

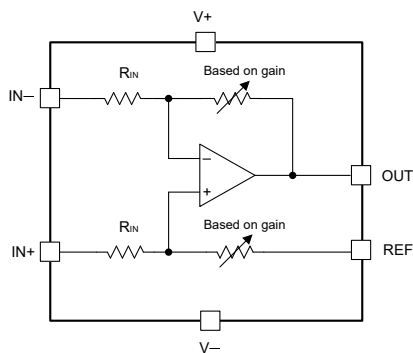
# INA600 Low Power, 2.7V to 40V Attenuating Difference Amplifier with >1MΩ Input Impedance for Cost-Optimized Designs

## 1 Features

- >1MΩ Ultra-high input impedance
- Gains of 1/5, 1/10, 1/12, 1/18, 1/24, and 1/36
- Good precision for 8-bit to 12-bit systems
  - CMRR: 100dB (typical,  $G = 1/5$ )
  - Gain error:  $\pm 0.01\%$  (typical)
  - Gain drift :  $\pm 1\text{ppm}/^\circ\text{C}$  (typical)
- –3dB Bandwidth:  $\geq 200\text{kHz}$
- Available gains:
  - INA600A: 1/5
  - INA600B: 1/10
  - INA600C: 1/12
  - INA600D: 1/18
  - INA600E: 1/24
  - INA600F: 1/36
- Drives 400pF with  $\leq 20\%$  overshoot (typical)
- Low quiescent current: 65μA (typical)
- Supply range: 2.7V ( $\pm 1.35\text{V}$ ) to 40V ( $\pm 20\text{V}$ )
- Specified temperature range:  $-40^\circ\text{C}$  to  $125^\circ\text{C}$

## 2 Applications

- [Battery cell formation and test equipment](#)
- [String inverter](#)
- [EV charging station power module](#)
- [Battery energy storage system](#)
- [Power tools](#)
- [Industrial AC-DC](#)
- [Wearable fitness and activity monitor](#)



**INA600 Simplified Internal Schematic**

## 3 Description

INA600 is a voltage sensing difference amplifier with precision matched resistors that offer attenuating gain options. The precision matched integrated resistors saves BOM costs and board space by removing the need for precise and low tolerance external resistors.

INA600 offers high input impedance of >1MΩ and low quiescent current of 65μA. The device can handle up to  $-40\text{V}$  to  $85\text{V}$  of input voltage, attenuate the voltage down with great accuracy, and interface the voltage to the low voltage ADC while rejecting any common-mode errors such as ground bounce, switching ripples, AC mains etc.. The device achieves a maximum gain error of  $\pm 0.05\%$ , and a maximum gain drift of  $5\text{ppm}/^\circ\text{C}$  along with 89dB of minimum common-mode rejection ratio ( $G = 1/5$ ).

The combination of specifications noted above make INA600 a great choice for a variety of level translation, differential to single-ended applications, including any voltage monitoring of batteries or power-rails. INA600 interfaces directly to low-speed,  $\leq 12$ -bit, analog-to-digital converters (ADC) and hence an excellent choice for replacing discrete implementation of difference amplifiers built with commodity amplifiers and discrete resistors. INA600 is offered in standard 6-pin packages such as SOT-23 and SC70.

### Package Information

PART NUMBER <sup>(1)</sup>	VERSION	PACKAGE <sup>(2)</sup>	PACKAGE SIZE <sup>(5)</sup>
INA600	A	DBV (SOT-23, 6)	2.9mm × 2.8mm
		DCK (SC70, 6) <sup>(3)</sup>	2.1mm × 1.25mm
	B	DBV (SOT-23, 6)	2.9mm × 2.8mm
		DCK (SC70, 6) <sup>(3)</sup>	2.1mm × 1.25mm
	C <sup>(4)</sup>	DBV (SOT-23, 6) <sup>(3)</sup>	2.9mm × 2.8mm
		DCK (SC70, 6) <sup>(3)</sup>	2.1mm × 1.25mm
	D <sup>(4)</sup>	DBV (SOT-23, 6) <sup>(3)</sup>	2.9mm × 2.8mm
		DCK (SC70, 6) <sup>(3)</sup>	2.1mm × 1.25mm
	E <sup>(4)</sup>	DBV (SOT-23, 6) <sup>(3)</sup>	2.9mm × 2.8mm
		DCK (SC70, 6) <sup>(3)</sup>	2.1mm × 1.25mm
	F	DBV (SOT-23, 6)	2.9mm × 2.8mm
		DCK (SC70, 6) <sup>(3)</sup>	2.1mm × 1.25mm

- (1) See [Device Comparison](#)
- (2) For more information, see [Section 11](#)
- (3) This package is preview only.
- (4) This version is preview only.
- (5) The package size (length × width) is a nominal value and includes pins, where applicable



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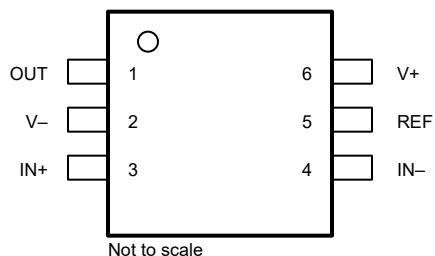
## 4 Device Comparison Table

DEVICE	VERSION	GAIN	NO. OF CHANNELS	PACKAGE LEADS	
				SOT-23 DBV	SC70 DCK <sup>(1)</sup>
INA600	A	1/5	1	6	6
	B	1/10	1	6	6
	C <sup>(2)</sup>	1/12	1	6	6
	D <sup>(2)</sup>	1/18	1	6	6
	E <sup>(2)</sup>	1/24	1	6	6
	F	1/36	1	6	6

(1) Package is preview only.

(2) Version is preview only.

## 5 Pin Configuration and Functions

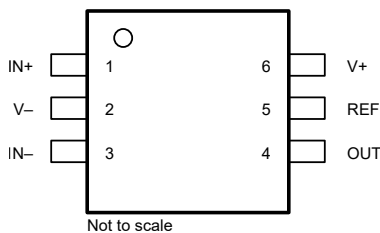


**Figure 5-1. INA600 DBV Package, 6-Pin SOT-23 (Top View)**

**Table 5-1. Pin Functions**

PIN		TYPE <sup>(1)</sup>	DESCRIPTION
NAME	SOT-23		
IN–	4	I	Negative (inverting) input
IN+	3	I	Positive (noninverting) input
OUT	1	O	Output
REF	5	I	Reference input
V–	2	—	Negative supply
V+	6	—	Positive supply

(1) I = input, O = output



**Figure 5-2. INA600 DCK Package, 6-Pin SC70 (Top View)**

**Table 5-2. Pin Functions**

PIN		TYPE <sup>(1)</sup>	DESCRIPTION
NAME	SC70		
IN–	3	I	Negative (inverting) input
IN+	1	I	Positive (non-inverting) input
OUT	4	O	Output
REF	5	I	Reference input
V–	2	—	Negative supply
V+	6	—	Positive supply

(1) I = input, O = output

## 6 Specifications

### 6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	MAX	UNIT
Supply voltage, $V_S = (V+) - (V-)$	Single Supply		42	V
	Dual Supply		±21	V
Signal input pins	Voltage	(V-) – 42	(V-) + 87	V
	Current	–10	10	mA
Output short-circuit <sup>(2)</sup>		Continuous		
Operating temperature, $T_A$		–55	150	°C
Junction temperature, $T_J$			150	
Storage temperature, $T_{stg}$		–65	150	

- (1) Operation outside the *Absolute Maximum Ratings* may cause permanent device damage. *Absolute Maximum Ratings* do not imply functional operation of the device at these or any other conditions beyond those listed under *Recommended Operating Conditions*. If used outside the *Recommended Operating Conditions* but within the *Absolute Maximum Ratings*, the device may not be fully functional, and this may affect device reliability, functionality, performance, and shorten the device lifetime.
- (2) Short-circuit to  $V_S / 2$ .

### 6.2 ESD Ratings

			VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±1000	V
		Charged-device model (CDM), per ANSI/ESDA/JEDEC JS-002 <sup>(1)</sup>	±1000	

- (1) JEDEC document JEP155 states that 500V HBM allows safe manufacturing with a standard ESD control process.

### 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	MAX	UNIT
Supply voltage $V_S = (V+) - (V-)$	Single-supply	2.7	40	V
	Dual-supply	±1.35	±20	
Input voltage range	Single-supply / Dual-supply	(V-) – 40	(V-) + 85	V
$C_{BYP}$	Bypass capacitor on the power supply pins <sup>(1)</sup>	0.1		μF
Specified temperature	Specified temperature	–40	125	°C

- (1) For  $C_{BYP}$ , use low-ESR ceramic capacitors between each supply pin and ground. Only one  $C_{BYP}$  is sufficient for single supply operation. Ensure that  $C_{BYP}$  is placed as close to the device as possible and the supply trace routes through  $C_{BYP}$  before reaching the supply pin.

### 6.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		INA600		UNIT
		DCK (SC70)	DBV (SOT-23)	
		6 PINS	6 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	TBD	195.9	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	TBD	115.5	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	TBD	77.1	°C/W
$\Psi_{JT}$	Junction-to-top characterization parameter	TBD	52.2	°C/W
$\Psi_{JB}$	Junction-to-board characterization parameter	TBD	76.8	°C/W

THERMAL METRIC <sup>(1)</sup>		INA600		UNIT
		DCK (SC70)	DBV (SOT-23)	
		6 PINS	6 PINS	
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance	TBD	n/a	°C/W

- (1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application note.

