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# LMH6682/6683 190MHz Single Supply, Dual and Triple Operational Amplifiers

Check for Samples: LMH6682, LMH6683

### **FEATURES**

 $V_S = \pm 5V$ ,  $T_A = 25^{\circ}C$ ,  $R_L = 100\Omega$ , A = +2 (Typical Values Unless Specified)

- DG error 0.01%
- DP error 0.08°
- -3dB BW (A = +2) 190MHz
- Slew rate (V<sub>S</sub> = ±5V) 940V/μs
- Supply Current 6.5mA/amp
- Output Current +80/-90mA
- Input Common Mode Voltage 0.5V Beyond V<sup>-</sup>,1.7V from V<sup>+</sup>
- Output Voltage Swing (R<sub>L</sub> = 2kΩ) 0.8V from Rails
- Input Voltage Noise (100KHz) 12nV/√Hz

### **APPLICATIONS**

- CD/DVD ROM
- ADC Buffer Amp
- Portable Video
- Current Sense Buffer
- Portable Communications

### DESCRIPTION

The LMH6682 and LMH6683 are high speed operational amplifiers designed for use in modern video systems. These single supply monolithic amplifiers extend Tl's feature-rich, high value video portfolio to include a dual and a triple version. The important video specifications of differential gain (± 0.01% typ.) and differential phase (±0.08 degrees) combined with an output drive current in each amplifier of 85mA make the LMH6682 and LMH6683 excellent choices for a full range of video applications.

Voltage feedback topology in operational amplifiers assures maximum flexibility and ease of use in high speed amplifier designs. The LMH6682/83 is fabricated in TI's VIP10 process. This advanced process provides a superior ratio of speed to quiescient current consumption and assures the user of high-value amplifier designs. Advanced technology and circuit design enables in these amplifiers a -3db bandwidth of 190MHz, a slew rate of 940V/µsec, and stability for gains of less than -1 and greater than +2.

The input stage design of the LM6682/83 enables an input signal range that extends below the negative rail. The output stage voltage range reaches to within 0.8V of either rail when driving a  $2k\Omega$  load. Other attractive features include fast settling and low distortion. Other applications for these amplifiers include servo control designs. These applications are sensitive to amplifiers that exhibit phase reversal when the inputs exceed the rated voltage range. The LMH6682/83 amplifiers are designed to be immune to phase reversal when the specified input range is exceeded. See applications section. This feature makes for design simplicity and flexibility in many industrial applications.

The LMH6682 dual operational amplifier is offered in miniature surface mount packages, SOIC-8, and VSSOP-8. The LMH6683 triple amplifier is offered in SOIC-14 and TSSOP-14.

ATA

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.



### **Connection Diagram**

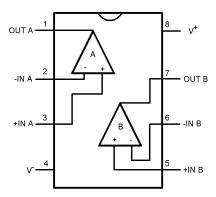


Figure 1. SOIC-8/VSSOP-8 (LMH6682) Top View

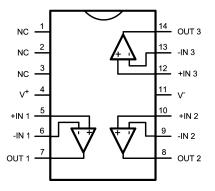


Figure 2. SOIC-14/TSSOP-14 (LMH6683) Top View



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

# **Absolute Maximum Ratings**(1)(2)

ESD Tolerance	Human Body Model	2KV <sup>(3)</sup>
	Machine Model	200V <sup>(4)</sup>
V <sub>IN</sub> Differential	<u> </u>	±2.5V
Output Short Circuit Duration		See <sup>(5)(6)</sup>
Input Current		±10mA
Supply Voltage (V <sup>+</sup> - V <sup>-</sup> )		12.6V
Voltage at Input/Output pins		V+ +0.8V, V0.8V
Soldering Information	Infrared or Convection (20 sec.)	235°C
	Wave Soldering (10 sec.)	260°C
Storage Temperature Range		-65°C to +150°C
Junction Temperature <sup>(7)</sup>		+150°C

- (1) Absolute maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not ensured. For ensured specifications and the test conditions, see the Electrical Characteristics.
- (2) If Military/Aerospace specified devices are required, please contact the TI Sales Office/ Distributors for availability and specifications.
- (3) Human body model, 1.5kΩ in series with 100pF.
- (4) Machine Model, 0Ω in series with 200pF.
- (5) Applies to both single-supply and split-supply operation. Continuous short circuit operation at elevated ambient temperature can result in exceeding the maximum allowed junction temperature of 150°C.
- (6) Output short circuit duration is infinite for  $V_S < 6V$  at room temperature and below. For  $V_S > 6V$ , allowable short circuit duration is 1.5ms.
- (7) The maximum power dissipation is a function of  $T_{J(MAX)}$ ,  $\theta_{JA}$ , and  $T_A$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(MAX)} T_A)/\theta_{JA}$ . All numbers apply for packages soldered directly onto a PC board.

### Operating Ratings<sup>(1)</sup>

Supply Voltage (V <sup>+</sup> – V <sup>-</sup> )		3V to 12V
Operating Temperature Range <sup>(2)</sup>		−40°C to +85°C
Package Thermal Resistance <sup>(2)</sup>	SOIC-8	190°C/W
	VSSOP-8	235°C/W
	SOIC-14	145°C/W
	TSSOP-14	155°C/W

- (1) Absolute maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not ensured. For ensured specifications and the test conditions, see the Electrical Characteristics.
- (2) The maximum power dissipation is a function of  $T_{J(MAX)}$ ,  $\theta_{JA}$ , and  $T_A$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(MAX)} T_A)/\theta_{JA}$ . All numbers apply for packages soldered directly onto a PC board.

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# **5V Electrical Characteristics**

Unless otherwise specified, all limits ensured for at  $T_J = 25^{\circ}C$ ,  $V^+ = 5V$ ,  $V^- = 0V$ ,  $V_O = V_{CM} = V^+/2$ , and  $R_L = 100\Omega$  to  $V^+/2$ ,  $R_F = 510\Omega$ . **Boldface** limits apply at the temperature extremes.

