacitors above 150 kHz. Multilayer ceramic capacitors have a low ESR and a resonant frequency higher than the bandwidth of the regulator. They can be used to reduce the reflected ripple current at the input as well as improve the transient response of the output.

#### 9.2.1.3 Tantalum, Polymer-Tantalum Capacitors

Polymer-tantalum type capacitors are recommended for applications where the ambient operating temperature is less than 0°C. The Sanyo POSCAP series and Kemet T530 capacitor series are recommended rather than many other tantalum types due to their lower ESR, higher rated surge, power dissipation, ripple current capability, and small package size. Tantalum capacitors that have no stated ESR or surge current rating are not recommended for power applications.

### 9.2.2 Input Capacitor

The LMZ31503 requires a minimum input capacitance of 68  $\mu\text{F}$  of ceramic and/or polymer-tantalum capacitors. The ripple current rating of the capacitor must be at least 450 mArms. [Table 5](#) includes a preferred list of capacitors by vendor.

### 9.2.3 Output Capacitor

The required output capacitance is determined by the output voltage of the LMZ31503. See [Table 3](#) for the amount of required capacitance. The required output capacitance must be comprised of all ceramic capacitors. When adding additional non-ceramic bulk capacitors, low-ESR devices like the ones recommended in [Table 5](#) are required. The required capacitance above the minimum is determined by actual transient deviation requirements. See [Table 4](#) for typical transient response values for several output voltage, input voltage and capacitance combinations. [Table 5](#) includes a preferred list of capacitors by vendor.

**Table 3. Required Output Capacitance**

$V_{\text{OUT}}$ RANGE (V)		MINIMUM REQUIRED $C_{\text{OUT}}$ ( $\mu\text{F}$ )
MIN	MAX	
0.8	< 1.2	6x 47 $\mu\text{F}$ ceramic
1.2	< 3.0	4x 47 $\mu\text{F}$ ceramic
3.0	< 4.0	2x 47 $\mu\text{F}$ ceramic
4.0	5.5	47 $\mu\text{F}$ ceramic

**Table 4. Output Voltage Transient Response**

C <sub>IN1</sub> = 22 µF CERAMIC, C <sub>IN2</sub> = 68 µF POSCAP, LOAD STEP = 1.5 A, 1 A/µs						
V <sub>OUT</sub> (V)	PV <sub>IN</sub> (V)	C <sub>OUT1</sub> Ceramic	C <sub>OUT2</sub> BULK	VOLTAGE DEVIATION (mV)	PEAK-PEAK (mV)	RECOVERY TIME (µs)
0.8	5	6x 47 µF	None	25	55	170
		6x 47 µF	330 µF	15	30	160
	12	6x 47 µF	None	20	35	180
		6x 47 µF	330 µF	15	30	170
1.0	5	6x 47 µF	None	20	40	170
		6x 47 µF	330 µF	15	30	170
	12	6x 47 µF	None	20	45	180
		6x 47 µF	330 µF	15	30	170
1.2	5	4x 47 µF	None	30	55	170
		4x 47 µF	220 µF	25	45	170
	12	4x 47 µF	None	30	55	180
		4x 47 µF	220 µF	25	50	170
1.8	5	4x 47 µF	None	35	65	180
		4x 47 µF	220 µF	30	55	180
	12	4x 47 µF	None	35	65	190
		4x 47 µF	220 µF	30	55	180
3.3	5	2x 47 µF	None	65	130	190
		2x 47 µF	100 µF	55	110	190
	12	2x 47 µF	None	65	130	200
		2x 47 µF	100 µF	60	120	200
5.0	12	1x 47 µF	None	100	200	210
		1x 47 µF	100 µF	85	170	210

**Table 5. Recommended Input/Output Capacitors<sup>(1)</sup>**

VENDOR	SERIES	PART NUMBER	CAPACITOR CHARACTERISTICS		
			WORKING VOLTAGE (V)	CAPACITANCE (µF)	ESR <sup>(2)</sup> (mΩ)
Murata	X5R	GRM32ER61E226K	16	22	2
TDK	X5R	C3225X5R0J476K	6.3	47	2
Murata	X5R	GRM32ER60J476M	6.3	47	2
Sanyo	POSCAP	16TQC68M	16	68	50
Kemet	T520	T520V107M010ASE025	10	100	25
Sanyo	POSCAP	6TPE100MI	6.3	100	25
Sanyo	POSCAP	2R5TPE220M7	2.5	220	7
Kemet	T530	T530D227M006ATE006	6.3	220	6
Kemet	T530	T530D337M006ATE010	6.3	330	10
Sanyo	POSCAP	2TPF330M6	2.0	330	6
Sanyo	POSCAP	6TPE330MFL	6.3	330	15

**(1) Capacitor Supplier Verification**

Please verify availability of capacitors identified in this table.

**RoHS, Lead-free and Material Details**

Please consult capacitor suppliers regarding material composition, RoHS status, lead-free status, and manufacturing process requirements.