## 6.5 Electrical Characteristics - INA600A

For  $V_S = (V_+) - (V_-) = 2.7V$  to  $40V$  ( $\pm 1.35V$  to  $\pm 20V$ ) at  $T_A = 25^\circ C$ ,  $V_{REF} = V_S / 2$ ,  $G = 1/5$ ,  $R_L = 10k\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = (V_{IN+} + V_{IN-}) / 2 = V_S / 2$ ,  $V_{IN} = (V_{IN+} - V_{IN-}) = 0V$  and  $V_{OUT} = V_S / 2$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
OFFSET							
V <sub>OSO</sub>	Offset voltage, RTO	V <sub>S</sub> = 2.7V and 40V	T <sub>A</sub> = 25°C		±1.1	±4.5	mV
	Offset voltage over T, RTO		T <sub>A</sub> = −40°C to 125°C		±5.0	mV	
	Offset temp drift, RTO <sup>(1)</sup>		T <sub>A</sub> = −40°C to 125°C		±2	±10	μV/°C
PSRR	Power-supply rejection ratio	V <sub>S</sub> = 4V to 40V	T <sub>A</sub> = 25°C		4	20	μV/V
PSRR	Power-supply rejection ratio	V <sub>S</sub> = 2.7V to 40V	T <sub>A</sub> = 25°C		5	25	μV/V
INPUT IMPEDANCE							
R <sub>IN-DM</sub>	Differential Resistance				2400		kΩ
R <sub>IN-CM</sub>	Common-mode Resistance				635		kΩ
INPUT VOLTAGE							
V <sub>CM</sub>	Input common-mode Range	V <sub>S</sub> = 2.7V		(V−) − 2.5		(V−) + 22.5	V
V <sub>CM</sub>	Input common-mode Range	V <sub>S</sub> = 4.5V		(V−) − 25		(V−) + 50	V
V <sub>CM</sub>	Input common-mode Range	V <sub>S</sub> = 9V to 40V		(V−) − 40		(V−) + 85	V
CMRR DC	Common-mode rejection ratio, RTO	2.7V ≤ V <sub>S</sub> < 4.5V	V <sub>CM</sub> = (V−) − 2.5V to (V−) + 22.5V	89			dB
CMRR DC	Common-mode rejection ratio, RTO	4.5V ≤ V <sub>S</sub> < 9V	V <sub>CM</sub> = (V−) − 25V to (V−) + 50V	89			dB
CMRR DC	Common-mode rejection ratio, RTO	9V ≤ V <sub>S</sub> ≤ 40V	V <sub>CM</sub> = (V−) − 40V to (V−) + 85V	89	100		dB
NOISE VOLTAGE							
e <sub>NI</sub>	Output voltage noise density	V <sub>S</sub> = 40V	f = 1kHz		245		nV/√Hz
			f = 10kHz		240		
E <sub>NI</sub>	Output voltage noise		f <sub>B</sub> = 0.1Hz to 10Hz		13.5		μV <sub>PP</sub>
			f <sub>B</sub> = 0.1Hz to 150kHz		650		μV <sub>PP</sub>
GAIN							
GE	Gain error <sup>(2)</sup>	V <sub>REF</sub> = V <sub>MID</sub>	V <sub>O</sub> = (V−) + 0.15V to (V+) − 0.15V		±0.003	±0.05	%
	Gain drift vs temperature <sup>(2)</sup>		T <sub>A</sub> = −40°C to 125°C			±5	ppm/°C
OUTPUT							
V <sub>OH</sub>	Positive and negative rail headroom	V <sub>S</sub> = 40V, V <sub>REF</sub> = V <sub>S</sub> , R <sub>L</sub> = 10kΩ to V <sub>MID</sub>			80	150	mV
V <sub>OL</sub>		V <sub>S</sub> = 40V, V <sub>REF</sub> = V <sub>S</sub> , R <sub>L</sub> = 2kΩ to V <sub>MID</sub>			400	650	mV
C <sub>L</sub> Drive	Load capacitance drive	V <sub>O</sub> = 100mV step, Overshoot < 20%			200		pF
Z <sub>O</sub>	Closed-loop output impedance	f = 10kHz			180		Ω
I <sub>SC</sub>	Short-circuit current	V <sub>S</sub> = 40V			±50		mA
FREQUENCY RESPONSE							

For  $V_S = (V_+) - (V_-) = 2.7V$  to  $40V$  ( $\pm 1.35V$  to  $\pm 20V$ ) at  $T_A = 25^\circ C$ ,  $V_{REF} = V_S / 2$ ,  $G = 1/5$ ,  $R_L = 10k\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = (V_{IN+} + V_{IN-}) / 2 = V_S / 2$ ,  $V_{IN} = (V_{IN+} - V_{IN-}) = 0V$  and  $V_{OUT} = V_S / 2$  (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
BW	Bandwidth, $-3dB$	$V_{IN} = 10mV_{pk-pk}$	200		kHz
THD + N	Total harmonic distortion + noise $V_S = 40V$ , $V_{REF} = 2.5V$ , $V_O = 5V_{pp}$ , $R_L = 100k\Omega$ $f = 1kHz$ , 80kHz measurement BW		0.03		%
EMIRR	Electro-magnetic interference rejection ratio $f = 1GHz$ , $V_{IN\_EMIRR} = 100mV$		105		dB
SR	Slew rate $V_S = 40V$ , $V_O = 1V$ step		0.32		V/ $\mu s$
$t_S$	Settling time To 0.1%, $V_S = 40V$ , $V_{OUT\_STEP} = 1V$ , $C_L = 10pF$		9.5		$\mu s$
$t_S$	Settling time To 0.01%, $V_S = 40V$ , $V_{OUT\_STEP} = 1V$ , $C_L = 10pF$		12		$\mu s$
$t_S$	Settling time To 0.1%, $V_S = 40V$ , $V_{OUT\_STEP} = 5V$ , $C_L = 10pF$		20		$\mu s$
$t_S$	Settling time To 0.01%, $V_S = 40V$ , $V_{OUT\_STEP} = 5V$ , $C_L = 10pF$		23		$\mu s$
	Overload recovery $V_S = 2.7V$ , $V_{IN-} = 0V$ , $V_{IN+} = 85V$ , and $V_{REF} = V_S / 2$		7.5		$\mu s$
<b>REFERENCE INPUT</b>					
REF - $V_{IN}$	Input voltage range $V_S = 40V$ , $V_{REF} = V_{MID}$	(V-)		(V+)	V
REF - G	Reference gain to output		1		V/V
REF - GE	Reference gain error <sup>(2)</sup> $V_S = 40V$		$\pm 0.002$	$\pm 0.1$	%
<b>POWER SUPPLY</b>					
$V_S$	Power-supply voltage Dual-supply	$\pm 1.35$		$\pm 20$	V
$I_Q$	Quiescent current $V_S = 2.7V$		60		$\mu A$
$I_Q$	Quiescent current $V_S = 40V$		65	80	$\mu A$
		$T_A = -40^\circ C$ to $125^\circ C$		85	

(1) Offset drifts are uncorrelated.

(2) Minimum and maximum values are specified by characterization.

## 6.6 Electrical Characteristics - INA600B

For  $V_S = (V_+) - (V_-) = 2.7V$  to  $40V$  ( $\pm 1.35V$  to  $\pm 20V$ ) at  $T_A = 25^\circ C$ ,  $V_{REF} = V_S / 2$ ,  $G = 1/10$ ,  $R_L = 10k\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = (V_{IN+} + V_{IN-}) / 2 = V_S / 2$ ,  $V_{IN} = (V_{IN+} - V_{IN-}) = 0V$  and  $V_{OUT} = V_S / 2$  (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>OFFSET</b>					
$V_{OSO}$	Offset voltage, RTO	$V_S = 2.7V$ and $40V$	$T_A = 25^\circ C$	$\pm 0.6$	$\pm 3.0$ mV
	Offset voltage over T, RTO		$T_A = -40^\circ C$ to $125^\circ C$		$\pm 3.5$ mV
	Offset temp drift, RTO <sup>(1)</sup>		$T_A = -40^\circ C$ to $125^\circ C$	$\pm 1.5$	$\pm 7$ $\mu V/^\circ C$
PSRR	Power-supply rejection ratio $V_S = 4V$ to $40V$	$T_A = 25^\circ C$	4	20	$\mu V/V$
PSRR	Power-supply rejection ratio $V_S = 2.7V$ to $40V$	$T_A = 25^\circ C$	5	25	$\mu V/V$
<b>INPUT IMPEDANCE</b>					
$R_{IN-DM}$	Differential Resistance		2400		k $\Omega$
$R_{IN-CM}$	Common-mode Resistance		635		k $\Omega$
$V_{CM}$	Input common-mode Range $V_S = 2.7V$	(V-) - 5		(V-) + 25	V
$V_{CM}$	Input common-mode Range $V_S = 4.5V$	(V-) - 30		(V-) + 55	V
<b>INPUT VOLTAGE</b>					
$V_{CM}$	Input common-mode Range $V_S = 9V$ to $40V$	(V-) - 40		(V-) + 85	V
CMRR DC	Common-mode rejection ratio, RTO $2.7V \leq V_S < 4.5V$	$V_{CM} = (V_-) - 5V$ to $(V_-) + 25V$	95		dB
CMRR DC	Common-mode rejection ratio, RTO $4.5V \leq V_S < 9V$	$V_{CM} = (V_-) - 30V$ to $(V_-) + 55V$	95		dB