Symbol	Parameter	Conditions	Min <sup>(1)</sup>	Min <sup>(1)</sup> Typ <sup>(2)</sup>		Units	
SSBW	-3dB BW	$A = +2, V_{OUT} = 200 \text{mV}_{PP}$	140	180			
		$A = -1$ , $V_{OUT} = 200 \text{mV}_{PP}$		180		MHz	
GFP	Gain Flatness Peaking	A = +2, V <sub>OUT</sub> = 200mV <sub>PP</sub> DC to 100MHz		2.1		dB	
GFR	Gain Flatness Rolloff	A = +2, V <sub>OUT</sub> = 200mV <sub>PP</sub> DC to 100MHz					
LPD 1°	1° Linear Phase Deviation	A = +2, V <sub>OUT</sub> = 200mV <sub>PP</sub> , ±1°		40		MHz	
GF <sub>0.1dB</sub>	0.1dB Gain Flatness	$A = +2, \pm 0.1 dB, V_{OUT} = 200 mV_{PP}$		25		MHz	
FPBW	Full Power -1dB Bandwidth	$A = +2$ , $V_{OUT} = 2V_{PP}$		110		MHz	
DG	Differential Gain NTSC 3.58MHz	A = +2, $R_L$ = 150 $\Omega$ to V <sup>+</sup> /2 Pos video only $V_{CM}$ = 2V		0.03		%	
DP	Differential Phase NTSC 3.58MHz	A = +2, R <sub>L</sub> = 150 $\Omega$ to V <sup>+</sup> /2 Pos video only V <sub>CM</sub> = 2V		0.05		deg	
Time Doma	in Response						
T <sub>r</sub> /T <sub>f</sub>	Rise and Fall Time	20-80%, V <sub>O</sub> = 1V <sub>PP</sub> , A <sub>V</sub> = +2		2.1			
		20-80%, V <sub>O</sub> = 1V <sub>PP</sub> , A <sub>V</sub> = −1		2		ns	
OS	Overshoot	$A = +2, V_O = 100 \text{mV}_{PP}$		22		%	
T <sub>s</sub>	Settling Time	$V_O = 2V_{PP}, \pm 0.1\%, A_V = +2$		49		ns	
SR	Slew Rate (3)	$A = +2, V_{OUT} = 3V_{PP}$		520		\//u0	
		$A = -1$ , $V_{OUT} = 3V_{PP}$		500		V/µs	
Distortion a	and Noise Response						
HD2	2 <sup>nd</sup> Harmonic Distortion	$f = 5MHz, V_O = 2V_{PP}, A = +2, R_L = 2k\Omega$		-60			
		$f = 5MHz, V_O = 2V_{PP}, A = +2, R_L = 100\Omega$		-61		dBc	
HD3	3 <sup>rd</sup> Harmonic Distortion	$f = 5MHz, V_O = 2V_{PP}, A = +2, R_L = 2k\Omega$		-77			
		$\begin{array}{l} f = 5 MHz, \ V_O = 2 V_{PP}, \ A = +2, \ R_L = \\ 100 \Omega \end{array}$		<b>-54</b>		dBc	
THD	Total Harmonic Distortion	$f = 5MHz$ , $V_O = 2V_{PP}$ , $A = +2$ , $R_L = 2k\Omega$		-60			
		$f = 5MHz, V_O = 2V_{PP}, A = +2, R_L = 100\Omega$		-53		dBc	
e <sub>n</sub>	Input Referred Voltage Noise	f = 1kHz		17		nV/√ <del>Hz</del>	
		f = 100kHz		12			
i <sub>n</sub>	Input Referred Current Noise	f = 1kHz		8		pA/√Hz	
		f = 100kHz		3			
СТ	Cross-Talk Rejection (Amplifier)	$ f = 5 \text{MHz}, \ A = +2, \ \text{SND:} \ R_L = 100 \Omega $ RCV: $R_F = R_G = 510 \Omega$		-77		dB	
Static, DC I	Performance						
A <sub>VOL</sub>	Large Signal Voltage Gain	$V_O = 1.25V \text{ to } 3.75V,$ $R_L = 2k\Omega \text{ to } V^+/2$	85	95			
		$V_O = 1.5V$ to 3.5V, $R_L = 150\Omega$ to $V^+/2$	75	85		dB	
		$V_O = 2V$ to 3V, $R_L = 50\Omega$ to $V^+/2$	70	80			
CMVR	Input Common-Mode Voltage Range	CMRR ≥ 50dB	-0.2 - <b>0.1</b>	-0.5		V	

<sup>(1)</sup> All limits are ensured by testing or statistical analysis.

<sup>(2)</sup> Typical values represent the most likely parametric norm.

<sup>(3)</sup> Slew rate is the average of the rising and falling slew rates



# **5V Electrical Characteristics (continued)**

Unless otherwise specified, all limits ensured for at  $T_J = 25^{\circ}C$ ,  $V^+ = 5V$ ,  $V^- = 0V$ ,  $V_O = V_{CM} = V^+/2$ , and  $R_L = 100\Omega$  to  $V^+/2$ ,  $R_F = 510\Omega$ . **Boldface** limits apply at the temperature extremes.

Symbol	Parameter	Conditions	Min <sup>(1)</sup>	Typ <sup>(2)</sup>	Max <sup>(1)</sup>	Units	
V <sub>OS</sub>	Input Offset Voltage			±1.1	±5 <b>±7</b>	mV	
TC V <sub>OS</sub>	Input Offset Voltage Average Drift	See <sup>(4)</sup>		±2		μV/°C	
I <sub>B</sub>	Input Bias Current	See <sup>(5)</sup>		<b>-</b> 5	-20 - <b>30</b>	μΑ	
TC <sub>IB</sub>	Input Bias Current Drift			0.01		nA/°C	
I <sub>OS</sub>	Input Offset Current			50	300 <b>500</b>	nA	
CMRR	Common Mode Rejection Ratio	V <sub>CM</sub> Stepped from 0V to 3.0V	72	82		dB	
+PSRR	Positive Power Supply Rejection Ratio	$V^{+} = 4.5V$ to 5.5V, $V_{CM} = 1V$	70	76		dB	
I <sub>S</sub>	Supply Current (per channel)	No load		6.5	9 <b>11</b>	mA	
Miscellane	ous Performance		·				
Vo	Output Swing High	$R_L = 2k\Omega$ to $V^+/2$	4.10 <b>3.8</b>	4.25			
		$R_L = 150\Omega$ to $V^+/2$	3.90 <b>3.70</b>	4.19		V	
		$R_L = 75\Omega$ to V <sup>+</sup> /2	3.75 <b>3.50</b>	4.15			
	Output Swing Low	$R_L = 2k\Omega$ to V <sup>+</sup> /2		800	920 <b>1100</b>		
		$R_L = 150\Omega$ to $V^+/2$		870	970 <b>1200</b>	mV	
		R <sub>L</sub> = $75\Omega$ to V <sup>+</sup> /2		885	1100 <b>1250</b>		
I <sub>OUT</sub>	Output Current	V <sub>O</sub> = 1V from either supply rail	±40	+80/-75		mA	
I <sub>SC</sub>	Output Short Circuit Current (6)(7)(8)	Sourcing to V <sup>+</sup> /2	-100 - <b>80</b>	-155		A	
		Sinking from V <sup>+</sup> /2	100 <b>80</b>	220		mA	
R <sub>IN</sub>	Common Mode Input Resistance			3		ΜΩ	
C <sub>IN</sub>	Common Mode Input Capacitance			1.6	_	pF	
R <sub>OUT</sub>	Output Resistance Closed Loop	$f = 1kHz, A = +2, R_L = 50\Omega$		0.02		0	
		$f = 1MHz, A = +2, R_L = 50\Omega$	0.12			Ω	