**(2) Maximum ESR @ 100kHz, 25°C.**

### 9.3 Transient Response

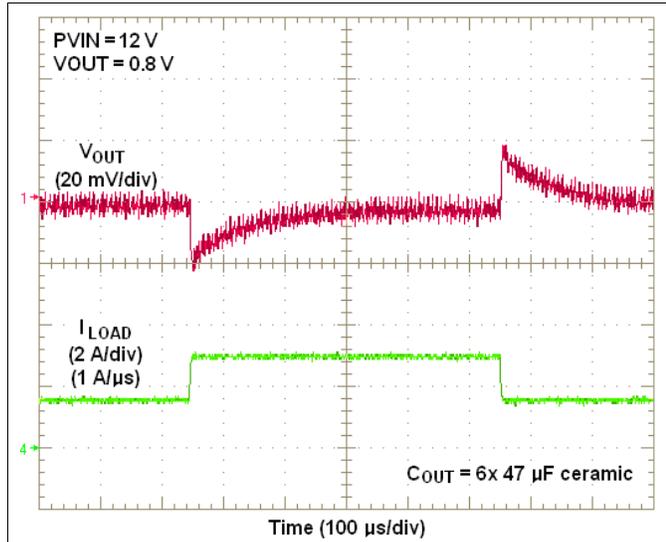


Figure 16.  $P_{VIN} = 12\text{ V}$ ,  $V_{OUT} = 0.8\text{ V}$ , 1.5A Load Step

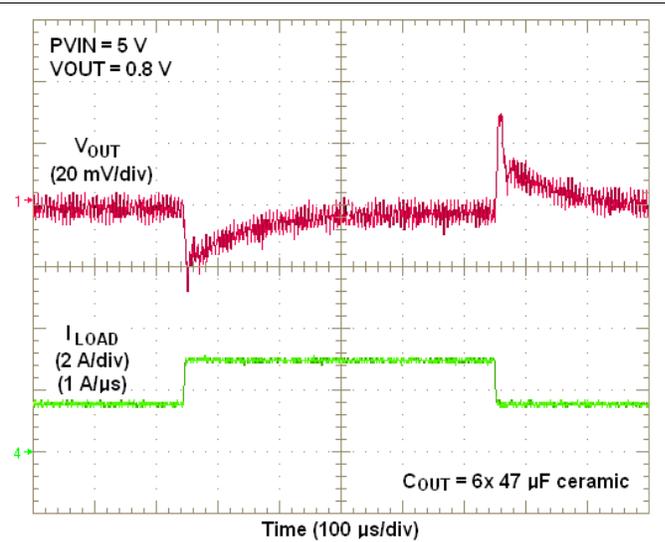


Figure 17.  $P_{VIN} = 5\text{ V}$ ,  $V_{OUT} = 0.8\text{ V}$ , 1.5A Load Step

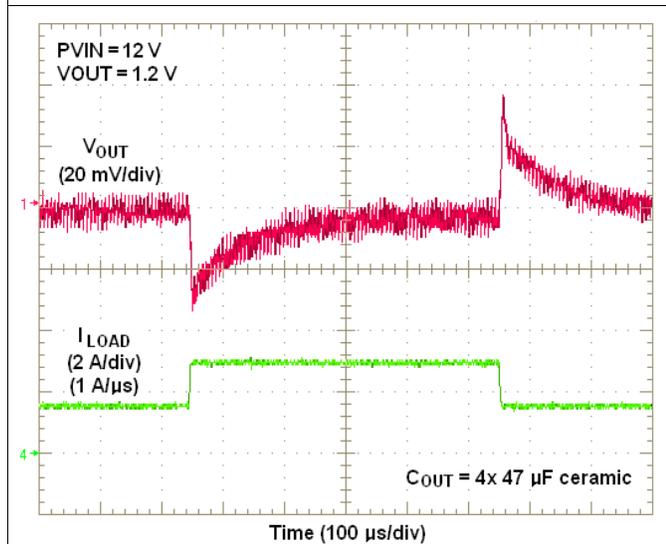


Figure 18.  $P_{VIN} = 12\text{ V}$ ,  $V_{OUT} = 1.2\text{ V}$ , 1.5A Load Step

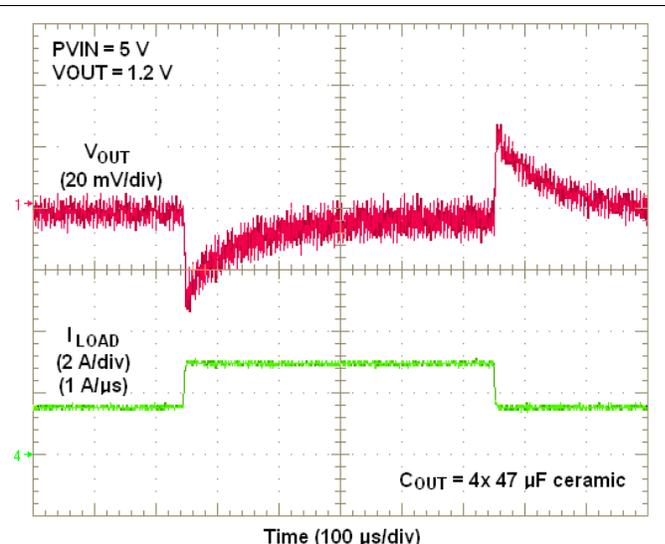
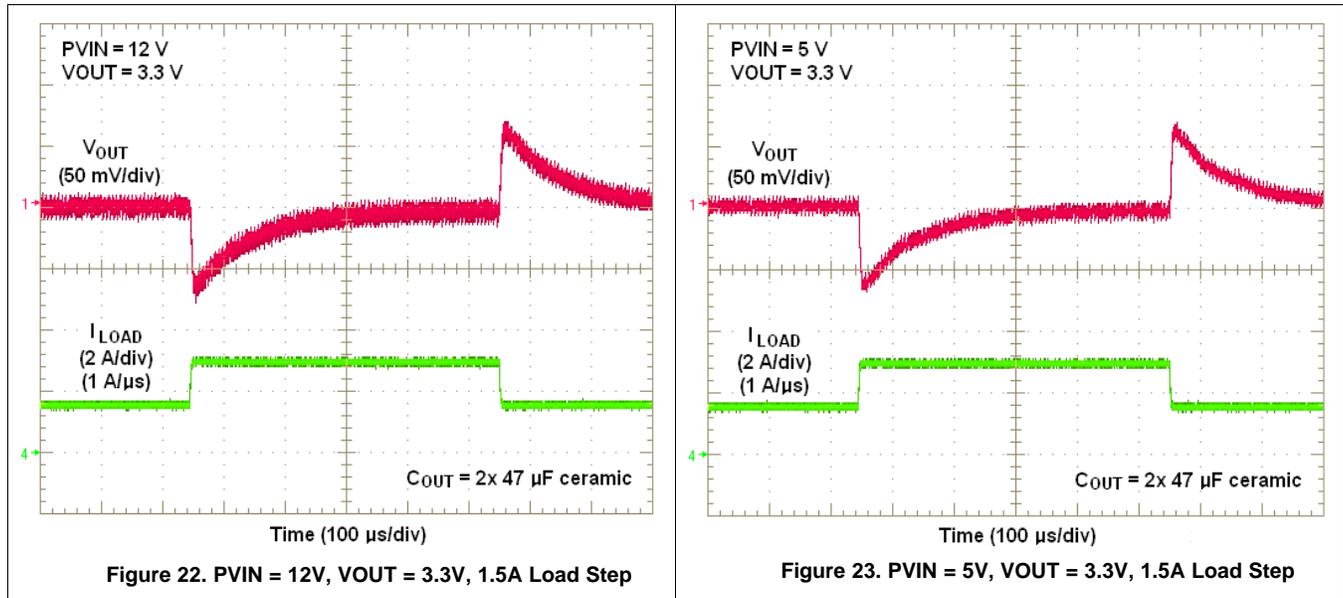
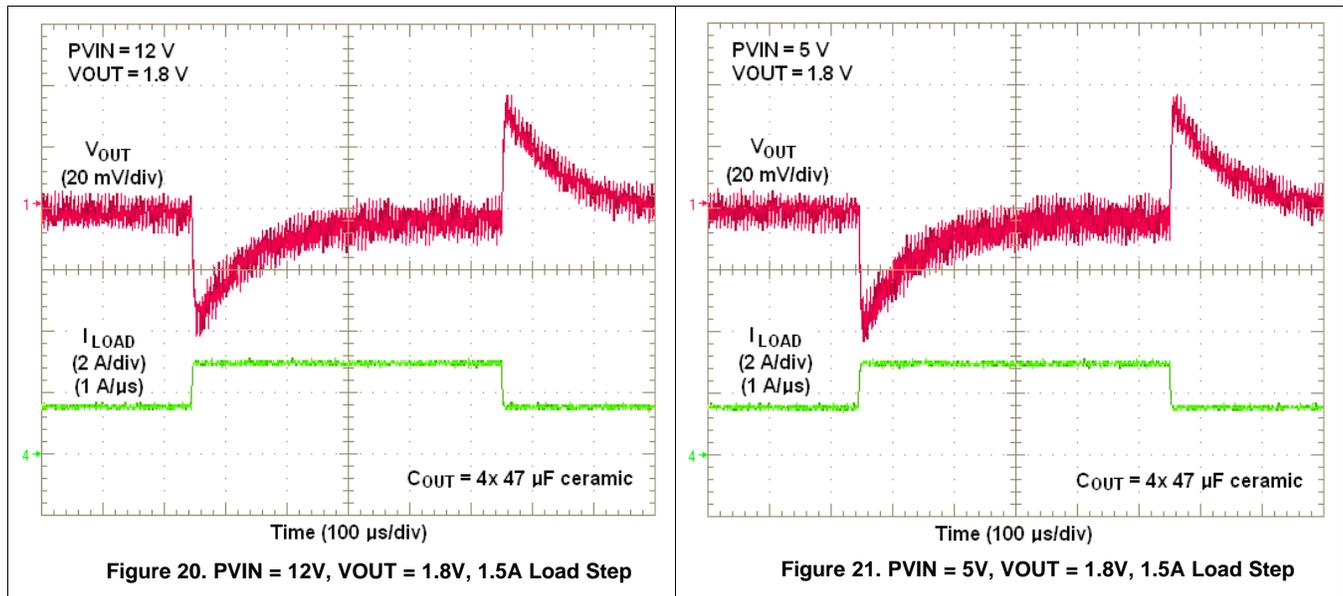
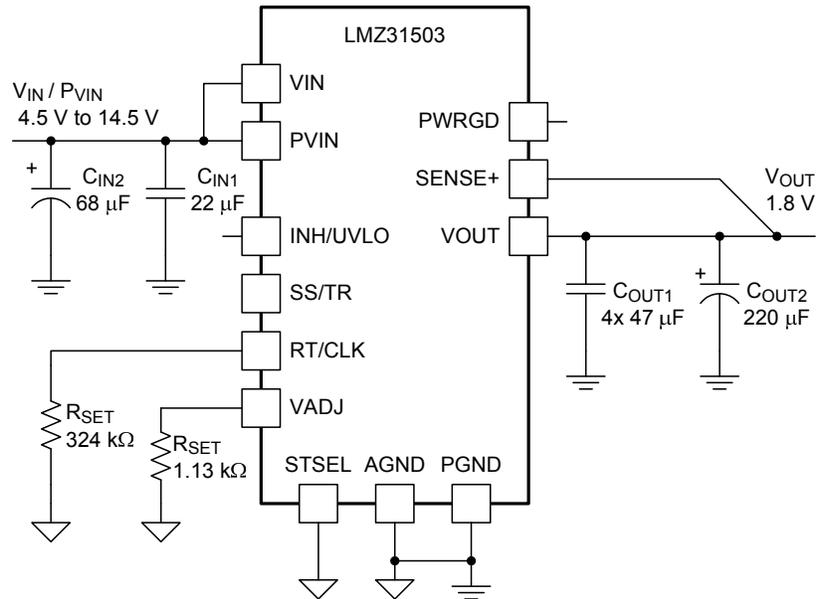


Figure 19.  $P_{VIN} = 5\text{ V}$ ,  $V_{OUT} = 1.2\text{ V}$ , 1.5A Load Step

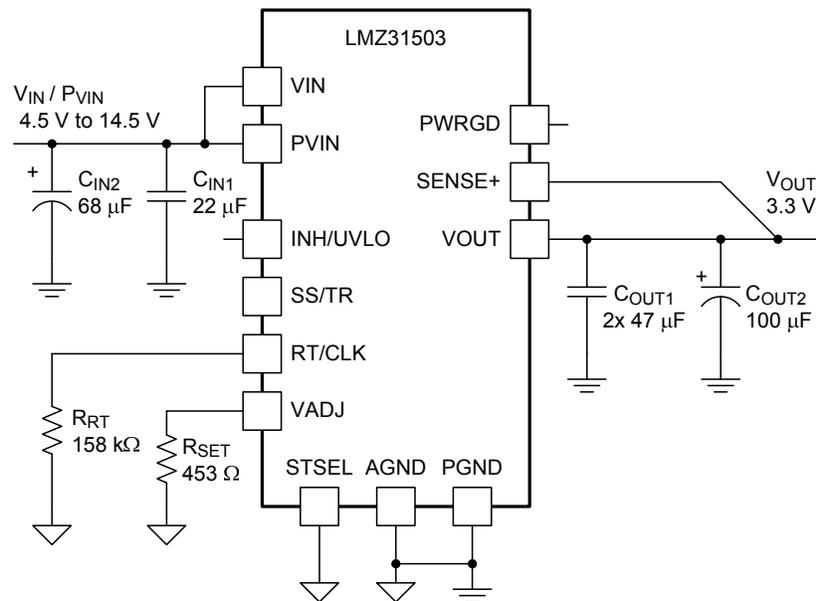
Transient Response (continued)



