

ISO5851 高 CMTI 2.5A/5A 絶縁型 IGBT、MOSFET ゲート・ドライバ、 アクティブ安全機能搭載

1 特長

- $V_{CM} = 1500V$ での最小同相過渡耐性 (CMTI): $100kV/\mu s$
- 2.5A ピーク・ソースおよび 5A ピーク・シンク電流
- 短い伝搬遅延: 76ns (標準値)、110ns (最大値)
- 2A のアクティブ・ミラー・クランプ
- 出力短絡クランプ
- 不飽和化検出時のフォルト・アラームは $\overline{FLT}$ により通知され、 $\overline{RST}$ によりリセット
- 入出力低電圧誤動作防止 (UVLO): レディ (RDY) ピンによる標示付き
- 低電源またはフローティング入力時のアクティブ出力プルダウンおよびデフォルト Low 出力
- 入力電源電圧: 3V~5.5V
- 出力ドライバ供給電圧: 15V~30V
- CMOS 互換の入力
- 20ns 未満の入力パルスと過渡ノイズを除去
- 動作温度: $-40^{\circ}C \sim +125^{\circ}C$ (周囲)
- 絶縁サージ耐久電圧 12800V_{PK}
- 安全関連の認定:
 - 8000V_{PK} V_{IOTM} および 2121V_{PK} V_{IORM} の、DIN V VDE V 0884-10 (VDE V 0884-10):2006-12 準拠の強化絶縁
 - UL1577 準拠で 5700V_{RMS} において 1 分間の絶縁
 - CSA Component Acceptance Notice 5A、IEC-60950-1、および IEC 60601-1 最終機器標準
 - EN 61010-1 および EN 60950-1 準拠の TUV 認定
 - GB4943.1-2011 CQC 認定

2 アプリケーション

- 次のような用途の絶縁 IGBT および MOSFET ドライバ
 - 産業用モーター制御ドライバ
 - 産業用電源
 - ソーラー・インバータ
 - HEV および EV の電源モジュール
 - 誘導加熱

3 概要

ISO5851 は、IGBT および MOSFET 用の 5.7kV_{RMS}、強化絶縁型ゲート・ドライバで、2.5A ソースおよび 5A シンク電流を持ちます。入力側は、単一の 3V および 5.5V 電源で動作します。出力側では、最小 15V から最大 30V までの電源電圧範囲が使用できます。2 つの相補 CMOS 入力により、ゲート・ドライバの出力状態が制御されます。伝搬時間が 76ns と短いため、出力ステージを正確に制御できます。

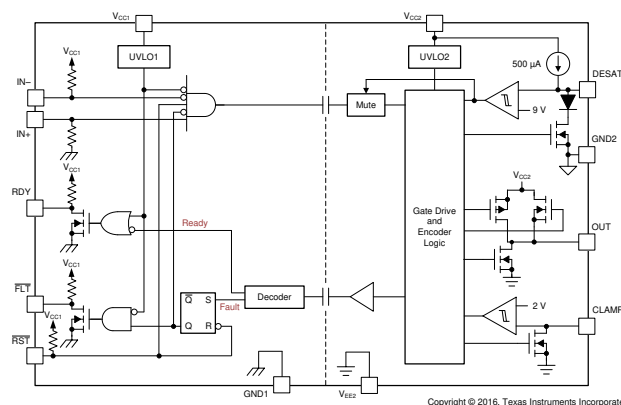
内部不飽和化 (DESAT) フォルト検出により、IGBT が過負荷状況にあることが認識されます。DESAT を検出すると、ゲート・ドライバ出力が V_{EE2} ポテンシャルまで Low に駆動され、IGBT はただちにオフになります。

不飽和化がアクティブのとき、絶縁バリアを通してフォルト信号が送信され、入力側の $\overline{FLT}$ 出力が Low になって、アイソレータ入力ブロックされます。この $\overline{FLT}$ 出力状況はラッチされ、 $\overline{RST}$ 入力の Low アクティブのパルスによりリセットできます。

製品情報 (1)

部品番号	パッケージ	本体サイズ (公称)
ISO5851	SOIC (16)	10.30mm × 7.50mm

- (1) 利用可能なすべてのパッケージについては、このデータシートの末尾にある注文情報を参照してください。



機能ブロック図



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4 Revision History

資料番号末尾の英字は改訂を表しています。その改訂履歴は英語版に準じています。

Changes from Revision B (January 2017) to Revision C (May 2023)	Page
• Added Additional manufacturing certification pending in the <i>Safety-Related Certifications</i> table.....	9

Changes from Revision A (June 2015) to Revision B (January 2017)	Page
• タイトルを「アクティブな安全機能」から「アクティブな保護機能」へ変更.....	1
• 「特長」の「サージ耐性 12800V _{PK} (IEC 61000-4-5 準拠)」を「絶縁サージ耐久電圧 12800V _{PK} 」へ変更.....	1
• 「安全性および規制の認定」に以下の「特長」を追加: 「EN 61010-1 および EN 60950-1 準拠の TUV 認定」.....	1
• Added the <i>Power Ratings</i> table	7
• Moved <i>Insulation Characteristics</i> to the <i>Specifications</i>	7
• Changed the Test Conditions and values for q_{pd} in <i>Insulation Characteristics</i>	7
• Changed R_{lO} From: $100^{\circ}\text{C} \leq T_A \leq \text{max To: } 100^{\circ}\text{C} \leq T_A \leq 125^{\circ}\text{C}$ in the <i>Insulation Characteristics</i>	7
• Moved <i>Safety-Related Certifications</i> to the <i>Specifications</i>	9
• Changed the CSA status from planned to certified.....	9
• Moved <i>Safety Limiting Values</i> to the <i>Specifications</i>	9
• Added the <i>Reinforced High-Voltage Capacitor Life Time Projection</i> figure to <i>Insulation Characteristics Curves</i>	12
• Changed the <i>Thermal Derating Curve for Limiting Current per VDE</i> figure and Added the <i>Thermal Derating Curve for Limiting Power per VDE</i> figure.....	12
• Added the <i>I_{CC1} Supply Current vs Temperature</i> figure to the <i>Typical Characteristics</i>	13
• Changed the <i>OUT Propagation Delay, Non-Inverting Configuration</i> figure	19
• Changed the <i>OUT Propagation Delay, Inverting Configuration</i> figure.....	19
• Added text ", but connecting CLAMP output of the gate driver to the IGBT gate is also not an issue." to <i>Supply and Active Miller Clamp</i>	22
• Changed the second paragraph of the セクション 10.2	24
• Added text "and RST input signal" to セクション 10.2.1	25
• Deleted text " and a 220-pF filtering capacitor." from <i>Recommended ISO5851 Application Circuit</i>	26

- Deleted text "thereby, providing protection against further catastrophic failures." From: the *Global-Shutdown and Reset* section.....28
- Changed the *Normal Operation - Bipolar Supply* and *Normal Operation - Unipolar Supply* figures.....33
- Changed the *PCB Material* section.....35

Changes from Revision * (June 2015) to Revision A (June 2015)
Page

- 1 ページの製品プレビューから完全なデータシートへ変更..... 1
-

5 概要 (続き)

バイポーラ電源による通常動作時に IGBT がオフになると、出力は V_{EE2} にハード・クランプされます。出力電源がユニポラールの場合、アクティブなミラー・クランプを使用でき、低インピーダンスのパスを通してミラー電流をシンクできるため、高電圧の過渡状態で IGBT が動的にオンになることが防止されます。

不飽和化がアクティブのとき、絶縁バリアを通してフォルト信号が送信され、入力側の $\overline{\text{FLT}}$ 出力が **Low** になって、アイソレータ入力がブロックされます。この $\overline{\text{FLT}}$ 出力状況はラッチされ、 $\overline{\text{RST}}$ 入力の **Low** アクティブのパルスによりリセットできます。

バイポーラ電源による通常動作時に IGBT がオフになると、出力は V_{EE2} にハード・クランプされます。出力電源がユニポラールの場合、アクティブなミラー・クランプを使用でき、低インピーダンスのパスを通してミラー電流をシンクできるため、高電圧の過渡状態で IGBT が動的にオンになることが防止されます。

ゲート・ドライバの動作準備は、入力側と出力側の電源を監視する 2 つの低電圧誤動作防止回路により制御されます。いずれかの側の電源が不十分な場合は **RDY** 出力が **Low** になり、そうでない場合はこの出力が **High** になります。

ISO5851 は、16 ピンの SOIC パッケージで供給されます。デバイスの動作は、 $-40^{\circ}\text{C} \sim +125^{\circ}\text{C}$ の周囲温度範囲について規定されています。

6 Pin Configuration and Function

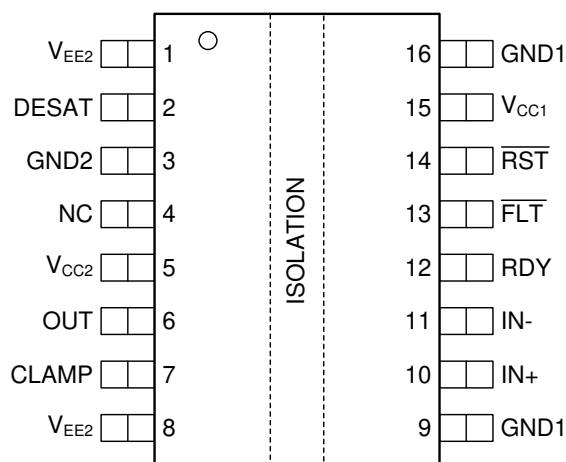


图 6-1. DW Package 16-Pin SOIC Top View

表 6-1. Pin Functions

PIN		I/O	DESCRIPTION
NAME	NO.		
CLAMP	7	O	Miller clamp output
DESAT	2	I	Desaturation voltage input
FLT	13	O	Fault output, low-active during DESAT condition
GND1	9, 16	—	Input ground
GND2	3	—	Gate drive common. Connect to IGBT emitter.
IN+	10	I	Non-inverting gate drive voltage control input
IN-	11	I	Inverting gate drive voltage control input
NC	4	—	Not connected
OUT	6	O	Gate drive voltage output
RDY	12	O	Power-good output, active high when both supplies are good.
RST	14	I	Reset input, apply a low pulse to reset fault latch.
V _{CC1}	15	—	Positive input supply (3 V to 5.5 V)
V _{CC2}	5	—	Most positive output supply potential.
V _{EE2}	1, 8	—	Output negative supply. Connect to GND2 for Unipolar supply application.

7 Specifications

7.1 Absolute Maximum Ratings

Over operating free-air temperature range (unless otherwise noted)⁽¹⁾

			MIN	MAX	UNIT
V _{CC1}	Supply voltage input side		GND1 – 0.3	6	V
V _{CC2}	Positive supply voltage output side	V _{CC2} – GND2	–0.3	35	V
V _{EE2}	Negative supply voltage output side	V _{EE2} – GND2	–17.5	0.3	V
V _(SUP2)	Total supply output voltage	V _{CC2} – V _{EE2}	–0.3	35	V
V _{OUT}	Gate driver output voltage		V _{EE2} – 0.3	V _{CC2} + 0.3	V
I _(OUTH)	Gate driver high output current	Gate driver high output current max pulse width = 10 μs, max duty cycle = 0.2%		2.7	A
I _(OUTL)	Gate driver low output current	Gate driver high output current max pulse width = 10 μs, max duty cycle = 0.2%		5.5	A
V _(LIP)	Voltage at IN+, IN–, FLT, RDY, RST		GND1 – 0.3	V _{CC1} + 0.3	V
I _(LOP)	Output current of FLT, RDY			10	mA
V _(DESAT)	Voltage at DESAT		GND2 – 0.3	V _{CC2} + 0.3	V
V _(CLAMP)	Clamp voltage		V _{EE2} – 0.3	V _{CC2} + 0.3	V
T _J	Junction temperature		–40	150	°C
T _{STG}	Storage temperature		–65	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

7.2 ESD Ratings

		VALUE	UNIT
V _(ESD)	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	±4000
		Charged-device model (CDM), per JEDEC specification JESD22-C101 ⁽²⁾	±1500

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
 (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
V _{CC1}	Supply voltage input side	3		5.5	V
V _{CC2}	Positive supply voltage output side (V _{CC2} – GND2)	15		30	V
V _{EE2}	Negative supply voltage output side (V _{EE2} – GND2)	–15		0	V
V _(SUP2)	Total supply voltage output side (V _{CC2} – V _{EE2})	15		30	V
V _{IH}	High-level input voltage (IN+, IN–, RST)	0.7 × V _{CC1}		V _{CC1}	V
V _{IL}	Low-level input voltage (IN+, IN–, RST)	0		0.3 × V _{CC1}	V
t _{UI}	Pulse width at IN+, IN– for full output (C _{LOAD} = 1 nF)	40			ns
t _{RST}	Pulse width at RST for resetting fault latch	800			ns
T _A	Ambient temperature	–40	25	125	°C

7.4 Thermal Information

THERMAL METRIC ⁽¹⁾		ISO5851	UNIT
		DW (SOIC)	
		16 PINS	
R _{θJA}	Junction-to-ambient thermal resistance	99.6	°C/W
R _{θJC(top)}	Junction-to-case (top) thermal resistance	48.5	°C/W

7.4 Thermal Information (continued)

THERMAL METRIC ⁽¹⁾		ISO5851	UNIT
		DW (SOIC)	
		16 PINS	
R _{θJB}	Junction-to-board thermal resistance	56.5	°C/W
ψ _{JT}	Junction-to-top characterization parameter	29.2	°C/W
ψ _{JB}	Junction-to-board characterization parameter	56.5	°C/W

(1) For more information about traditional and new thermal metrics, see [Semiconductor and IC Package Thermal Metrics](#) (SPRA953).

7.5 Power Ratings

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
P _D	Maximum power dissipation ⁽¹⁾			1255	mW
P _{ID}	Maximum input power dissipation			175	mW
P _{OD}	Maximum output power dissipation			1080	mW

(1) Full chip power dissipation is de-rated 10.04 mW/°C beyond 25°C ambient temperature. At 125°C ambient temperature, a maximum of 251 mW total power dissipation is allowed. Power dissipation can be optimized depending on ambient temperature and board design, while ensuring that Junction temperature does not exceed 150°C.