<sup>4)</sup> Offset Voltage average drift determined by dividing the change in V<sub>OS</sub> at temperature extremes into the total temperature change.

8) Positive current corresponds to current flowing into the device.

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<sup>(5)</sup> Positive current corresponds to current flowing into the device.

<sup>(6)</sup> Short circuit test is a momentary test. See next note.

<sup>(7)</sup> Output short circuit duration is infinite for  $V_S < 6V$  at room temperature and below. For  $V_S > 6V$ , allowable short circuit duration is 1.5ms.



# ±5V Electrical Characteristics

Unless otherwise specified, all limits ensured for at  $T_J = 25^{\circ}C$ ,  $V^+ = 5V$ ,  $V^- = -5V$ ,  $V_O = V_{CM} = 0V$ , and  $R_L = 100\Omega$  to 0V,  $R_F = 510\Omega$ . **Boldface** limits apply at the temperature extremes.

Symbol	Parameter	Conditions	Min <sup>(1)</sup>	Min <sup>(1)</sup> Typ <sup>(2)</sup>		Units
SSBW	-3dB BW	$A = +2, V_{OUT} = 200 \text{mV}_{PP}$	150	190		
		$A = -1$ , $V_{OUT} = 200 \text{mV}_{PP}$		190		MHz
GFP	Gain Flatness Peaking	A = +2, V <sub>OUT</sub> = 200mV <sub>PP</sub> DC to 100MHz		1.7		dB
GFR	Gain Flatness Rolloff	A = +2, V <sub>OUT</sub> = 200mV <sub>PP</sub> DC to 100MHz				
LPD 1°	1° Linear Phase Deviation	A = +2, V <sub>OUT</sub> = 200mV <sub>PP</sub> , ±1°		40		MHz
GF <sub>0.1dB</sub>	0.1dB Gain Flatness	$A = +2, \pm 0.1 dB, V_{OUT} = 200 mV_{PP}$		25		MHz
FPBW	Full Power -1dB Bandwidth	$A = +2$ , $V_{OUT} = 2V_{PP}$		120		MHz
DG	Differential Gain NTSC 3.58MHz	$A = +2$ , $R_L = 150Ω$ to 0V		0.01		%
DP	Differential Phase NTSC 3.58MHz	$A = +2$ , $R_L = 150\Omega$ to $0V$		0.08		deg
Time Doma	in Response	•				
T <sub>r</sub> /T <sub>f</sub>	Rise and Fall Time	20-80%, V <sub>O</sub> = 1V <sub>PP</sub> , A = +2		1.9		200
		20-80%, V <sub>O</sub> = 1V <sub>PP</sub> , A = −1		2		ns
OS	Overshoot	$A = +2, V_O = 100 \text{mV}_{PP}$		19		%
Ts	Settling Time	$V_O = 2V_{PP}$ , ±0.1%, A = +2		42		ns
SR	Slew Rate <sup>(3)</sup>	$A = +2$ , $V_{OUT} = 6V_{PP}$		940		V/µs
		$A = -1$ , $V_{OUT} = 6V_{PP}$		900		ν/μ5
Distortion a	nd Noise Response					
HD2	2 <sup>nd</sup> Harmonic Distortion	$f = 5MHz$ , $V_O = 2V_{PP}$ , $A = +2$ , $R_L = 2k\Omega$		-63		
		$\begin{array}{l} f = 5 MHz, \ V_O = 2 V_{PP}, \ A = +2, \ R_L = \\ 100 \Omega \end{array}$		-66		dBc
HD3	3 <sup>rd</sup> Harmonic Distortion	$f = 5MHz$ , $V_O = 2V_{PP}$ , $A = +2$ , $R_L = 2k\Omega$		-82		
		$f = 5MHz, V_O = 2V_{PP}, A = +2, R_L = 100\Omega$		-54		dBc
THD	Total Harmonic Distortion	$f = 5MHz,  V_O = 2V_PP,  A = +2,  R_L = 2k\Omega$		-63		
		$f = 5MHz, V_O = 2V_{PP}, A = +2, R_L = 100\Omega$		-54		dBc
e <sub>n</sub>	Input Referred Voltage Noise	f = 1kHz		18		nV/√Hz
		f = 100kHz		12		
i <sub>n</sub>	Input Referred Current Noise	f = 1kHz		6		pA/√Hz
		f = 100kHz		3		
СТ	Cross-Talk Rejection (Amplifier)	$ f = 5 \text{MHz}, \ A = +2, \ \text{SND:} \ R_L = 100 \Omega $ RCV: $R_F = R_G = 510 \Omega$		<del>-</del> 78		dB
Static, DC F	Performance			1		
A <sub>VOL</sub>	Large Signal Voltage Gain	$V_O = -3.75V \text{ to } 3.75V,$ $R_L = 2k\Omega \text{ to } V^+/2$	87	100		
		$V_O = -3.5V$ to 3.5V, $R_L = 150\Omega$ to $V^+/2$	80	90		dB
		$V_O = -3V$ to 3V, $R_L = 50\Omega$ to $V^+/2$	75	85		
CMVR	Input Common Mode Voltage Range	CMRR ≥ 50dB	-5.2 <b>-5.1</b>	-5.5		V
			3.0	3.3		V

<sup>(1)</sup> All limits are ensured by testing or statistical analysis.

Product Folder Links: LMH6682 LMH6683

<sup>(2)</sup> Typical values represent the most likely parametric norm.