## 9.4 Application Schematics

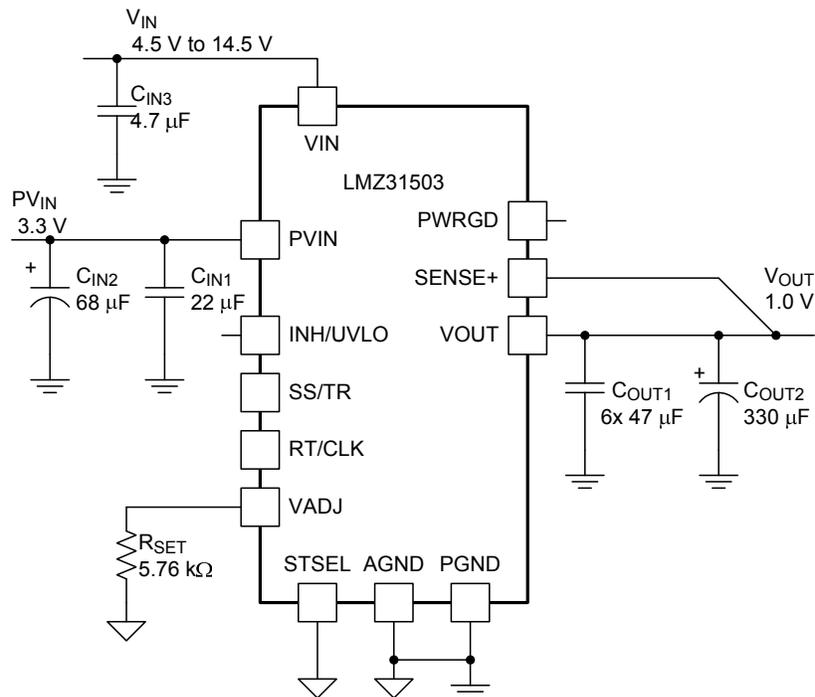


**Figure 24. Typical Schematic**  
**PVIN = VIN = 4.5 V to 14.5 V, VOUT = 1.8 V**



**Figure 25. Typical Schematic**  
**PVIN = VIN = 4.5 V to 14.5 V, VOUT = 3.3 V**

**Application Schematics (continued)**



**Figure 26. Typical Schematic**  
**PVIN = 3.3 V, VIN = 4.5 V to 14.5 V, VOUT = 1.0 V**

## 9.5 Custom Design With WEBENCH® Tools

[Click here](#) to create a custom design using the LMZ31503 device with the WEBENCH® Power Designer.

1. Start by entering the input voltage ( $V_{IN}$ ), output voltage ( $V_{OUT}$ ), and output current ( $I_{OUT}$ ) requirements.
2. Optimize the design for key parameters such as efficiency, footprint, and cost using the optimizer dial.
3. Compare the generated design with other possible solutions from Texas Instruments.

The WEBENCH Power Designer provides a customized schematic along with a list of materials with real-time pricing and component availability.

In most cases, these actions are available:

- Run electrical simulations to see important waveforms and circuit performance
- Run thermal simulations to understand board thermal performance
- Export customized schematic and layout into popular CAD formats
- Print PDF reports for the design, and share the design with colleagues

Get more information about WEBENCH tools at [www.ti.com/WEBENCH](http://www.ti.com/WEBENCH).

## 9.6 VIN and PVIN Input Voltage

The LMZ31503 allows for a variety of applications by using the VIN and PVIN pins together or separately. The VIN voltage supplies the internal control circuits of the device. The PVIN voltage provides the input voltage to the power converter system.

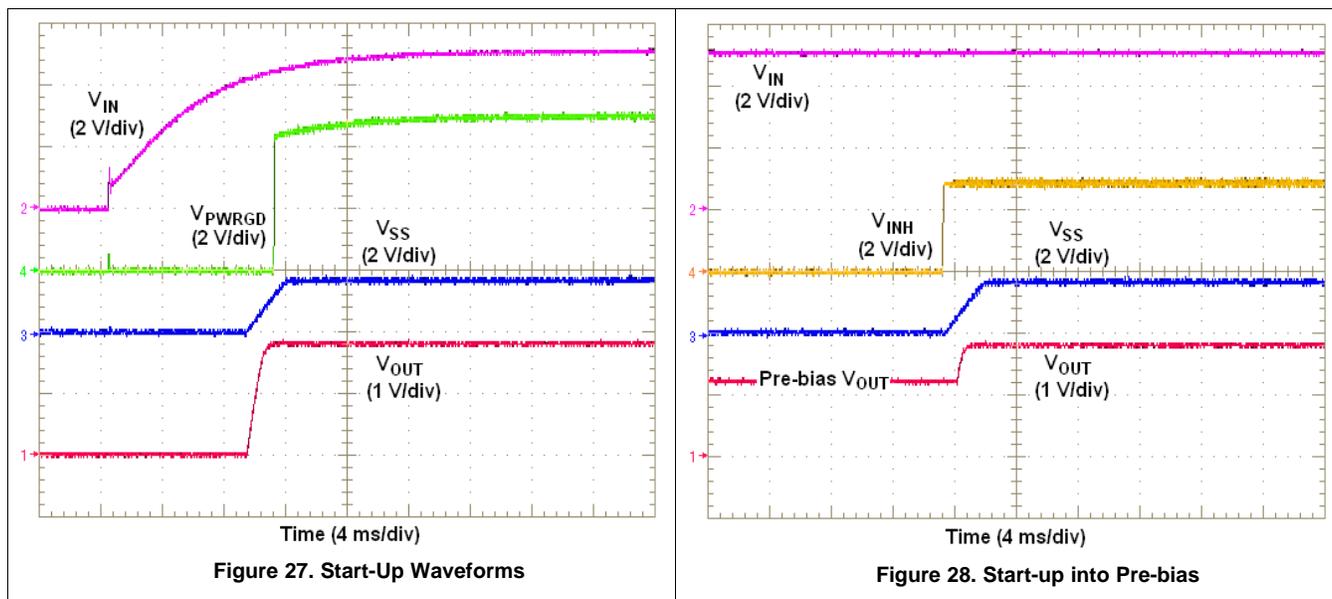
If tied together, the input voltage for the VIN pin and the PVIN pin can range from 4.5 V to 14.5 V. If using the VIN pin separately from the PVIN pin, the VIN pin must be between 4.5 V and 14.5 V, and the PVIN pin can range from as low as 1.6 V to 14.5 V. A voltage divider connected to the INH/UVLO pin can adjust the either input voltage UVLO appropriately. See the [Programmable Undervoltage Lockout \(UVLO\)](#) section of this datasheet for more information.

## 9.7 Power Good (PWRGD)

The PWRGD pin is an open drain output. Once the voltage on the SENSE+ pin is between 94% and 106% of the set voltage, the PWRGD pin pull-down is released and the pin floats. The recommended pull-up resistor value is between 10 k $\Omega$  and 100 k $\Omega$  to a voltage source that is 5.5 V or less. The PWRGD pin is in a defined state once VIN is greater than 1.0 V, but with reduced current sinking capability. The PWRGD pin achieves full current sinking capability once the VIN pin is above 4.5V. The PWRGD pin is pulled low when the voltage on SENSE+ is lower than 91% or greater than 109% of the nominal set voltage. Also, the PWRGD pin is pulled low if the input UVLO or thermal shutdown is asserted, the INH pin is pulled low, or the SS/TR pin is below 1.4 V.

## 9.8 Power-Up Characteristics

When configured as shown in the front page schematic, the LMZ31503 produces a regulated output voltage following the application of a valid input voltage. During the power-up, internal soft-start circuitry slows the rate that the output voltage rises, thereby limiting the amount of in-rush current that can be drawn from the input source. The soft-start circuitry introduces a short time delay from the point that a valid input voltage is recognized. Figure 27 shows the start-up waveforms for a LMZ31503, operating from a 5-V input ( $P_{VIN}=V_{IN}$ ) and with the output voltage adjusted to 1.8 V. Figure 28 shows the start-up waveforms for a LMZ31503 starting up into a pre-biased output voltage. The waveforms were measured with a 2-A constant current load.



## 9.9 Pre-Biased Start-Up

The LMZ31503 has been designed to prevent discharging a pre-biased output. During monotonic pre-biased startup, the LMZ31503 does not allow current to sink until the SS/TR pin voltage is higher than 1.4 V.

## 9.10 Remote Sense

The SENSE+ pin must be connected to  $V_{OUT}$  at the load, or at the device pins.