7.6 Insulation Characteristics

PARAMETER	TEST CONDITIONS	SPECIFICATION	UNIT
CLR	External clearance ⁽¹⁾	Shortest terminal-to-terminal distance through air	8 mm
CPG	External creepage ⁽¹⁾	Shortest terminal-to-terminal distance across the package surface	8 mm
DTI	Distance through the insulation	Minimum internal gap (internal clearance)	21 μm
CTI	Comparative tracking index	DIN EN 60112 (VDE 0303-11); IEC 60112; UL 746A	>600 V
	Material group	According to IEC 60664-1	I
	Overvoltage category per IEC 60664-1	Rated mains voltage ≤ 600 V _{RMS}	I-IV
		Rated mains voltage ≤ 1000 V _{RMS}	I-III
DIN V VDE V 0884-10 (VDE V 0884-10):2006-12⁽²⁾			
V _{IORM}	Maximum repetitive peak isolation voltage	AC voltage (bipolar)	2121 V _{PK}
V _{IOWM}	Maximum isolation working voltage	AC voltage. Time dependent dielectric breakdown (TDDb) Test, see 7-1	1500 V _{RMS}
		DC voltage	2121 V _{DC}
V _{IOTM}	Maximum Transient isolation voltage	V _{TEST} = V _{IOTM} , t = 60 sec (qualification), t = 1 sec (100% production)	8000 V _{PK}
V _{IOSM}	Maximum surge isolation voltage ⁽³⁾	Test method per IEC 60065, 1.2/50 μs waveform, V _{TEST} = 1.6 × V _{IOSM} = 12800 V _{PK} (qualification)	8000 V _{PK}
q _{pd}	Apparent charge ⁽⁴⁾	Method a: After I/O safety test subgroup 2/3, V _{ini} = V _{IOTM} , t _{ni} = 60 s; V _{pd(m)} = 1.2 × V _{IORM} = 2545 V _{PK} , t _m = 10 s	≤5 pC
		Method a: After environmental tests subgroup 1, V _{ini} = V _{IOTM} , t _{ni} = 60 s; V _{pd(m)} = 1.6 × V _{IORM} = 3394 V _{PK} , t _m = 10 s	≤5 pC
		Method b1: At routine test (100% production) and preconditioning (type test) V _{ini} = V _{IOTM} , t _{ni} = 60 s; V _{pd(m)} = 1.875 × V _{IORM} = 3977 V _{PK} , t _m = 10 s	≤5 pC
R _{IO}	Isolation resistance, input to output ⁽⁵⁾	V _{IO} = 500 V at T _s	> 10 ⁹ Ω
		V _{IO} = 500 V, T _A = 25°C	> 10 ¹² Ω
		V _{IO} = 500 V, 100°C ≤ T _A ≤ 125°C	> 10 ¹¹ Ω
C _{IO}	Barrier capacitance, input to output ⁽⁵⁾	V _{IO} = 0.4 x sin (2πft), f = 1 MHz	~1 pF
	Pollution degree		2
	Climatic category		40/125/21

7.6 Insulation Characteristics (continued)

PARAMETER	TEST CONDITIONS	SPECIFICATION	UNIT
UL 1577			
V_{ISO} Withstanding Isolation voltage	$V_{TEST} = V_{ISO}$, $t = 60$ sec (qualification), $V_{TEST} = 1.2 \times V_{ISO} = 6840$ V_{RMS} , $t = 1$ sec (100% production)	5700	V_{RMS}

- (1) Creepage and clearance requirements should be applied according to the specific equipment isolation standards of an application. Care should be taken to maintain the creepage and clearance distance of a board design to ensure that the mounting pads of the isolator on the printed-circuit board do not reduce this distance. Creepage and clearance on a printed-circuit board become equal in certain cases. Techniques such as inserting grooves and/or ribs on a printed circuit board are used to help increase these specifications.
- (2) This coupler is suitable for safe electrical insulation only within the safety ratings. Compliance with the safety ratings shall be ensured by means of suitable protective circuits.
- (3) Testing is carried out in air or oil to determine the intrinsic surge immunity of the isolation barrier.
- (4) Apparent charge is electrical discharge caused by a partial discharge (pd).
- (5) All pins on each side of the barrier tied together creating a two-terminal device.
- (6) Testing is carried out in air or oil to determine the intrinsic surge immunity of the isolation barrier.

7.7 Safety-Related Certifications

VDE	CSA	UL	CQC	TUV
Certified according to DIN V VDE V 0884-10 (VDE V 0884-10):2006-12 and DIN EN 60950-1 (VDE 0805 Teil 1):2011-01	Certified according to CSA Component Acceptance Notice 5A, IEC 60950-1, and IEC 60601-1	Certified according to UL 1577 Component Recognition Program	Certified according to GB 4943.1-2011	Certified according to EN 61010-1:2010 (3rd Ed) and EN 60950-1:2006/A11:2009/A1:2010/A12:2011/A2:2013
Reinforced Insulation Maximum Transient isolation voltage, 8000 V _{PK} ; Maximum surge isolation voltage, 8000 V _{PK} ; Maximum repetitive peak isolation voltage, 2121 V _{PK}	Isolation Rating of 5700 V _{RMS} ; Reinforced insulation per CSA 60950-1- 07+A1+A2 and IEC 60950-1 (2nd Ed.), 800 V _{RMS} max working voltage (pollution degree 2, material group I) ; 2 MOPP (Means of Patient Protection) per CSA 60601-1:14 and IEC 60601-1 Ed. 3.1, 250 V _{RMS} (354 V _{PK}) max working voltage	Single Protection, 5700 V _{RMS}	Reinforced Insulation, Altitude ≤ 5000m, Tropical climate, 400 V _{RMS} maximum working voltage	5700 V _{RMS} Reinforced insulation per EN 61010-1:2010 (3rd Ed) up to working voltage of 600 V _{RMS} 5700 V _{RMS} Reinforced insulation per EN 60950-1:2006/A11:2009/A1:2010/A12:2011/A2:2013 up to working voltage of 800 V _{RMS}
Certification completed Certificate number: 40040142	Certification completed Master contract number: 220991	Certification completed File number: E181974	Certification completed Certificate number: CQC16001141761 Additional manufacturing certification pending	Certification completed Client ID number: 77311

7.8 Safety Limiting Values

Safety limiting intends to minimize potential damage to the isolation barrier upon failure of input or output circuitry. A failure of the I/O can allow low resistance to ground or the supply and, without current limiting, dissipate sufficient power to overheat the die and damage the isolation barrier, potentially leading to secondary system failures.

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
I _S Safety input, output or supply current	R _{θJA} = 99.6°C/W, V _I = 3.6 V, T _J = 150°C, T _A = 25°C			349	mA
	R _{θJA} = 99.6°C/W, V _I = 5.5 V, T _J = 150°C, T _A = 25°C			228	
	R _{θJA} = 99.6°C/W, V _I = 15 V, T _J = 150°C, T _A = 25°C			84	
	R _{θJA} = 99.6°C/W, V _I = 30 V, T _J = 150°C, T _A = 25°C			42	
P _S Safety input, output, or total power	R _{θJA} = 99.6°C/W, T _J = 150°C, T _A = 25°C			1255 ⁽¹⁾	mW
T _S Maximum ambient safety temperature				150	°C

(1) Input, output, or the sum of input and output power should not exceed this value

The safety-limiting constraint is the maximum junction temperature specified in the data sheet. The power dissipation and junction-to-air thermal impedance of the device installed in the application hardware determines the junction temperature. The assumed junction-to-air thermal resistance in the [セクション 7.4](#) table is that of a device installed on a high-K test board for leaded surface-mount packages. The power is the recommended maximum input voltage times the current. The junction temperature is then the ambient temperature plus the power times the junction-to-air thermal resistance.

7.9 Electrical Characteristics

Over recommended operating conditions unless otherwise noted. All typical values are at $T_A = 25^\circ\text{C}$, $V_{CC1} = 5\text{ V}$, $V_{CC2} - \text{GND2} = 15\text{ V}$, $\text{GND2} - V_{EE2} = 8\text{ V}$

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
VOLTAGE SUPPLY						
$V_{IT+}(\text{UVLO1})$	Positive-going UVLO1 threshold voltage input side ($V_{CC1} - \text{GND1}$)				2.25	V
$V_{IT-}(\text{UVLO1})$	Negative-going UVLO1 threshold voltage input side ($V_{CC1} - \text{GND1}$)		1.7			V
$V_{HYS}(\text{UVLO1})$	UVLO1 Hysteresis voltage ($V_{IT+} - V_{IT-}$) input side			0.24		V
$V_{IT+}(\text{UVLO2})$	Positive-going UVLO2 threshold voltage output side ($V_{CC2} - \text{GND2}$)			12	13	V
$V_{IT-}(\text{UVLO2})$	Negative-going UVLO2 threshold voltage output side ($V_{CC2} - \text{GND2}$)		9.5	11		V
$V_{HYS}(\text{UVLO2})$	UVLO2 Hysteresis voltage ($V_{IT+} - V_{IT-}$) output side			1		V
I_{Q1}	Input supply quiescent current			2.8	4.5	mA
I_{Q2}	Output supply quiescent current			3.6	6	mA
LOGIC I/O						
$V_{IT+}(\text{IN}, \text{RST})$	Positive-going input threshold voltage (IN+, IN-, RST)				$0.7 \times V_{CC1}$	V
$V_{IT-}(\text{IN}, \text{RST})$	Negative-going input threshold voltage (IN+, IN-, RST)		$0.3 \times V_{CC1}$			V
$V_{HYS}(\text{IN}, \text{RST})$	Input hysteresis voltage (IN+, IN-, RST)			$0.15 \times V_{CC1}$		V
I_{IH}	High-level input leakage at (IN+)	$\text{IN+} = V_{CC1}$		100		μA
I_{IL}	Low-level input leakage at (IN-, RST)	$\text{IN-} = \text{GND1}$, $\text{RST} = \text{GND1}$		-100		μA
I_{PU}	Pull-up current of FLT, RDY	$V(\text{RDY}) = \text{GND1}$, $V(\text{FLT}) = \text{GND1}$		100		μA
V_{OL}	Low-level output voltage at FLT, RDY	$I(\text{FLT}) = 5\text{ mA}$			0.2	V
GATE DRIVER STAGE						
V_{OUTPD}	Active output pulldown voltage	$I_{\text{OUT}} = 200\text{ mA}$, $V_{CC2} = \text{open}$			2	V
V_{OUTH}	High-level output voltage	$I_{\text{OUT}} = -20\text{ mA}$	$V_{CC2} - 0.5$	$V_{CC2} - 0.24$		V
V_{OUTL}	Low-level output voltage	$I_{\text{OUT}} = 20\text{ mA}$		$V_{EE2} + 13$	$V_{EE2} + 50$	mV
I_{OUTH}	High-level output peak current	$\text{IN+} = \text{high}$, $\text{IN-} = \text{low}$, $V_{\text{OUT}} = V_{CC2} - 15\text{ V}$	1.5	2.5		A
I_{OUTL}	Low-level output peak current	$\text{IN+} = \text{low}$, $\text{IN-} = \text{high}$, $V_{\text{OUT}} = V_{EE2} + 15\text{ V}$	3.4	5		A
ACTIVE MILLER CLAMP						
V_{CLP}	Low-level clamp voltage	$I_{\text{CLP}} = 20\text{ mA}$		$V_{EE2} + 0.015$	$V_{EE2} + 0.08$	V
I_{CLP}	Low-level clamp current	$V_{\text{CLAMP}} = V_{EE2} + 2.5\text{ V}$	1.6	2.5		A
V_{CLTH}	Clamp threshold voltage		1.6	2.1	2.5	V
SHORT CIRCUIT CLAMPING						
$V_{\text{CLP_OUT}}$	Clamping voltage ($V_{\text{OUT}} - V_{CC2}$)	$\text{IN+} = \text{high}$, $\text{IN-} = \text{low}$, $t_{\text{CLP}} = 10\text{ }\mu\text{s}$, $I_{\text{OUTH}} = 500\text{ mA}$		0.8	1.3	V
$V_{\text{CLP_CLAMP}}$	Clamping voltage ($V_{\text{CLP}} - V_{CC2}$)	$\text{IN+} = \text{high}$, $\text{IN-} = \text{low}$, $t_{\text{CLP}} = 10\text{ }\mu\text{s}$, $I_{\text{CLP}} = 500\text{ mA}$		1.3		V
$V_{\text{CLP_CLAMP}}$	Clamping voltage at CLAMP	$\text{IN+} = \text{High}$, $\text{IN-} = \text{Low}$, $I_{\text{CLP}} = 20\text{ mA}$		0.7	1.1	V
DESAT PROTECTION						
I_{CHG}	Blanking capacitor charge current	$V_{\text{DESAT}} - \text{GND2} = 2\text{ V}$	0.42	0.5	0.58	mA
I_{DCHG}	Blanking capacitor discharge current	$V_{\text{DESAT}} - \text{GND2} = 6\text{ V}$	9	14		mA
V_{DSTH}	DESAT threshold voltage with respect to GND2		8.3	9	9.5	V
V_{DSL}	DESAT voltage with respect to GND2, when OUT is driven low		0.4		1	V

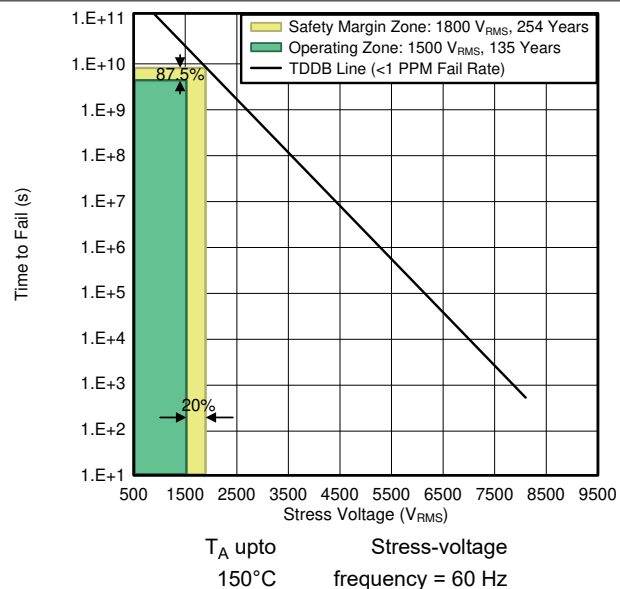
7.10 Switching Characteristics

Over recommended operating conditions unless otherwise noted. All typical values are at $T_A = 25^\circ\text{C}$, $V_{CC1} = 5\text{ V}$, $V_{CC2} - \text{GND2} = 15\text{ V}$, $\text{GND2} - V_{EE2} = 8\text{ V}$

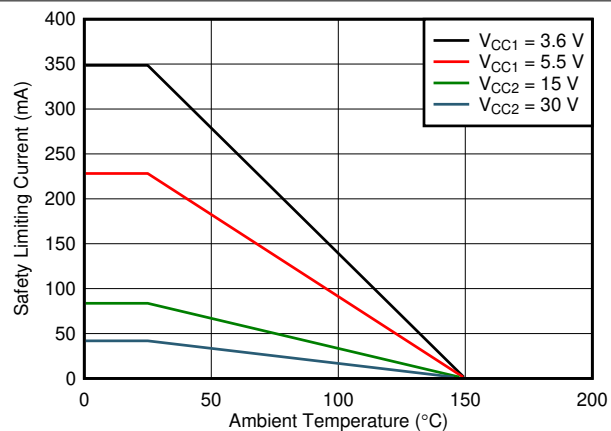
PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
t_r	Output signal rise time	$C_{\text{LOAD}} = 1\text{ nF}$, see FIG 8-1 , FIG 8-2 , and FIG 8-3	12	20	35	ns
t_f	Output signal fall time		12	20	37	ns
$t_{\text{PLH}}, t_{\text{PHL}}$	Propagation Delay			76	110	ns
$t_{\text{sk-p}}$	Pulse Skew $ t_{\text{PHL}} - t_{\text{PLH}} $				20	ns
$t_{\text{sk-pp}}$	Part-to-part skew				30 ⁽¹⁾	ns
t_{GF}	Glitch filter on IN^+ , IN^- , RST		20	30	40	ns
$t_{\text{DESAT}} (10\%)$	DESAT sense to 10% OUT delay		300	415	500	ns
$t_{\text{DESAT}} (\text{GF})$	DESAT glitch filter delay			330		ns
$t_{\text{DESAT}} (\text{FLT})$	DESAT sense to FLT -low delay	see FIG 8-3		2000	2420	ns
t_{LEB}	Leading edge blanking time	see FIG 8-1 and FIG 8-2	330	400	500	ns
$t_{\text{GF}}(\text{RSTFLT})$	Glitch filter on RST for resetting FLT		300		800	ns
C_i	Input capacitance ⁽²⁾	$V_i = V_{CC1} / 2 + 0.4 \times \sin(2\pi f t)$, $f = 1\text{ MHz}$, $V_{CC1} = 5\text{ V}$		2		pF
CMTI	Common-mode transient immunity	$V_{\text{CM}} = 1500\text{ V}$, see FIG 8-4	100	120		kV/ μs

- (1) Measured at same supply voltage and temperature condition
(2) Measured from input pin to ground.