<sup>(3)</sup> Slew rate is the average of the rising and falling slew rates



# ±5V Electrical Characteristics (continued)

Unless otherwise specified, all limits ensured for at  $T_J = 25^{\circ}C$ ,  $V^+ = 5V$ ,  $V^- = -5V$ ,  $V_O = V_{CM} = 0V$ , and  $R_L = 100\Omega$  to 0V,  $R_F = 1000$  to 100 to 100510 $\Omega$ . **Boldface** limits apply at the temperature extremes.

Symbol	Parameter	Conditions	Min <sup>(1)</sup>	Typ <sup>(2)</sup>	Max <sup>(1)</sup>	Units
V <sub>OS</sub>	Input Offset Voltage			±1	±5 ±7	mV
TC V <sub>OS</sub>	Input Offset Voltage Average Drift	See <sup>(4)</sup>		±2		μV/°C
I <sub>B</sub>	Input Bias Current	See (5)		<b>-</b> 5	-20 <b>-30</b>	μΑ
TC <sub>IB</sub>	Input Bias Current Drift			0.01		nA/°C
I <sub>OS</sub>	Input Offset Current			50	300 <b>500</b>	nA
CMRR	Common Mode Rejection Ratio	V <sub>CM</sub> Stepped from -5V to 3.0V	75	84		dB
+PSRR	Positive Power Supply Rejection Ratio	$V^{+} = 8.5V \text{ to } 9.5V,$ $V^{-} = -1V$	75	82		dB
-PSRR	Negative Power Supply Rejection Ratio	$V^{-} = -4.5V$ to $-5.5V$ , $V^{+} = 5V$	78	85		dB
I <sub>S</sub>	Supply Current (per channel)	No load		6.5	9.5 <b>11</b>	mA
Miscellane	ous Performance		·	•		
Vo	Output Swing High	$R_L = 2k\Omega$ to 0V	4.10 <b>3.80</b>	4.25		
		$R_L = 150\Omega$ to 0V	3.90 <b>3.70</b>	4.20		V
		$R_L = 75\Omega$ to 0V	3.75 <b>3.50</b>	4.18		
	Output Swing Low	$R_L = 2k\Omega$ to 0V		-4.19	-4.07 <b>-3.80</b>	
		$R_L = 150\Omega$ to 0V		-4.05	-3.89 <b>-3.65</b>	mV
		R $_{L}$ = 75 $\Omega$ to 0V		-4.00	-3.70 <b>-3.50</b>	
I <sub>OUT</sub>	Output Current	V <sub>O</sub> = 1V from either supply rail	±45	+85/-80		mA
I <sub>SC</sub>	Output Short Circuit Current <sup>(6)(7)(8)</sup>	Sourcing to 0V	-120 - <b>100</b>	-180		m ^
		Sinking from 0V	120 <b>100</b>	230		mA
R <sub>IN</sub>	Common Mode Input Resistance			4		МΩ
C <sub>IN</sub>	Common Mode Input Capacitance			1.6		pF
R <sub>OUT</sub>	Output Resistance Closed Loop					0
		$f = 1MHz, A = +2, R_L = 50\Omega$		0.12		Ω

Offset Voltage average drift determined by dividing the change in  $V_{OS}$  at temperature extremes into the total temperature change. Positive current corresponds to current flowing into the device.

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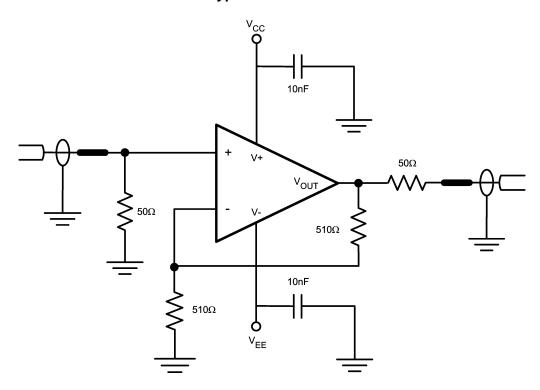
Short circuit test is a momentary test. See next note.

Output short circuit duration is infinite for  $V_S < 6V$  at room temperature and below. For  $V_S > 6V$ , allowable short circuit duration is 1.5ms.

Positive current corresponds to current flowing into the device.



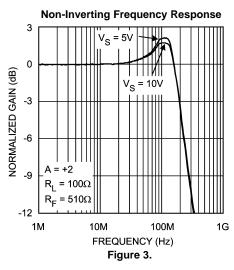
# **Typical Schematic**



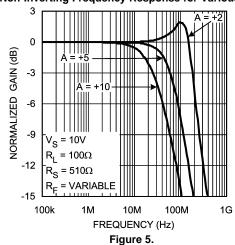


# **Typical Performance Characteristics**

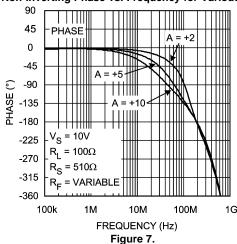
At  $T_A = 25^{\circ}\text{C}$ ,  $V^+ = +5\text{V}$ ,  $V^- = -5\text{V}$ ,  $R_F = 510\Omega$  for A = +2; unless otherwise specified.

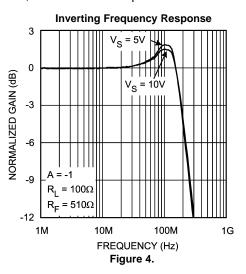


# Non-Inverting Frequency Response for Various Gain

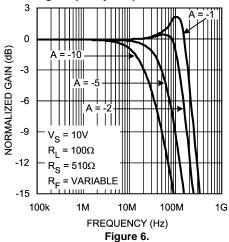


### Non-Inverting Phase vs. Frequency for Various Gain

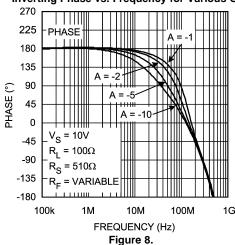




#### **Inverting Frequency Response for Various Gain**



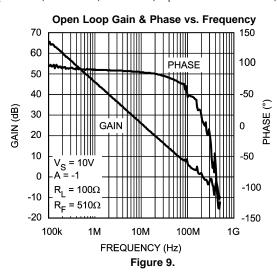
### Inverting Phase vs. Frequency for Various Gain

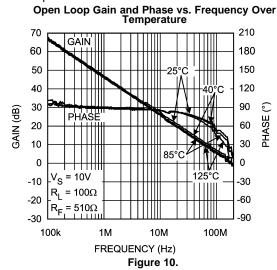


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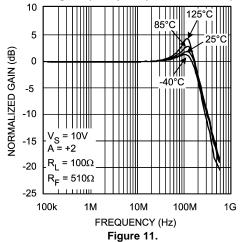


At  $T_A = 25$ °C,  $V^+ = +5V$ ,  $V^- = -5V$ ,  $R_F = 510\Omega$  for A = +2; unless otherwise specified.