Connecting the SENSE+ pin to  $V_{OUT}$  at the load improves the load regulation performance of the device by allowing it to compensate for any I-R voltage drop between its output pins and the load. An I-R drop is caused by the high output current flowing through the small amount of pin and trace resistance. This should be limited to a maximum of 300 mV.

### NOTE

The remote sense feature is not designed to compensate for the forward drop of nonlinear or frequency dependent components that may be placed in series with the converter output. Examples include OR-ing diodes, filter inductors, ferrite beads, and fuses. When these components are enclosed by the SENSE+ connection, they are effectively placed inside the regulation control loop, which can adversely affect the stability of the regulator.

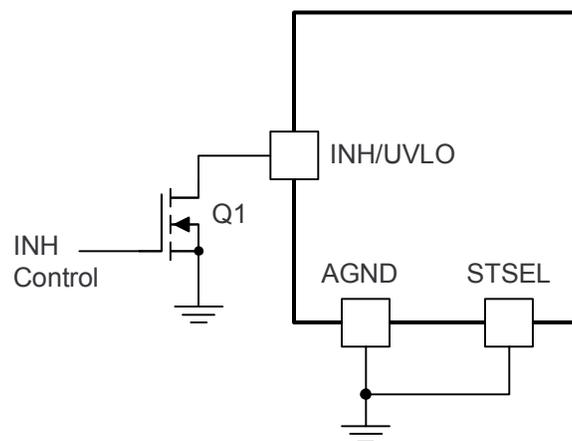
## 9.11 Output On/Off Inhibit (INH)

The INH pin provides electrical on/off control of the device. Once the INH pin voltage exceeds the threshold voltage, the device starts operation. If the INH pin voltage is pulled below the threshold voltage, the regulator stops switching and enters low quiescent current state.

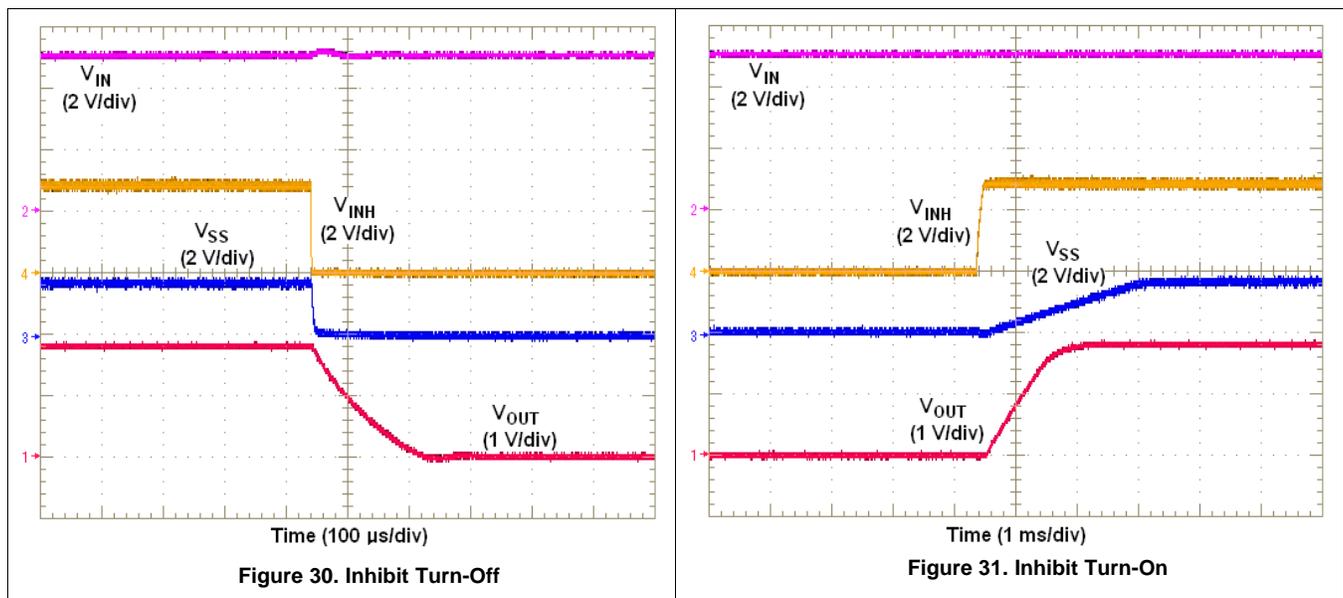
The INH pin has an internal pull-up current source, allowing the user to float the INH pin for enabling the device. If an application requires controlling the INH pin, use an open drain/collector device, or a suitable logic gate to interface with the pin.

Figure 29 shows the typical application of the inhibit function. The Inhibit control has its own internal pull-up to VIN potential. An open-collector or open-drain device is recommended to control this input.

Turning Q1 on applies a low voltage to the inhibit control (INH) pin and disables the output of the supply, shown in Figure 30. If Q1 is turned off, the supply executes a soft-start power-up sequence, as shown in Figure 31. A regulated output voltage is produced within 10 ms. The waveforms were measured with a 2-A constant resistance load.



**Figure 29. Typical Inhibit Control**



### 9.12 Slow Start (SS/TR)

Connecting the STSEL pin to AGND and leaving SS/TR pin open enables the internal SS capacitor with a slow start interval of approximately 1.1 ms. Adding additional capacitance between the SS pin and AGND increases the slow start time. Table 6 shows an additional SS capacitor connected to the SS/TR pin and the STSEL pin connected to AGND. See Table 6 below for SS capacitor values and timing interval.

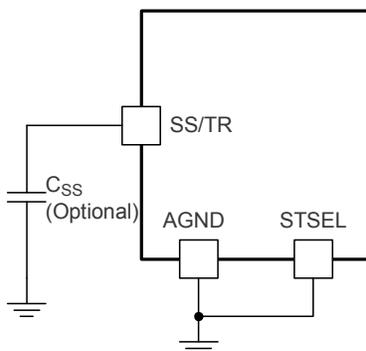


Figure 32. Slow-Start Capacitor ( $C_{SS}$ ) and STSEL Connection

Table 6. Slow-Start Capacitor Values and Slow-Start Time

$C_{SS}$ (pF)	open	2200	4700	10000	15000	22000	25000
SS Time (msec)	1.1	1.9	2.8	4.6	6.4	8.8	9.8

### 9.13 Overcurrent Protection

For protection against load faults, the LMZ31503 incorporates output overcurrent protection. Applying a load that exceeds the regulator's overcurrent threshold causes the regulated output to shut down. Following shutdown, the output voltage periodically attempts to recover by initiating a soft-start power-up. This is described as a *hiccup* mode of operation, whereby the module continues in a cycle of successive shutdown and power up until the load fault is removed, as shown in Figure 33. During this period, the average current flowing into the fault is significantly reduced. Once the fault is removed, the module automatically recovers and returns to normal operation, as shown in Figure 34.

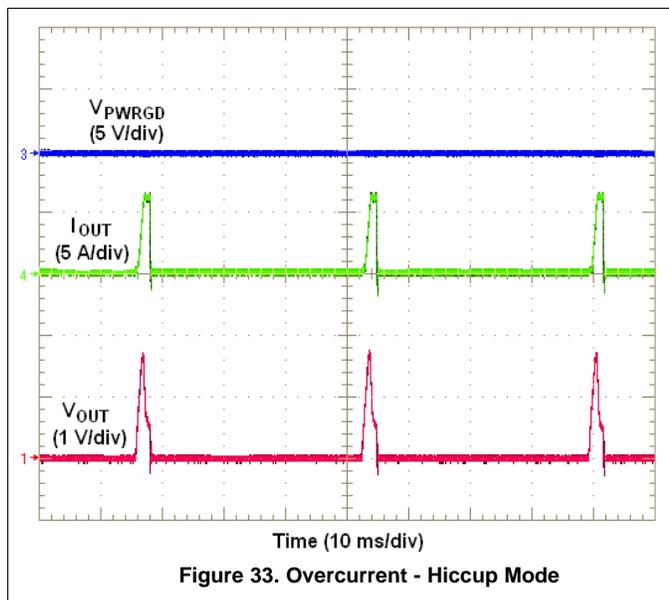


Figure 33. Overcurrent - Hiccup Mode

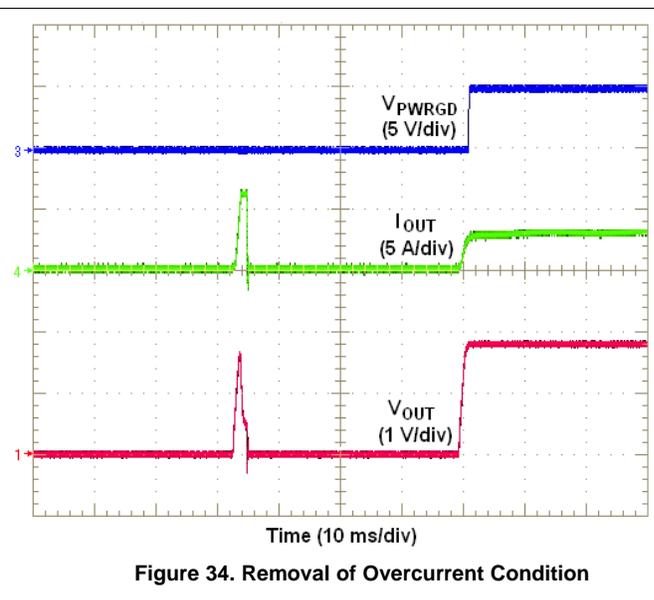
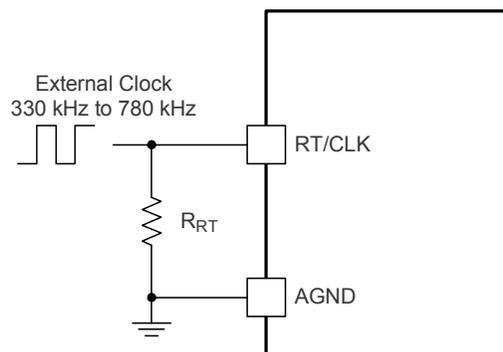