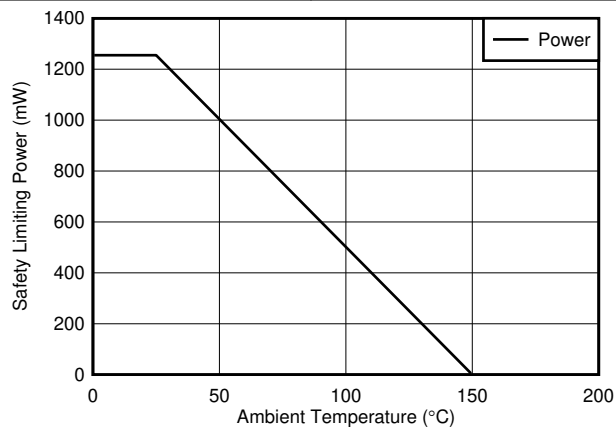
7.11 Insulation Characteristics Curves



7-1. Reinforced High-Voltage Capacitor Life Time Projection

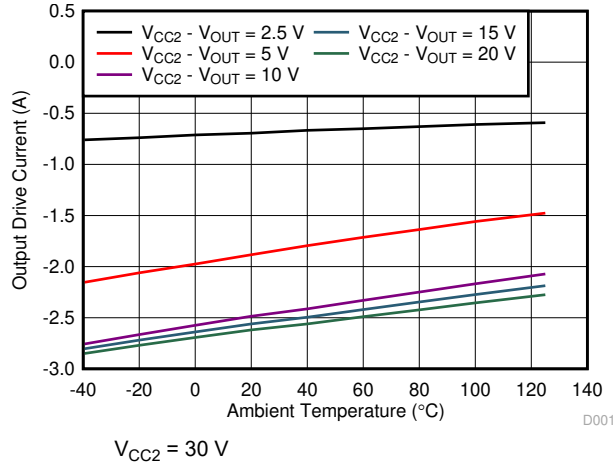


7-2. Thermal Derating Curve for Limiting Current per VDE

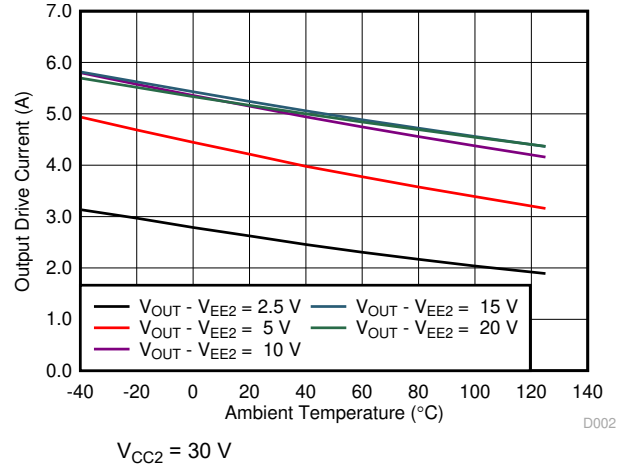


7-3. Thermal Derating Curve for Limiting Power per VDE

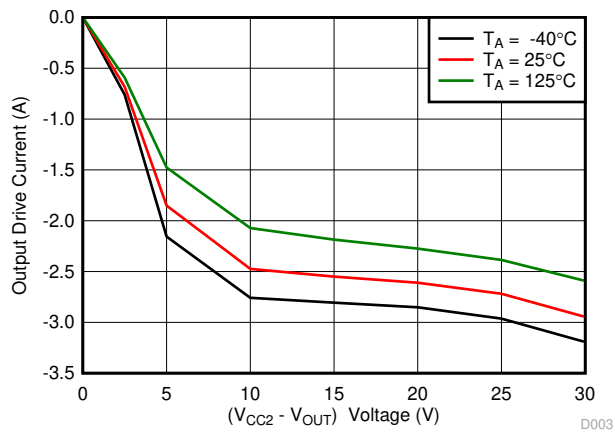
7.12 Typical Characteristics



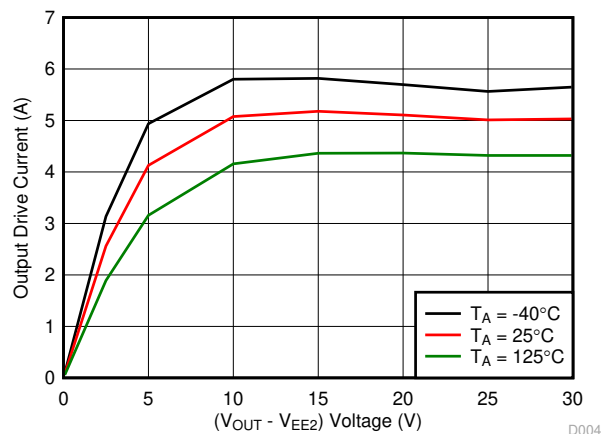
7-4. Output High Drive Current vs Temperature



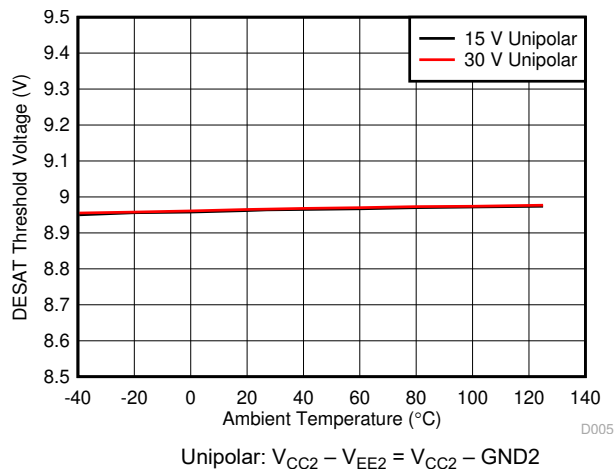
7-5. Output Low Drive Current vs Temperature



7-6. Output High Drive Current vs Output Voltage

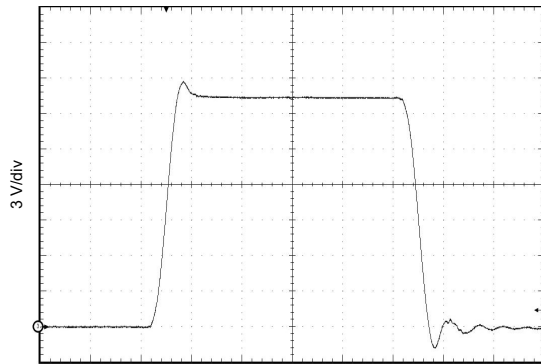


7-7. Output Low Drive Current vs Output Voltage



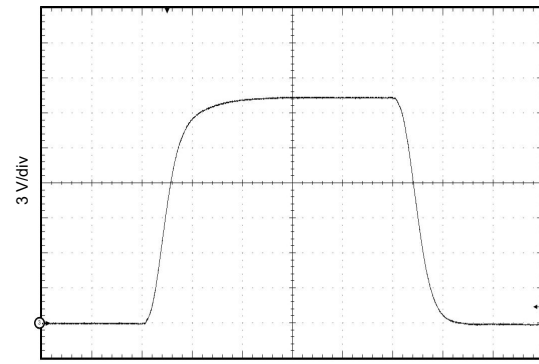
7-8. DESAT Threshold Voltage vs Temperature

7.12 Typical Characteristics (continued)



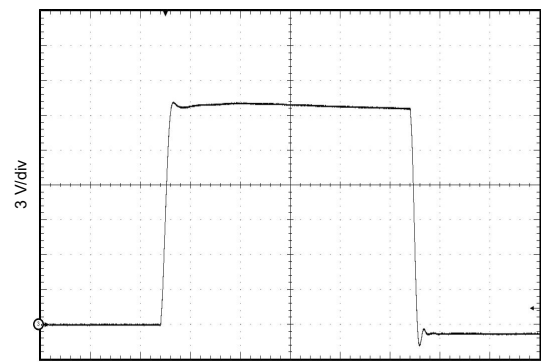
Time - 50 ns/div
 $C_L = 1 \text{ nF}$ $R_G = 0 \Omega$
 $V_{CC2} - V_{EE2} = V_{CC2} - \text{GND2} = 20 \text{ V}$

7-9. OUT Transient Waveform



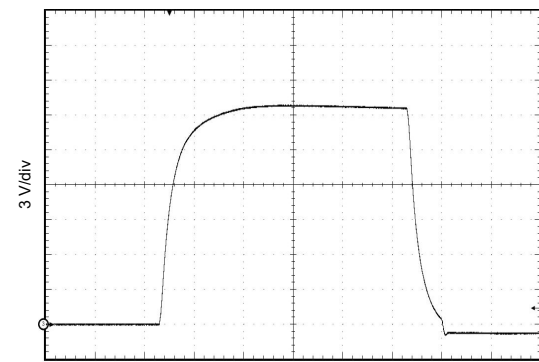
Time - 50 ns/div
 $C_L = 1 \text{ nF}$ $R_G = 10 \Omega$
 $V_{CC2} - V_{EE2} = V_{CC2} - \text{GND2} = 20 \text{ V}$

7-10. OUT Transient Waveform



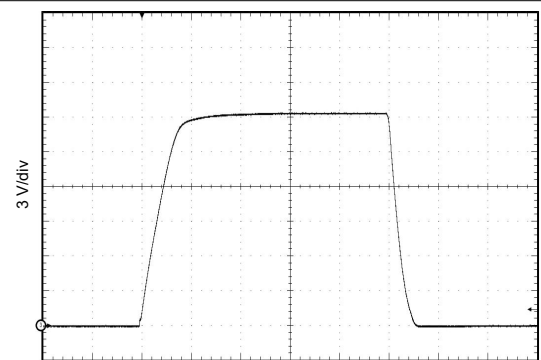
Time - 500 ns/div
 $C_L = 10 \text{ nF}$ $R_G = 0 \Omega$
 $V_{CC2} - V_{EE2} = V_{CC2} - \text{GND2} = 20 \text{ V}$

7-11. OUT Transient Waveform



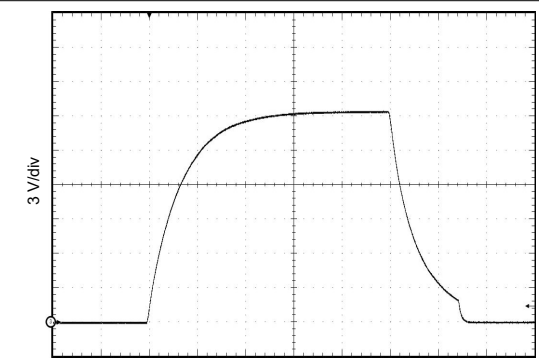
Time - 500 ns/div
 $C_L = 10 \text{ nF}$ $R_G = 10 \Omega$
 $V_{CC2} - V_{EE2} = V_{CC2} - \text{GND2} = 20 \text{ V}$

7-12. OUT Transient Waveform



Time - 1 μs/div
 $C_L = 100 \text{ nF}$ $R_G = 0 \Omega$
 $V_{CC2} - V_{EE2} = V_{CC2} - \text{GND2} = 20 \text{ V}$

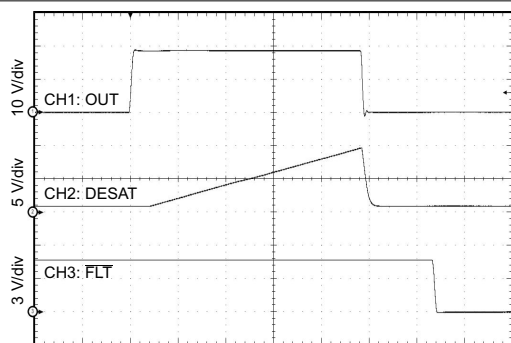
7-13. OUT Transient Waveform



Time - 2 μs/div
 $C_L = 100 \text{ nF}$ $R_G = 10 \Omega$
 $V_{CC2} - V_{EE2} = V_{CC2} - \text{GND2} = 20 \text{ V}$

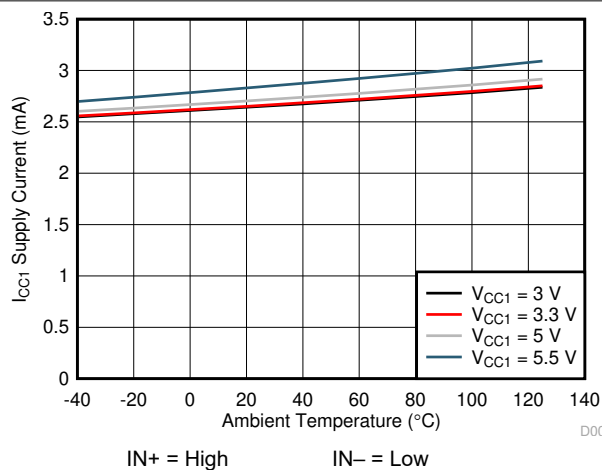
7-14. OUT Transient Waveform

7.12 Typical Characteristics (continued)

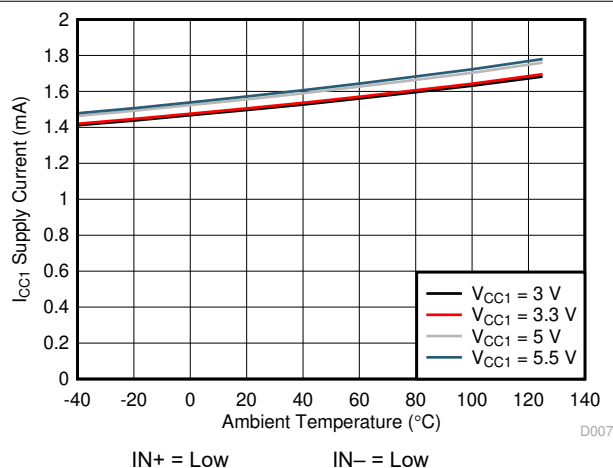


$C_L = 100$ nF $R_G = 10$ Ω
 $V_{CC2} - V_{EE2} = V_{CC2} - GND2 = 20$ V

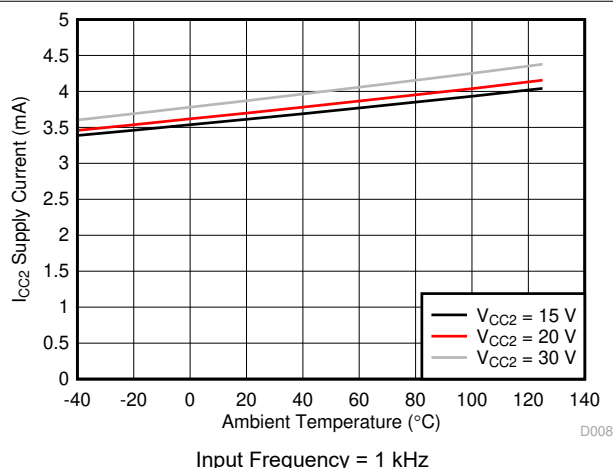
7-15. OUT Transient Waveform DESAT and FLT