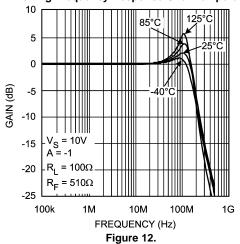


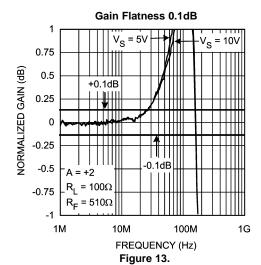


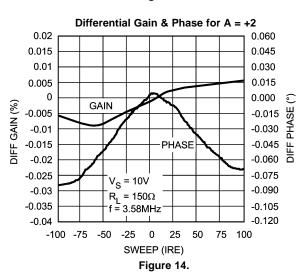






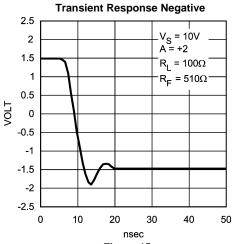




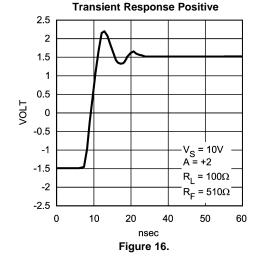




At  $T_A = 25$ °C,  $V^+ = +5V$ ,  $V^- = -5V$ ,  $R_F = 510\Omega$  for A = +2; unless otherwise specified.







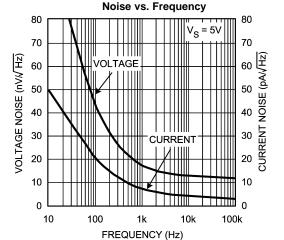
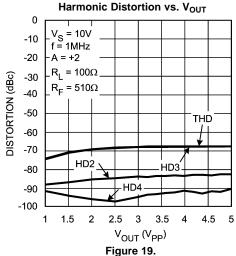
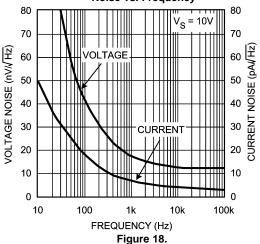


Figure 17.



Noise vs. Frequency



Harmonic Distortion vs. Vout

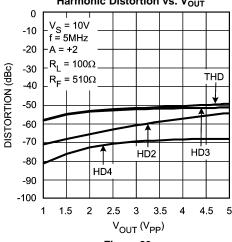
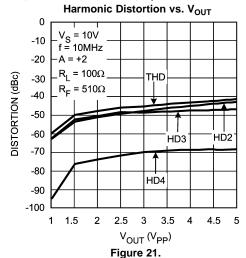


Figure 20.

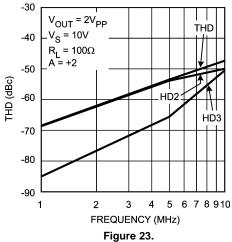
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At  $T_A = 25$ °C,  $V^+ = +5V$ ,  $V^- = -5V$ ,  $R_F = 510\Omega$  for A = +2; unless otherwise specified.







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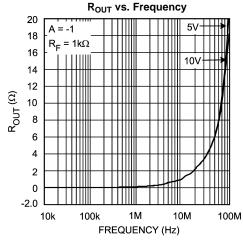
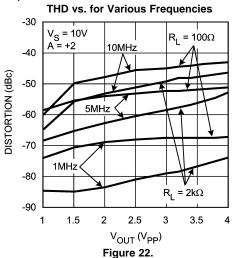
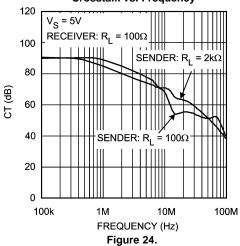


Figure 25.



Crosstalk vs. Frequency



 $I_{\text{OS}}$  vs.  $V_{\text{SUPPLY}}$  Over Temperature

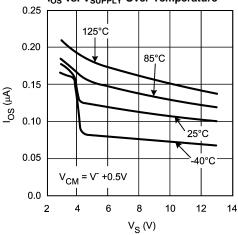
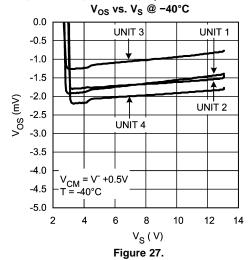
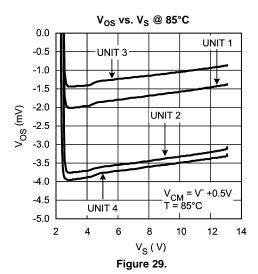


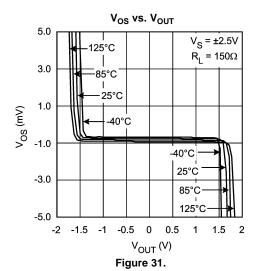
Figure 26.

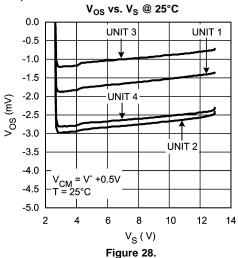


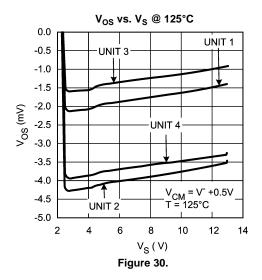
At  $T_A = 25$ °C,  $V^+ = +5V$ ,  $V^- = -5V$ ,  $R_F = 510\Omega$  for A = +2; unless otherwise specified.

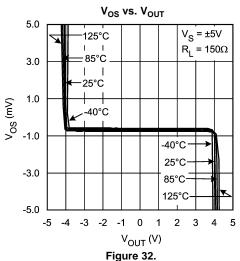








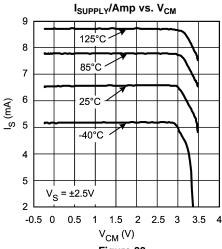




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At  $T_A = 25$ °C,  $V^+ = +5V$ ,  $V^- = -5V$ ,  $R_F = 510\Omega$  for A = +2; unless otherwise specified.





