









INA851

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INA851 高精度、低ノイズ、完全差動出力計測アンプ、減衰ゲインおよび出力 クランプ付き

1 特長

Texas

INSTRUMENTS

- 外付け抵抗を使用してG=0.2~10,000の範囲でゲ インをプログラム可能
- 完全差動出力、クランプ機能内蔵
- 低いオフセット電圧:10µV (標準値)、35µV (最大値)
- 小さいオフセット・ドリフト:0.1µV/℃ (標準値)、0.3µV/ ℃(最大値)
- 低い入力バイアス電流:5nA (標準値)
- 入力段ノイズ:3.2nV/√Hz、0.8pA/√Hz
- 広い帯域幅:G=0.2 で 22MHz、 G = 1 で 15MHz
- 同相除去:G=10で106dB(最小値)、100≤G≤ 1000 で 120dB (最小値)
- 電源除去:110dB(最小值、G=1)
- 消費電流:6mA (標準値)
- 高低の電源電圧に対して ±40V までの入力過電圧保 ٠ 護機能
- 電源電圧範囲:
 - 単一電源:8V~36V
 - デュアル電源:±4V~±18V
- 仕様温度範囲:-40℃~+125℃ 超小型パッケージ:16 ピン VQFN

2 アプリケーション

- アナログ入力モジュール
- 流量トランスミッタ
- LCD テスト
- 心電図 (ECG)
- 外科用機器
- オシロスコープ (DSO)
- 重量計
- 半導体試験装置

3 説明

INA851 は、業界初の完全差動出力を備えた高精度計測 アンプです。このデバイスは、完全差動入力を持つ最新の 高性能 A/D コンバータ (ADC) の入力駆動用に最適化さ れています。INA851 は、非常に広い範囲の単一電源ま たはデュアル電源電圧で動作します。出力段のゲインは、 2本のピンを短絡させると 0.2 に設定され、フローティング にすると1に設定されます。1個の外付け抵抗により、1~ 10.000の範囲で任意の入力段ゲインを設定できます。

INA851 は、スーパーベータ入力トランジスタを採用したこ とにより、同じクラスの他のアンプと比較すると、非常に低 い入力バイアス電流および入力換算電流ノイズを実現し ています。最新の製造プロセスにより、非常に低い電圧ノ イズ、入力オフセット電圧、オフセット電圧ドリフトが得られ ます。追加の回路により、電源電圧を最大 ±40V 上回る過 電圧からデバイス入力を保護します。デバイス出力にはク ランプ回路が内蔵され、オーバードライブによる損傷から ADC または下流のデバイスを保護します。

このデバイスは、最小 8V から最大 36V までの単一電 源、または ±4V から ±18V までのデュアル電源で動作す るように設計されています。

パッケージ棒却

	ハンフ ノ 同報	
部品番号	パッケージ ⁽¹⁾	本体サイズ (公称)
INA851	RGT (VQFN、16)	3.00mm × 3.00mm

利用可能なパッケージについては、データシートの末尾にあるパ (1)ッケージ・オプションについての付録を参照してください。



INA851 の ADC ドライバ・アプリケーション

英語版の TI 製品についての情報を翻訳したこの資料は、製品の概要を確認する目的で便宜的に提供しているものです。該当する正式な英語版の最新情報は、 🐼 www.ti.com で閲覧でき、その内容が常に優先されます。 TI では翻訳の正確性および妥当性につきましては一切保証いたしません。 実際の設計などの前には、必ず 最新版の英語版をご参照くださいますようお願いいたします。



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4 Revision History 資料番号末尾の英字は改訂を表しています。その改訂履歴は英語版に準じています。

CI	nanges from Revision * (March 2	2022) to Revision A (Oct	ober 2022)	Page
•	INA851を事前情報 (プレビュー)カ	から量産データ (アクティブ)	に変更	1



5 Related Products

DEVICE	DESCRIPTION	GAIN EQUATION	RG PINS AT PIN
INA159	G = 0.2 V differential amplifier for \pm 10-V to 3-V and 5-V conversion	G = 0.2 V/V	N/A
INA818	35-µV offset, 0.4-µV/°C V_{OS} drift, 8-nV/ \sqrt{Hz} noise, low-power, precision instrumentation amplifier	G = 1 + 50 kΩ / RG	1, 8
INA819	35-µV offset, 0.4-µV/°C V_{OS} drift, 8-nV/ \sqrt{Hz} noise, low-power, precision instrumentation amplifier	G = 1 + 50 kΩ / RG	2, 3
INA821	35-µV offset, 0.4-µV/°C V_{OS} drift, 7-nV/ \sqrt{Hz} noise, high-bandwidth, precision instrumentation amplifier	G = 1 + 49.4 kΩ / RG	2, 3
INA828	50-µV offset, 0.5-µV/°C V_{OS} drift, 7-nV/ \sqrt{Hz} noise, low-power, precision instrumentation amplifier	G = 1 + 50 kΩ / RG	1, 8
INA333	25-µV V_{OS}, 0.1-µV/°C V_{OS} drift, 1.8-V to 5-V, RRO, 50-µA $I_Q,$ chopper-stabilized INA	G = 1 + 100 kΩ / RG	1, 8
INA848	Ultra-low-noise (1.5-nV/ $\sqrt{\text{Hz}}),$ high-bandwidth instrumentation amplifier with fixed gain of 2000	G = 2000 V/V	N/A
INA849	Ultra-low-noise (1-nV/ \sqrt{Hz}), high-bandwidth instrumentation amplifier	G = 1 + 6 kΩ / RG	2, 3
PGA280	20-mV to ±10-V programmable gain IA with 3-V or 5-V differential output; analog supply up to ±18 V	Digital programmable	N/A
PGA281	Precision, zero-drift, programmable gain IA with differential output; binary gain steps from 1/8 V/V to 128 V/V	Digital programmable	N/A
PGA112	Precision programmable gain op amp with SPI	Digital programmable	N/A



6 Pin Configuration and Functions



図 6-1. RGT (16-Pin VQFN) Package, Top View

表 6-1. Pin Functions

PIN		TYPE	DESCRIPTION	
NAME	NO.	ITPE	DESCRIPTION	
FDA_IN-	15	Input	Connection to output driver summing node.	
FDA_IN+	6	Input	Connection to output driver summing node.	
G02–	9	Input	Connection to gain network. Short to OUT– for output stage gain G _{OUT} of 0.2 V/V.	
G02+	12	Input	Connection to gain network. Short to OUT+ for output stage gain G_{OUT} of 0.2 V/V.	
IN–	1	Input	Negative (inverting) input.	
IN+	4	Input	Positive (noninverting) input.	
NC	8	_	No connect	
OUT-	10	Output	Negative Output	
OUT+	11	Output	Positive Output	
RG	2,3	_	Gain setting pin. Place a gain resistor between pin 2 and pin 3.	
VCLAMP-	5	Input	Level set for output clamp value. Connect either to an external supply that is at least 1.5 V above VS– or connect to VS– if clamping function is not required.	
VCLAMP+	16	Input	Level set for output clamp value. Connect either to an external supply that is at least 1.5 V below VS+ or connect to VS+ if clamping function is not required.	
VOCM	13	Input	Level set for output common mode value.	
VS-	7	Power	Negative supply	
VS+	14	Power	Positive supply	
Thermal Pad	Thermal pad		The thermal pad must be soldered to the printed-circuit board (PCB). Connect thermal pad to a plane or large copper pour electrically connected to the most negative supply or VS–.	