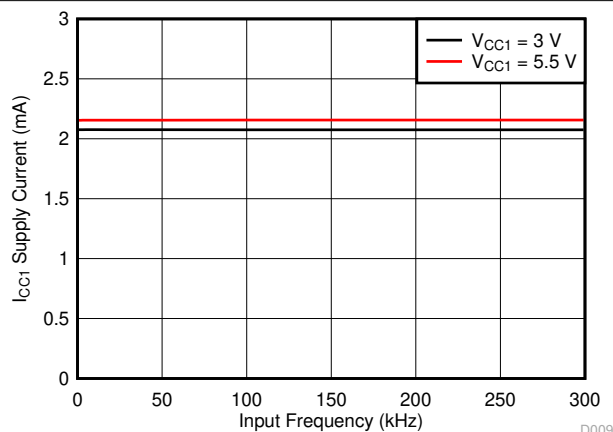
7-16. I_{CC1} Supply Current vs Temperature



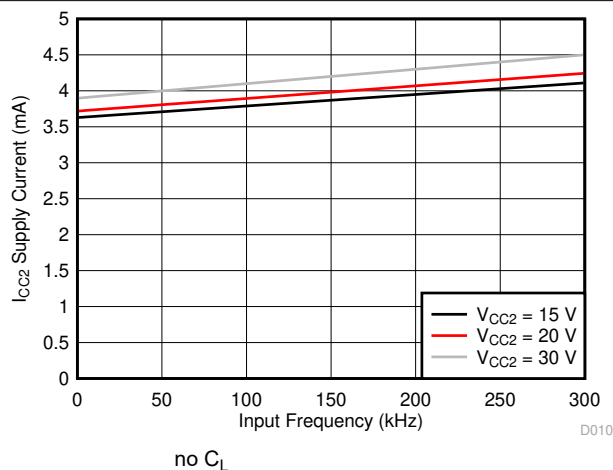
7-17. I_{CC1} Supply Current vs Temperature



7-18. I_{CC2} Supply Current vs Temperature



7-19. I_{CC1} Supply Current vs Input Frequency



7-20. I_{CC2} Supply Current vs Input Frequency

7.12 Typical Characteristics (continued)

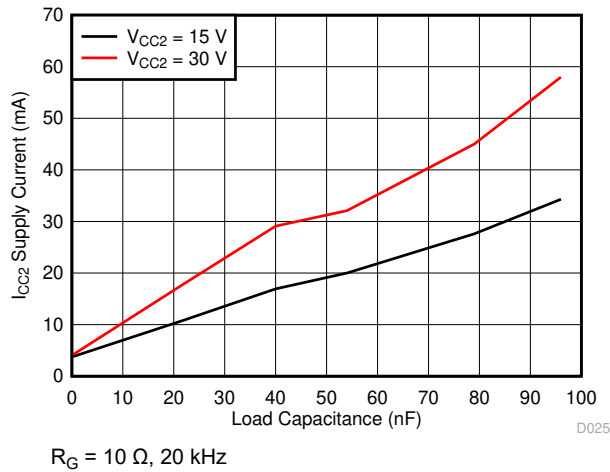


Figure 7-21. I_{CC2} Supply Current vs Load Capacitance

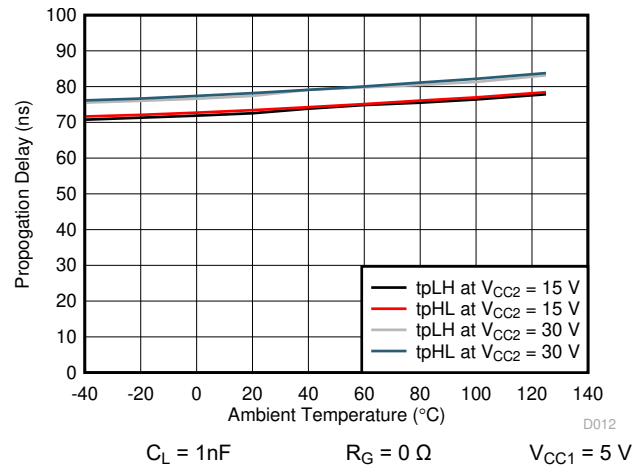


Figure 7-22. V_{CC1} Propagation Delay vs Temperature

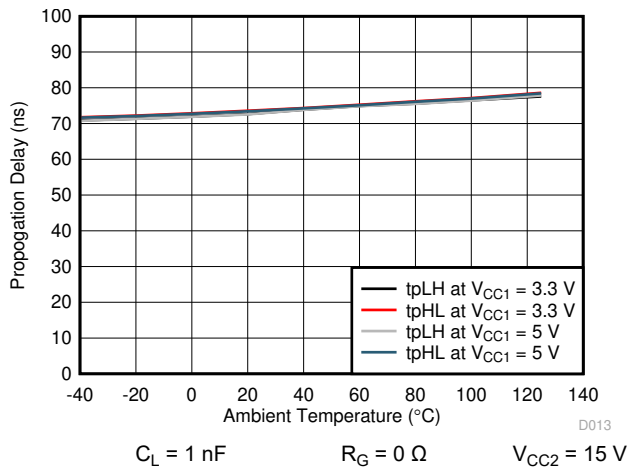


Figure 7-23. V_{CC2} Propagation Delay vs Temperature

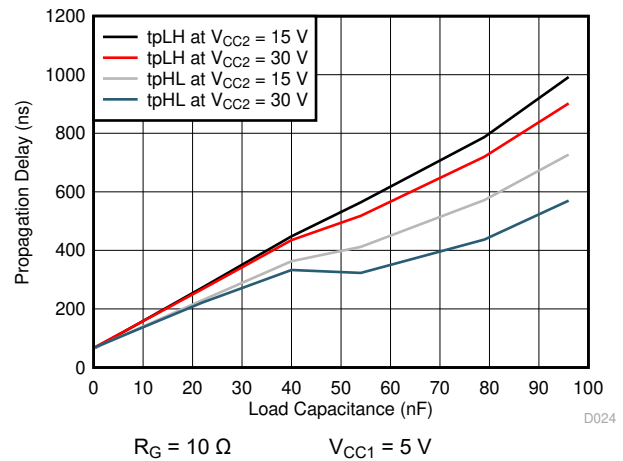


Figure 7-24. Propagation Delay vs Load Capacitance

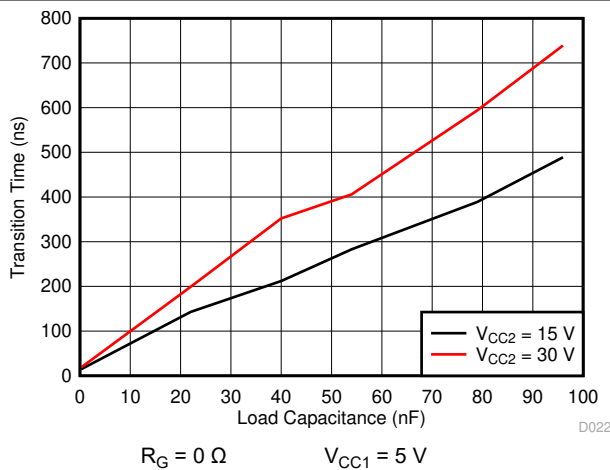


Figure 7-25. t_r Rise Time vs Load Capacitance

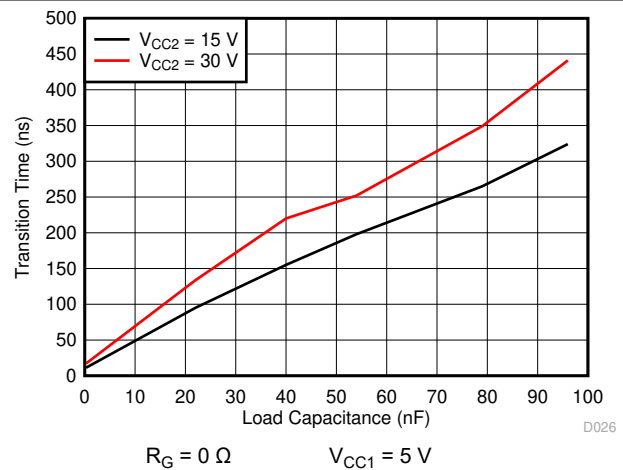


Figure 7-26. t_f Fall Time vs Load Capacitance

7.12 Typical Characteristics (continued)

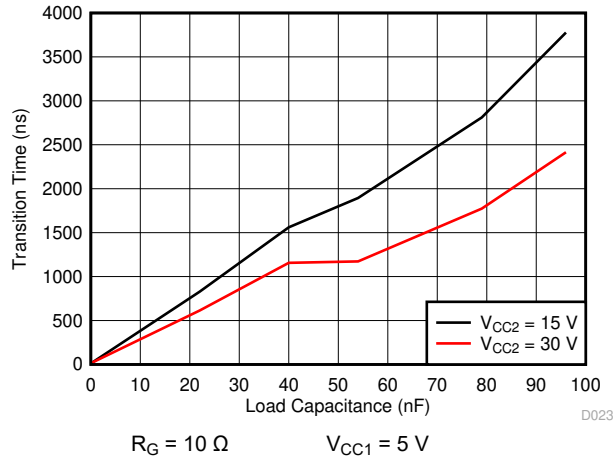


Figure 7-27. t_r Rise Time vs Load Capacitance

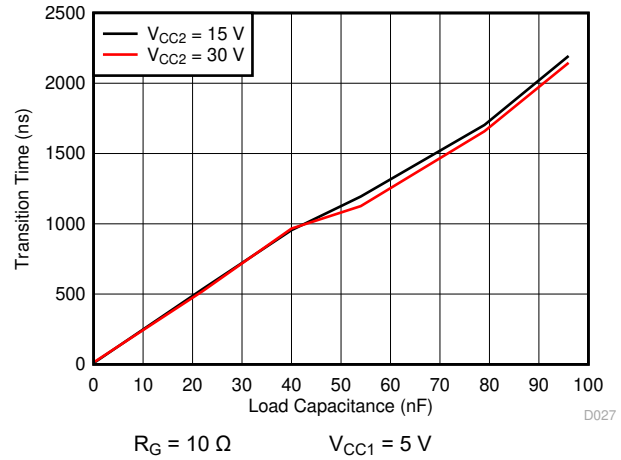


Figure 7-28. t_f Fall Time vs Load Capacitance

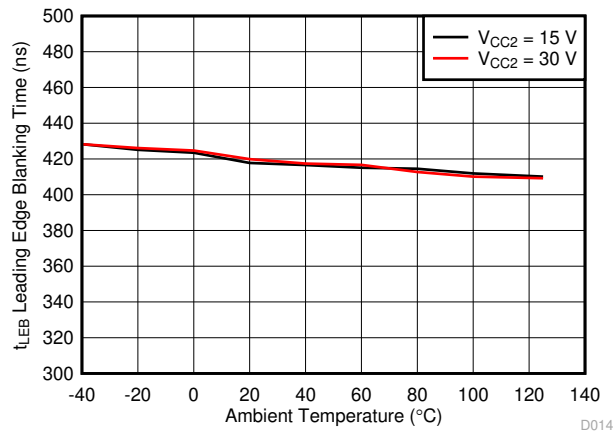


Figure 7-29. Leading Edge Blanking Time With Temperature

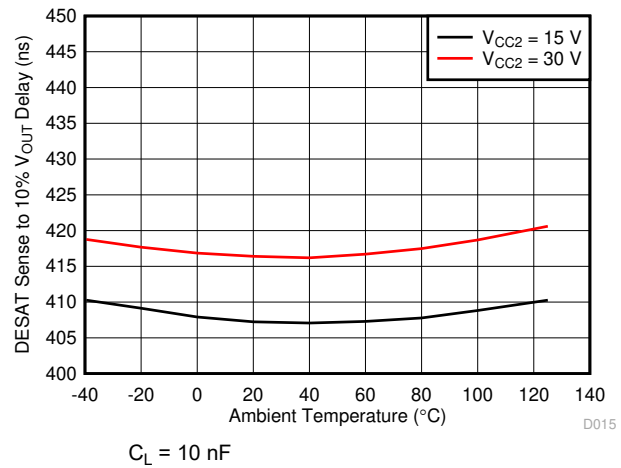


Figure 7-30. DESAT Sense to V_{OUT} 10% Delay vs Temperature

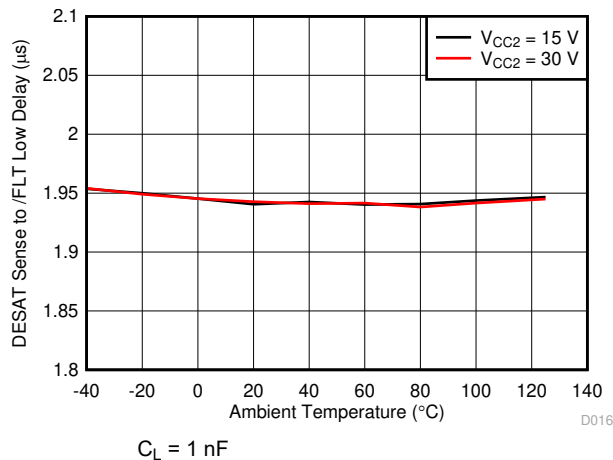


Figure 7-31. DESAT Sense to $\overline{FLT}$ Low Delay vs Temperature

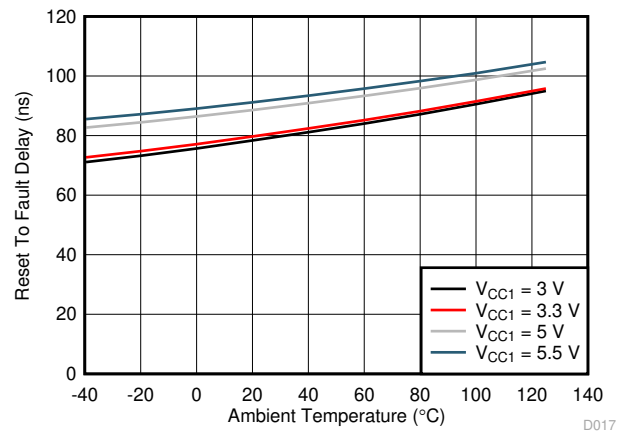


Figure 7-32. Reset to Fault Delay Across Temperature

7.12 Typical Characteristics (continued)

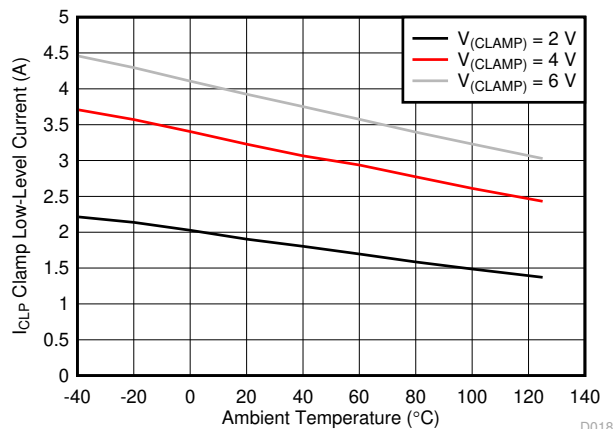


Figure 7-33. Miller Clamp Current vs Temperature

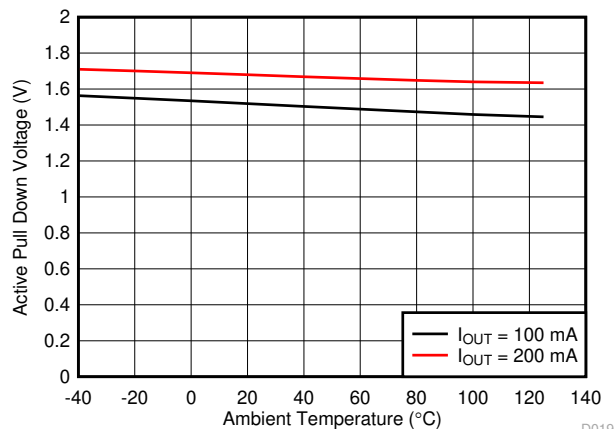


Figure 7-34. Active Pulldown Voltage vs Temperature

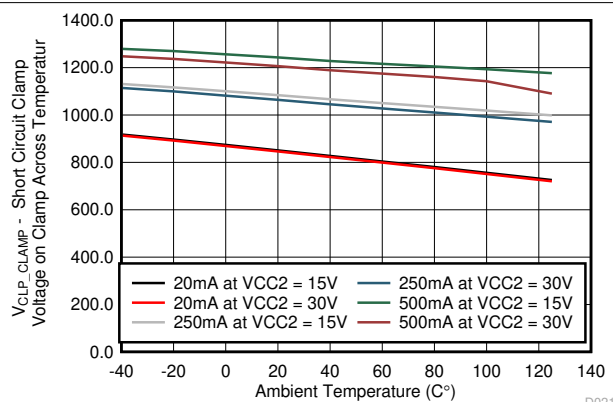


Figure 7-35. V_{CLP_CLAMP} - Short Circuit Clamp Voltage on Clamp Across Temperature