For  $V_S = (V_+) - (V_-) = 2.7V$  to  $40V$  ( $\pm 1.35V$  to  $\pm 20V$ ) at  $T_A = 25^\circ C$ ,  $V_{REF} = V_S / 2$ ,  $G = 1/10$ ,  $R_L = 10k\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = (V_{IN+} + V_{IN-}) / 2 = V_S / 2$ ,  $V_{IN} = (V_{IN+} - V_{IN-}) = 0V$  and  $V_{OUT} = V_S / 2$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
CMRR DC	Common-mode rejection ratio, RTO	$9V \leq V_S \leq 40V$	$V_{CM} = (V_-) - 40V$ to $(V_-) + 85V$	95	106		dB
<b>NOISE VOLTAGE</b>							
$e_{NI}$	Output voltage noise density	$V_S = 40V$	$f = 1kHz$		145		nV/ $\sqrt{Hz}$
			$f = 10kHz$		155		
$E_{NI}$	Output voltage noise		$f_B = 0.1Hz$ to $10Hz$		9		$\mu V_{PP}$
			$f_B = 0.1Hz$ to $150kHz$		400		$\mu V_{PP}$
<b>GAIN</b>							
GE	Gain error <sup>(2)</sup>	$V_{REF} = V_{MID}$	$V_O = (V_-) + 0.15V$ to $(V_+) - 0.15V$		$\pm 0.003$	$\pm 0.05$	%
	Gain drift vs temperature <sup>(2)</sup>		$T_A = -40^\circ C$ to $125^\circ C$			$\pm 5$	ppm/ $^\circ C$
<b>OUTPUT</b>							
$V_{OH}$	Positive and negative rail headroom	$V_S = 40V$ , $V_{REF} = V_S$ , $R_L = 10k\Omega$ to $V_{MID}$			80	150	mV
$V_{OL}$		$V_S = 40V$ , $V_{REF} = V_S$ , $R_L = 2k\Omega$ to $V_{MID}$			400	650	mV
$C_L$ Drive	Load capacitance drive	$V_O = 100mV$ step, Overshoot < 20%			200		pF
$Z_O$	Closed-loop output impedance	$f = 10kHz$			150		$\Omega$
$I_{SC}$	Short-circuit current	$V_S = 40V$			$\pm 50$		mA
<b>FREQUENCY RESPONSE</b>							
BW	Bandwidth, -3dB	$V_{IN} = 10mV_{pk-pk}$			250		kHz
THD + N	Total harmonic distortion + noise	$V_S = 40V$ , $V_{REF} = 2.5V$ , $V_O = 5V_{PP}$ , $R_L = 100k\Omega$ $f = 1kHz$ , 80kHz measurement BW			0.03		%
EMIRR	Electro-magnetic interference rejection ratio	$f = 1GHz$ , $V_{IN\_EMIRR} = 100mV$			105		dB
SR	Slew rate	$V_S = 40V$ , $V_O = 1V$ step			0.22		V/ $\mu s$
$t_s$	Settling time	To 0.1%, $V_S = 40V$ , $V_{STEP} = 1V$ , $C_L = 10pF$			9.5		$\mu s$
$t_s$	Settling time	To 0.01%, $V_S = 40V$ , $V_{STEP} = 1V$ , $C_L = 10pF$			12		$\mu s$
$t_s$	Settling time	To 0.1%, $V_S = 40V$ , $V_{STEP} = 5V$ , $C_L = 10pF$			25		$\mu s$
$t_s$	Settling time	To 0.01%, $V_S = 40V$ , $V_{STEP} = 5V$ , $C_L = 10pF$			28		$\mu s$
	Overload recovery	$V_S = 2.7V$ , $V_{IN-} = 0V$ , $V_{IN+} = 85V$ , and $V_{REF} = V_S / 2$			7.5		$\mu s$
<b>REFERENCE INPUT</b>							
REF - $V_{IN}$	Input voltage range	$V_S = 40V$ , $V_{REF} = V_{MID}$		(V-)		(V+)	V
REF - G	Reference gain to output				1		V/V
REF - GE	Reference gain error <sup>(2)</sup>	$V_S = 40V$			$\pm 0.002$	$\pm 0.1$	%
<b>POWER SUPPLY</b>							
$V_S$	Power-supply voltage	Dual-supply		$\pm 1.35$		$\pm 20$	V
$I_Q$	Quiescent current	$V_S = 2.7V$			60		$\mu A$
$I_Q$	Quiescent current	$V_S = 40V$			65	80	$\mu A$
		$V_S = 40V$	$T_A = -40^\circ C$ to $125^\circ C$			85	

- (1) Offset drifts are uncorrelated.  
(2) Minimum and maximum values are specified by characterization.

## 6.7 Electrical Characteristics - INA600F

For  $V_S = (V_+) - (V_-) = 2.7V$  to  $40V$  ( $\pm 1.35V$  to  $\pm 20V$ ) at  $T_A = 25^\circ C$ ,  $V_{REF} = V_S / 2$ ,  $G = 1/36$ ,  $R_L = 10k\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = (V_{IN+} + V_{IN-}) / 2 = V_S / 2$ ,  $V_{IN} = (V_{IN+} - V_{IN-}) = 0V$  and  $V_{OUT} = V_S / 2$  (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>OFFSET</b>					

For  $V_S = (V_+) - (V_-) = 2.7V$  to  $40V$  ( $\pm 1.35V$  to  $\pm 20V$ ) at  $T_A = 25^\circ C$ ,  $V_{REF} = V_S / 2$ ,  $G = 1/36$ ,  $R_L = 10k\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = (V_{IN+} + V_{IN-}) / 2 = V_S / 2$ ,  $V_{IN} = (V_{IN+} - V_{IN-}) = 0V$  and  $V_{OUT} = V_S / 2$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS		MIN	TYP	MAX	UNIT
$V_{OSO}$	Offset voltage, RTO	$V_S = 2.7V$ and $40V$	$T_A = 25^\circ C$		$\pm 0.4$	$\pm 2.0$	mV
	Offset voltage over $T$ , RTO		$T_A = -40^\circ C$ to $125^\circ C$			$\pm 2.4$	mV
	Offset temp drift, RTO <sup>(1)</sup>		$T_A = -40^\circ C$ to $125^\circ C$		$\pm 0.8$	$\pm 4.0$	$\mu V/^\circ C$
PSRR	Power-supply rejection ratio	$V_S = 4V$ to $40V$	$T_A = 25^\circ C$		4	20	$\mu V/V$
PSRR	Power-supply rejection ratio	$V_S = 2.7V$ to $40V$	$T_A = 25^\circ C$		5	25	$\mu V/V$
<b>INPUT IMPEDANCE</b>							
$R_{IN-DM}$	Differential Resistance	$V_S = 4.5V$ to $40V$			2400		k $\Omega$
$R_{IN-CM}$	Common-mode Resistance	$V_S = 2.7V$ to $4.5V$			610		k $\Omega$
$V_{CM}$	Input common-mode Range	$V_S = 2.7V$		$(V_-) - 20$		$(V_-) + 30$	V
<b>INPUT VOLTAGE</b>							
$V_{CM}$	Input common-mode Range	$V_S = 4.5V$ to $40V$		$(V_-) - 40$		$(V_-) + 85$	V
CMRR DC	Common-mode rejection ratio, RTO	$2.7V \leq V_S < 4.5V$	$V_{CM} = (V_-) - 20V$ to $(V_-) + 30V$	106			dB
CMRR DC	Common-mode rejection ratio, RTO	$4.5V \leq V_S \leq 40V$	$V_{CM} = (V_-) - 40V$ to $(V_-) + 85V$	106	117		dB
<b>NOISE VOLTAGE</b>							
$e_{NI}$	Output voltage noise density	$V_S = 40V$	$f = 1kHz$		70		$nV/\sqrt{Hz}$
			$f = 10kHz$		85		
$E_{NI}$	Output voltage noise		$f_B = 0.1Hz$ to $10Hz$		5.5		$\mu V_{PP}$
			$f_B = 0.1Hz$ to $150kHz$		200		$\mu V_{PP}$
<b>GAIN</b>							
GE	Gain error <sup>(2)</sup>	$V_{REF} = V_{MID}$	$V_O = (V_-) + 0.15V$ to $(V_+) - 0.15V$		$\pm 0.003$	$\pm 0.05$	%
	Gain drift vs temperature <sup>(2)</sup>		$T_A = -40^\circ C$ to $125^\circ C$			$\pm 5$	ppm/ $^\circ C$
<b>OUTPUT</b>							
$V_{OH}$	Positive and negative rail headroom	$V_S = 40V$ , $V_{REF} = V_S$ , $R_L = 10k\Omega$ to $V_{MID}$			80	150	mV
$V_{OL}$		$V_S = 40V$ , $V_{REF} = V_S$ , $R_L = 2k\Omega$ to $V_{MID}$			400	650	mV
$C_L$ Drive	Load capacitance drive	$V_O = 100mV$ step, Overshoot $< 20\%$			200		pF
$Z_O$	Closed-loop output impedance	$f = 10kHz$			120		$\Omega$
$I_{SC}$	Short-circuit current	$V_S = 40V$			$\pm 50$		mA
<b>FREQUENCY RESPONSE</b>							
BW	Bandwidth, $-3dB$	$V_{IN} = 10mV_{pk-pk}$			300		kHz
THD + N	Total harmonic distortion + noise	$V_S = 40V$ , $V_{REF} = 2.5V$ , $V_O = 1V_{PP}$ , $R_L = 100k\Omega$ $f = 1kHz$ , 80kHz measurement BW			0.03		%
EMIRR	Electro-magnetic interference rejection ratio	$f = 1GHz$ , $V_{IN\_EMIRR} = 100mV$			105		dB
SR	Slew rate	$V_S = 40V$ , $V_O = 1V$ step			0.14		V/ $\mu s$
$t_S$	Settling time	To 0.1%, $V_S = 40V$ , $V_{OUT\_STEP} = 1V$ , $C_L = 10pF$			12		$\mu s$
$t_S$	Settling time	To 0.01%, $V_S = 40V$ , $V_{OUT\_STEP} = 1V$ , $C_L = 10pF$			15		$\mu s$
$t_S$	Settling time	To 0.1%, $V_S = 40V$ , $V_{OUT\_STEP} = 2V$ , $C_L = 10pF$			18		$\mu s$
$t_S$	Settling time	To 0.01%, $V_S = 40V$ , $V_{OUT\_STEP} = 2V$ , $C_L = 10pF$			22		$\mu s$
	Overload recovery	$V_S = 2.7V$ , $V_{IN-} = 0V$ , $V_{IN+} = 85V$ , and $V_{REF} = V_S / 2$			7.5		$\mu s$
<b>REFERENCE INPUT</b>							
REF - $V_{IN}$	Input voltage range	$V_S = 40V$ , $V_{REF} = V_{MID}$		$(V_-)$		$(V_+)$	V



For  $V_S = (V_+ - V_-) = 2.7V$  to  $40V$  ( $\pm 1.35V$  to  $\pm 20V$ ) at  $T_A = 25^\circ C$ ,  $V_{REF} = V_S / 2$ ,  $G = 1/36$ ,  $R_L = 10k\Omega$  connected to  $V_S / 2$ ,  $V_{CM} = (V_{IN+} + V_{IN-}) / 2 = V_S / 2$ ,  $V_{IN} = (V_{IN+} - V_{IN-}) = 0V$  and  $V_{OUT} = V_S / 2$  (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
REF - G	Reference gain to output			1		V/V
REF - GE	Reference gain error <sup>(2)</sup>	$V_S = 40V$		$\pm 0.002$	$\pm 0.1$	%
<b>POWER SUPPLY</b>						
$V_S$	Power-supply voltage	Dual-supply	$\pm 1.35$		$\pm 20$	V
$I_Q$	Quiescent current	$V_S = 2.7V$		60		$\mu A$
$I_Q$	Quiescent current	$V_S = 40V$		65	80	$\mu A$
		$V_S = 40V$ $T_A = -40^\circ C$ to $125^\circ C$			85	

(1) Offset drifts are uncorrelated.