7 Specifications

7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)⁽¹⁾

			MIN	MAX	UNIT	
Vs	Supply voltage on VS+, VS- pins; $V_S = (V_{S+}) - (V_{S+})$	/ _{S-})	0	40	V	
V _{IN}	Input voltage on IN+, IN- pins		(V _{S-}) – 40	(V _{S+}) + 40		
VDIEF	Differential input voltage, $V_{DIFF} = (V_{IN+}) - (V_{IN-})$ Output voltage on OUT+, OUT- pins	G _{IN} = 1 V/V, continuous	$(-V_{\rm S}) - 40$	V _S + 40	V	
▼ DIFF		G _{IN} > 1 V/V ⁽³⁾	$(-V_{\rm S}) - 40$	V _S + 40		
	Output voltage on OUT+, OUT- pins		(V _S _) – 0.5	(V _{S+}) + 0.5	V	
	FDA_IN+, FDA_IN-, G02+, G02-, VCLAMP+, VCLAMP-, VOCM pins voltage		(V _S _) – 0.5	(V _{S+}) + 0.5	V	
	Output short-circuit ⁽²⁾		Continuc	bus		
T _A	Operating temperature		-40	125	°C	
TJ	Junction temperature			175	°C	
T _{stg}	Storage temperature		-65	150	°C	

(1) Operation outside the Absolute Maximum Ratings may cause permanent device damage. Absolute Maximum Ratings do not imply functional operation of the device at these or any other conditions beyond those listed under Recommended Operating Conditions. If used outside the Recommended Operating Conditions but within the Absolute Maximum Ratings, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.

(2) Short-circuit to V_S / 2.

(3) Keep operation below 1% duty cycle of device lifecycle.

7.2 ESD Ratings

			VALUE	UNIT	
V	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	±2500	V	
V(ESD)	Electrostatic discharge	Charged-device model (CDM), per ANSI/ESDA/JEDEC JS-002 ⁽²⁾	±1000	- V	

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

			MIN	MAX	UNIT	
Vs	Supply voltage	Single supply, $V_S = (V_{S+})$, GND = (V_{S-})	8	36	V	
	Dual supply, $V_S = (V_{S+}) - (V_{S-})$		±4	±18	v	
V _{IN}	Input voltage on IN+, IN– pins		–V _S	Vs	V	
V _{DIFF}	Differential input voltage,	G _{IN} = 1 V/V	–V _S	Vs	V	
	$V_{DIFF} = (V_{IN+}) - (V_{IN-})$	G _{IN} > 1 V/V ⁽¹⁾	$-1 - (V_S) / G_{IN}$	1 + (V _S) / G _{IN}	v	
T _A	A Specified temperature		-40	125	°C	

(1) See also INA851 Calculator Tool.



7.4 Thermal Information

		INA851	
	THERMAL METRIC ⁽¹⁾	RGT (VQFN)	UNIT
		16 PINS	
R _{0JA}	Junction-to-ambient thermal resistance	47.3	°C/W
R _{0JC(top)}	Junction-to-case (top) thermal resistance	53.2	°C/W
R _{θJB}	Junction-to-board thermal resistance	22.1	°C/W
Ψ _{JT}	Junction-to-top characterization parameter	1.4	°C/W
Ψ _{JB}	Junction-to-board characterization parameter	22.1	°C/W
R _{0JC(bot)}	Junction-to-case (bottom) thermal resistance	7.8	°C/W

(1) For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.

7.5 Electrical Characteristics

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
INPUT							
V	Input stage offset				±10	±35	
VOSI	voltage ⁽¹⁾	$T_A = -40^{\circ}C \text{ to } +125^{\circ}C^{(4)}$				±65	μv
	Input stage offset voltage drift ⁽²⁾	$T_A = -40^{\circ}C$ to $+125^{\circ}C^{(4)}$	$r_A = -40^{\circ}$ C to +125°C ⁽⁴⁾		±0.1	±0.3	μV/°C
V	Output stage offset	G = 0.2			±150	±1150	
VOSO	voltage ⁽¹⁾	G = 1			±150	±650	μv
	Output stage offset	$T = 40^{\circ}C t_{0} \pm 125^{\circ}C(4)$	G = 0.2		±5	±15	
	voltage drift ⁽²⁾	$T_{A} = -40 C 10 + 125 C^{10}$	G = 1		±5	±15	μν/ Ο
	Power-supply rejection ratio	ower-supply rejection $\pm 4 \text{ V} \le \text{V}_{\text{S}} \le \pm 18 \text{ V}, \text{ RTI}$	G = 0.2	100	120		
			G = 1	110	126		dB
PSRR			G _{IN} = 10	120	140		
			G _{IN} = 100	126	140		
			G _{IN} = 1000	130	140		
z _{id}	Differential impedance				1 100		pF GΩ
z _{ic}	Common-mode impedance				7 100		pF∥GΩ
V _{IN}	Input voltage ^{(4) (5)}	See also INA851 Calculator Tool		(V _{S-}) + 2.5		$(V_{S^+}) - 2.5$	V
	Protected input voltage ⁽⁸⁾			(V _{S-}) – 40		(V _{S+}) + 40	V
	Input current in overvoltage mode ⁽⁹⁾	$(V_{S-}) - 40 V \le V_{IN} \le (V_{S+}) + 40 V^{(3)}$			16		mA
			G = 0.2	76	90		dB
			G = 1	86	96		
CMRR	Common-mode rejection	At dc to 60 Hz, RTI, $V_{CM} = (V_S) + 2.5 V$ to $(V_{SI}) - 2.5 V$	G _{IN} = 10	106	116		
		- CIVI (75-7 2.0 1.0 (1.3+7) 2.0 V	G _{IN} = 100	120	132		
			G _{IN} = 1000	120	134		
				-			



7.5 Electrical Characteristics (continued)

	PARAMETER	TEST COND	DITIONS	MIN	TYP MAX	UNIT	
BIAS CU	RRENT			•			
	Input biog ourrent				5 15		
IB	Input bias current	$T_A = -40^{\circ}C \text{ to } +125^{\circ}C^{(4)}$			18	nA	
	Input bias current drift	T _A = -40°C to +125°C			25	pA/°C	
	Input offect oursent				0.5 5.5		
IOS	Input onset current	$T_A = -40^{\circ}C \text{ to } +125^{\circ}C^{(4)}$			6		
	Input offset current drift	$T_A = -40^{\circ}C$ to $+125^{\circ}C$			5	pA/°C	
NOISE V	OLTAGE						
e _{NI}	Input stage voltage noise density	f = 1 kHz, G = 1000			3.2	nV/√Hz	
	Input stage voltage noise	f _B = 0.1 Hz to 10 Hz, G = 1000			0.1	μV _{PP}	
			G = 0.2		83		
eno.	Output stage voltage	f = 1 kHz	G = 1		52	nV/√Hz	
	noise density ⁽⁷⁾		G = 1; G _{IN} = 5, G _{OUT} = 0.2		12		
	Output stage voltage		G = 0.2		5.0	μV _{PP}	
	noise ⁽⁷⁾	$T_{\rm B} = 0.1$ Hz to 10 Hz	G = 1		2.8	μV _{PP}	
	Current noise density	= 1 kHz, G _{IN} = 1000			0.8	pA/√Hz	
In	Current noise	_B = 0.1 Hz to 10 Hz, G = 100			37	рА _{РР}	
GAIN				•			
	Gain equation	$G = G_{IN} \times G_{OUT}$	$G = G_{IN} \times G_{OUT}$		$(1 + (6 k\Omega / R_G)) \times (0.2 \text{ or } 1)$		
G	Cain	G _{OUT} = 0.2		0.2	2000		
G	Gain	G _{OUT} = 1		1	10000	V	
		G = 0.2, V _O = ±2 V			±0.1		
GE	Gain error	G = 1, V _O = ±10 V			±0.02	%	
		$G_{IN} \ge 10, V_O = \pm 10 V$	_		±0.2		
			G = 0.2		±5		
	Gain drift ⁽⁶⁾	$T_A = -40^{\circ}C$ to $+125^{\circ}C^{(4)}$	G = 1		±5	ppm/°C	
					±35		
	Gain nonlinearity	G = 0.2, V_0 = -2 V to +2 V			±5	ppm	
		G = 1, V_0 = -10 V to +10 V			±5	PP	
OUTPUT	1	1	1	1			
N.		lour = 10 mA	No output clamping ($V_{CLAMP+} = V_{S+}$, $V_{CLAMP-} = V_{S-}$)	(V _{S-}) + 1.4	(V _{S+}) – 1.4	V	
v0	V_0 Output voltage swing $T_A = -40^{\circ}C$ to +125°C		Output clamping enabled ($V_{CLAMP+} = V_{S+} - 1.5 V$, $V_{CLAMP-} = V_{S-} + 1.5 V$)	(V _{CLAMP} _) - 0.1	(V _{CLAMP+}) + 0.1	v	
CL	Load capacitance	Stable operation for differential load	1		100	pF	
zo	Closed-loop output impedance	f = 1 MHz			0.9	Ω	
I _{SC}	Short-circuit current	$T_A = -40^{\circ}$ C to 125°C, continuous to	0 V _S / 2	±37		mA	