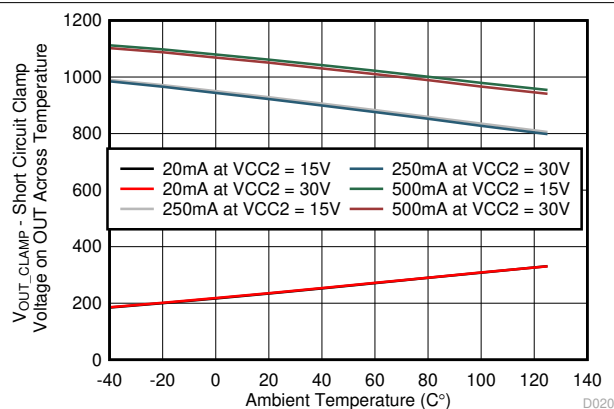
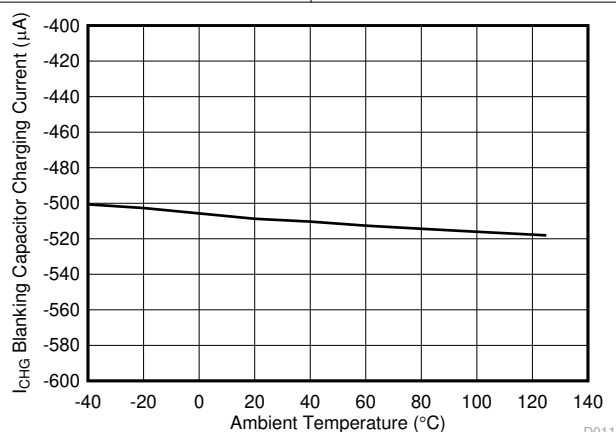


Figure 7-36. V_{OUT_CLAMP} - Short Circuit Clamp Voltage on OUT Across Temperature

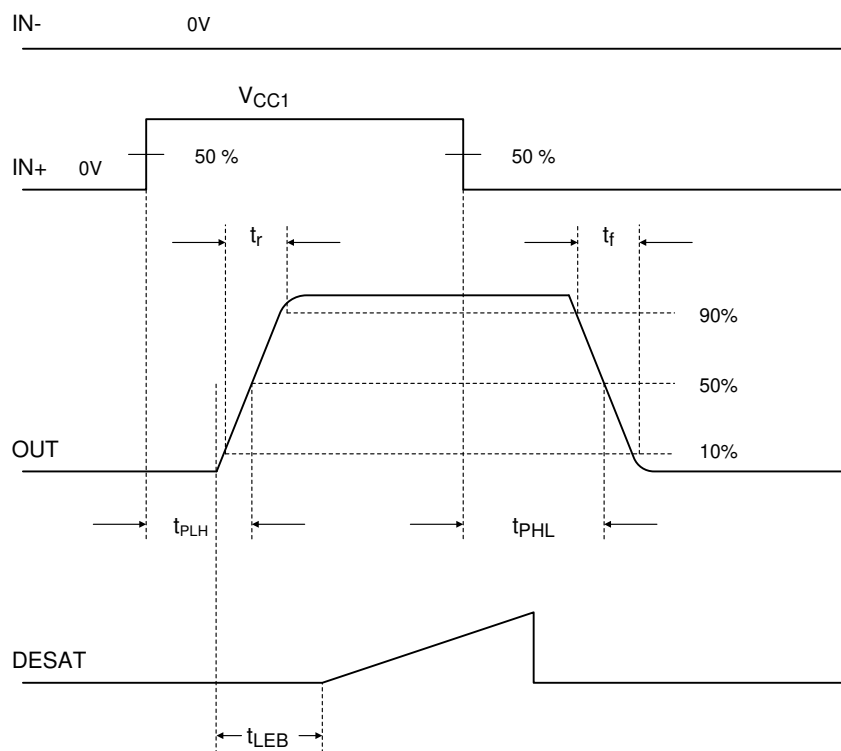


$V_{CC2} = 15V$

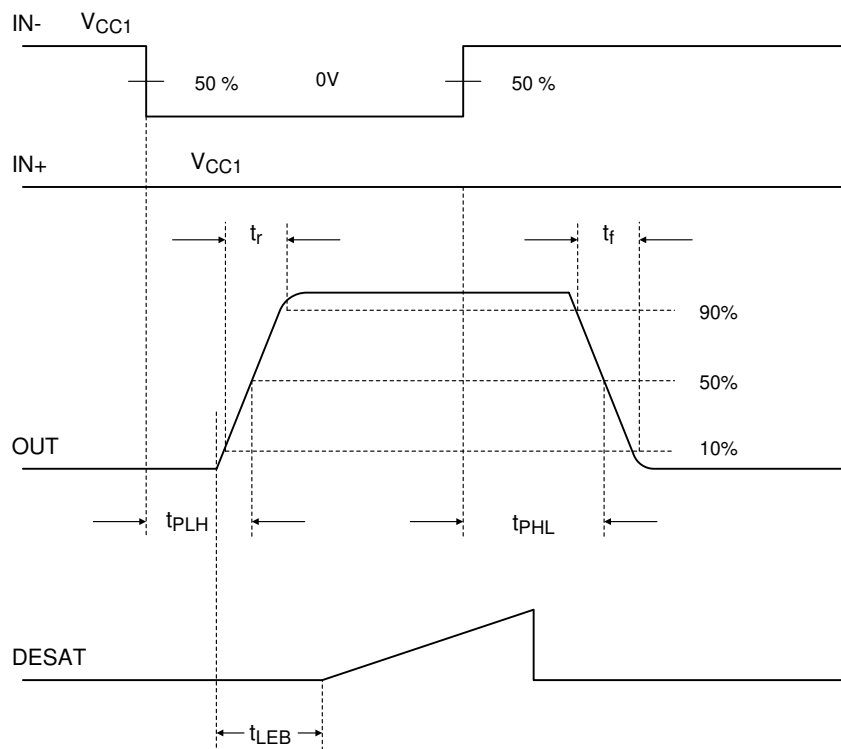
$DESAT = 6V$

Figure 7-37. Blanking Capacitor Charging Current vs Temperature

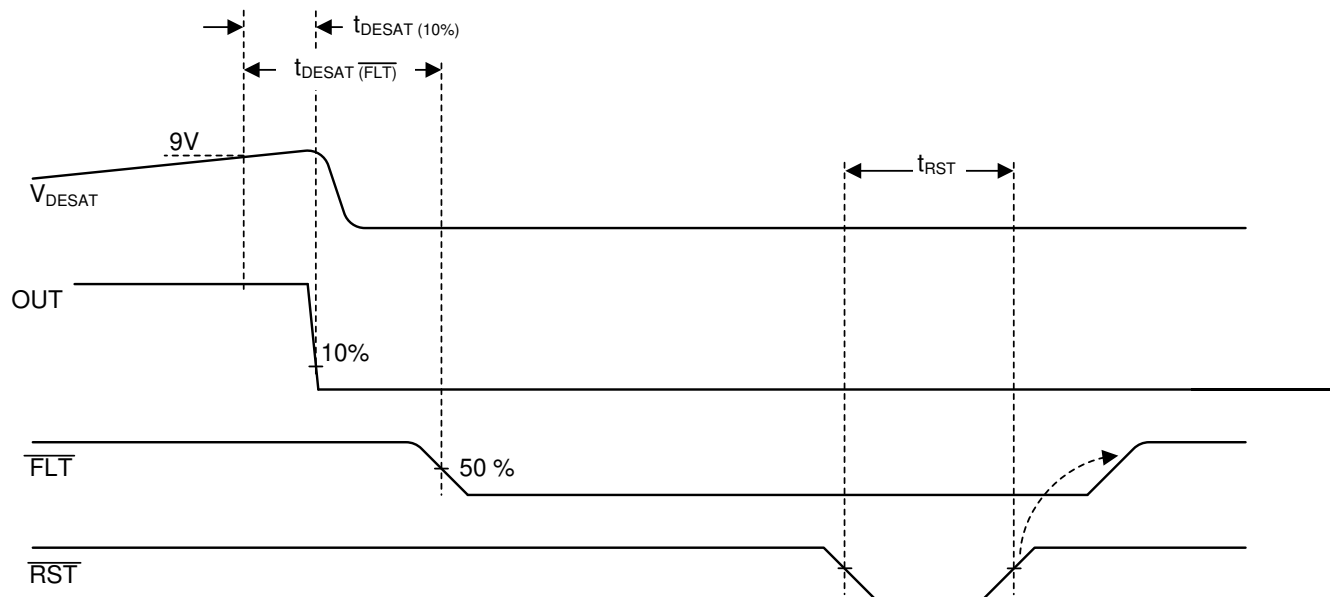
8 Parameter Measurement Information



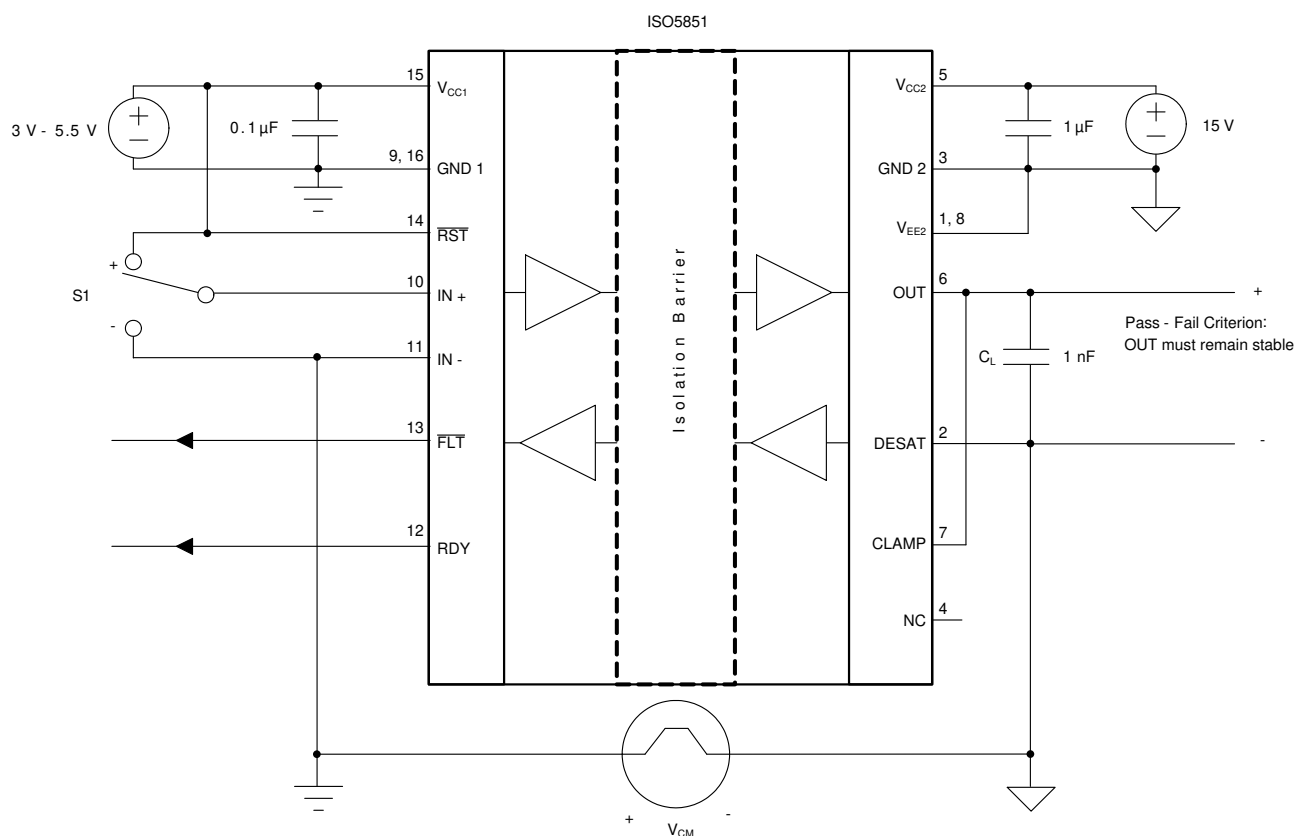
8-1. OUT Propagation Delay, Non-Inverting Configuration



8-2. OUT Propagation Delay, Inverting Configuration



8-3. DESAT, OUT, $\overline{FLT}$, $\overline{RST}$ Delay



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8-4. Common-Mode Transient Immunity Test Circuit