Figure 34. Removal of Overcurrent Condition

## 9.14 Synchronization (CLK)

An internal phase locked loop (PLL) has been implemented to allow synchronization between 330 kHz and 780 kHz, and to easily switch from RT mode to CLK mode. To implement the synchronization feature, connect a square wave clock signal to the RT/CLK pin with a duty cycle between 20% to 80%. The clock signal amplitude must transition lower than 0.8 V and higher than 2.0 V. The start of the switching cycle is synchronized to the falling edge of RT/CLK pin. In applications where both RT mode and CLK mode are needed, the device can be configured as shown in .

Before the external clock is present, the device works in RT mode and the switching frequency is set by RT resistor ( $R_{RT}$ ). When the external clock is present, the CLK mode overrides the RT mode. The first time the CLK pin is pulled above the RT/CLK high threshold (2.0 V), the device switches from RT mode to th CLK mode and the RT/CLK pin becomes high impedance as the PLL starts to lock onto the frequency of the external clock. It is not recommended to switch from CLK mode back to RT mode because the internal switching frequency drops to 100 kHz and may shut-down due to internal protection circuits before returning to the switching frequency set by the RT resistor.



**Figure 35. CLK/RT Configuration**

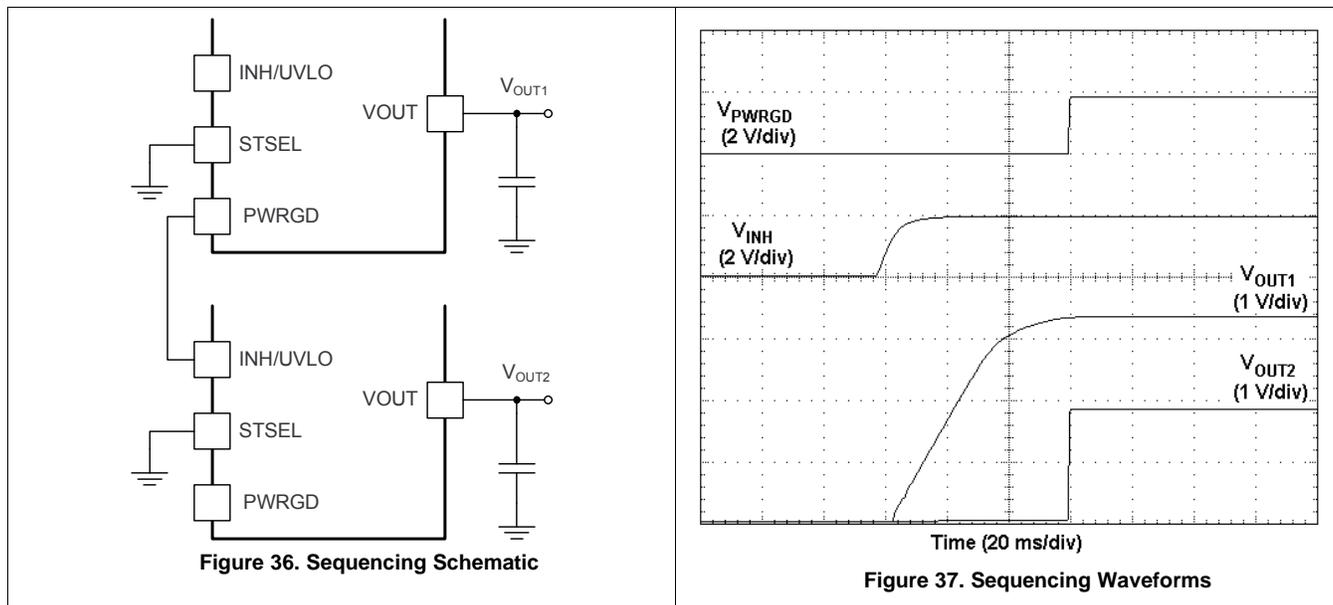
The synchronization frequency must be selected based on the output voltages of the devices being synchronized. [Table 7](#) shows the allowable frequencies for a given range of output voltages. For the most efficient solution, always synchronize to the lowest allowable frequency. For example, an application requires synchronizing three LMZ31503 devices with output voltages of 1.2 V, 1.8 V and 2.5 V, all powered from  $P_{VIN} = 12\text{ V}$ . [Table 7](#) shows that all three output voltages can be synchronized to frquencies between 480 kHz to 630 kHz. For best efficiency, choose 480 kHz as the sychronization frequency.

**Table 7. Synchronization Frequency vs Output Voltage**

SYNCHRONIZATION FREQUENCY (kHz)	$R_{RT}$ (k $\Omega$ )	$P_{VIN} = 12\text{ V}$		$P_{VIN} = 5\text{ V}$	
		$V_{OUT}$ RANGE (V)		$V_{OUT}$ RANGE (V)	
		MIN	MAX	MIN	MAX
330	OPEN	0.8	1.5	0.8	4.3
380	1000	0.8	1.7		
430	499	0.8	2.1		
480	324	0.9	2.5		
530	237	1.0	2.9		
580	191	1.1	3.2		
630	158	1.2	3.7		
680	137	1.3	4.1		
730	118	1.4	4.7		
780	105	1.5	5.5		

### 9.15 Sequencing (SS/TR)

Many of the common power supply sequencing methods can be implemented using the SS/TR, INH and PWRGD pins. The sequential method is illustrated in Figure 36 using two LMZ31503 devices. The PWRGD pin of the first device is coupled to the INH pin of the second device which enables the second power supply once the primary supply reaches regulation. Figure 37 shows sequential turn-on waveforms of two LMZ31503 devices.



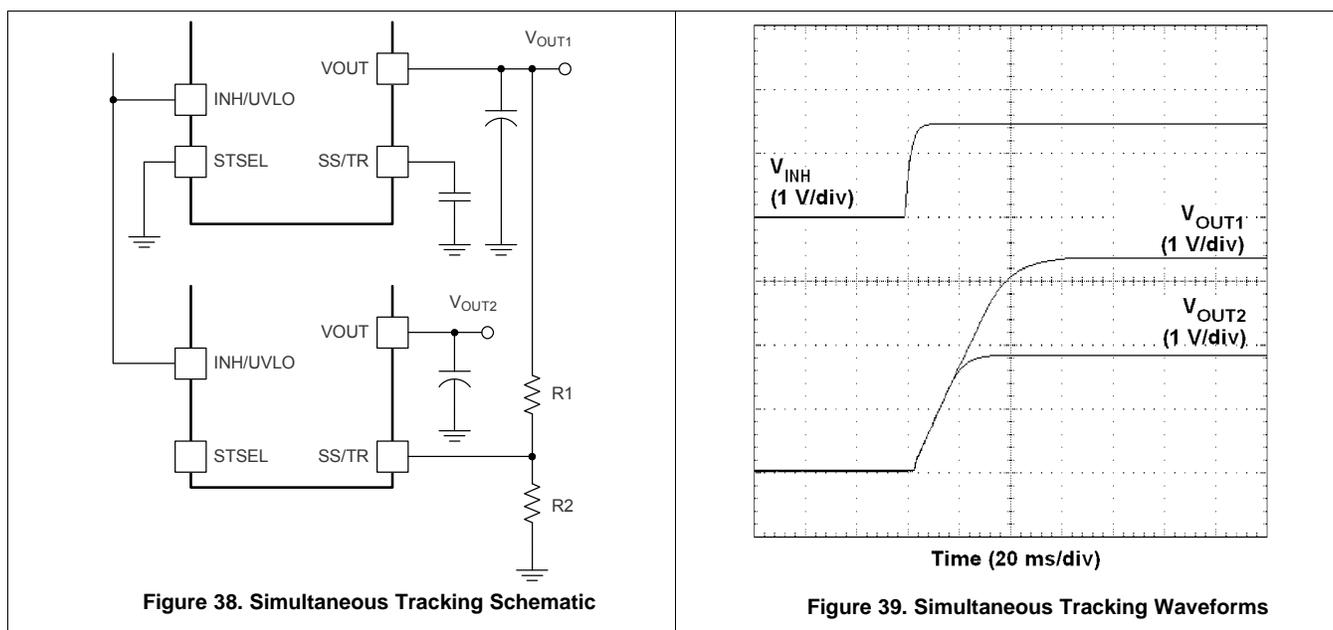
Simultaneous power supply sequencing can be implemented by connecting the resistor network of R1 and R2 shown in Figure 38 to the output of the power supply that needs to be tracked or to another voltage reference source. Figure 39 shows simultaneous turn-on waveforms of two LMZ31503 devices. Use Equation 2 and Equation 3 to calculate the values of R1 and R2.

$$R1 = \frac{(V_{OUT2} \times 12.6)}{0.8} \text{ (k}\Omega\text{)}$$

(2)

$$R2 = \frac{0.8 \times R1}{(V_{OUT2} - 0.8)} \text{ (k}\Omega\text{)}$$

(3)



### 9.16 Programmable Undervoltage Lockout (UVLO)

The LMZ31503 implements internal UVLO circuitry on the VIN pin. The device is disabled when the VIN pin voltage falls below the internal VIN UVLO threshold. The internal VIN UVLO rising threshold is 4.5 V(max) with a typical hysteresis of 150 mV.