7.5 Electrical Characteristics (continued)

at T_A = 25°C, V_S = ±15 V, V_{ICM} = V_{OCM} = midsupply, V_{CLAMP+} = V_{S+}, V_{CLAMP-} = V_{S-}, G = G_{IN} = G_{OUT} = 1 V/V, and R_L = 10 k Ω (unless otherwise noted)

	PARAMETER	TEST COND	ITIONS	MIN TY	'P MAX	UNIT	
FREQUE	NCY RESPONSE					•	
		G = 0.2		22			
		G = 1, G _{IN} = 5, G _{OUT} = 0.2	2	22	1		
DW	Dondwidth 2 dD	G = 1			15		
DVV	Bandwidth, -3 dB	G _{IN} = 10			11		
		G _{IN} = 100		5	1		
		G _{IN} = 1000		0	.8	1	
SR	Slew rate	G = 1, V _O = ±10 V		:	37	V/µs	
			G = 0.2, V _{STEP} = 2 V	0.2	24		
		0.04%	G = 1, V _{STEP} = 10 V	0.2	24	1	
		0.01%	G _{IN} = 10, 100, V _{STEP} = 10 V	0	.5	μs	
			G _{IN} = 1000, V _{STEP} = 10 V 1.7				
t _S	Settling time		G = 0.2, V _{STEP} = 2 V	0.5	55		
		0.001%	G = 1, V _{STEP} = 10 V	0.5	55		
			G _{IN} = 10,100, V _{STEP} = 10 V	2	.1	μs	
			G _{IN} = 1000, V _{STEP} = 10 V	2	.5		
	Total harmonic distortion		G = 0.2, V _O = 2 V _{PP}	-10)9	dB	
I HD+N	plus noise	Differential input, f = 10 kHz	G = 1, V _O = 10 V _{PP}	-1	10	dB	
	Second-order harmonic		G = 0.2, V _O = 2 V _{PP}	-1:	31		
HD2	distortion	Differential input, f = 10 kHz	G = 1, V _O = 10 V _{PP}	-12	28	dB	
	Third-order harmonic		G = 0.2, V _O = 2 V _{PP}	-1	19		
HD3	distortion	Differential input, f = 10 kHz	G = 1, V _O = 10 V _{PP}	-12	21	ar ar	
OUTPUT	COMMON-MODE VOLTAG	E (V _{OCM}) CONTROL					
			No output clamping	(V _{S-}) + 2.5	(V _{S+}) – 2.5		
	V _{OCM} Input voltage	$T_A = -40^{\circ}C$ to $+125^{\circ}C$	Output clamp enabled	(V _{CLAMP-}) + 1	(V _{CLAMP+}) – 1	V	
	Small-signal bandwidth from V _{OCM} pin	V _{OCM} = 100 mV _{PP}		:	30	MHz	
	Large-signal bandwidth from V _{OCM} pin	V _{OCM} = 0.5-V step			1 7	MHz	
	Slew rate from V _{OCM} pin	V _{OCM} = 0.5-V step	V _{OCM} = 0.5-V step		37	V/µs	
	DC output balance	V_{OCM} fixed midsupply (V _O = ±1 V)			70	dB	
	Input impedance V _{VOCM} pin			250	1	kΩ∥pF	
	V _{OCM} offset from mid- supply	V _{OCM} pin floating		:	±2 ±6	mV	
	V _{OCM} common-mode				±2 ±6		
	offset voltage	$v_{OCM} = v_{ICM}, v_O = 0 V$	$T_A = -40^{\circ}C$ to $+125^{\circ}C$		±10	∣ m∨	
	V _{OCM} common-mode offset voltage drift	$V_{OCM} = V_{ICM}, V_O = 0 V, T_A = -40^{\circ}C$	to +125°C	±ź	20 ±60	µV/°C	



7.5 Electrical Characteristics (continued)

at $T_A = 25^{\circ}$ C, $V_S = \pm 15$ V, $V_{ICM} = V_{OCM}$ = midsupply, $V_{CLAMP+} = V_{S+}$, $V_{CLAMP-} = V_{S-}$, $G = G_{IN} = G_{OUT} = 1$ V/V, and $R_L = 10$ k Ω (unless otherwise noted)

	PARAMETER	TEST CONDI	TIONS	MIN	TYP	MAX	UNIT
OUTPUT	CLAMPING			•			
V	Begitive clamp voltage ⁽¹⁰⁾	$T = 40^{\circ}C t_{0} \pm 125^{\circ}C$	No output clamping		V _{S+}		V
V CLAMP+		T _A = -40 C 10 +123 C	Output clamp enabled			V _{S+} – 1.5	v
V	Negative clamp	$T = 40^{\circ}C t_{0} \pm 125^{\circ}C$	No output clamping		V _{S-}		V
V CLAMP-	voltage ⁽¹⁰⁾	T _A = -40 C 10 +123 C	Output clamp enabled	V _{S-} + 1.5			v
ΔV_{CLAMP}	Clamp voltage ⁽¹⁰⁾	$\Delta V_{CLAMP} = (V_{CLAMP+}) - (V_{CLAMP-})$		3			V
	Power-supply rejection ratio from V_{CLAMP} to V_{O} ⁽³⁾				120		dB
	Fail-safe current V _{CLAMP+}	V _{S+} = V _{S-} = 0 V, V _{CLAMP+} = 10 V			2		mA
I _{CLAMP+}	Positive clamp current	$V_{CLAMP+} \le V_{S+} - 1.5 V$		-80	-60		μΑ
I _{CLAMP-}	Negative clamp current	V _{CLAMP} _ ≥ V _S _ + 1.5 V			60	80	μΑ
POWER	SUPPLY	·		•			
1.		X = 0 X			6	7	m۸
^I Q			$T_{A} = -40^{\circ}C \text{ to } +125^{\circ}C$			9	mA

(1) Offset voltages are uncorrelated. Total offset voltage, referred-to-input (RTI): V_{OS} = √[V_{OSI}² + (V_{OSO(Gout1 or Gout0.2)} / G_{IN})²]. See more details on *Offset Voltage* section.