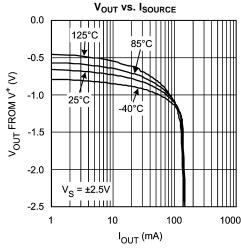
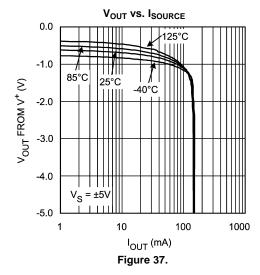


Figure 35.



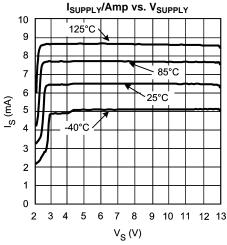
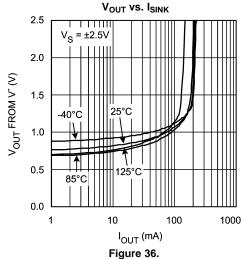
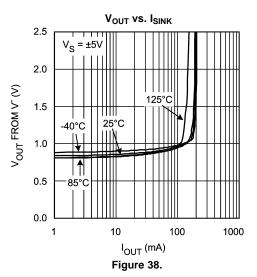


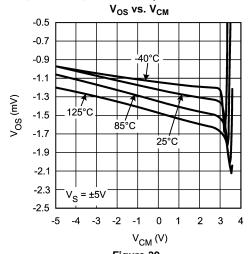
Figure 34.







At  $T_A = 25$ °C,  $V^+ = +5V$ ,  $V^- = -5V$ ,  $R_F = 510\Omega$  for A = +2; unless otherwise specified.





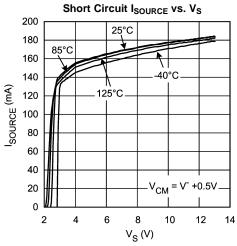
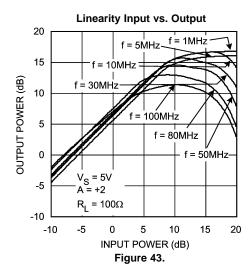


Figure 41.



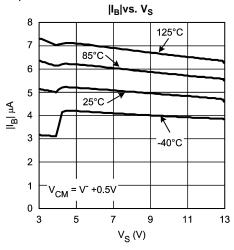
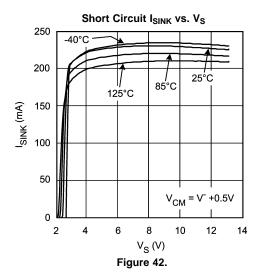
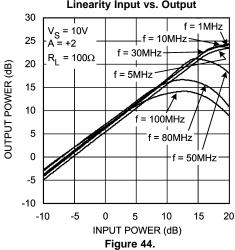


Figure 40.



Linearity Input vs. Output



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At  $T_A = 25$ °C,  $V^+ = +5V$ ,  $V^- = -5V$ ,  $R_F = 510\Omega$  for A = +2; unless otherwise specified.

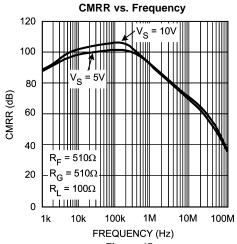
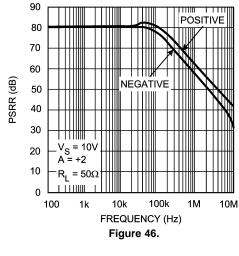


Figure 45.



**PSRR vs. Frequency** 

Small Signal Pulse Response for A = +2

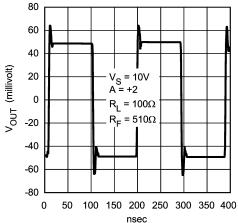


Figure 47.

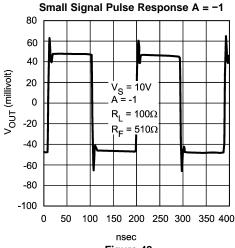
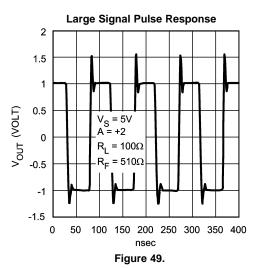
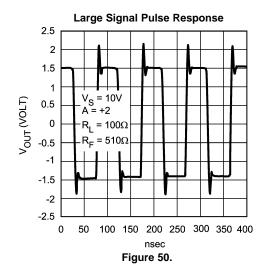


Figure 48.







#### APPLICATIONS SECTION

#### LARGE SIGNAL BEHAVIOR

Amplifying high frequency signals with large amplitudes (as in video applications) has some special aspects to look after. The bandwidth of the Op Amp for large amplitudes is less than the small signal bandwidth because of slew rate limitations. While amplifying pulse shaped signals the slew rate properties of the OpAmp become more important at higher amplitude ranges. Due to the internal structure of an Op Amp the output can only change with a limited voltage difference per time unit (dV/dt). This can be explained as follows: To keep it simple, assume that an Op Amp consists of two parts; the input stage and the output stage. In order to stabilize the Op Amp, the output stage has a compensation capacitor in its feedback path. This Miller C integrates the current from the input stage and determines the pulse response of the Op Amp. The input stage must charge/discharge the feedback capacitor, as can be seen in Figure 51.

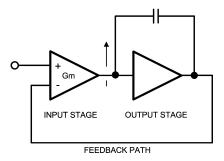


Figure 51.

When a voltage transient is applied to the non inverting input of the Op Amp, the current from the input stage will charge the capacitor and the output voltage will slope up. The overall feedback will subtract the gradually increasing output voltage from the input voltage. The decreasing differential input voltage is converted into a current by the input stage (Gm).

$$I^*\Delta t = C *\Delta V \tag{1}$$

$$\Delta V/\Delta t = I/C$$
 (2)

$$I=\Delta V^*Gm$$
 (3)

where I = current

t = time

C = capacitance

V = voltage

Gm = transconductance

Slew rate  $\Delta V/\Delta t = \text{volt/second}$ 

In most amplifier designs the current I is limited for high differential voltages (Gm becomes zero). The slew rate will than be limited as well:

$$\Delta V/\Delta t = Imax/C \tag{4}$$

The LMH6682/83 has a different setup of the input stage. It has the property to deliver more current to the output stage when the input voltage is higher (class AB input). The current into the Miller capacitor exhibits an exponential character, while this current in other Op Amp designs reaches a saturation level at high input levels: (see Figure 52)

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(5)



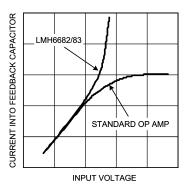


Figure 52.