If an application requires either a higher UVLO threshold on the VIN pin or a higher UVLO threshold for a combined VIN and PVIN, then the UVLO pin can be configured as shown in Figure 40 or Figure 41. Table 8 lists standard values for  $R_{UVLO1}$  and  $R_{UVLO2}$  to adjust the VIN UVLO voltage up.

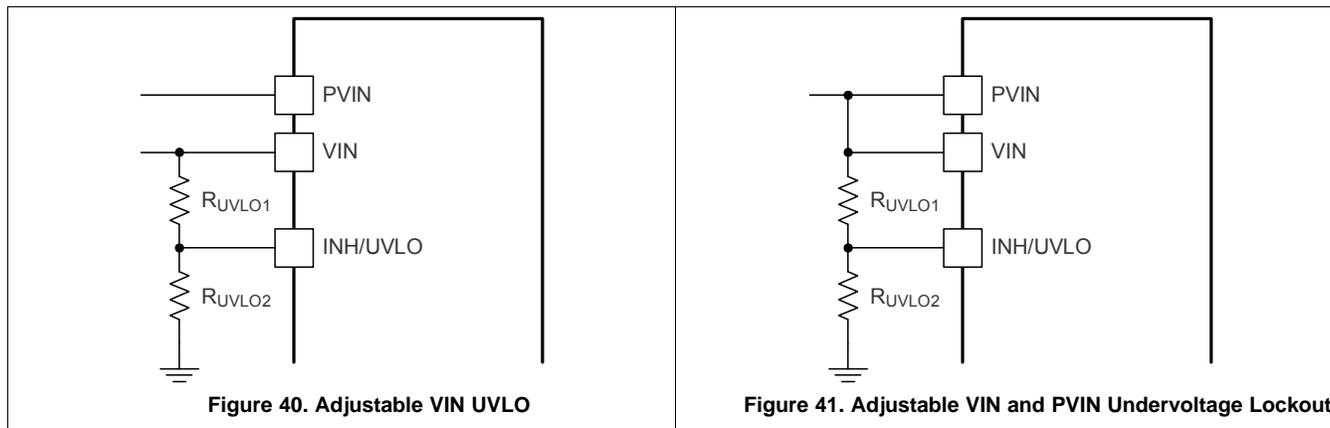


Table 8. Standard Resistor values for Adjusting VIN UVLO

VIN UVLO (V)	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5	10.0
$R_{UVLO1}$ (k $\Omega$ )	68.1	68.1	68.1	68.1	68.1	68.1	68.1	68.1	68.1	68.1	68.1
$R_{UVLO2}$ (k $\Omega$ )	21.5	18.7	16.9	15.4	14.0	13.0	12.1	11.3	10.5	9.76	9.31
Hysteresis (mV)	400	415	430	450	465	480	500	515	530	550	565

For a split rail application, if a secondary UVLO on PVIN is required, VIN must be  $\geq 4.5V$ . Figure 42 shows the PVIN UVLO configuration. Use Table 9 to select  $R_{UVLO1}$  and  $R_{UVLO2}$  for PVIN. If PVIN UVLO is set for less than 3.0 V, a 5.1-V zener diode should be added to clamp the voltage on the UVLO pin below 6 V.

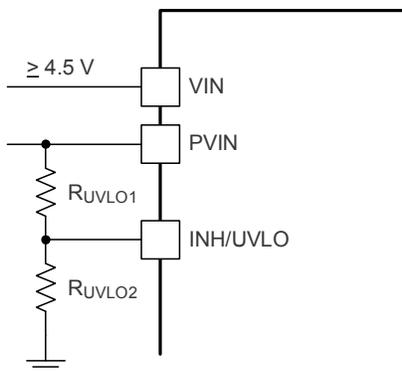


Figure 42. Adjustable PVIN Undervoltage Lockout, (VIN  $\geq 4.5$  V)

Table 9. Standard Resistor Values for Adjusting PVIN UVLO, (VIN  $\geq 4.5$  V)

PVIN UVLO (V)	2.0	2.5	3.0	3.5	4.0	4.5	
$R_{UVLO1}$ (k $\Omega$ )	68.1	68.1	68.1	68.1	68.1	68.1	For higher PVIN UVLO voltages see Table UV for resistor values
$R_{UVLO2}$ (k $\Omega$ )	95.3	60.4	44.2	34.8	28.7	24.3	
Hysteresis (mV)	300	315	335	350	365	385	

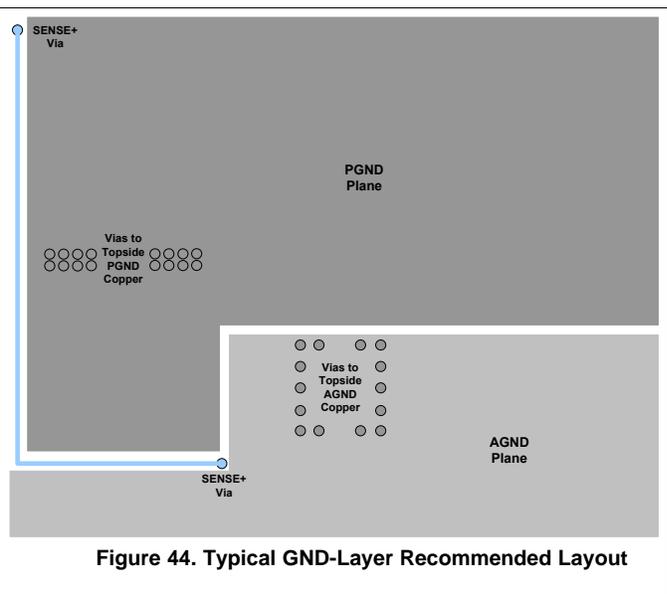
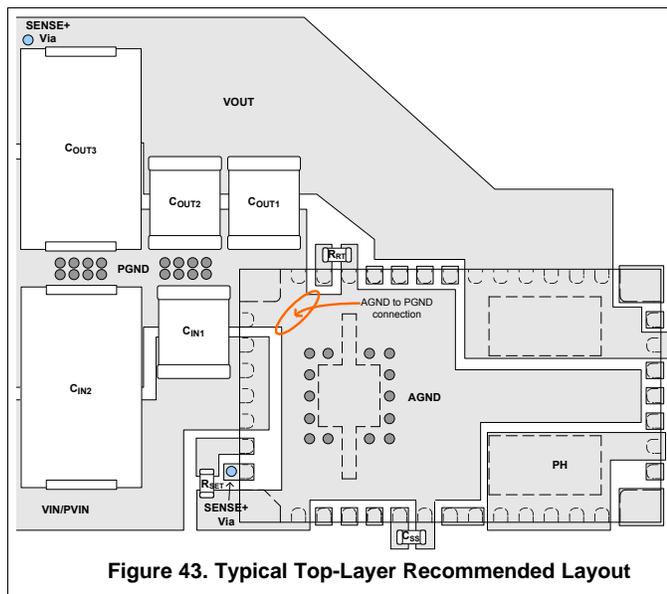
### 9.17 Thermal Shutdown

The internal thermal shutdown circuitry forces the device to stop switching if the junction temperature exceeds 175°C typically. The device reinitiates the power up sequence when the junction temperature drops below 165°C typically.

### 9.18 Layout Considerations

To achieve optimal electrical and thermal performance, an optimized PCB layout is required. Figure 43 and Figure 44 show two layers of a typical PCB layout. Some considerations for an optimized layout are:

- Use large copper areas for power planes (VIN, VOUT, and PGND) to minimize conduction loss and thermal stress.
- Place ceramic input and output capacitors close to the module pins to minimize high frequency noise.
- Locate additional output capacitors between the ceramic capacitor and the load.
- Place a dedicated AGND copper area beneath the LMZ31503.
- Isolate the PH copper area from the VOUT copper area using the AGND copper area.
- Connect the AGND and PGND copper area at one point; near the output capacitors.
- Place  $R_{SET}$ ,  $R_{RT}$ , and  $C_{SS}$  as close as possible to their respective pins.
- Use multiple vias to connect the power planes to internal layers.