(2) Offset drifts are uncorrelated. Offset drift, referred-to-input (RTI): $\Delta V_{OS(RTI)} = \sqrt{[\Delta V_{OSI}^2 + (\Delta V_{OSO} / G_{IN})^2]}$.

(3) Specified by design.

(4) Specified by characterization.

(5) Input voltage range of the instrumentation amplifier input stage. The valid input range depends on the common-mode voltage, differential voltage, gain, and V_{OCM}. See also the *Input Common-Mode Range* section.

(6) The values specified for G > 1 do not include the effects of the external gain-setting resistor, R_G .

(7) e_{NO} refers to output stage noise referred to the input of the FDA. See also the *Noise Equivalent Model* section.

(8) See also the Input Protection section.

(9) See also the *Typical Characteristics* section.

(10) See also the Output Clamping section.



7.6 Typical Characteristics

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•



7.6 Typical Characteristics

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at $T_A = 25^{\circ}$ C, $V_S = \pm 15$ V, $V_{ICM} = V_{OCM}$ = midsupply, $V_{CLAMP+} = V_{S+}$, $V_{CLAMP-} = V_{S-}$, $G = G_{IN} = G_{OUT} = 1$ V/V, and $R_L = 10$ k Ω (unless otherwise noted)



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at $T_A = 25^{\circ}$ C, $V_S = \pm 15$ V, $V_{ICM} = V_{OCM}$ = midsupply, $V_{CLAMP+} = V_{S+}$, $V_{CLAMP-} = V_{S-}$, $G = G_{IN} = G_{OUT} = 1$ V/V, and $R_L = 10$ k Ω (unless otherwise noted)





at $T_A = 25^{\circ}$ C, $V_S = \pm 15$ V, $V_{ICM} = V_{OCM}$ = midsupply, $V_{CLAMP+} = V_{S+}$, $V_{CLAMP-} = V_{S-}$, $G = G_{IN} = G_{OUT} = 1$ V/V, and $R_L = 10$ k Ω (unless otherwise noted)



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8 Detailed Description

8.1 Overview

The INA851 is a monolithic, precision instrumentation amplifier that incorporates a current-feedback input stage and a four-resistor, fully differential amplifier output stage. The schematic in \boxtimes 8-1 shows how the differential input voltage is buffered by Q₁ and Q₂, and is forced across R_G, which causes a signal current to flow through R_G, R₁, and R₂. The fully differential amplifier, A₃, removes the common-mode component of the input signal and refers the output signal to the VOCM pin. The V_{BE} and voltage drop across R₁ and R₂ produce output voltages on A₁ and A₂ that are approximately 0.8 V less than the input voltages.



8-1. Detailed Schematic



8.2 Functional Block Diagram



8.3 Feature Description

8.3.1 Adjustable Gain Setting

 \boxtimes 8-2 shows that the INA851 input-stage gain is set by a single external resistor (R_G) connected between the RG pins. The gain of the output stage can be set to a unity gain of 1 V/V by floating the G02+ and G02– pins, or to an attenuating gain of 0.2 V/V by shorting those pins to the respective OUT+ and OUT– pins.





If the output stage is in the unity gain configuration, the value of R_G is selected according to the following equation:

$$G = \left(1 + \frac{6k\Omega}{R_G}\right) \tag{1}$$

When OUT+ is shorted to G02+ (pin 11 to pin 12) and OUT– is shorted to G02– (pin 9 to pin 10) so that the output stage is in the attenuating configuration, the gain equation becomes:

$$G = 0.2 \times \left(1 + \frac{6k\Omega}{R_G}\right) \tag{2}$$

 \pm 8-1 lists several commonly used gains and resistor values, as well as the additional gain error that is contributed by the gain resistors. The 6-kΩ term in the gain equation is a result of the sum of the two internal 3-kΩ feedback resistors. These on-chip resistors are laser-trimmed to accurate absolute values. The accuracy and temperature coefficients of these resistors are included in the gain accuracy and drift specifications of the

INA851. The 5-k Ω and 1.25-k Ω resistors used in the output stage are ratiometrically matched to achieve stable 1-V/V and 0.2-V/V gain terms; although, the resistor values can shift up to 15%, depending on production.

	20 11 0011111			
DESIRED GAIN (V/V)	R _G (Ω)	NEAREST 1% R _G (Ω)	CALCULATED GAIN (V/V)	CONTRIBUTED GAIN ERROR (%)
0.2	NC, short OUT+ to G02+ and OUT– to G02–	NC	0.200	N/A
0.5	4 k, short OUT+ to G02+ and OUT– to G02–	4.02 k	0.499	0.30
1	NC	NC	1.000	N/A
2	6 k	5.97 k	2.005	-0.25
5	1.5 k	1.5 k	5.000	0.00
10	666.67	665	10.023	-0.23
20	315.79	316	19.987	0.06
50	122.45	124	49.387	1.23
100	60.61	60.4	100.338	-0.34
200	30.15	30.1	200.336	-0.17
500	12.02	12.1	496.868	0.63
1000	6.01	6.04	994.377	0.56
10000	600 m	604 m	9934.775	0.65

表 8-1. Commonly Used Gains and Resistor Values

As shown in 🗵 8-2 and explained in more detail in 2223 > 9.4, make sure to connect low-ESR, 0.1-µF ceramic bypass capacitors between each supply pin and ground, and to place these capacitors as close as possible to the device pins.

8.3.1.1 Gain Drift

The stability and temperature drift of external gain setting resistor R_G also affects gain. The contribution of R_G to gain accuracy and drift is determined from \vec{x} 1. The best gain drift of 5 ppm/°C (maximum) is achieved when the INA851 uses G = 1 in the input stage, without R_G connected. In this case, gain drift is limited by the mismatch of the temperature coefficient of the integrated resistors in fully differential amplifier A_3 . When the output stage is in attenuating gain mode (OUT- shorted to G02- and OUT+ shorted to G02+), both the 1.25-k Ω and the 5-k Ω resistors contribute mismatch, as do the traces between the G02x and OUTx pins. Only the 5-k Ω resistors contribute mismatch when the output stage is in unity gain mode (with G02- and G02+ floating).

At input stage gains greater than 1, gain drift increases as a result of the individual drift of the 3-k Ω resistors in the feedback of A₁ and A₂, relative to the drift of external gain resistor R_G. The low temperature coefficient of the internal feedback resistors improves the overall temperature stability of applications using input-stage gains greater than 1 V/V over alternate solutions. The low resistor values required for high gain make wiring resistance an important consideration. Sockets add to the wiring resistance and contribute additional gain error (such as a possible unstable gain error) at gains of approximately 20 or greater. To maintain stability, avoid parasitic capacitance of more than a few picofarads at the R_G connections. Careful matching of any parasitics on the R_G pins maintains optimal CMRR over frequency.



8.3.2 Offset Voltage

Low offset voltage is one of the key parameters for an instrumentation amplifier (INA). In a current-feedback INA, this error source is classified in three stages: input, output, and intermediate. The input-stage dc offset (V_{OSI}) is mainly caused by the mismatch of the input transistors Q1 and Q2, (see \boxtimes 8-1). The output-stage dc offset (V_{OSO}) is caused partially by the mismatch of the output amplifier A3. In the INA851, A3 is a fully-differential amplifier and gained up by the noise gain of the circuit (1 + R_5 / R_3). An additional intermediate stage offset contribution error adds to V_{OSO} that is caused by the mismatch of the current mirrors in the front end (through R1 and R2).