This property of the LMH6682/83 guaranties a higher slew rate at higher differential input voltages.  $\Delta V/\Delta t = \Delta V^*Gm/C$ 

In Figure 53 one can see that a higher transient voltage than will lead to a higher slew rate.

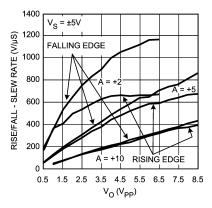


Figure 53.

#### HANDLING VIDEO SIGNALS

When handling video signals, two aspects are very important especially when cascading amplifiers in a NTSC- or PAL video system. A composite video signal consists of both amplitude and phase information. The amplitude represents saturation while phase determines color (color burst is 3.59MHz for NTSC and 4.58MHz for PAL systems). In this case it is not only important to have an accurate amplification of the amplitude but also it is important not to add a varying phase shift to the video signals. It is a known phenomena that at different dc levels over a certain load the phase of the amplified signal will vary a little bit. In a video chain many amplifiers will be cascaded and all errors will be added together. For this reason, it is necessary to have strict requirements for the variation in gain and phase in conjunction to different dc levels. As can be seen in the tables the number for the differential gain for the LMH6682/83 is only 0.01% and for the differential phase it is only 0.08° at a supply voltage of ±5V. Note that the phase is very dependent of the load resistance, mainly because of the dc current delivered by the parts output stage into the load. For more information about differential gain and phase and how to measure it see Application Note OA-24 SNOA370 which can be found on via TI's home page http://www.ti.com

Product Folder Links: LMH6682 LMH6683



#### **OUTPUT PHASE REVERSAL**

This is a problem with some operational amplifiers. This effect is caused by phase reversal in the input stage due to saturation of one or more of the transistors when the inputs exceed the normal expected range of voltages. Some applications, such as servo control loops among others, are sensitive to this kind of behavior and would need special safeguards to ensure proper functioning. The LMH6682/6683 is immune to output phase reversal with input overload. With inputs exceeded, the LMH6682/6683 output will stay at the clamped voltage from the supply rail. Exceeding the input supply voltages beyond the Absolute Maximum Ratings of the device could however damage or otherwise adversely effect the reliability or life of the device.

### **DRIVING CAPACITIVE LOADS**

The LMH6682/6683 can drive moderate values of capacitance by utilizing a series isolation resistor between the output and the capacitive load. Capacitive load tolerance will improve with higher closed loop gain values. Applications such as ADC buffers, among others, present complex and varying capacitive loads to the Op Amp; best value for this isolation resistance is often found by experimentation and actual trial and error for each application.

### **DISTORTION**

Applications with demanding distortion performance requirements are best served with the device operating in the inverting mode. The reason for this is that in the inverting configuration, the input common mode voltage does not vary with the signal and there is no subsequent ill effects due to this shift in operating point and the possibility of additional non-linearity. Moreover, under low closed loop gain settings (most suited to low distortion), the non-inverting configuration is at a further disadvantage of having to contend with the input common voltage range. There is also a strong relationship between output loading and distortion performance (i.e.  $2k\Omega$  vs.  $100\Omega$  distortion improves by about 15dB @1MHz) especially at the lower frequency end where the distortion tends to be lower. At higher frequency, this dependence diminishes greatly such that this difference is only about 5dB at 10MHz. But, in general, lighter output load leads to reduced HD3 term and thus improves THD. (See Harmonic Distortion plots, Figures 19 through 23).

### PRINTED CIRCUIT BOARD LAYOUT AND COMPONENT VALUES SELECTION

Generally it is a good idea to keep in mind that for a good high frequency design both the active parts and the passive ones are suitable for the purpose you are using them for. Amplifying frequencies of several hundreds of MHz is possible while using standard resistors but it makes life much easier when using surface mount ones. These resistors (and capacitors) are smaller and therefore parasitics have lower values and will have less influence on the properties of the amplifier. Another important issue is the PCB, which is no longer a simple carrier for all the parts and a medium to interconnect them. The board becomes a real part itself, adding its own high frequency properties to the overall performance of the circuit. It's good practice to have at least one ground plane on a PCB giving a low impedance path for all decouplings and other ground connections. Care should be taken especially that on board transmission lines have the same impedance as the cables they are connected to (i.e.  $50\Omega$  for most applications and  $75\Omega$  in case of video and cable TV applications). These transmission lines usually require much wider traces on a standard double sided PCB than needed for a 'normal' connection. Another important issue is that inputs and outputs must not 'see' each other or are routed together over the PCB at a small distance. Furthermore it is important that components are placed as flat as possible on the surface of the PCB. For higher frequencies a long lead can act as a coil, a capacitor or an antenna. A pair of leads can even form a transformer. Careful design of the PCB avoids oscillations or other unwanted behavior. When working with really high frequencies, the only components which can be used will be the surface mount ones (for more information see OA-15 SNOA367).

As an example of how important the component values are for the behavior of your circuit, look at the following case: On a board with good high frequency layout, an amplifier is placed. For the two (equal) resistors in the feedback path, 5 different values are used to set the gain to +2. The resistors vary from  $200\Omega$  to  $3k\Omega$ .

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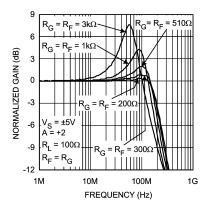


Figure 54.

In Figure 54 it can be seen that there's more peaking with higher resistor values, which can lead to oscillations and bad pulse responses. On the other hand the low resistor values will contribute to higher overall power consumption.

TI suggests the following evaluation boards as a guide for high frequency layout and as an aid in device testing and characterization.