(2) Minimum and maximum values are specified by characterization.

## 7 Detailed Description

### 7.1 Overview

INA600 is a voltage sensing difference amplifier with precision matched resistors that offer attenuating gain options. The precision matched integrated resistors saves BOM costs and board space by removing the need for precise and low tolerance external resistors. The device achieves a maximum gain error of  $\pm 0.05\%$ , and a maximum gain drift of  $5\text{ppm}/^\circ\text{C}$  along with  $89\text{dB}$  of minimum common-mode rejection ratio ( $G = 1/5$ ). INA600 can be used in 8-bit system without any calibration. Further calibration of offset and gain error at a system level can improve system resolution and accuracy, enabling use in higher resolution ( $\geq 10$ -bit) systems.

High input impedance of  $>1\text{M}\Omega$  along with just  $65\mu\text{A}$  of quiescent current makes INA600 very useful in single cell battery monitoring applications. The device can handle up to  $-40\text{V}$  to  $85\text{V}$  of input voltage, attenuate the voltage down with great accuracy, and interface the voltage to the low voltage ADC while rejecting any common-mode errors such as ground bounce, switching ripples, and AC mains. Most of the errors including offset, offset drift, CMRR and noise are referred to the output so as to enable easy calculation of signal-to-noise ratio (SNR) and effective number of bits (ENOB) closer to the analog-to-digital converter (ADC).

INA600 is offered in six attenuating gain options across six variants. INA600A version offers the lowest attenuation gain option of  $1/5$ , while the INA600F offers the highest attenuation gain option of  $1/36$ . INA600 gain options are designed for level translation applications that interface with a wide variety of differential ( $\pm 24\text{V}$ ,  $\pm 12\text{V}$ ,  $\pm 10\text{V}$ ,  $\pm 5\text{V}$ , and so forth) and single-ended ( $0\text{V}$  to  $48\text{V}$ ,  $0\text{V}$  to  $24\text{V}$ ,  $0\text{V}$  to  $12\text{V}$ ,  $0\text{V}$  to  $10\text{V}$ ,  $0\text{V}$  to  $5\text{V}$ , and so forth) high voltage signals. These high voltage signals can be level translated into wide variety of low voltage ( $0\text{V}$  to  $5\text{V}$ ,  $0\text{V}$  to  $3.3\text{V}$ ,  $0\text{V}$  to  $2.5\text{V}$ , and so forth) ADC ranges. This can be useful in a variety of end equipments such as battery testers, solar string inverters, power tools, analog input modules, and battery energy storage systems where multiple high voltage signals and supply domains must be monitored. The device also has enough bandwidth ( $\geq 200\text{kHz}$ ) to directly drive low-speed ( $\leq 10\text{kps}$ ) ADCs.

The INA600 is designed for space-constrained applications such as robotics, power banks, and chargers, as the device can save valuable PCB area compared to the discrete implementation of difference amplifiers. For easy use in automotive and industrial applications, the device is available in standard, leaded packages such as SOT-23 and SC70.

### 7.2 Functional Block Diagram

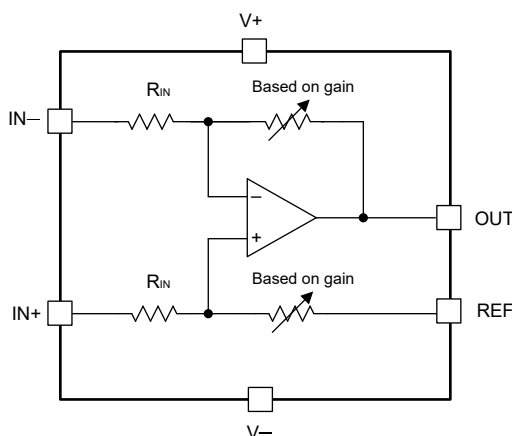


Figure 7-1. INA600 Simplified Internal Schematic

## 7.3 Feature Description

### 7.3.1 Gain Options and Resistors

The gain value of the INA600 is given by the ratio of feedback resistor and input resistor. The gain options are offered across different device variants as provided in [Table 7-1](#). While the typical value of input and feedback resistors are shown in the following table, it is important to note that these values can vary together by approximately  $\pm 15\%$  while maintaining tighter gain error (tolerance) numbers as specified in the [Electrical Characteristics](#) table.

**Table 7-1. Gain Selection**

DEVICE	VERSION	INPUT RESISTOR	FEEDBACK RESISTOR	GAIN
INA600	A	1.2M $\Omega$	240k $\Omega$	1/5
	B	1.2M $\Omega$	120k $\Omega$	1/10
	C	1.2M $\Omega$	100k $\Omega$	1/12
	D	1.2M $\Omega$	66.66k $\Omega$	1/18
	E	1.2M $\Omega$	50k $\Omega$	1/24
	F	1.2M $\Omega$	33.33k $\Omega$	1/36

#### 7.3.1.1 Gain Error and Drift

Gain error in the INA600 is dictated by the mismatch of the integrated precision resistors. Gain error is a tested parameter and maximum gain error is under or  $\pm 0.05\%$  for all gains. Gain drift of the INA600 is limited by the mismatch of the temperature coefficient of the integrated resistors. Since these integrated resistors are precision matched with low temperature coefficient resistors to begin with, the overall gain drift is much better in comparison to discrete implementation of the difference amplifiers built using external resistors. Note that the gain drift is not a tested parameter and the maximum gain drift is specified based on characterization results with sufficient guard-banding. Maximum gain error of  $\pm 0.02\%$  can be expected for inputs from the reference pin that sets output common-mode voltage.

### 7.3.2 Input Common-Mode Voltage Range

The INA600 difference-amplifier rejects the input common mode. This rejection capability is largely based on the matching of the internal resistors. Input voltage range of INA600 is extended well beyond the supply rails using a special design technique. This technique makes the input voltage range to not be overly limited by gain configuration or the supply voltage. Input voltage range spans from  $-40V$  below negative rail to  $85V$  above negative rail for supply voltages starting from  $9V$  across all gains. Below  $9V$ , TI recommends to refer to the valid input range values within the [Electrical Characteristics](#) table for the gain option of interest.

Common-mode rejection ratio values are referred to the output to enable easy error calculation with respect to ADC full scale. For example, an input common-mode error signal of  $1V$  applied to INA600A ( $G = 1/5$ ) at  $12V$  supply is attenuated to  $10\mu V$  at the output of INA600A, as the typical CMRR specification (referred to output) is  $100dB$  starting from a  $9V$  supply.

### 7.3.3 EMI Rejection

The INA600 uses integrated electromagnetic interference (EMI) filtering to reduce the effects of EMI from sources such as wireless communications and densely-populated boards with a mix of analog signal chain and digital components. EMI immunity can be improved with circuit design techniques; the INA600 benefits from these design improvements. Texas Instruments can accurately measure and quantify the immunity of an operational amplifier over a broad frequency spectrum extending from  $10MHz$  to  $6GHz$ . The [EMI Rejection Ratio of Operational Amplifiers](#) application note contains detailed information on the topic of EMIRR performance relating to op amps and is available for download from [www.ti.com](http://www.ti.com).

### 7.3.4 Typical Specifications and Distributions

Designers often have questions about a typical specification of an amplifier to design a more robust circuit. Due to natural variation in process technology and manufacturing procedures, every specification of an amplifier exhibits some amount of deviation from the ideal value, like the offset voltage of an amplifier. These deviations

often follow *Gaussian (bell curve)*, or *normal* distributions, and circuit designers can leverage this information to guard band their system, even when there is not a minimum or maximum specification in the *Electrical Characteristics* table.