Unlike typical instrumentation amplifiers that incorporate a difference amplifier (A3) with a fixed output gain, the INA851 has two different output gain stages that subsequently contribute differently to V_{OSO}; see Gaussian distributions for $G = G_{OUT} = 1 \text{ V/V}$ in \boxtimes 7-3 and for $G = G_{OUT} = 0.2 \text{ V/V}$ in \boxtimes 7-4.

The following equation calculates the total offset voltage error referred to the input:

$$V_{OS} = \sqrt{V_{OSI}^{2} + \left(\frac{V_{OSO}(G_{OUT} = 1 \text{ or } G_{OUT} = 0.2)}{G_{IN}}\right)^{2}}$$
(3)

8.3.3 Input Common-Mode Range

The linear input voltage range of the INA851 input circuitry extends within 2.5 V (maximum) of both power supplies, and maintains excellent common-mode rejection throughout this range. The valid input common-mode range is a function of the input common-mode voltage, input differential voltage, gain, and output common-mode voltage.

The common-mode range is best calculated using the INA851 Input-Output Range Design Calculator .

The common-mode range for the most common operating conditions are shown in \boxtimes 8-3 to \boxtimes 8-9.



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8.3.4 Input Protection

The inputs of the INA851 device are individually protected for voltages up to ±40 V beyond the power supply rails. For example, a condition of $V_{S-} = -55$ V on one input and $V_{S+} = 55$ V on the other input does not cause damage. Internal circuitry on each input provides low series impedance under normal signal conditions. \boxtimes 8-10 shows that if the input is overloaded, the protection circuitry limits the input current to a value of approximately 16 mA.



図 8-10. Input Current During an Overvoltage Condition

 \boxtimes 8-11 shows that during an input overvoltage condition, current flows through the input protection diodes into the power supplies. If the power supplies are unable to sink current, then place Zener diode clamps (ZD1 and ZD2 in \boxtimes 8-11) on the power supplies to provide a current pathway to ground.



図 8-11. Input Current Path During an Overvoltage Condition

If an input stage gain greater than $G_{IN} = 1$ V/V is implemented, where a gain resistor is present across the RG pins, the inputs are still well protected against overvoltage conditions; however, make sure that the input differential voltage limitations of the INA851 are not exceeded. For example, a condition of (V_{S+}) + 40 V on both inputs does not cause damage. However, a condition of (V_{S-}) – 40 V on one input and (V_{S+}) + 40 V on the other input can cause damage. Precautions can include the use of external resistors in series with each of the inputs.



8.3.5 Output Clamping

The INA851 features a unique output clamping function that protects the downstream device against damage that results from inadvertent over-driving. Usually the downstream device is an ADC that typically operates at a lower supply voltage than the INA851.

To implement this function, use the VCLAMP+ and VCLAMP– pins to limit the supply voltage range of the differential output drive amplifier. For typical operation, use a low-impedance connection from the pins to the power supplies of the ADC. For proper operation of the clamp circuitry, set the V_{S+} or V_{S-} supply voltages at least 1.5 V beyond the respective V_{CLAMP+} and V_{CLAMP-} clamping voltages. In addition, for the output driver to function correctly, the V_{CLAMP+} and V_{CLAMP-} voltages must be at least 3 V apart. If the output clamping functionality is not desired, short the VCLAMP+ and VCLAMP- pins to the amplifier VS+ and VS- supply pins.

The output driver operates up to the V_{CLAMP+} or V_{CLAMP-} limits without experiencing distortion. When the clamping function is in use the output voltage is clamped at approximately 600 mV beyond the clamp voltage.), so that the device output spans the full input range of the ADC. However, if the predriver output swings beyond the V_{CLAMP+} or V_{CLAMP-} voltage, the output driver begins to run out of headroom as a result of the clamped supply voltage, shown in \boxtimes 8-12.

The output is unable to swing greater than approximately 500 mV beyond the V_{CLAMP+} or V_{CLAMP-} voltage (at zero load), helping prevent or reduce damage to the ADC from overvoltage conditions.

The linear operation becomes distorted when the driver load becomes higher than 20 mA, see 🗵 8-13.



図 8-12. Simplified Schematic of Output Driver Clamping Structure

注

Be aware that instead of providing an immediate *hard-stop* voltage limit, the output driver is not clamped until V_{CLAMP+} or V_{CLAMP-} voltage has been exceeded, and the driver starts to run out of headroom. This configuration prevents distortion of the amplifier output when operating near the V_{CLAMP+} and V_{CLAMP-} rails. However, the output voltage exceeds V_{CLAMP+} and V_{CLAMP-} by several hundreds of millivolts before the clamps turn on strongly. When used in conjunction with several tens of ohms of resistance between the amplifier output and ADC input pins (commonly implemented as part of a low-pass filter for proper ADC acquisition), output clamping helps severely diminish any potential damage to the ADC that can otherwise result.





図 8-13. Output Voltage With Output Clamping Enabled

The VCLAMP+ pin features a fail-safe against power-up sequencing issues between the INA851 and a downstream device. For example, a condition of $V(_{CLAMP+}) + 10$ V on this pin does not cause damage. Therefore, the ADC supply can safely turn on while the INA851 supply is still off or just beginning to turn on. In this case, the current draw through the VCLAMP+ pin is limited to a safe value of typically 3 mA.

8.3.6 Low Noise

An output noise calculation helps design a low-noise circuit to drive high-precision ADC applications and optimize the signal-to-noise ratio (SNR).

 \boxtimes 8-14 shows a simplified noise model for the INA851. The e_{NO} noise refers to the input resistor network of the FDA. This term incorporates the thermal noise of the internal feedback resistors, and the interaction of the internal current noise density of the output stage with the internal feedback resistors.



図 8-14. Simplified Noise Model for the INA851

The internal feedback resistor network is considered in the e_{NO} specification; therefore, the calculation of the total input-referred noise, $e_{N(RTI)}$, is simplified to the following equation:

$$e_{N(RTI)} = \sqrt{e_{NI}^{2} + \left(\frac{e_{NO}(G_{OUT} = 1 \text{ or } G_{OUT} = 0.2)}{G_{IN}}\right)^{2}}$$
(4)

The total output-referred noise, $e_{N(RTO)}$, multiplies directly by the output stage gain, G_{OUT} , by $G_{OUT} = 0.2$ V/V or $G_{OUT} = 1$ V/V respectively, as shown in the following equation:

$$e_{N(RTO)} = \sqrt{(e_{NI} \times G_{IN} \times 0.2 \text{ V/V or } 1 \text{ V/V})^{2} + (e_{NO}(G_{OUT} = 1 \text{ or } G_{OUT} = 0.2) \times 0.2 \text{ V/V or } 1 \text{ V/V})^{2}}$$
(5)

8.4 Device Functional Modes

The INA851 has a single functional mode and operates when the power-supply voltage is greater than 8 V (\pm 4 V). The maximum power-supply voltage for the INA851 is 36 V (\pm 18 V).



9 Application and Implementation

注

以下のアプリケーション情報は、TIの製品仕様に含まれるものではなく、TIではその正確性または完全性を保証いたしません。個々の目的に対する製品の適合性については、お客様の責任で判断していただくことになります。お客様は自身の設計実装を検証しテストすることで、システムの機能を確認する必要があります。

9.1 Application Information

9.1.1 Output Common-Mode Pin

The output voltage of the INA851 is developed with respect to the voltage on the output common-mode pin, VOCM. The starting point for most designs is to assign an output common-mode voltage for the INA851. For accoupled signal paths, this voltage is often the default midsupply voltage, so as to retain the most available output swing around the voltage centered at V_{OCM} . For dc-coupled signal paths, set this voltage between a minimum of $V_{S+} - 2.5$ V and maximum of $V_{S-} + 2.5$ V. For precision ADC applications, this voltage is typically the input common mode voltage of the ADC.