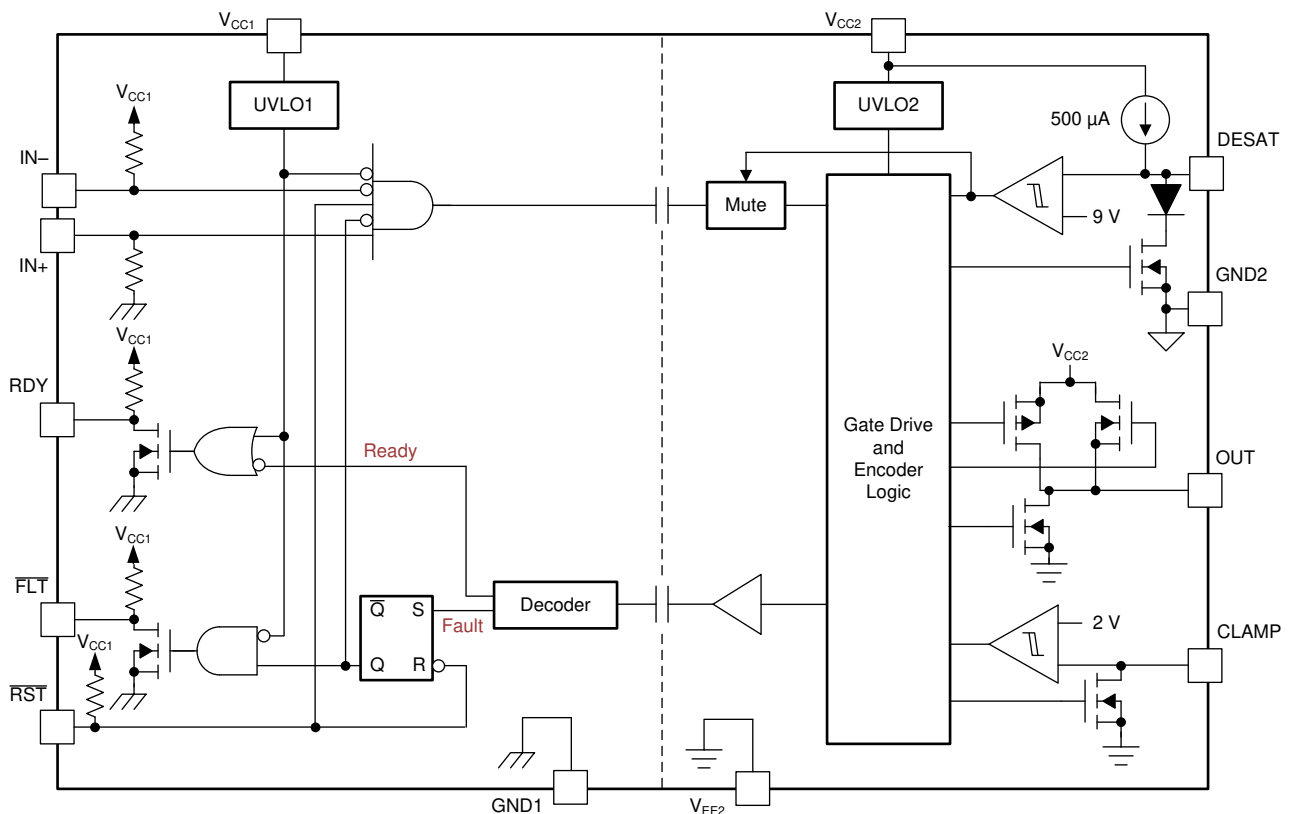
9 Detailed Description

9.1 Overview

The ISO5851 is an isolated gate driver for IGBTs and MOSFETs. Input CMOS logic and output power stage are separated by a capacitive, silicon dioxide (SiO₂), isolation barrier.

The IO circuitry on the input side interfaces with a micro controller and consists of gate drive control and RESET (RST) inputs, READY (RDY) and FAULT (FLT) alarm outputs. The power stage consists of power transistors to supply 2.5-A pullup and 5-A pulldown currents to drive the capacitive load of the external power transistors, as well as DESAT detection circuitry to monitor IGBT collector-emitter overvoltage under short circuit events. The capacitive isolation core consists of transmit circuitry to couple signals across the capacitive isolation barrier, and receive circuitry to convert the resulting low-swing signals into CMOS levels. The ISO5851 also contains under voltage lockout circuitry to prevent insufficient gate drive to the external IGBT, and active output pulldown feature which ensures that the gate-driver output is held low, if the output supply voltage is absent. The ISO5851 also has an active Miller clamp function which can be used to prevent parasitic turn-on of the external power transistor, due to Miller effect, for unipolar supply operation.

9.2 Functional Block Diagram



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9.3 Feature Description

9.3.1 Supply and Active Miller Clamp

The ISO5851 supports both bipolar and unipolar power supply with active Miller clamp.

For operation with bipolar supplies, the IGBT is turned off with a negative voltage on its gate with respect to its emitter. This prevents the IGBT from unintentionally turning on because of current induced from its collector to its gate due to Miller effect. In this condition it is not necessary to connect CLAMP output of the gate driver to the IGBT gate, but connecting CLAMP output of the gate driver to the IGBT gate is also not an issue. Typical values of V_{CC2} and V_{EE2} for bipolar operation are 15 V and –8 V with respect to GND2.

For operation with unipolar supply, typically, V_{CC2} is connected to 15-V with respect to GND2, and V_{EE2} is connected to GND2. In this use case, the IGBT can turn-on due to additional charge from IGBT Miller capacitance caused by a high voltage slew rate transition on the IGBT collector. To prevent IGBT to turn on, the CLAMP pin is connected to IGBT gate and Miller current is sunk through a low impedance CLAMP transistor.

Miller CLAMP is designed for Miller current up to 2 A. When the IGBT is turned-off and the gate voltage transitions below 2 V the CLAMP current output is activated.

9.3.2 Active Output Pulldown

The active output pulldown feature ensures that the IGBT gate OUT is clamped to V_{EE2} to ensure safe IGBT off-state when the output side is not connected to the power supply.

9.3.3 Undervoltage Lockout (UVLO) With Ready (RDY) Pin Indication Output

Undervoltage lockout (UVLO) ensures correct switching of IGBT. The IGBT is turned-off, if the supply V_{CC1} drops below $V_{IT-(UVLO1)}$, irrespective of IN+, IN– and RST input till V_{CC1} goes above $V_{IT+(UVLO1)}$.

In similar manner, the IGBT is turned-off, if the supply V_{CC2} drops below $V_{IT-(UVLO2)}$, irrespective of IN+, IN– and RST input till V_{CC2} goes above $V_{IT+(UVLO2)}$.

Ready (RDY) pin indicates status of input and output side Under Voltage Lock-Out (UVLO) internal protection feature. If either side of device have insufficient supply (V_{CC1} or V_{CC2}), the RDY pin output goes low; otherwise, RDY pin output is high. RDY pin also serves as an indication to the micro-controller that the device is ready for operation.

9.3.4 Fault ($\overline{FLT}$) and Reset ($\overline{RST}$)

During IGBT overload condition, to report desaturation error $\overline{FLT}$ goes low. If $\overline{RST}$ is held low for the specified duration, $\overline{FLT}$ is cleared at rising edge of $\overline{RST}$. $\overline{RST}$ has an internal filter to reject noise and glitches. By asserting $\overline{RST}$ for at-least the specified minimum duration, device input logic can be enabled or disabled.

9.3.5 Short Circuit Clamp

Under short circuit events it is possible that currents are induced back into the gate-driver OUT and CLAMP pins due to parasitic Miller capacitance between the IGBT collector and gate terminals. Internal protection diodes on OUT and CLAMP help to sink these currents while clamping the voltages on these pins to values slightly higher than the output side supply.

9.4 Device Functional Modes

表 9-1 lists the functional modes for the ISO5851 device.

In ISO5851 OUT to follow IN+ in normal functional mode, $\overline{\text{FLT}}$ must be in high state.

表 9-1. Function Table⁽¹⁾

V _{CC1}	V _{CC2}	IN+	IN–	RST	RDY	OUT
PU	PD	X	X	X	Low	Low
PD	PU	X	X	X	Low	Low
PU	PU	X	X	Low	High	Low
PU	Open	X	X	X	Low	Low
PU	PU	Low	X	X	High	Low
PU	PU	X	High	X	High	Low
PU	PU	High	Low	High	High	High

(1) PU: Power Up (V_{CC1} ≥ 2.25-V, V_{CC2} ≥ 13-V), PD: Power Down (V_{CC1} ≤ 1.7-V, V_{CC2} ≤ 9.5-V), X: Irrelevant

10 Application and Implementation

注

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10.1 Application Information

The ISO5851 is an isolated gate driver for power semiconductor devices such as IGBTs and MOSFETs. It is intended for use in applications such as motor control, industrial inverters and switched mode power supplies. In these applications, sophisticated PWM control signals are required to turn the power devices on and off, which at the system level eventually may determine, for example, the speed, position, and torque of the motor or the output voltage, frequency and phase of the inverter. These control signals are usually the outputs of a micro controller, and are at low voltage levels such as 3.3 V or 5 V. The gate controls required by the MOSFETs and IGBTs, on the other hand, are in the range of 30 V (using a unipolar output supply) to 15 V (using bipolar output supply), and need high current capability to be able to drive the large capacitive loads offered by those power transistors. Not only that, the gate drive needs to be applied with reference to the Emitter of the IGBT (Source for MOSFET), and by construction, the emitter node in a gate drive system may swing between 0 to the DC bus voltage, that can be several hundreds of volts in magnitude.

The ISO5851 is thus used to level shift the incoming 3.3-V and 5-V control signals from the microcontroller to the 30 V (using a unipolar output supply) to 15 V (using bipolar output supply) drive required by the power transistors while ensuring high-voltage isolation between the driver side and the microcontroller side.

10.2 Typical Applications

✎ 10-1 shows the typical application of a three-phase inverter using six ISO5851 isolated gate drivers. Three-phase inverters are used for variable-frequency drives to control the operating speed and torque of AC motors and for high power applications such as high-voltage DC (HVDC) power transmission.

The basic three-phase inverter consists of six power switches, and each switch is driven by one SO5851. The switches are driven on and off at high switching frequency with specific patterns that to converter dc bus voltage to three-phase AC voltages.

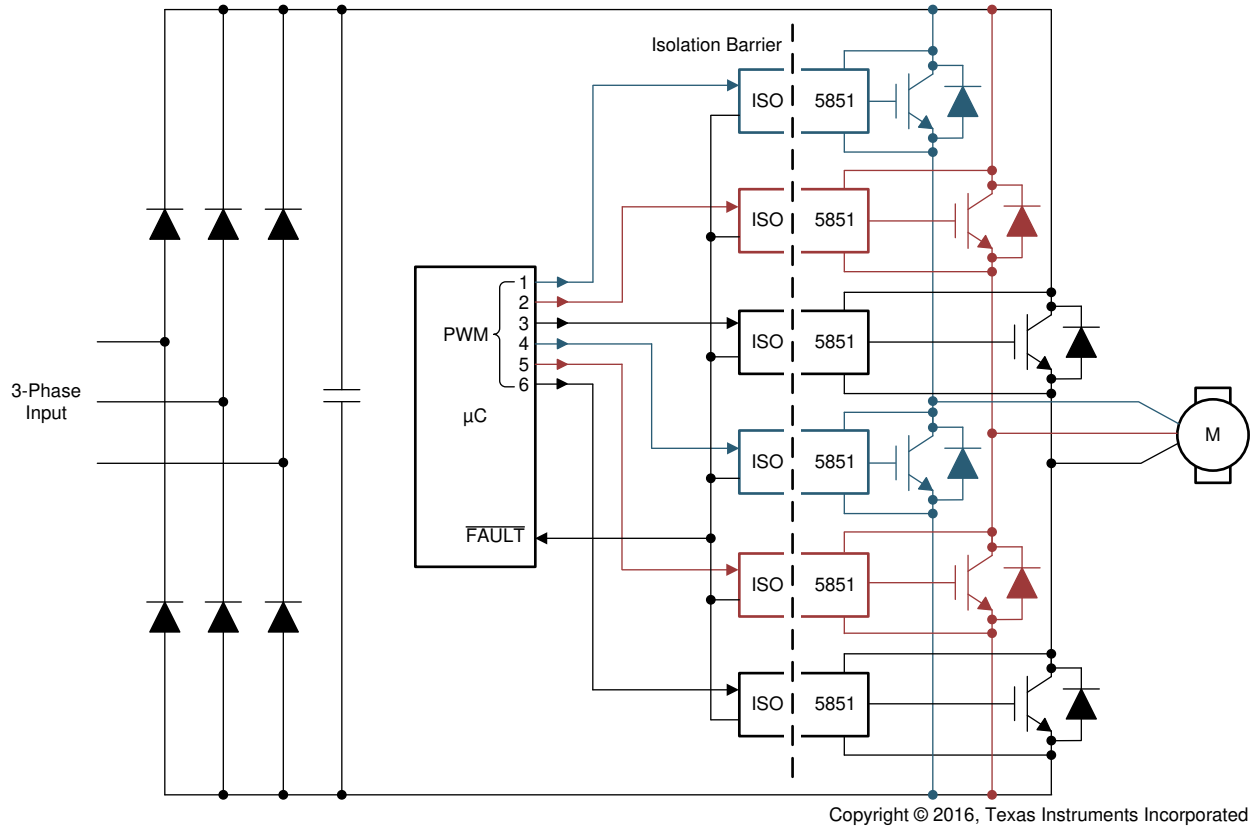


图 10-1. Typical Motor Drive Application

10.2.1 Design Requirements

Unlike optocoupler based gate drivers which need external current drivers and biasing circuitry to provide the input control signals, the input control to the ISO5851 is CMOS and can be directly driven by the microcontroller. Other design requirements include decoupling capacitors on the input and output supplies, a pullup resistor on the common drain FLT output signal and RST input signal, and a high-voltage protection diode between the IGBT collector and the DESAT input. Further details are explained in the subsequent sections. 表 10-1 shows the allowed range for Input and Output supply voltage, and the typical current output available from the gate-driver.

表 10-1. Design Parameters

PARAMETER	VALUE
Input supply voltage	3 V to 5.5 V
Unipolar output supply voltage ($V_{CC2} - GND2 = V_{CC2} - V_{EE2}$)	15 V to 30 V
Bipolar output supply voltage ($V_{CC2} - V_{EE2}$)	15 V to 30 V
Bipolar output supply voltage ($GND2 - V_{EE2}$)	0 V to 15 V
Output current	2.5 A

10.2.2 Detailed Design Procedure

10.2.2.1 Recommended ISO5851 Application Circuit

The ISO5851 has both, inverting and non-inverting gate control inputs, an active low reset input, and an open drain fault output suitable for wired-OR applications. The recommended application circuit in [Figure 10-2](#) shows a typical gate driver implementation with unipolar output supply and [Figure 10-3](#) shows a typical gate driver implementation with bipolar output supply using the ISO5851.

A 0.1- μF bypass capacitor, recommended at input supply pin V_{CC1} and 1- μF bypass capacitor, recommended at output supply pin V_{CC2} , provide the large transient currents necessary during a switching transition to ensure reliable operation. The 220 pF blanking capacitor disables DESAT detection during the off-to-on transition of the power device. The DESAT diode (D_{DST}) and its 1-k Ω series resistor are external protection components. The R_G gate resistor limits the gate charge current and indirectly controls the IGBT collector voltage rise and fall times. The open-drain FLT output and RDY output has a passive 10-k Ω pullup resistor. In this application, the IGBT gate driver is disabled when a fault is detected and will not resume switching until the microcontroller applies a reset signal.