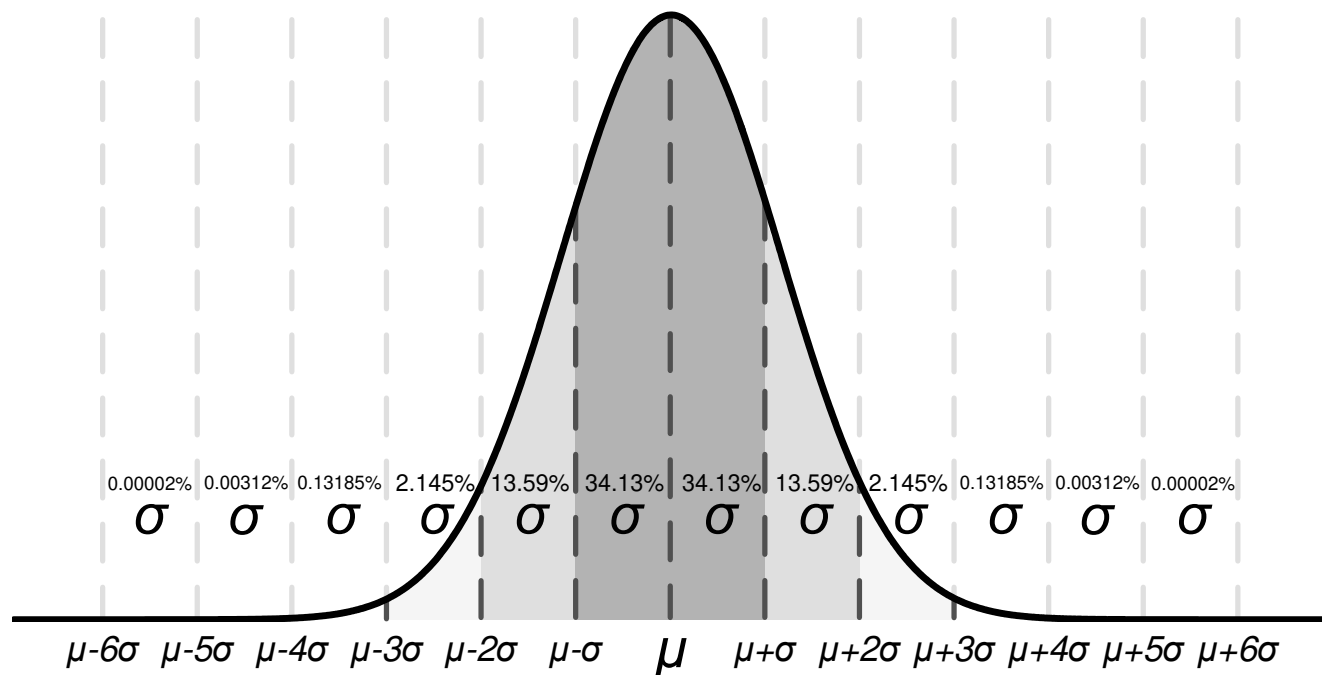


Figure 7-2. Ideal Gaussian Distribution

Figure 7-2 shows an example distribution, where  $\mu$ , or  $\mu$ , is the mean of the distribution, and where  $\sigma$ , or  $\sigma$ , is the standard deviation of a system. For a specification that exhibits this kind of distribution, approximately two-thirds (68.26%) of all units can be expected to have a value within one standard deviation, or one sigma, of the mean (from  $\mu - \sigma$  to  $\mu + \sigma$ ).

Depending on the specification, values listed in the *typical* column of the *Electrical Characteristics* table are represented in different ways. As a general rule, if a specification naturally has a nonzero mean (for example, like gain bandwidth), then the typical value is equal to the mean ( $\mu$ ). However, if a specification naturally has a mean near zero (like offset voltage), then the typical value is equal to the mean plus one standard deviation ( $\mu + \sigma$ ) to most accurately represent the typical value.

This chart can be used to calculate approximate probability of a specification in a unit; for example, the INA600A typical offset voltage is 1100 $\mu$ V, so 68.2% of all INA600A devices are expected to have an offset from  $-1100\mu$ V to  $+1100\mu$ V. At  $4\sigma$  ( $\pm 4400\mu$ V), 99.9937% of the distribution has an offset voltage less than  $\pm 4400\mu$ V, which means 0.0063% of the population is outside of these limits, which corresponds to about 1 in 15,873 units.

Specifications with a value in the minimum or maximum column are verified by TI, and units outside these limits are removed from production material. For example, the INA600A family has a maximum gain error of  $\pm 0.05\%$  at  $25^\circ\text{C}$ , and even though this corresponds to  $5\sigma$  (equals approximately 1 in 3.5 million units), which is extremely unlikely, TI verifies that any unit with larger offset than  $\pm 0.05\%$  are removed from production material.

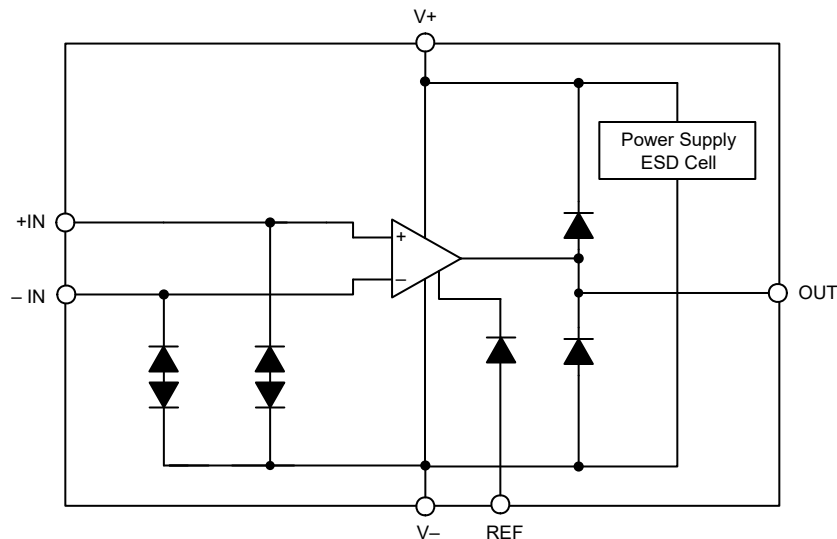
For specifications with no value in the minimum or maximum column, consider selecting a sigma value of sufficient guard band for the application, and design worst-case conditions using this value. A  $6\sigma$  value corresponds to about 1 in 500 million units, which is an extremely unlikely chance, and can be an option as a wide guard band to design a system around.

### 7.3.5 Electrical Overstress

Designers often ask questions about the capability of an operational amplifier to withstand electrical overstress. These questions tend to focus on the device inputs, but can involve the supply voltage pins or even the output pin. Each of these different pin functions have electrical stress limits determined by the voltage breakdown characteristics of the particular semiconductor fabrication process and specific circuits connected to the pin. Additionally, internal electrostatic discharge (ESD) protection is built into these circuits to protect them from accidental ESD events both before and during product assembly.

Having a good understanding of this basic ESD circuitry and the relevance to an electrical overstress event is helpful. Figure 7-3 shows the ESD circuits contained in the INA600 devices. On the input pins, the ESD protection circuitry involves local high impedance diode structures and do not route the ESD current to power supply ESD cell. On the output pin, there are reverse biased diodes to both the power supply rails. These diode structures route the ESD current back to the internal power supply lines, where there is an absorption power supply ESD cell internal to the difference amplifier. On the reference pin, the ESD protection is local and does not route current to the power supply ESD cell.

All of the ESD protection circuitry is intended to remain inactive during normal circuit operation.



**Figure 7-3. Equivalent Internal ESD Circuitry**

### 7.4 Device Functional Modes

The INA600 has only one functional mode. The device powers on, starts drawing quiescent current and is functional as long as the power supply voltages are in the recommended operating voltage range of 2.7V ( $\pm 1.35V$ ) to 40V ( $\pm 20V$ ). Operational temperature range of INA600 is from  $-40^{\circ}C$  to  $125^{\circ}C$ .

## 8 Application and Implementation

### Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes, as well as validating and testing their design implementation to confirm system functionality.

### 8.1 Application Information

#### 8.1.1 Reference Pin

The output voltage of the INA600 is developed with respect to the voltage on the reference pin (REF). Often in dual-supply operation, REF pin connects to the system ground. However, in single-supply operation, offsetting the output signal to a precise mid-supply level is useful and required (for example, 2.5V in a 5.0V supply environment). To accomplish this level shift, a voltage source must be connected to the REF pin to level-shift the output so that the INA can drive a single-supply ADC. This is accomplished using an external reference buffer configured in unity gain, voltage follower configuration as shown in [Figure 8-1](#).

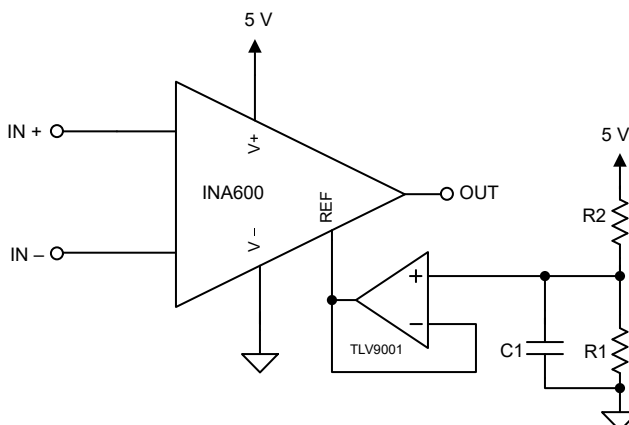


Figure 8-1. INA600 with External Reference Buffer

## 8.2 Typical Applications

### 8.2.1 48V Battery Monitoring Using Difference Amplifier

The INA600 is an integrated difference amplifier that processes large differential voltages while simultaneously rejecting larger common-mode voltages. The device offers a low power consumption of 65 $\mu$ A (typical) and has a smaller form factor.

With the specifications above, the device is a good fit for applications using 48V batteries such as robotics, power tools and so forth. While, battery monitoring ICs are often used to perform sophisticated functions including cell balancing, protection, voltage and current sensing and so forth, these systems still require basic monitoring of battery voltages, internal DC bus voltages, and load voltages when driving various motors using control-loops. In these scenarios, the amplifier-based monitoring application shown below can be used.

Figure 8-2 shows an example circuit that monitors a 48V battery voltage and interfaces the voltage to an ADC that is powered using a 5V power supply. The main advantage for using difference amplifiers in this application is the elimination of ground bounce, which is a common-mode signal, when measuring the battery voltage. These ground bounce signals, when not rejected, are capable of causing errors in the range of few milli-volts to tens or hundreds of milli-volts.