The voltage at the VOCM pin is internally buffered to bias the fully differential output amplifier, eliminating the need for an additional external V_{OCM} buffer. While the buffer input is high-ohmic, the VOCM pin also connects through internal 500-k Ω resistors to V_{CLAMP+} and V_{CLAMP-} , which sets the output common-mode voltage to midsupply in the event that the pin is floating.

While the V_{OCM} buffer has high small-signal bandwidth, be aware that large-signal steps with fast edges at the VOCM pin cause delays in the output. For best tracking between the buffer input and output signals, use rise times of 200 ns or greater for large steps.

9.1.2 Output-Stage Gain Selection and Noise-Gain Shaping

In the default unity-gain configuration, the INA851 fully differential amplifier output stage uses $5-k\Omega$ feedback resistors between the OUT+ and OUT– outputs and the inverting and noninverting inputs, respectively. However, the INA851 also features internal 1.25-k Ω feedback resistors between those inputs and the G02+ and G02– pins. By shorting the G02+ pin to the OUT+ pin, and the G02– pin to the OUT– pin, the amplifier is placed in an attenuating gain of 0.2 V/V.

Additionally, access directly to the inverting and noninverting inputs of the fully differential amplifier is provided through the FDA_IN- and FDA_IN+ pins, respectively. This option allows circuit designers to add external feedback capacitors in parallel with the internal feedback resistors to implement noise filtering or noise-gain shaping techniques. These pins can also be used to implement customized attenuating gains for the output stage. Do not treat these pins as outputs, nor use the pins to source or sink current.

注

These pins are internally disconnected on preliminary samples of the INA851; these pins will be connected to the aforementioned internal nodes in the final device release.



9.1.3 Input Bias Current Return Path

The input impedance of the INA851 is very high at approximately 1 G Ω . However, a path must be provided for the input bias current of both inputs. This input bias current is typically 5 nA. High input impedance means that this input bias current changes very little with varying input voltage.

For proper operation, input circuitry must provide a path for input bias current. \boxtimes 9-1 shows various provisions for an input bias current path. Without a bias current path, the inputs float to a potential that exceeds the common-mode range of the INA851, and the input amplifiers saturate. If the differential source resistance is low, the thermocouple example in \boxtimes 9-1 shows that the bias current return path can connect to one input. With a higher source impedance, using two equal resistors provides a balanced input with the possible advantages of a lower input offset voltage as a result of bias current and better high-frequency common-mode rejection.

For more details about why a valid input bias current return path is necessary, see the *Importance of Input Bias Current Return Paths in Instrumentation Amplifier Applications* application report.



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図 9-1. Providing an Input Common-Mode Current Path



9.1.4 Thermal Effects due to Power Dissipation

The INA851 dissipates approximately 180 mW of power under quiescent conditions at a ±15-V supply voltage. The internal resistor network and output load drive causes an additional power dissipation that depends on the input signal. The small silicon area of the INA851 causes the internal circuitry to experience temperature gradients that can adversely affect the electrical performance.

Precision parameters, such as offset voltage, linearity, common-mode rejection ratio, and total harmonic distortion, can be impacted as a result of these thermal effects in the silicon. The thermal gradient particularly affects the performance of low-frequency input signals with higher gains (> 10) and large output voltage variation. \boxtimes 9-2 shows that the thermal effect can be minimized by lowering the supply voltage, if the application permits.

To properly dissipate heat from the INA851, connect the thermal pad with sufficient thermal vias to a large copper plane that is connected to the negative supply, VS-. A thorough PCB layout is of key importance (see also セクション 9.4).



☑ 9-2. Linearity vs Supply Voltage for G = 1000



9.2 Typical Applications

9.2.1 Three-Pin Programmable Logic Controller (PLC)

⊠ 9-3 shows a three-pin programmable-logic controller (PLC) design for the INA851. This PLC reference design accepts inputs of ± 10 V or ± 20 mA. The output is a differential voltage of ± 4.95 V with a V_{OCM} of 2.5 V (or 25 mV to 4.975 V on OUT+ and OUT-) to be measured by the ADS8920B SAR ADC.



図 9-3. PLC Input with INA851 (±10 V, 4 mA to 20 mA)

9.2.1.1 Design Requirements

For this application, the design requirements are as follows:

- 4-mA to 20-mA input with less than 20-Ω burden
- ±20-mA input with less than 20-Ω burden
- ± 10 -V input with impedance of approximately 100 k Ω
- Maximum 4-mA to 20-mA or ±20-mA burden voltage equal to ±0.4 V
- Output range within 0 V to 5 V

9.2.1.2 Detailed Design Procedure

There are two modes of operation for the circuit shown in \boxtimes 9-3: current input and voltage input. This design requires $R_1 \gg R_2 \gg R_3$. Given this relationship, the following equation calculates the current input mode transfer function.

$$V_{OUT} = V_{DIFF} \times G = -(I_{IN} \times R_3)$$

where

- V_{OUT} represents the differential voltage at the INA851 outputs in current input mode.
- V_{DIFF} represents the differential voltage at the INA851 inputs.
- G represents the total gain of the INA851
- I_{IN} is the input current to the PLC.

(6)



The following equation shows the transfer function for the voltage input mode:

$$V_{OUT} = V_{DIFF} \times G = -\left(V_{IN} \times \left(\frac{R_2}{R_2 + R_1}\right)\right)$$
(7)

where

- V_{OUT} represents the differential voltage at the INA851 outputs in voltage input mode.
- V_{IN} is the input voltage to the PLC.

The voltages on the output pins of the INA851 follow the relationships in $\exists 3$ and $\exists 9$.

$$V_{OUT +} = V_{DIFF} \times \frac{G}{2} + V_{OCM}$$
(8)

$$V_{OUT-} = -V_{DIFF} \times \frac{G}{2} + V_{OCM}$$
(9)

 R_1 sets the input impedance of the voltage input mode. The minimum typical input impedance is 100 k Ω . The R_1 value is 100 k Ω because increasing the R_1 value also increases noise. The value of R_3 must be extremely small compared to R_1 and R_2 . A 20- Ω value is selected for R_3 because that resistance value is much smaller than R_1 and yields an input voltage of ±400 mV when operated in current mode (±20 mA).

Use $\neq 10$ to calculate R₂ given V_{DIFF} = ±400 mV, V_{IN} = ±10 V, and R₁ = 100 k Ω .

$$V_{DIFF} = V_{IN} \times \frac{R_2}{R_1 + R_2} \rightarrow R_2 = \frac{R_1 \times V_{DIFF}}{V_{IN} - V_{DIFF}} = 4.167 \text{ k}\Omega$$
(10)

The value obtained from $\neq 10$ is not a standard 0.1% value; therefore, 4.17 k Ω is selected. R₁ and R₂ also use 0.1% tolerance resistors to minimize error.

Use $rac{d}{d}$ 11 to calculate the gain of the instrumentation amplifier.

$$G = \frac{V_{OUT}}{V_{DIFF}} = \frac{4.95 V}{400 mV} = 12.375 V/V$$
(11)

式 12 calculates the gain-setting resistor value using the INA851 gain equation for G_{OUT} = 1 V/V (式 1).

$$R_{\rm G} = \frac{6\,\mathrm{k}\Omega}{\mathrm{G}-1} = \frac{6\,\mathrm{k}\Omega}{12.375-1} = 527.473\,\,\Omega\tag{12}$$

Use a standard 0.1% resistor value of 530 Ω for this design.