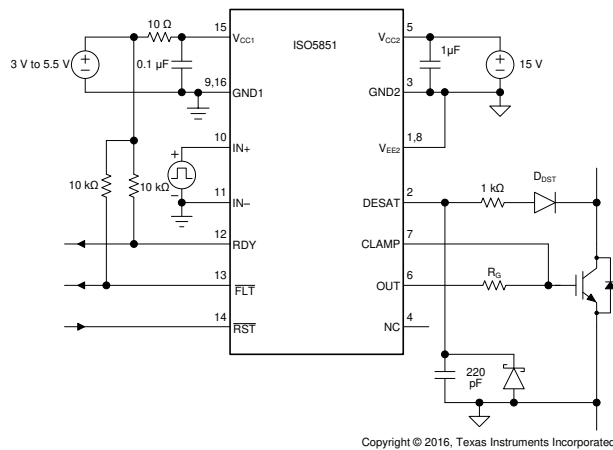


Figure 10-2. Unipolar Output Supply

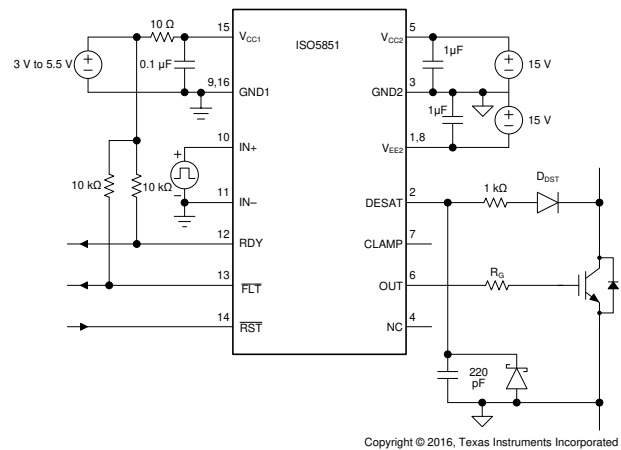
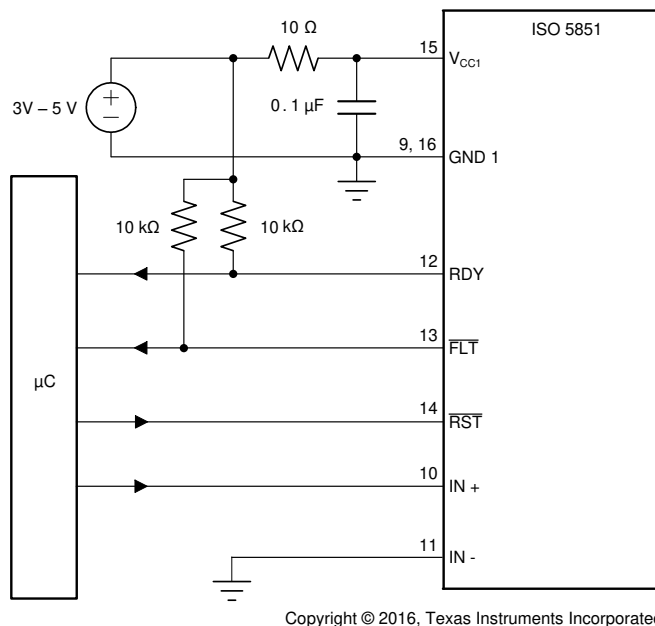


Figure 10-3. Bipolar Output Supply

10.2.2.2 $\overline{\text{FLT}}$ and RDY Pin Circuitry

There is 50k pullup resistor internally on $\overline{\text{FLT}}$ and RDY pins. The $\overline{\text{FLT}}$ and RDY pin is an open-drain output. A 10-k Ω pullup resistor can be used to make it faster rise and to provide logic high when $\overline{\text{FLT}}$ and RDY is inactive, as shown in [Figure 10-4](#).

Fast common mode transients can inject noise and glitches on $\overline{\text{FLT}}$ and RDY pins due to parasitic coupling. This is dependent on board layout. If required, additional capacitance (100 pF to 300 pF) can be included on the $\overline{\text{FLT}}$ and RDY pins.



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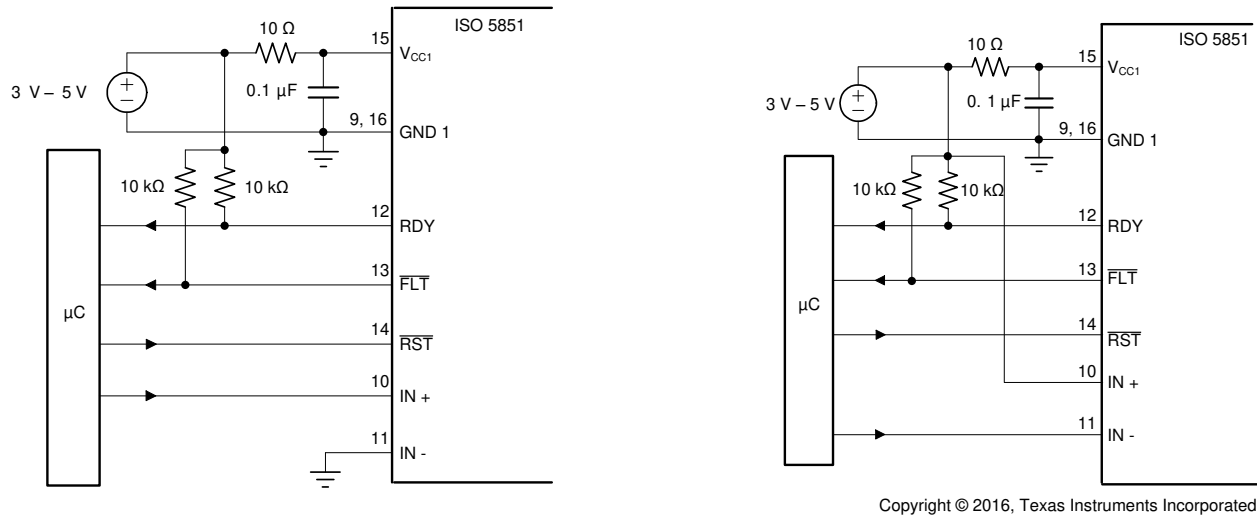
Figure 10-4. $\overline{\text{FLT}}$ and RDY Pin Circuitry for High CMTI

10.2.2.3 Driving the Control Inputs

The amount of common-mode transient immunity (CMTI) can be curtailed by the capacitive coupling from the high-voltage output circuit to the low-voltage input side of the ISO5851. For maximum CMTI performance, the digital control inputs, IN+ and IN–, must be actively driven by standard CMOS, push-pull drive circuits. This type of low-impedance signal source provides active drive signals that prevent unwanted switching of the ISO5851 output under extreme common-mode transient conditions. Passive drive circuits, such as open-drain configurations using pullup resistors, must be avoided. There is a 20 ns glitch filter which can filter a glitch up to 20 ns on IN+ or IN–.

10.2.2.4 Local Shutdown and Reset

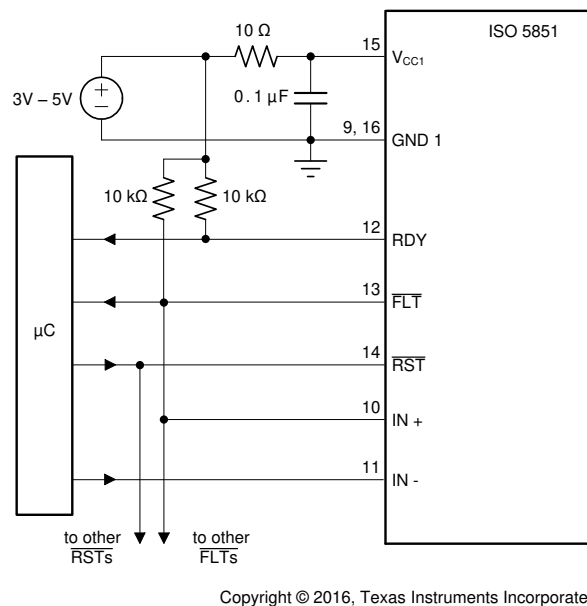
In applications with local shutdown and reset, the $\overline{\text{FLT}}$ output of each gate driver is polled separately, and the individual reset lines are asserted low independently to reset the motor controller after a fault condition.



10-5. Local Shutdown and Reset for Noninverting (Left) and Inverting Input Configuration (Right)

10.2.2.5 Global-Shutdown and Reset

When configured for inverting operation, the ISO5851 can be configured to shutdown automatically in the event of a fault condition by tying the $\overline{\text{FLT}}$ output to IN+. For high reliability drives, the open drain $\overline{\text{FLT}}$ outputs of multiple ISO5851 devices can be wired together forming a single, common fault bus for interfacing directly to the micro-controller. When any of the six gate drivers of a three-phase inverter detects a fault, the active low $\overline{\text{FLT}}$ output disables all six gate drivers simultaneously.

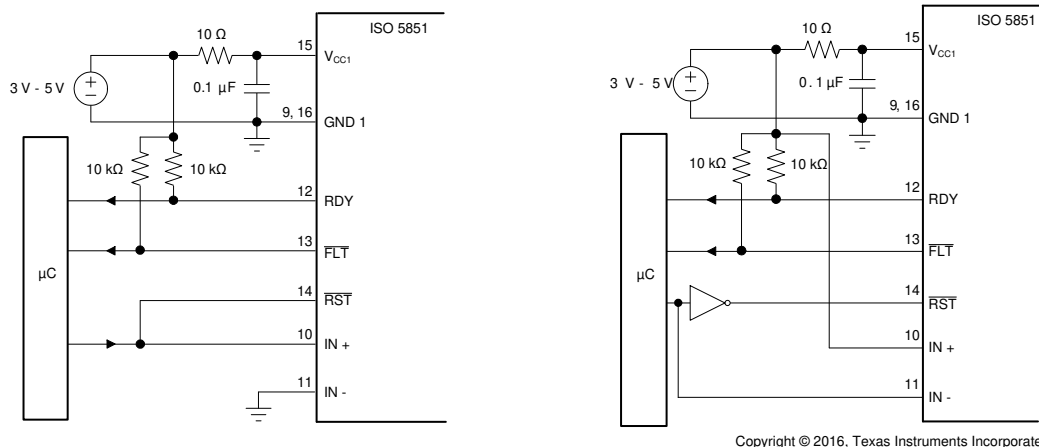


❏ 10-6. Global Shutdown with Inverting Input Configuration

10.2.2.6 Auto-Reset

In this case, the gate control signal at IN+ is also applied to the $\overline{\text{RST}}$ input to reset the fault latch every switching cycle. Incorrect $\overline{\text{RST}}$ makes output go low. A fault condition, however, the gate driver remains in the latched fault state until the gate control signal changes to the 'gate low' state and resets the fault latch.

If the gate control signal is a continuous PWM signal, the fault latch will always be reset before IN+ goes high again. This configuration protects the IGBT on a cycle by cycle basis and automatically resets before the next 'on' cycle.



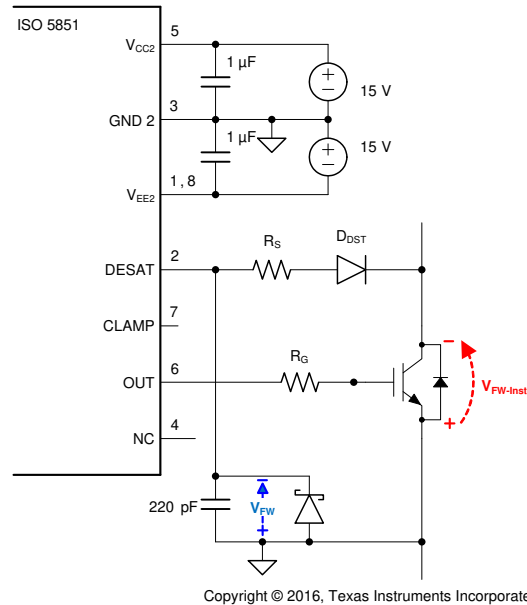
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10-7. Auto Reset for Non-inverting and Inverting Input Configuration

10.2.2.7 DESAT Pin Protection

Switching inductive loads causes large instantaneous forward voltage transients across the freewheeling diodes of IGBTs. These transients result in large negative voltage spikes on the DESAT pin which draw substantial current out of the device. To limit this current below damaging levels, a 100-Ω to 1-kΩ resistor is connected in series with the DESAT diode.

Further protection is possible through an optional Schottky diode, whose low forward voltage assures clamping of the DESAT input to GND2 potential at low voltage levels.



10-8. DESAT Pin Protection With Series Resistor and Schottky Diode

10.2.2.8 DESAT Diode and DESAT Threshold

The DESAT diode's function is to conduct forward current, allowing sensing of the IGBT's saturated collector-to-emitter voltage, $V_{(CESAT)}$, (when the IGBT is *on*) and to block high voltages (when the IGBT is *off*). During the short transition time when the IGBT is switching, there is commonly a high dV_{CE}/dt voltage ramp rate across the IGBT. This results in a charging current $I_{(CHARGE)} = C_{(D-DESAT)} \times dV_{CE}/dt$, charging the blanking capacitor. $C_{(D-DESAT)}$ is the diode capacitance at DESAT.

To minimize this current and avoid false DESAT triggering, fast switching diodes with low capacitance are recommended. As the diode capacitance builds a voltage divider with the blanking capacitor, large collector voltage transients appear at DESAT attenuated by the ratio of $1 + C_{(BLANK)} / C_{(D-DESAT)}$.

Because the sum of the DESAT diode forward-voltage and the IGBT collector-emitter voltage make up the voltage at the DESAT-pin, $V_F + V_{CE} = V_{(DESAT)}$, the V_{CE} level, which triggers a fault condition, can be modified by adding multiple DESAT diodes in series: $V_{CE-FAULT(TH)} = 9\text{ V} - n \times VF$ (where n is the number of DESAT diodes).

When using two diodes instead of one, diodes with half the required maximum reverse-voltage rating may be chosen.

10.2.2.9 Determining the Maximum Available, Dynamic Output Power, P_{OD-max}

The ISO5851 maximum allowed total power consumption of $P_D = 251\text{ mW}$ consists of the total input power, P_{ID} , the total output power, P_{OD} , and the output power under load, P_{OL} :

$$P_D = P_{ID} + P_{OD} + P_{OL} \quad (1)$$

With:

$$P_{ID} = V_{CC1-max} \times I_{CC1-max} = 5.5\text{ V} \times 4.5\text{ mA} = 24.75\text{ mW} \quad (2)$$

and:

$$P_{OD} = (V_{CC2} - V_{EE2}) \times I_{CC2-max} = (15\text{ V} - (-8\text{ V})) \times 6\text{ mA} = 138\text{ mW} \quad (3)$$

then:

$$P_{OL} = P_D - P_{ID} - P_{OD} = 251\text{ mW} - 24.75\text{ mW} - 138\text{ mW} = 88.25\text{ mW} \quad (4)$$

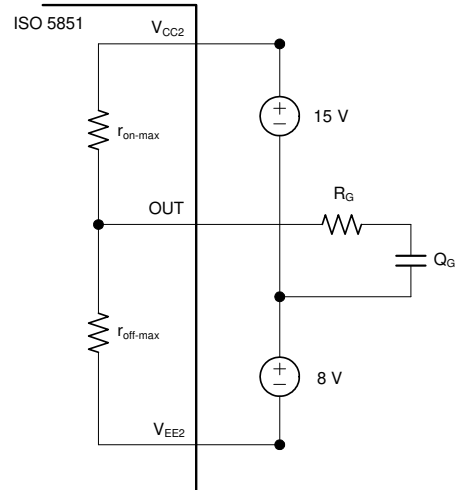
In comparison to P_{OL} , the actual dynamic output power under worst case condition, P_{OL-WC} , depends on a variety of parameters:

$$P_{OL-WC} = 0.5 \times f_{INP} \times Q_G \times (V_{CC2} - V_{EE2}) \times \left(\frac{r_{on-max}}{r_{on-max} + R_G} + \frac{r_{off-max}}{r_{off-max} + R_G} \right) \quad (5)$$

where

- f_{INP} = signal frequency at the control input IN+
- Q_G = power device gate charge
- V_{CC2} = positive output supply with respect to GND2
- V_{EE2} = negative output supply with respect to GND2
- r_{on-max} = worst case output resistance in the on-state: 4Ω
- $r_{off-max}$ = worst case output resistance in the off-state: 2.5Ω
- R_G = gate resistor

Once R_G is determined, 式 5 is to be used to verify whether $P_{OL-WC} < P_{OL}$. 図 10-9 shows a simplified output stage model for calculating P_{OL-WC} .