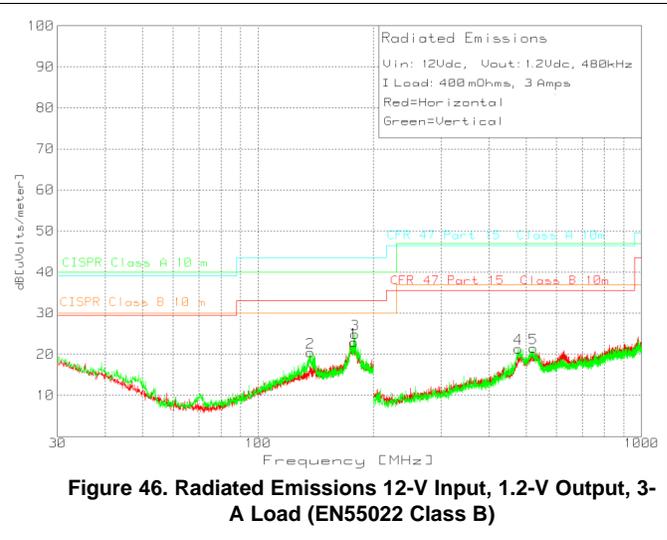
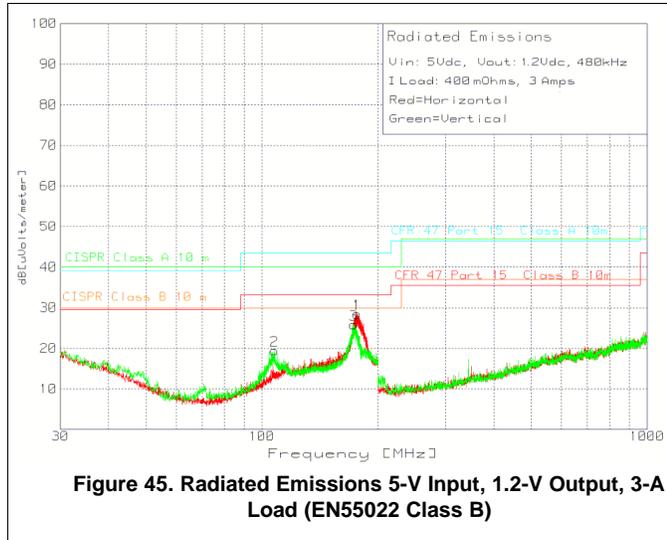
# LMZ31503

JAJSBV0B – JULY 2013 – REVISED APRIL 2018

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## 9.19 EMI

The LMZ31503 is compliant with EN55022 Class B radiated emissions. [Figure 45](#) and [Figure 46](#) show typical examples of radiated emissions plots for the LMZ31503 operating from 5V and 12V respectively. Both graphs include the plots of the antenna in the horizontal and vertical positions.



## 10 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

<b>Changes from Revision A (June 2017) to Revision B</b>	<b>Page</b>
• LMZ31503用のWEBENCH®設計リンクを追加.....	1
• Increased the peak reflow temperature and maximum number of reflows to JEDEC specifications for improved manufacturability.....	2
• 「デバイス・サポート」セクションを追加 .....	28
• 「メカニカル、パッケージ、および注文情報」セクションを追加.....	29

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<b>Changes from Original (July 2013) to Revision A</b>	<b>Page</b>
• Added peak reflow and maximum number of reflows information .....	2

## 11 デバイスおよびドキュメントのサポート

### 11.1 デバイス・サポート

#### 11.1.1 開発サポート

##### 11.1.1.1 WEBENCH®ツールによるカスタム設計

[ここをクリック](#)すると、WEBENCH® Power Designerにより、LMZ31503を使用するカスタム設計を作成できます。

1. 最初に、入力電圧( $V_{IN}$ )、出力電圧( $V_{OUT}$ )、出力電流( $I_{OUT}$ )の要件を入力します。
2. オプティマイザのダイヤルを使用して、効率、占有面積、コストなどの主要なパラメータについて設計を最適化します。
3. 生成された設計を、テキサス・インスツルメンツが提供する他のソリューションと比較します。

WEBENCH Power Designerでは、カスタマイズされた回路図と部品リストを、リアルタイムの価格と部品の在庫情報と併せて参照できます。

ほとんどの場合、次の操作を実行可能です。

- 電氣的なシミュレーションを実行し、重要な波形と回路の性能を確認する。
- 熱シミュレーションを実行し、基板の熱特性を把握する。
- カスタマイズされた回路図やレイアウトを、一般的なCADフォーマットでエクスポートする。
- 設計のレポートをPDFで印刷し、同僚と設計を共有する。

WEBENCHツールの詳細は、[www.ti.com/WEBENCH](http://www.ti.com/WEBENCH)でご覧になれます。

### 11.2 ドキュメントのサポート

#### 11.2.1 関連資料

関連資料については、以下を参照してください。

[『BQFNパッケージのハンダ付け要件』](#)

### 11.3 ドキュメントの更新通知を受け取る方法

ドキュメントの更新についての通知を受け取るには、[ti.com](http://ti.com)のデバイス製品フォルダを開いてください。右上の隅にある「通知を受け取る」をクリックして登録すると、変更されたすべての製品情報に関するダイジェストを毎週受け取れます。変更の詳細については、修正されたドキュメントに含まれている改訂履歴をご覧ください。

### 11.4 コミュニティ・リソース

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

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### 11.5 商標

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### 11.6 静電気放電に関する注意事項



すべての集積回路は、適切なESD保護方法を用いて、取扱いと保存を行うようにして下さい。

静電気放電はわずかな性能の低下から完全なデバイスの故障に至るまで、様々な損傷を与えます。高精度の集積回路は、損傷に対して敏感であり、極めてわずかなパラメータの変化により、デバイスに規定された仕様に適合しなくなる場合があります。

## 11.7 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

## 12 メカニカル、パッケージ、および注文情報

以降のページには、メカニカル、パッケージ、および注文に関する情報が記載されています。この情報は、そのデバイスについて利用可能な最新のデータです。このデータは予告なく変更されることがあり、ドキュメントが改訂される場合もあります。本データシートのブラウザ版を使用されている場合は、画面左側の説明をご覧ください。

**PACKAGING INFORMATION**

Orderable part number	Status (1)	Material type (2)	Package   Pins	Package qty   Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
<a href="#">LMZ31503RUQR</a>	Active	Production	B1QFN (RUQ)   47	500   LARGE T&R	Exempt	NIPDAU	Level-3-245C-168 HR	-40 to 85	LMZ31503
LMZ31503RUQR.A	Active	Production	B1QFN (RUQ)   47	500   LARGE T&R	Exempt	NIPDAU	Level-3-245C-168 HR	-40 to 85	LMZ31503
<a href="#">LMZ31503RUQT</a>	Active	Production	B1QFN (RUQ)   47	250   SMALL T&R	Exempt	NIPDAU	Level-3-245C-168 HR	-40 to 85	LMZ31503
LMZ31503RUQT.A	Active	Production	B1QFN (RUQ)   47	250   SMALL T&R	Exempt	NIPDAU	Level-3-245C-168 HR	-40 to 85	LMZ31503
LMZ31503RUQTG4	Active	Production	B1QFN (RUQ)   47	250   SMALL T&R	Yes	NIPDAU	Level-3-245C-168 HR	-40 to 85	LMZ31503
LMZ31503RUQTG4.A	Active	Production	B1QFN (RUQ)   47	250   SMALL T&R	Yes	NIPDAU	Level-3-245C-168 HR	-40 to 85	LMZ31503
LMZ31503RUQTG4.B	Active	Production	B1QFN (RUQ)   47	250   SMALL T&R	Yes	NIPDAU	Level-3-245C-168 HR	-40 to 85	LMZ31503

(1) **Status:** For more details on status, see our [product life cycle](#).

(2) **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

(3) **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

(4) **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

(5) **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

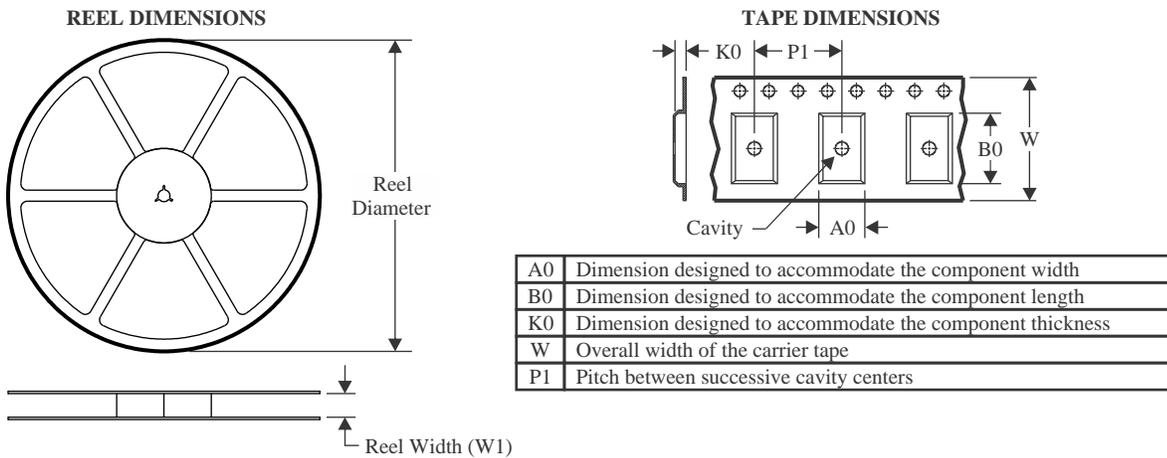
(6) **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "-" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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**TAPE AND REEL INFORMATION**