The ADS8920B is selected because of the differential input, 1-MSPS sampling rate, and integrated reference buffer. Implement the antialiasing R-C-R filter using two 47.4- Ω resistors, a COG or NPO-type 510-pF differential capacitor, and two ceramic 51-pF common-mode capacitors. The REF5050 is selected to create a 5-V reference voltage for the ADC. Use well-matched precision resistors to create a voltage divider that generates a stable 2.5-V V_{OCM} reference. Connect the VCLAMP+ and VCLAMP- pins of the INA851 to the supplies of the ADC to protect against overdrive damage in the event of a fault. Consider implementing a TVS diode from the ADC supply to GND for additional protection, and include 100-nF decoupling capacitors between the amplifier and ADC supplies and GND.

9.2.1.3 アプリケーション曲線

図 9-4 および図 9-5 に、図 9-3 の回路の標準的特性曲線を示します。





9.2.2 20-Bit, 1-MSPS ADS8900B Driver Circuit With FDA Noise Filter

The application circuit in \boxtimes 9-6 shows the schematic of a complete input and reference driver circuit for the ADS8900B, a 20-bit, precision, 1-MSPS, successive approximation register (SAR), analog-to-digital converter (ADC). This circuit is used to measure the driving capability of the INA851 with the ADS8900B ADC.

To test the complete dynamic range of the circuit, the common-mode voltage V_{OCM} of the input of the ADC is established at a value of V_{REF} / 2.

To exclude noise caused by supply voltage, the test circuit uses the TPS7A4700, a low-noise 4-µVRMS, RF LDO voltage regulator, to generate the 5.2-V supply rail.

For V_{OCM}, the circuit uses the REF5050, a low-noise, low-drift, 5-V reference, a 20k-20k voltage divider to establish VREF/2 and an additional RC filter (10 Ω , 150 pF) into the VOCM pin. See also the ADS8900EVM-PDK user's guide.







9.2.2.1 Design Requirements

The requirements for the application driving the ADS8900B ADC are listed in the following table.

PARAMETER	VALUE
Differential to differential conversion	V _{INDIFF} to V _{OUTDIFF}
Supply voltages	VS± = ± 15 V, VDD = 5.2 V, VREF = 5 V
Full-scale range of ADC for FSR	FSR = ± 5 V
Driver configuration	See 表 9-2
Circuit bandwidth	f _(-3dB) = 31.7 kHz
Output RC elements	See ADS8900B input requirements

表 9-1. Design Parameters

To eliminate ground loops, unwanted parasitic effects, and distortion, use appropriate PCB layout and grounding techniques (see also セクション 9.4).

9.2.2.2 Application Curves

表 9-2 show the typical signal-to-noise (SNR) and total harmonic distortion (THD) of the INA851 driving the ADS8900B SAR ADC at full-scale range and at different gain configurations. The RC filter combination (R_{FIL}, C_{FIL}) shown in ⊠ 9-6 helps attenuate the nonlinear charge kickback of the ADC and optimize for best THD performance. The combination of the RC filter and the feedback capacitor C_{FB} allow for the best trade-off between harmonic distortion and maintaining stability of the FDA. Low voltage-coefficient C0G capacitors are used everywhere in the signal path (C_{FB}, C_{FIL}) for the low-distortion properties.

For other bandwidth requirements, adjust the feedback capacitor accordingly, and verify the circuit performance using a SPICE simulation using the INA851 TINA-TI[™] SPICE Model. The amplifier output voltage must settle within the ADC bit accuracy during the ADC acquisition time window. Verify the desired circuit is stable; that is, the FDA has more than a 45° phase margin.

INPUT AMPLITUDE (Vpk)	RG RESISTOR (Ω)	G _{IN} (V/V)	G _{OUT} (V/V)	SNR (dB)	THD (dB)	ENOB (Bits)
23.7378	None	1	0.2	100.7	-117.3	16.42
4.7476	None	1	1	100.6	-122.7	16.41
0.2374	316	20	1	99.1	-112.0	16.10
0.0475	60.4	100	1	91.1	-99.0	14.64

表 9-2. INA851 + ADS8900B FFT Data Summary







9.2.3 24-Bit, 200 kSPS, Delta-Sigma ADS127L11 ADC Driver Circuit With FDA Noise Filter

The application circuit in \boxtimes 9-9 shows an schematic for a 24-bit-precision, 200-kSPS, delta-sigma, ADC. The circuit is used to measure the driving capacity of the INA851 with the ADS127L11 ADC.

The ADS127L11 ADC offers two digital filters to optimize for ac applications (wideband filter) or dc applications (Sinc4 filter). Application Curves shows measurement results in both filter settings. For detailed design procedure to operate the ADS127L11 ADC, see the ADS127L11EVM-PDK evaluation module.



2 9-9. Driving the Delta-Sigma ADC ADS127L11

9.2.3.1 Design Requirements

The design requirements for the application driving the ADS127L11 ADC are listed in the following table.

PARAMETER	VALUE
Differential-to-differential conversion	V _{INDIFF} to V _{OUTDIFF}
Supply voltages	VS± = ±15 V, AVDD = 5.2 V, VREF = 2.5 V
Full-scale range of ADC for FSR	FSR = ± 5 V
Data rate of ADC	f _{DATA} = 187.5 kSPS
ADC filter configuration	(1) High-speed mode, Sinc4 filter, OSR = 64
	(2) High-speed mode, wideband filter, OSR = 64
INA gain and filter configuration	See 表 9-4 and 表 9-5
Signal frequency	f _{IN} = 1 kHz
RC kickback filter ⁽¹⁾	$R_{FIL} = 47.4 \ \Omega + C_{DIFF} = 510 \ pF + R_{FIL} = 47.4 \ \Omega, \ C_{FIL} = 51 \ pF$

表 9-3. Design Parameter	表 9-3.	. Design	Parameters
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(1) A trade-off must be considered between THD, frequency response and drift. The differential current drift into the ADC can interact with this filter resistors and result in higher drift errors. However, low resistance degrades the phase margin of the INA851. For low drift applications, keep $R_{FIL} < 50 \Omega$.



For optimized linearity and THD performance, use good printed circuit board (PCB) layout practice. For proper heat dissipation of the INA851, connect the thermal pad to a plane or a large copper pour at the bottom connected to VS- (see also セクション 9.4.2).

9.2.3.2 Application Curves

表 9-4 and 表 9-5 show the typical signal-to-noise (SNR) and total harmonic distortion (THD) of the INA851 driving the ADS127L11 delta-sigma ADC at full-scale range and at different gain configurations.

The RC filter combination is dimensioned such to help attenuate the nonlinear charge kickback and optimize for best THD performance. The ADC requires a low impedance input for lowest distortion performance; however, driving heavier loads degrades the phase margin of the INA851. Use a feedback capacitor (C_{FB}) in the range of 47 pF to 100 pF to optimize for stability versus THD performance. Low voltage-coefficient COG capacitors are used everywhere in the signal path (C_{FB} , C_{DIFF} , C_{CM}) for their low distortion properties.

For other bandwidth requirements, adjust the feedback capacitor accordingly and verify the circuit performance using a SPICE simulation using INA851 TINA-TI™ SPICE Model. Confirm that the desired circuit is stable; that is, the FDA has more than a 45° phase margin.