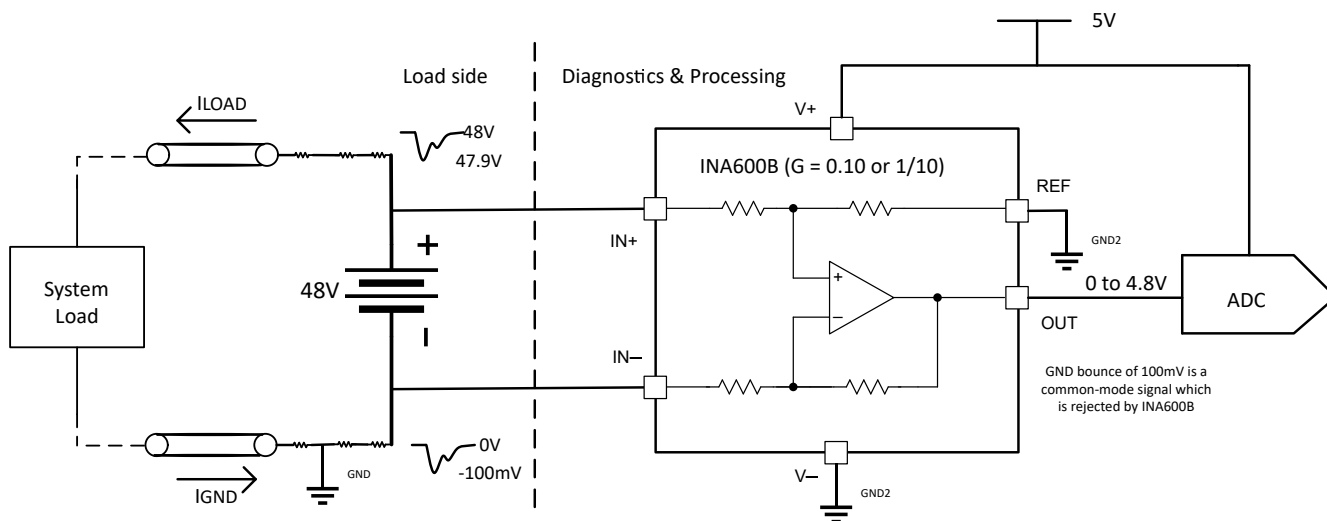


Figure 8-2. 48V Battery Monitoring Circuitry

### 8.2.1.1 Design Requirements

For this application, the design requirements are as provided in [Table 8-1](#).

**Table 8-1. Design Requirements**

DESCRIPTION	VALUE
Battery voltage	$V_{BAT} = 48V$
Supply voltage	$V_S = 5V$
Full-scale range of ADC	$V_{ADC(fs)} = V_{OUT} = 5V$
Quiescent current	125 $\mu$ A
ADC Resolution	8 bits
Effective number of bis (ENOB)	7.5 bits
Common-mode rejection ratio	80dB or a factor of 10000

### 8.2.1.2 Detailed Design Procedure

This section provides basic calculations for the INA600B difference amplifier with respect to the given design requirements.

Firstly, the 48V battery voltage must be attenuated and interfaced to ADC reference voltage of 5V. This requires a  $G = 1/10$  or 0.10V/V and therefore the INA600B is chosen for the application.

$$\text{Gain} = \frac{V_{ADC}}{V_{BAT}} = \frac{5}{48} \text{ is approximately } 0.10 \quad (1)$$

The maximum common-mode range of INA600 in a gain of 1/10 at 5V supply is given to be  $(V_-) + 55V$  from the INA600B [Electrical Characteristics](#) table.

This is well within the requirements for sensing 48V battery voltage and the common-mode rejection ratio (CMRR) referred to output is a minimum of 95dB as per INA600B [Electrical Characteristics](#) table. This corresponds to a attenuation factor of  $\frac{1}{56234}$ . This helps attenuate the 100mV common-mode error shown in the [Figure 8-2](#) to just under 2 $\mu$ V.

When referring to the INA600B output, [Equation 2](#) calculates the common-mode error, RTO to approximately 2 $\mu$ V.

$$CM_{Err\_RTO} = \frac{100mV}{56231} \cong 2\mu V \quad (2)$$

Next, INA600B has input impedance of 1.2M $\Omega$  as per the [Electrical Characteristics](#) table. Assuming a full battery voltage of 48V, the input current through the resistor is calculated as:

$$I_{R_{IN}} = \frac{V_{BAT}}{R_{IN}} = \frac{48}{1.20M} = 40\mu A \quad (3)$$

This input current through the resistor adds to the amplifier quiescent current of 65 $\mu$ A resulting in a total current consumption of 105 $\mu$ A, which meets the design requirement of 125 $\mu$ A.

$$I_{total} = I_{R_{IN}} + I_Q \quad (4)$$

The next step is to calculate the other error sources in the application. Maximum gain error and offset error as per [Electrical Characteristics](#) table are 0.05% and 3.0mV for the Gain = 0.2V/V.

$$\text{Total Error} = \sqrt{(0.0005 \times 48)^2 + 0.0030^2} = 24.2mV \quad (5)$$

For an 8-bit, 5V ADC,  $V_{LSB}$  is calculated as:



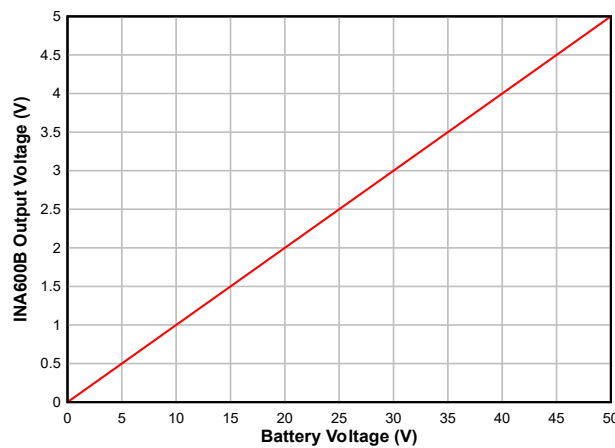
$$V_{LSB} = \frac{5}{2^8} = 19.5\text{mV} \quad (6)$$

The total error of 24.2mV that was calculated is approximately 1.25LSB of ADC full scale voltage of 5V and hence achieves almost 8 bits (approximately 7.998) of ENOB, comfortably meeting the requirement of 7.5 bits.

Note that the errors across temperature are not calculated here but can be easily included in the error analysis based on the drift specifications provided in the [Electrical Characteristics](#) table as per the temperature requirements of the application. These drift errors and noise often do not heavily affect the performance at 8-bit accuracy levels. Finally, calibration of offset and gain error can improve the accuracy beyond 10 to 12 bits as these factors can be the major sources of error in the application.

### 8.2.1.3 Application Curves

The following typical characteristic curve is for the circuit in [Figure 8-2](#).



**Figure 8-3. Battery Input Voltage vs INA600B Output Voltage**

## 8.3 Power Supply Recommendations

The nominal performance of the INA600 is specified with a midsupply reference voltage from  $\pm 1.35$  (2.7V) to  $\pm 20\text{V}$  (40V). The device also operates using non-midsupply reference voltages with good performance. Many specifications apply from  $-40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ . The [Electrical Characteristics](#) table presents parameters that can exhibit significant variance due to operating voltage or temperature.

TI highly recommends to add low-ESR ceramic bypass capacitors ( $C_{BYP}$ ) between each supply pin and ground. Only one  $C_{BYP}$  is sufficient for single supply operation. Place the  $C_{BYP}$  as close to the device as possible to reduce coupling errors from noisy or high-impedance power supplies. Ensure the power supply trace routes through  $C_{BYP}$  before reaching the amplifier power supply terminals. For more information, see [Layout Guidelines](#).

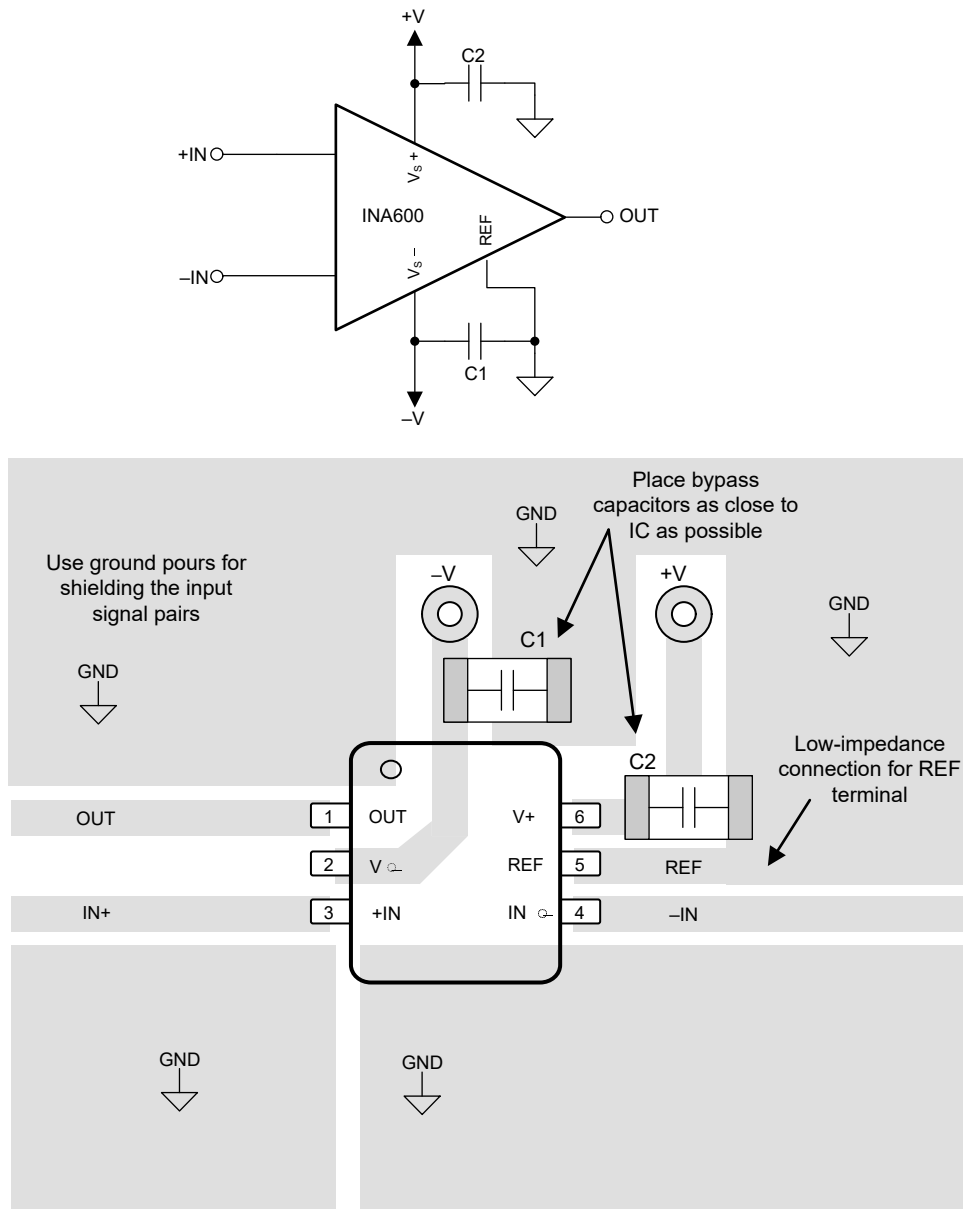
## 8.4 Layout

### 8.4.1 Layout Guidelines

Attention to good layout practices is always recommended. For best operational performance of the device, use the following PCB layout practices:

- Ensure that both input paths are well-matched for source impedance and capacitance to avoid converting common-mode signals into differential signals.
- Use bypass capacitors to reduce the coupled noise by providing low-impedance power sources local to the analog circuitry.
  - Connect low-ESR, 0.1µF ceramic bypass capacitors between each supply pin and ground, placed as close to the device as possible. A single bypass capacitor from V+ to ground is applicable for single-supply applications.
- Route the input traces as far away from the supply or output traces as possible to reduce parasitic coupling. If these traces cannot be kept separate, crossing the sensitive trace perpendicular is much better than crossing in parallel with the noisy trace.
- Place the external components as close to the device as possible.
- Keep the traces as short as possible.

### 8.4.2 Layout Example



**Figure 8-4. Example Schematic and Associated PCB Layout for DBV Package**

## 9 Device and Documentation Support

### 9.1 Device Support

#### 9.1.1 Development Support

- [SPICE-based analog simulation program — TINA-TI software folder](#)
- [Analog Engineers Calculator](#)

##### 9.1.1.1 PSpice® for TI

PSpice® for TI is a design and simulation environment that helps evaluate performance of analog circuits. Create subsystem designs and prototype solutions before committing to layout and fabrication, reducing development cost and time to market.

### 9.2 Documentation Support

#### 9.2.1 Related Documentation

For related documentation see the following:

- Texas Instruments, [EMI Rejection Ratio of Operational Amplifiers application note](#)

### 9.3 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on [ti.com](#). Click on *Notifications* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 9.4 Support Resources

TI E2E™ [support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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### 9.5 Trademarks

TI E2E™ is a trademark of Texas Instruments.

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### 9.6 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

### 9.7 Glossary

[TI Glossary](#) This glossary lists and explains terms, acronyms, and definitions.

## 10 Revision History

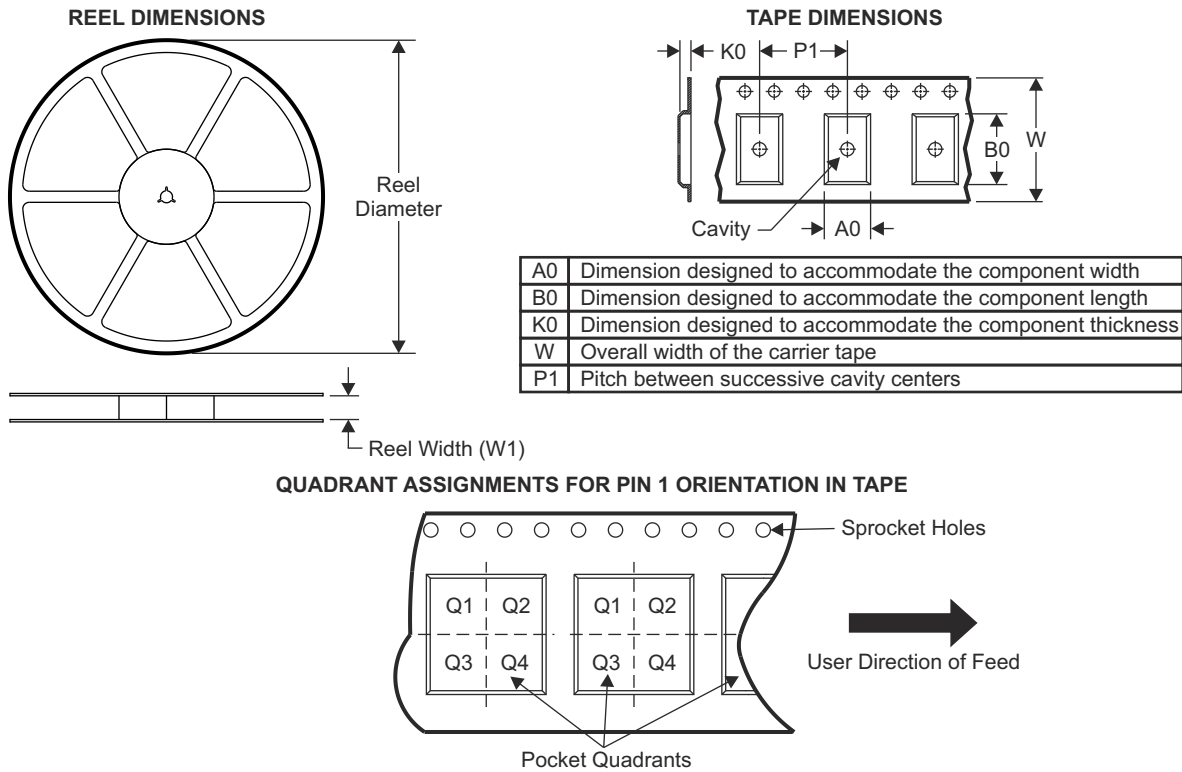
NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

DATE	REVISION	NOTES
July 2025	*	Initial Release

## 11 Mechanical, Packaging, and Orderable Information

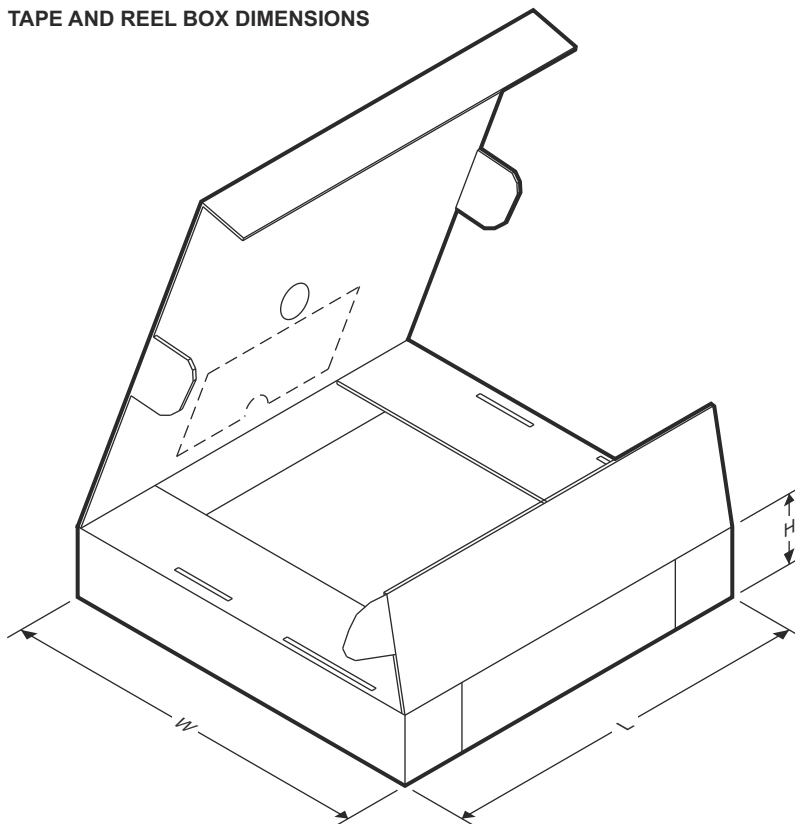
The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

### 11.1 Tape and Reel Information



Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
PINA600AIDBVR	SOT-23	DBV	6	3000	180	8.4	3.2	3.2	1.4	4	8	Q3
PINA600BIDBVR	SOT-23	DBV	6	3000	180	8.4	3.2	3.2	1.4	4	8	Q3
PINA600FIDBVR	SOT-23	DBV	6	3000	180	8.4	3.2	3.2	1.4	4	8	Q3