**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**

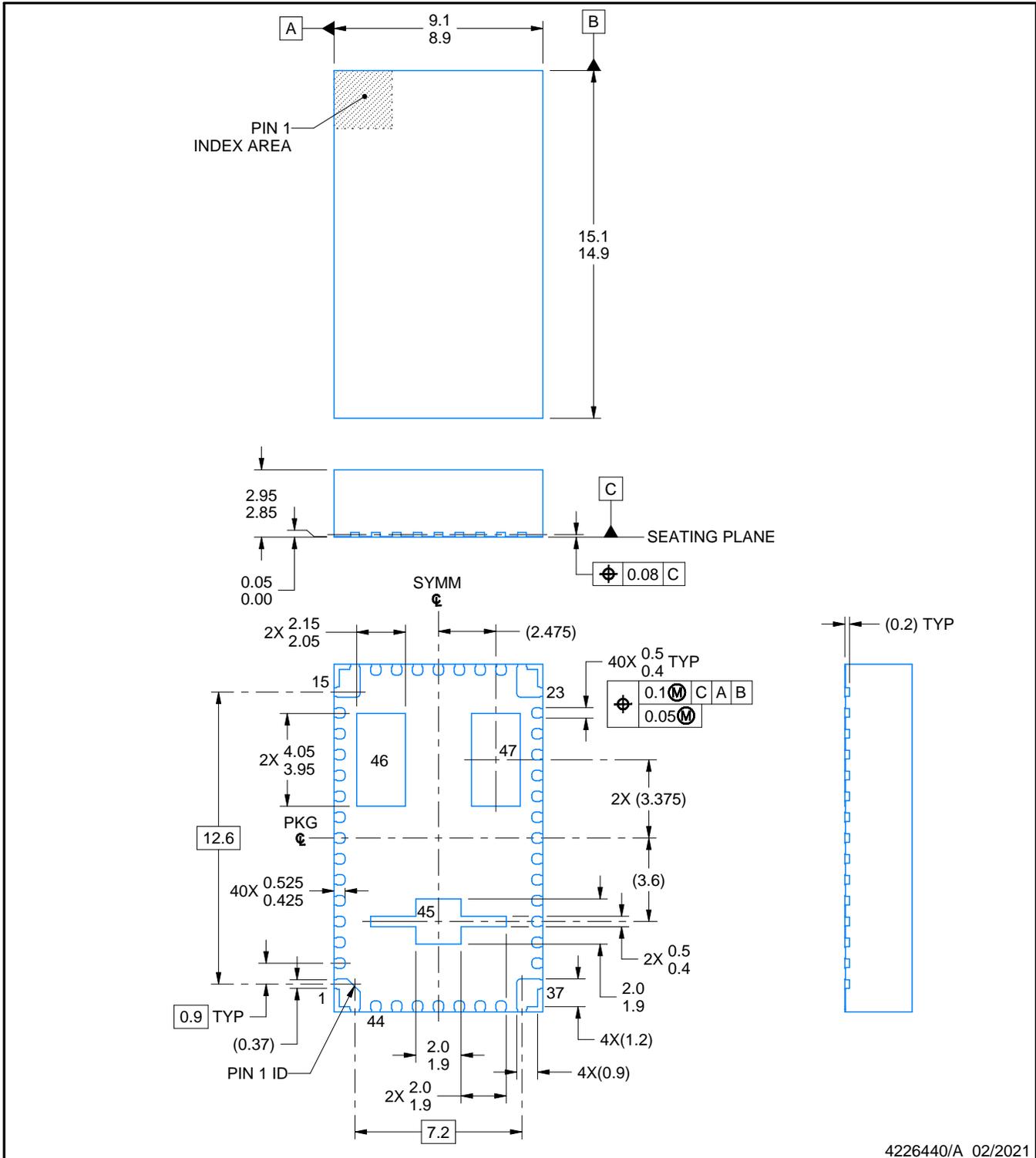
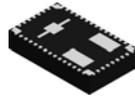

\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LMZ31503RUQR	B1QFN	RUQ	47	500	330.0	24.4	9.35	15.35	3.1	16.0	24.0	Q1
LMZ31503RUQT	B1QFN	RUQ	47	250	330.0	24.4	9.35	15.35	3.1	16.0	24.0	Q1
LMZ31503RUQTG4	B1QFN	RUQ	47	250	330.0	24.4	9.35	15.35	3.1	16.0	24.0	Q1

**TAPE AND REEL BOX DIMENSIONS**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LMZ31503RUQR	B1QFN	RUQ	47	500	383.0	353.0	58.0
LMZ31503RUQT	B1QFN	RUQ	47	250	383.0	353.0	58.0
LMZ31503RUQTG4	B1QFN	RUQ	47	250	383.0	353.0	58.0



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**NOTES:**

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pads must be soldered to the printed circuit board for optimal thermal and mechanical performance.

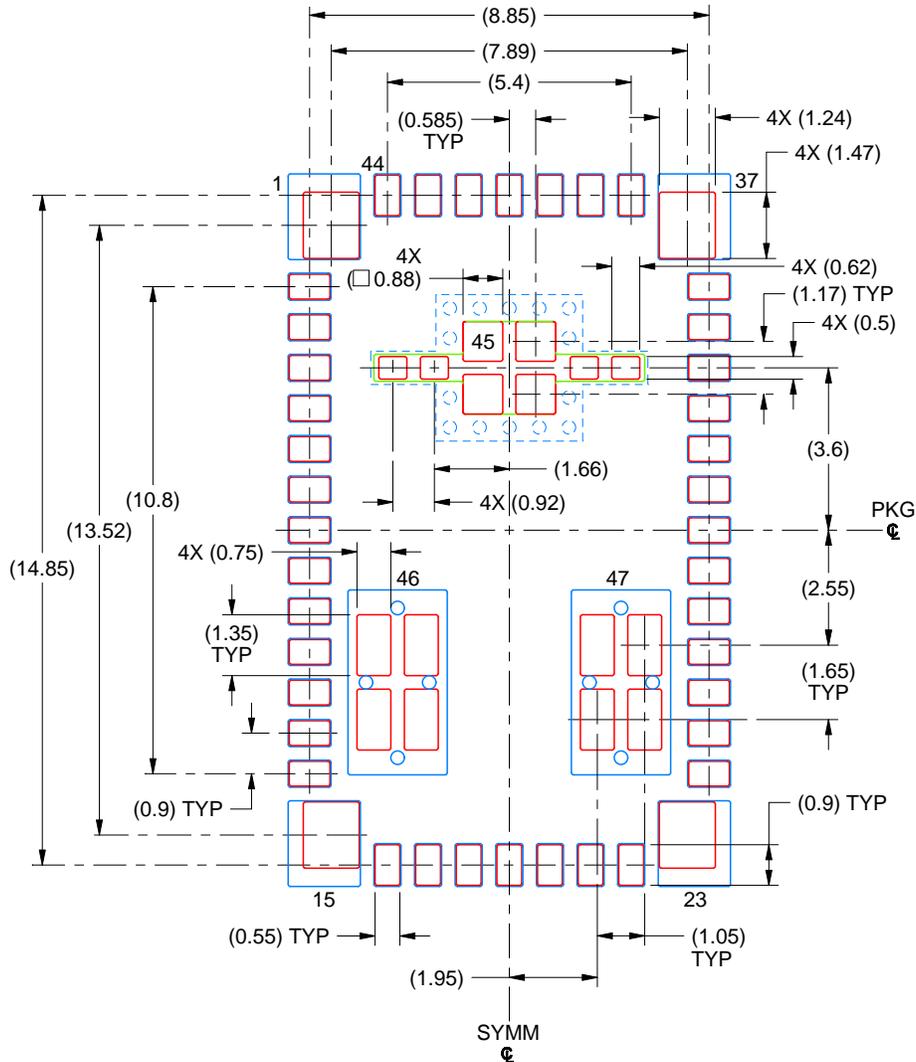


# EXAMPLE STENCIL DESIGN

**RUQ0047A**

**B1QFN - 2.95 mm max height**

PLASTIC QUAD FLATPACK - NO LEAD



**SOLDER PASTE EXAMPLE**  
 BASED ON 0.1 mm STENCIL THICKNESS

CORNER PINS 1, 15, 23 & 37:  
 60% PRINTED SOLDER COVERAGE BY AREA UNDER PACKAGE

EXPOSED PAD 45:  
 66% PRINTED SOLDER COVERAGE BY AREA UNDER PACKAGE

EXPOSED PAD 46 & 47:  
 45% PRINTED SOLDER COVERAGE BY AREA UNDER PACKAGE  
 SCALE:6X

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NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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