INPUT AMPLITUDE (Vpk)	RG RESISTOR (Ω)	G _{IN} (V/V)	G _{OUT} (V/V)	SNR (dB)	THD (dB)	ENOB (Bits)
23.7378	None	1	0.2	106.8	-116.0	17.36
4.7476	None	1	1	105.9	-122.0	17.28
2.3738 ⁽¹⁾	1500	5	0.2	107.2	-113.8	17.25
0.2374	316	20	1	102.5	-112.0	16.59
0.0475	60.4	100	1	92.5	-99.0	14.81

表 9-4. INA851 + ADS127L11 (Sinc4 Filter) FFT Data Summary



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INPUT AMPLITUDE (Vpk)	RG RESISTOR (Ω)	G _{IN} (V/V)	G _{OUT} (V/V)	SNR (dB)	THD (dB)	ENOB (Bits)				
23.76015	None	1	0.2	105.3	-116.2	17.14				
4.7476	None	1	1	103.1	-120.0	16.81				
2.3738	1500	5	0.2	104.2	-113.0	16.85				
0.2360	316	20	1	99.0	-112.0	16.08				
0.0472	60.4	100	1	89.3	-99.0	14.40				



表 9-5. INA851 + ADS127L11 (Wideband Filter) FFT Data Summary



9.3 Power Supply Recommendations

The nominal performance of the INA851 is specified with a supply voltage of ±15 V, and V_{ICM} and V_{OCM} at midsupply. The device also operates using power supplies from ±4 V (8 V) to ±18 V (36 V) and non-midsupply input and output common-mode voltages with excellent performance.

9.4 Layout

9.4.1 Layout Guidelines

Attention to good layout practices is always recommended. For best operational performance of the device, use good printed circuit board (PCB) layout practices:

- To avoid converting common-mode signals into differential signals and thermal electromotive forces (EMFs), make sure that both input paths are symmetrical and well-matched for source impedance and capacitance.
- As shown in ⊠ 9-14, keep the external gain resistor close to the RG pins to keep the loop inductance as low
 as possible and to avoid a potential parasitic coupling path. Even slight mismatch in parasitic capacitance at
 the gain setting pins can degrade CMRR over frequency. In applications that implement gain switching using
 switches or PhotoMOS[®] relays to change the value of R_G, select the component so that the switch
 capacitance is as small as possible, and most importantly, so that capacitance mismatch between the RG
 pins is minimized.
- Noise can propagate into analog circuitry through the power pins of the device and of the circuit as a whole. Bypass capacitors reduce the coupled noise by providing low-impedance power sources local to the analog circuitry.
 - Connect low-ESR, 0.1-µF ceramic bypass capacitors between each supply pin and ground, placed as close as possible to the device. A single bypass capacitor from V+ to ground is applicable for singlesupply applications.
- To reduce parasitic coupling, run the input traces as far away as possible from the supply or output traces. If these traces cannot be kept separate, crossing the sensitive trace perpendicular to the noisy trace is much better than in parallel.
- Leakage on the FDA_IN+ and FDA_IN- pins can cause in a dc offset error in the output voltages. Additionally, excessive parasitic capacitance at these pins can result in decreased phase margin and affect the stability of the output stage. If these pins are not used to implement deliberate capacitive feedback, follow best practices to minimize leakage and parasitic capacitance. Consider implementing *keep-out* areas in any ground planes that lie immediately below the pins.
- Minimize the number of thermal junctions. Ideally, the signal path is routed within a single layer without vias.
- Keep sufficient distance from major thermal energy sources (circuits with high power dissipation). If not possible, place the device so that the effects of the thermal energy source on the high and low sides of the differential signal path are evenly matched.
- Solder the thermal pad to the PCB. For the INA851 to properly dissipate heat, connect the thermal pad to a plane or large copper pour that is electrically connected to VS–, even for low-power applications.
- Keep the traces as short as possible.



9.4.2 Layout Example





2 9-14. Example Schematic and Associated PCB Layout



10 Device and Documentation Support

10.1 Device Support

10.1.1 Development Support

10.1.1.1 PSpice[®] for TI

PSpice[®] for TI は、アナログ回路の性能評価に役立つ設計およびシミュレーション環境です。レイアウトと製造に移る前に、サブシステムの設計とプロトタイプ・ソリューションを作成することで、開発コストを削減し、市場投入までの期間を短縮できます。

10.1.1.2 TINA-TI™ シミュレーション・ソフトウェア (無償ダウンロード)

TINA-TI[™] シミュレーション・ソフトウェアは、SPICE エンジンをベースにした単純かつ強力な、使いやすい回路シミュレーション・プログラムです。TINA-TI シミュレーション・ソフトウェアは、TINA[™] ソフトウェアのすべての機能を持つ無償バージョンで、パッシブ・モデルとアクティブ・モデルに加えて、マクロモデルのライブラリがプリロードされています。TINA-TI シミュレーション・ソフトウェアには、SPICE の標準的な DC 解析、過渡解析、周波数ドメイン解析などの全機能に加え、追加の設計機能が搭載されています。

TINA-TI シミュレーション・ソフトウェアは設計ツールとシミュレーション Web ページから無料でダウンロードでき、ユーザ ーが結果をさまざまな方法でフォーマットできる、広範な後処理機能を備えています。仮想計測器により、入力波形を選 択し、回路ノード、電圧、および波形をプローブして、動的なクイック・スタート・ツールを作成できます。

注

これらのファイルを使用するには、TINA ソフトウェアまたは TINA-TI ソフトウェアがインストールされている必要 があります。TINA-TI™ ソフトウェア・フォルダから、無償の TINA-TI シミュレーション・ソフトウェアをダウンロー ドしてください。

10.2 Documentation Support

10.2.1 Related Documentation

For related documentation see the following:

- Texas Instruments, Comprehensive Error Calculation for Instrumentation Amplifiers application note
- Texas Instruments, Importance of Input Bias Current Return Paths in Instrumentation Amplifier Applications application note

10.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. Click on *Subscribe to updates* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

10.4 サポート・リソース

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10.6 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

10.7 Glossary

TI Glossary This glossary lists and explains terms, acronyms, and definitions.

11 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.



PACKAGING INFORMATION

Orderable part number	Status	Material type	Package Pins	Package qty Carrier	RoHS	Lead finish/	MSL rating/	Op temp (°C)	Part marking
	(1)	(2)			(3)	Ball material	Peak reflow		(6)
						(4)	(5)		
INA851RGTR	Active	Production	VQFN (RGT) 16	3000 LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	INA851
INA851RGTR.B	Active	Production	VQFN (RGT) 16	3000 LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	INA851
INA851RGTT	Active	Production	VQFN (RGT) 16	250 SMALL T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	INA851
INA851RGTT.B	Active	Production	VQFN (RGT) 16	250 SMALL T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	INA851

⁽¹⁾ **Status:** For more details on status, see our product life cycle.

⁽²⁾ Material type: When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

⁽³⁾ RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

⁽⁴⁾ Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

⁽⁵⁾ MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

⁽⁶⁾ Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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TAPE AND REEL INFORMATION





QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All	*All dimensions are nominal												
	Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
	INA851RGTR	VQFN	RGT	16	3000	330.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2
	INA851RGTT	VQFN	RGT	16	250	180.0	12.4	3.3	3.3	1.1	8.0	12.0	Q2



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PACKAGE MATERIALS INFORMATION

11-Nov-2022



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
INA851RGTR	VQFN	RGT	16	3000	367.0	367.0	35.0
INA851RGTT	VQFN	RGT	16	250	210.0	185.0	35.0

GENERIC PACKAGE VIEW

VQFN - 1 mm max height PLASTIC QUAD FLATPACK - NO LEAD



Images above are just a representation of the package family, actual package may vary. Refer to the product data sheet for package details.



RGT0016C



PACKAGE OUTLINE

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M. 2. This drawing is subject to change without notice.
- 3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.



RGT0016C

EXAMPLE BOARD LAYOUT

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).

5. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.



RGT0016C

EXAMPLE STENCIL DESIGN

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.



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