Device	Package	Evaluation Board PN
LMH6682MA	8-Pin SOIC	CLC730036
LMH6682MM	8-Pin VSSOP	CLC730123
LMH6683MA	14-Pin SOIC	CLC730031
LMH6683MT	14-Pin TSSOP	CLC730131

### SNOSA43A -MAY 2004-REVISED APRIL 2013



# **REVISION HISTORY**

Cł	nanges from Original (April 2013) to Revision A	Pa	ge
•	Changed layout of National Data Sheet to TI format		19

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# **PACKAGING INFORMATION**

Orderable part number	Status (1)	Material type	Package   Pins	Package qty   Carrier	<b>RoHS</b> (3)	Lead finish/ Ball material	MSL rating/ Peak reflow	Op temp (°C)	Part marking (6)
LMH6682MA/NOPB	Active	Production	SOIC (D)   8	95   TUBE	Yes	SN	Level-1-260C-UNLIM	-40 to 85	LMH66 82MA
LMH6682MA/NOPB.A	Active	Production	SOIC (D)   8	95   TUBE	Yes	SN	Level-1-260C-UNLIM	-40 to 85	LMH66 82MA
LMH6682MAX/NOPB	Active	Production	SOIC (D)   8	2500   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	LMH66 82MA
LMH6682MAX/NOPB.A	Active	Production	SOIC (D)   8	2500   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	LMH66 82MA
LMH6682MM/NOPB	Active	Production	VSSOP (DGK)   8	1000   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	A90A
LMH6682MM/NOPB.A	Active	Production	VSSOP (DGK)   8	1000   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	A90A
LMH6682MMX/NOPB	Active	Production	VSSOP (DGK)   8	3500   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	A90A
LMH6682MMX/NOPB.A	Active	Production	VSSOP (DGK)   8	3500   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	A90A
LMH6683MA/NOPB	Active	Production	SOIC (D)   14	55   TUBE	Yes	NIPDAU   SN	Level-1-260C-UNLIM	-40 to 85	LMH66 83MA
LMH6683MA/NOPB.A	Active	Production	SOIC (D)   14	55   TUBE	Yes	SN	Level-1-260C-UNLIM	-40 to 85	LMH66 83MA
LMH6683MAX/NOPB	Active	Production	SOIC (D)   14	2500   LARGE T&R	Yes	NIPDAU   SN	Level-1-260C-UNLIM	-40 to 85	LMH66 83MA
LMH6683MAX/NOPB.A	Active	Production	SOIC (D)   14	2500   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 85	LMH66 83MA
LMH6683MT/NOPB	Active	Production	TSSOP (PW)   14	94   TUBE	Yes	NIPDAU   SN	Level-1-260C-UNLIM	-40 to 85	LMH66 83MT
LMH6683MT/NOPB.A	Active	Production	TSSOP (PW)   14	94   TUBE	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	LMH66 83MT
LMH6683MTX/NOPB	Active	Production	TSSOP (PW)   14	2500   LARGE T&R	Yes	NIPDAU   SN	Level-1-260C-UNLIM	-40 to 85	LMH66 83MT
LMH6683MTX/NOPB.A	Active	Production	TSSOP (PW)   14	2500   LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 85	LMH66 83MT

<sup>(1)</sup> **Status:** For more details on status, see our product life cycle.



# PACKAGE OPTION ADDENDUM

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- (2) Material type: When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.
- (3) RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.
- (4) Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.
- (5) MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.
- (6) Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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**PACKAGE MATERIALS INFORMATION** 

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### TAPE AND REEL INFORMATION





	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



#### \*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LMH6682MAX/NOPB	SOIC	D	8	2500	330.0	12.4	6.5	5.4	2.0	8.0	12.0	Q1
LMH6682MM/NOPB	VSSOP	DGK	8	1000	177.8	12.4	5.3	3.4	1.4	8.0	12.0	Q1
LMH6682MMX/NOPB	VSSOP	DGK	8	3500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
LMH6683MAX/NOPB	SOIC	D	14	2500	330.0	16.4	6.5	9.35	2.3	8.0	16.0	Q1
LMH6683MTX/NOPB	TSSOP	PW	14	2500	330.0	12.4	6.95	5.6	1.6	8.0	12.0	Q1
LMH6683MTX/NOPB	TSSOP	PW	14	2500	330.0	12.4	6.9	5.6	1.6	8.0	12.0	Q1



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\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LMH6682MAX/NOPB	SOIC	D	8	2500	367.0	367.0	35.0
LMH6682MM/NOPB	VSSOP	DGK	8	1000	208.0	191.0	35.0
LMH6682MMX/NOPB	VSSOP	DGK	8	3500	367.0	367.0	35.0
LMH6683MAX/NOPB	SOIC	D	14	2500	367.0	367.0	35.0
LMH6683MTX/NOPB	TSSOP	PW	14	2500	367.0	367.0	35.0
LMH6683MTX/NOPB	TSSOP	PW	14	2500	353.0	353.0	32.0

# **PACKAGE MATERIALS INFORMATION**

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### **TUBE**



\*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	T (µm)	B (mm)
LMH6682MA/NOPB	D	SOIC	8	95	495	8	4064	3.05
LMH6682MA/NOPB.A	D	SOIC	8	95	495	8	4064	3.05
LMH6683MA/NOPB	D	SOIC	14	55	495	8	4064	3.05
LMH6683MA/NOPB.A	D	SOIC	14	55	495	8	4064	3.05
LMH6683MT/NOPB	PW	TSSOP	14	94	495	8	2514.6	4.06
LMH6683MT/NOPB	PW	TSSOP	14	94	530	10.2	3600	3.5
LMH6683MT/NOPB.A	PW	TSSOP	14	94	495	8	2514.6	4.06
LMH6683MT/NOPB.A	PW	TSSOP	14	94	530	10.2	3600	3.5





### NOTES:

- 1. All linear dimensions are in millimeters. Dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.

  2. This drawing is subject to change without notice.

  3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not
- exceed 0.15 mm, per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.43 mm, per side.
- 5. Reference JEDEC registration MS-012, variation AB.





NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.





NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.







# NOTES:

- 1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.
- 2. This drawing is subject to change without notice.
- 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed .006 [0.15] per side.
- 4. This dimension does not include interlead flash.
- 5. Reference JEDEC registration MS-012, variation AA.





NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.





### NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.







### NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.

  2. This drawing is subject to change without notice.

  3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not
- exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- 5. Reference JEDEC registration MO-153.





NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.





NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.







### NOTES:

PowerPAD is a trademark of Texas Instruments.

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.

  2. This drawing is subject to change without notice.

  3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not
- exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- 5. Reference JEDEC registration MO-187.





NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 8. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.
- 9. Size of metal pad may vary due to creepage requirement.





NOTES: (continued)

- 11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 12. Board assembly site may have different recommendations for stencil design.



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