# TAPE AND REEL BOX DIMENSIONS



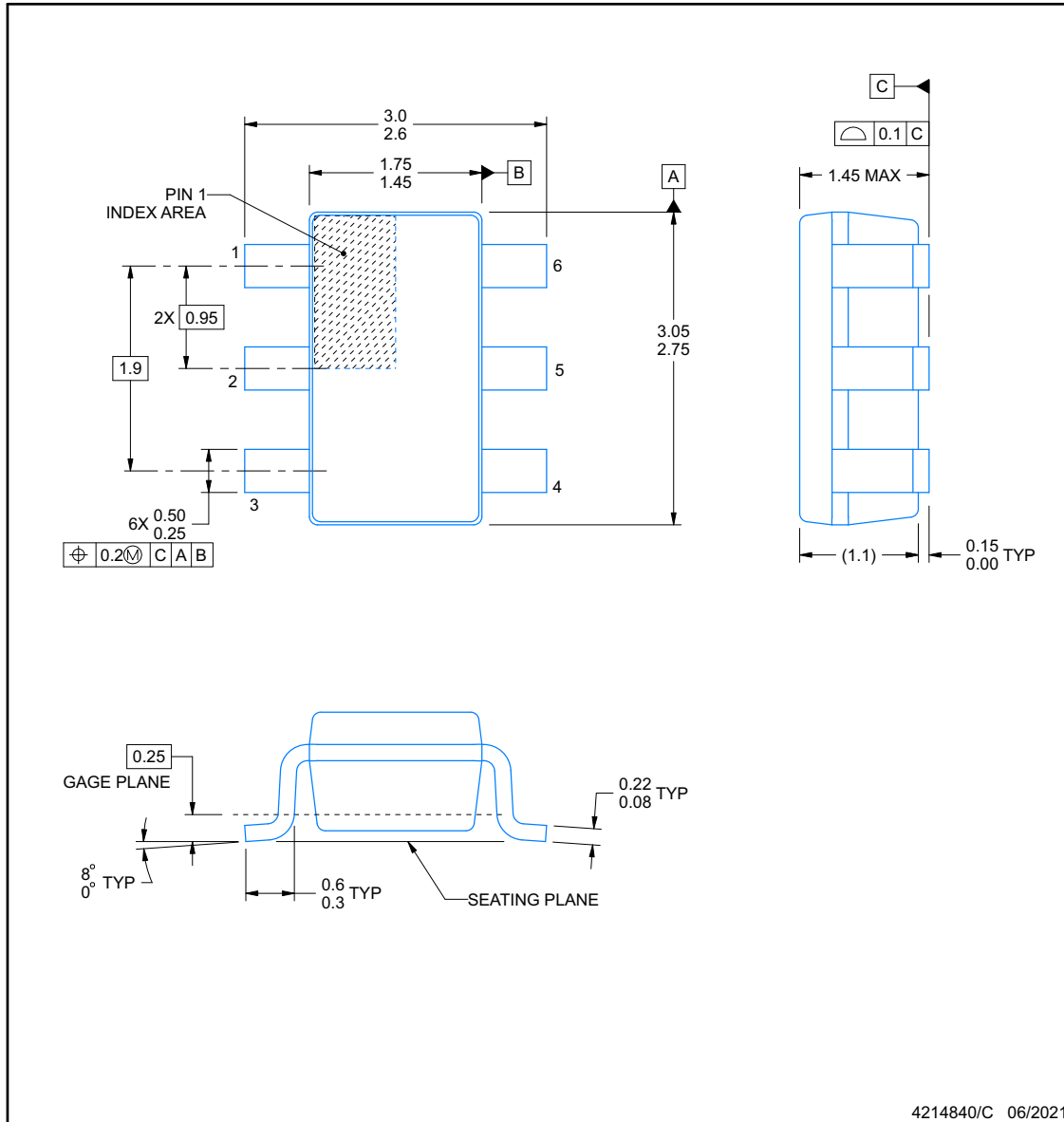
Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
PINA600AIDBVR	SOT-23	DBV	6	3000	210	185	35
PINA600BIDBVR	SOT-23	DBV	6	3000	210	185	35
PINA600FIDBVR	SOT-23	DBV	6	3000	210	185	35



**DBV0006A**

**PACKAGE OUTLINE**  
**SOT-23 - 1.45 mm max height**

SMALL OUTLINE TRANSISTOR



**NOTES:**

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. Body dimensions do not include mold flash or protrusion. Mold flash and protrusion shall not exceed 0.25 per side.
4. Leads 1,2,3 may be wider than leads 4,5,6 for package orientation.
5. Reference JEDEC MO-178.

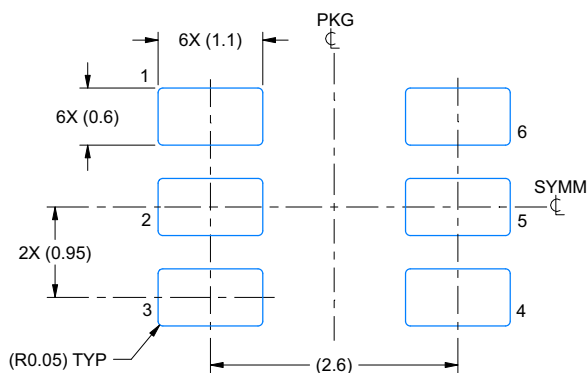
## EXAMPLE BOARD LAYOUT

**DBV0006A**

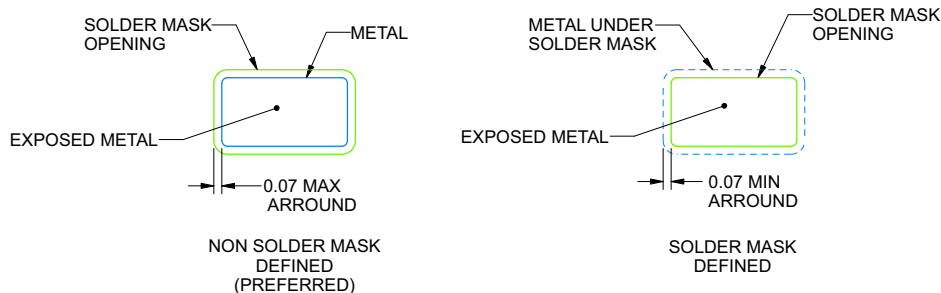
**SOT-23 - 1.45 mm max height**

SMALL OUTLINE TRANSISTOR

ADVANCE INFORMATION



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:15X



SOLDER MASK DETAILS

4214840/C 06/2021

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

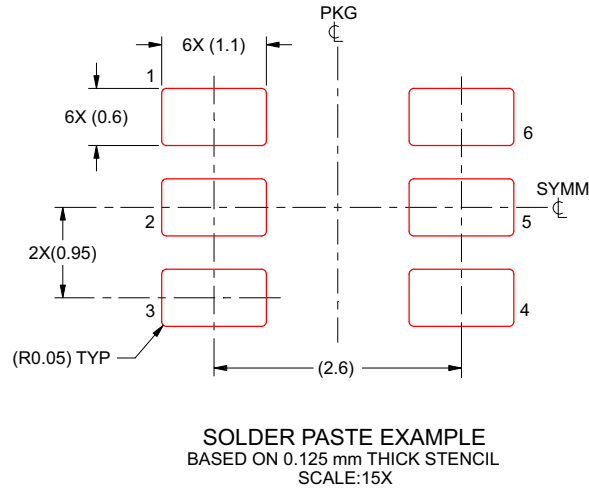


## EXAMPLE STENCIL DESIGN

**DBV0006A**

**SOT-23 - 1.45 mm max height**

SMALL OUTLINE TRANSISTOR



4214840/C 06/2021

NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.

## PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package   Pins	Package qty   Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
<a href="#">XINA600AIDBVR</a>	Active	Preproduction	SOT-23 (DBV)   6	3000   LARGE T&R	-	Call TI	Call TI	-40 to 125	
<a href="#">XINA600BIDBVR</a>	Active	Preproduction	SOT-23 (DBV)   6	3000   LARGE T&R	-	Call TI	Call TI	-40 to 125	
<a href="#">XINA600FIDBVR</a>	Active	Preproduction	SOT-23 (DBV)   6	3000   LARGE T&R	-	Call TI	Call TI	-40 to 125	

<sup>(1)</sup> **Status:** For more details on status, see our [product life cycle](#).

<sup>(2)</sup> **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

<sup>(3)</sup> **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

<sup>(4)</sup> **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

<sup>(5)</sup> **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

<sup>(6)</sup> **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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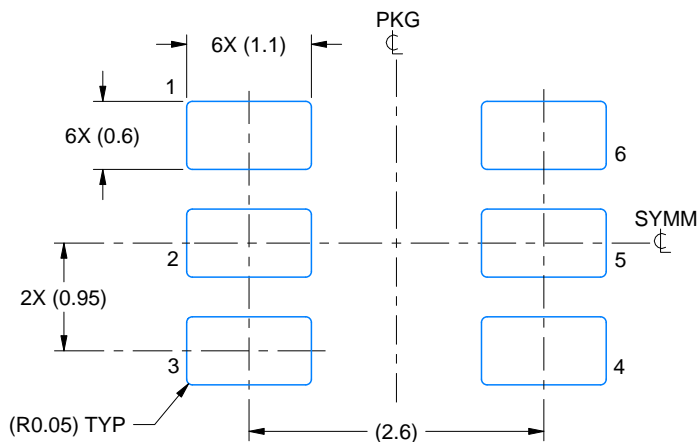


# EXAMPLE BOARD LAYOUT

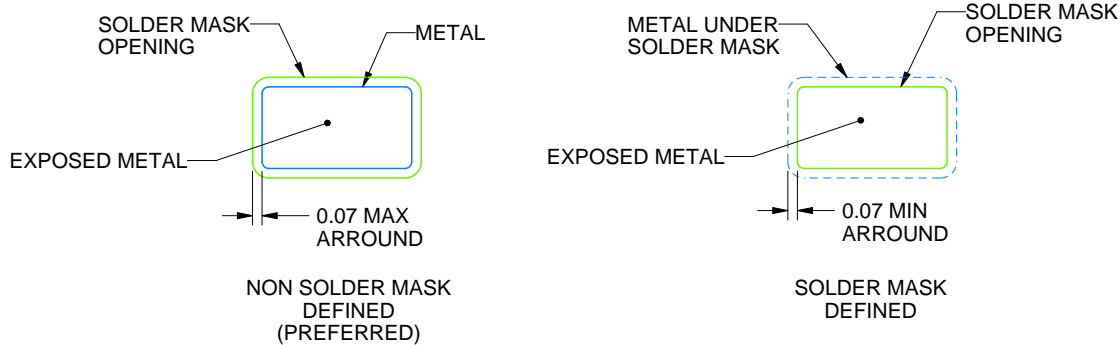
DBV0006A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE  
EXPOSED METAL SHOWN  
SCALE:15X



SOLDER MASK DETAILS

4214840/G 08/2024

NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

## EXAMPLE STENCIL DESIGN

DBV0006A

SOT-23 - 1.45 mm max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 mm THICK STENCIL  
SCALE:15X

4214840/G 08/2024

NOTES: (continued)

8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.

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