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10-9. Simplified Output Model for Calculating P_{OL-WC}
10.2.2.10 Example

This examples considers an IGBT drive with the following parameters:

$$I_{ON-PK} = 2 \text{ A}, Q_G = 650 \text{ nC}, f_{INP} = 20 \text{ kHz}, V_{CC2} = 15 \text{ V}, V_{EE2} = -8 \text{ V} \quad (6)$$

Applying the value of the gate resistor $R_G = 10 \Omega$.

Then, calculating the worst-case output power consumption as a function of R_G , using 式 5 r_{on-max} = worst case output resistance in the on-state: 4Ω , $r_{off-max}$ = worst case output resistance in the off-state: 2.5Ω , R_G = gate resistor yields

$$P_{OL-WC} = 0.5 \times 20 \text{ kHz} \times 650 \text{ nC} \times (15 \text{ V} - (-8 \text{ V})) \times \left(\frac{4 \Omega}{4 \Omega + 10 \Omega} + \frac{2.5 \Omega}{2.5 \Omega + 10 \Omega} \right) = 72.61 \text{ mW} \quad (7)$$

Because $P_{OL-WC} = 72.61 \text{ mW}$ is below the calculated maximum of $P_{OL} = 88.25 \text{ mW}$, the resistor value of $R_G = 10 \Omega$ is suitable for this application.

10.2.2.11 Higher Output Current Using an External Current Buffer

To increase the IGBT gate drive current, a non-inverting current buffer (such as the npn/pnp buffer shown in [Figure 10-10](#)) may be used. Inverting types are not compatible with the desaturation fault protection circuitry and must be avoided. The MJD44H11/MJD45H11 pair is appropriate for currents up to 8 A, the D44VH10/ D45VH10 pair for up to 15 A maximum.

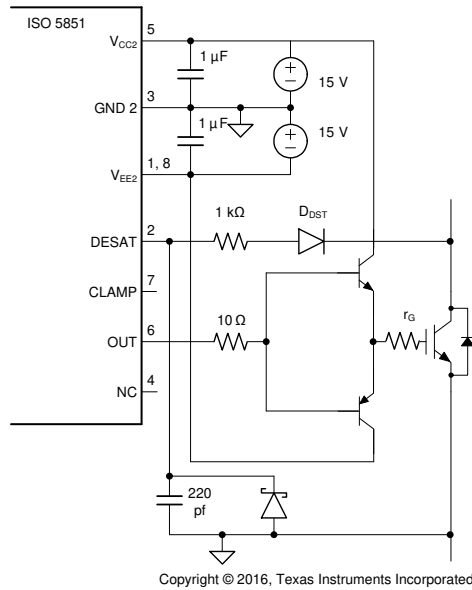
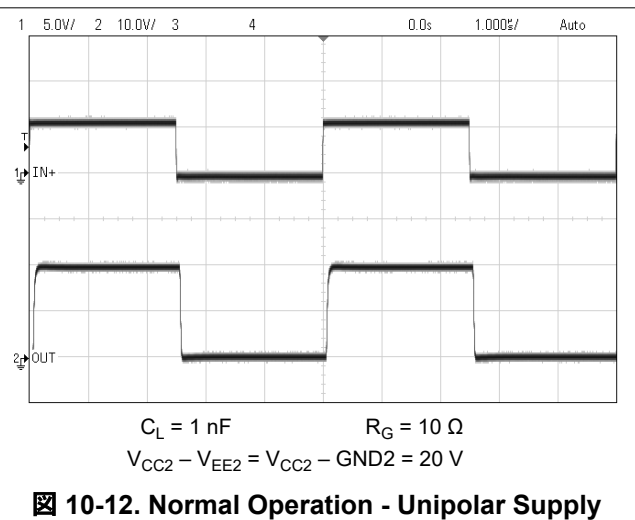
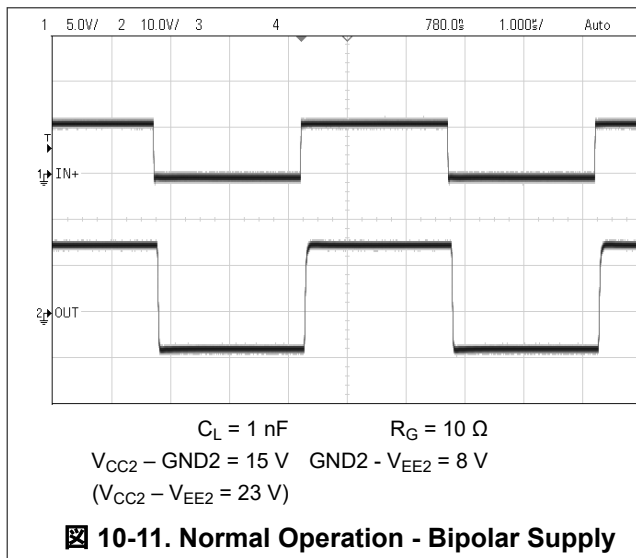


Figure 10-10. Current Buffer for Increased Drive Current

10.2.3 Application Curves



11 Power Supply Recommendations

To help ensure reliable operation at all data rates and supply voltages, a 0.1- μ F bypass capacitor is recommended at input supply pin V_{CC1} and 1- μ F bypass capacitor is recommended at output supply pin V_{CC2} . The capacitors should be placed as close to the supply pins as possible. The recommended placement of the capacitors is 2-mm maximum from the input and output power supply pin (V_{CC1} and V_{CC2}).

12 Layout

12.1 Layout Guidelines

A minimum of four layers is required to accomplish a low EMI PCB design (see [Figure 12-1](#)). Layer stacking should be in the following order (top-to-bottom): high-current or sensitive signal layer, ground plane, power plane and low-frequency signal layer.

- Routing the high-current or sensitive traces on the top layer avoids the use of vias (and the introduction of their inductances) and allows for clean interconnects between the gate driver and the microcontroller and power transistors. Gate driver control input, Gate driver output OUT and DESAT should be routed in the top layer.
- Placing a solid ground plane next to the sensitive signal layer provides an excellent low-inductance path for the return current flow. On the driver side, use GND2 as the ground plane.
- Placing the power plane next to the ground plane creates additional high-frequency bypass capacitance of approximately 100 pF/inch². On the gate-driver V_{EE2} and V_{CC2} can be used as power planes. They can share the same layer on the PCB as long as they are not connected together.
- Routing the slower speed control signals on the bottom layer allows for greater flexibility as these signal links usually have margin to tolerate discontinuities such as vias.

For detailed layout recommendations, see the [Digital Isolator Design Guide](#) (SLLA284).

12.2 Layout Example

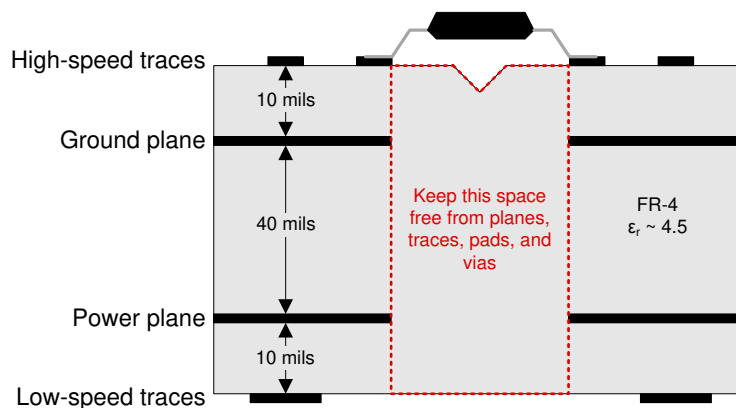


Figure 12-1. Recommended Layer Stack

12.3 PCB Material

For digital circuit boards operating at less than 150 Mbps, (or rise and fall times greater than 1 ns), and trace lengths of up to 10 inches, use standard FR-4 UL94V-0 printed circuit board. This PCB is preferred over cheaper alternatives because of lower dielectric losses at high frequencies, less moisture absorption, greater strength and stiffness, and the self-extinguishing flammability-characteristics.

13 Device and Documentation Support

13.1 Device Support

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13.2 Documentation Support

13.2.1 Related Documentation

For related documentation see the following:

- [ISO5851 Evaluation Module \(EVM\) User's Guide](#)
- [Digital Isolator Design Guide](#)
- [Isolation Glossary](#)

13.3 ドキュメントの更新通知を受け取る方法

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14 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package Pins	Package qty Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
ISO5851DW	Obsolete	Production	SOIC (DW) 16	-	-	Call TI	Call TI	-40 to 125	ISO5851
ISO5851DWR	Active	Production	SOIC (DW) 16	2000 LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	ISO5851
ISO5851DWR.A	Active	Production	SOIC (DW) 16	2000 LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 125	ISO5851
ISO5851DWR.B	Active	Production	SOIC (DW) 16	2000 LARGE T&R	-	Call TI	Call TI	-40 to 125	

⁽¹⁾ **Status:** For more details on status, see our [product life cycle](#).

⁽²⁾ **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

⁽³⁾ **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

⁽⁴⁾ **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

⁽⁵⁾ **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

⁽⁶⁾ **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "-" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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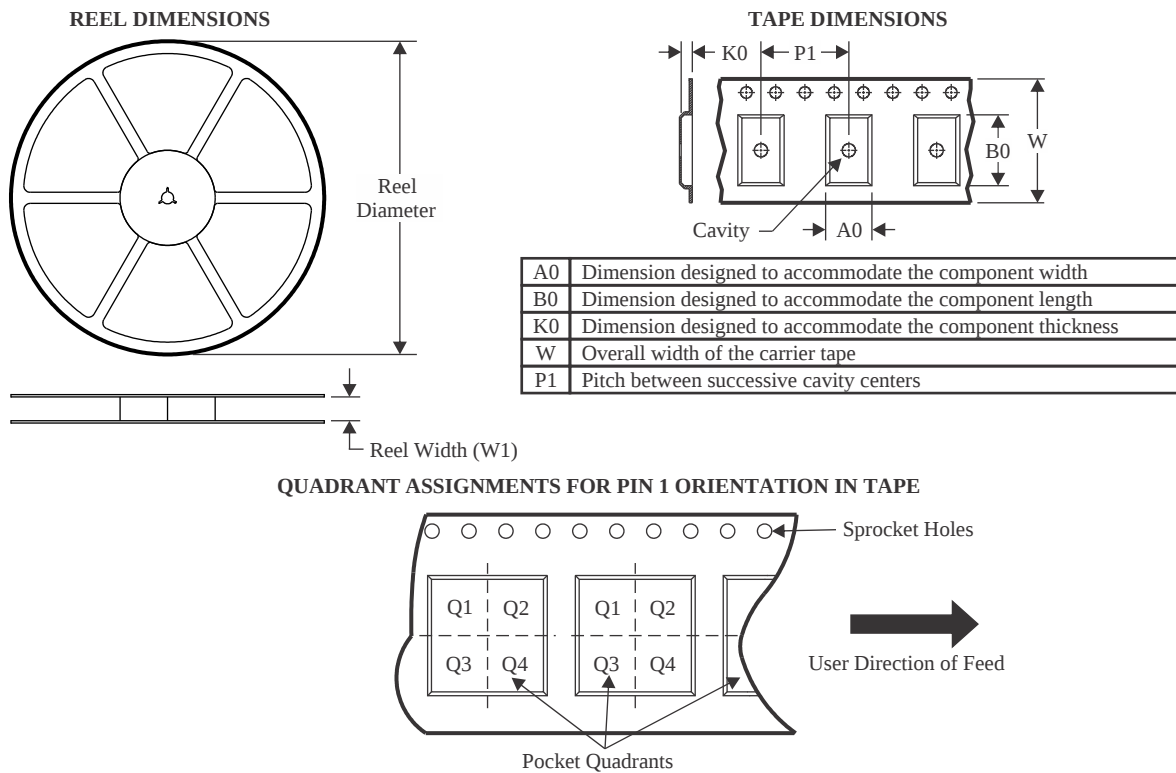
OTHER QUALIFIED VERSIONS OF ISO5851 :

- Automotive : [ISO5851-Q1](#)

NOTE: Qualified Version Definitions:

- Automotive - Q100 devices qualified for high-reliability automotive applications targeting zero defects

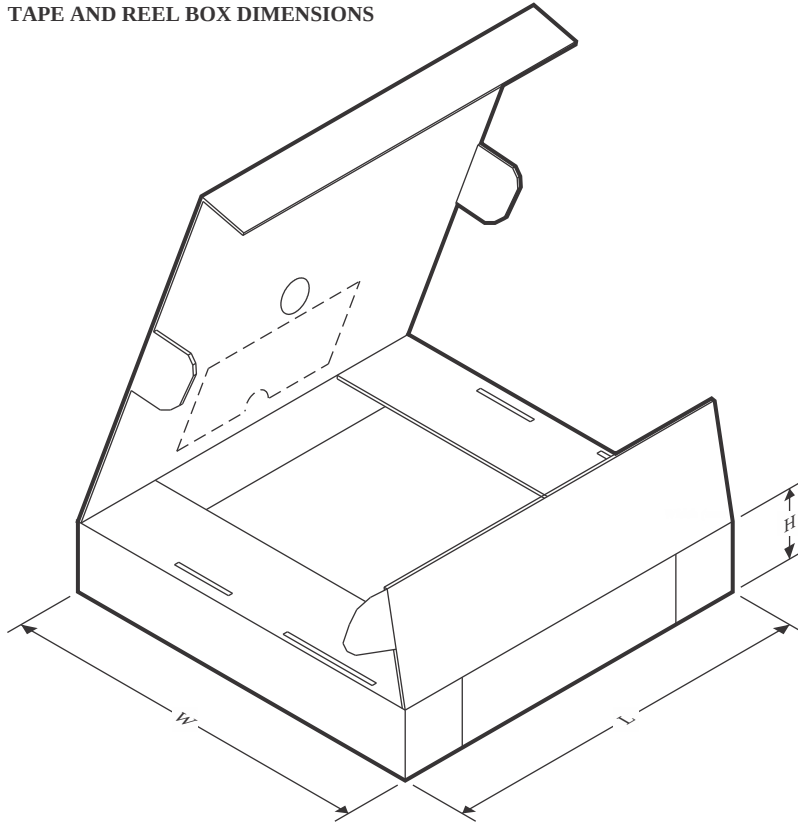
TAPE AND REEL INFORMATION



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
ISO5851DWR	SOIC	DW	16	2000	330.0	16.4	10.75	10.7	2.7	12.0	16.0	Q1

TAPE AND REEL BOX DIMENSIONS



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
ISO5851DWR	SOIC	DW	16	2000	353.0	353.0	32.0

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