

# DRV8816 DMOS Dual 1/2-H-Bridge Motor Drivers

## 1 Features

- H-Bridge Motor Driver Individual
  - Drives a DC Motor or Other Loads
  - Low  $R_{DS(on)}$  MOSFETs (0.4- $\Omega$  TYP)
- Low-Power Sleep Mode
- 100% PWM Supported
- 8- to 38-V Operating Supply Voltage Range
- Thermally Enhanced Surface Mount Package
- Configurable Overcurrent Limit
- Protection Features
  - VBB Undervoltage Lockout (UVLO)
  - Charge Pump Undervoltage (CPUV)
  - Overcurrent Protection (OCP)
  - Short-to-Supply Protection (STS)
  - Short-to-Ground Protection (STG)
  - Overtemperature Warning (OTW)
  - Overtemperature Shutdown (OTS)
  - Fault Condition Indication Pin (nFAULT)

## 2 Applications

- Printers
- Industrial Automation
- Robotics
- Motorized Levers

## 3 Description

The DRV8816 provides a versatile power driver solution with two independent 1/2-H bridge drivers. The device can drive one brushed DC motor or one winding of a stepper motor, as well as other devices like solenoids. A simple INx/ENx interface allows easy interfacing to controller circuits.

The output stages use N-channel power MOSFETs configured as 1/2-H-bridges. The DRV8816 is capable of peak output currents up to  $\pm 2.8$  A and operating voltages up to 38 V. An internal charge pump generates needed gate drive voltages.

A low-power sleep mode is provided which shuts down internal circuitry to achieve very-low quiescent current draw. This sleep mode can be set using a dedicated nSLEEP pin.

Internal protection functions are provided for UVLO, charge pump fault, OCP, short-to-supply protection, short-to-ground protection, overtemperature warning, and overtemperature shutdown. Fault conditions are indicated through a nFAULT pin

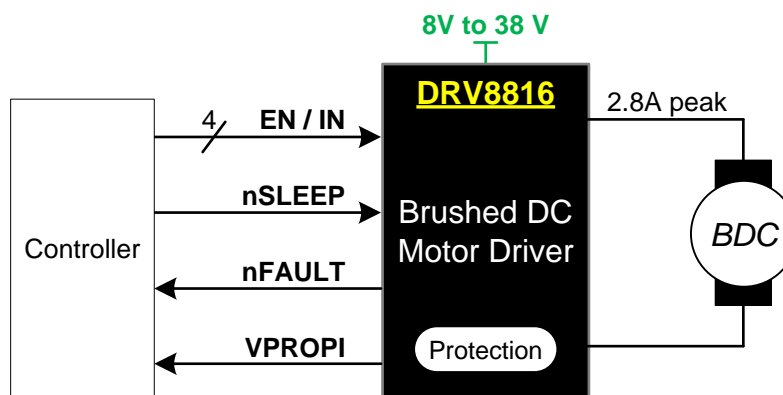
The DRV8816 is packaged in a 16-pin HTSSOP package with PowerPAD™ (Eco-friendly: RoHS & no Sb/Br)

### Device Information<sup>(1)</sup>

PART NUMBER	PACKAGE	BODY SIZE (NOM)
DRV8816	HTSSOP (16)	4.40 mm x 5.00 mm

(1) For all available packages, see the orderable addendum at the end of the data sheet.

### Simplified Schematic



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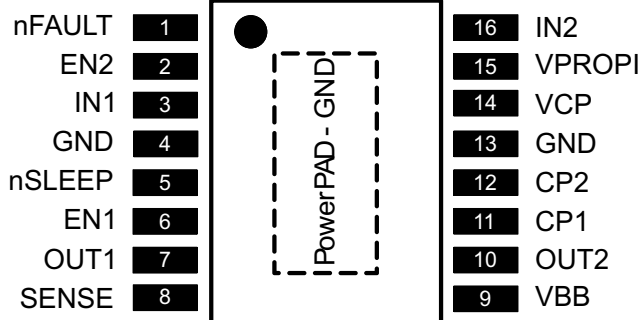
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## 4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

<b>Changes from Revision B (October 2014) to Revision C</b>	<b>Page</b>
• Updated description for nFAULT pin. ....	3
• Removed the $R_{VPROPI}$ component.....	3
• Changed the <i>Functional Block Diagram</i> image .....	8
• Changed the <i>Typical Application</i> image .....	13
• Changed the <i>Layout Example</i> image .....	18
<b>Changes from Original (September 2013) to Revision A</b>	<b>Page</b>
• Added <i>Handling Rating</i> table, <i>Feature Description</i> section, <i>Device Functional Modes</i> , <i>Application and Implementation</i> section, <i>Power Supply Recommendations</i> section, <i>Layout</i> section, <i>Device and Documentation Support</i> section, and <i>Mechanical, Packaging, and Orderable Information</i> section .....	4
• Updated Figure 5.....	12

## 5 Pin Configuration and Functions



**Pin Functions**

PIN		TYPE	DESCRIPTION	
NAME	NO.			
POWER AND GROUND				
CP1	11	PWR	Charge pump switching node	Connect a 0.1-μF X7R capacitor rated for VBB between CP1 and CP2
CP2	12	—		
GND	4, 13, PPAD	PWR	Device ground	Connect to system ground
VBB	9	PWR	Power supply input	Connect to main power supply. Bypass to GND with a 0.1-μF ceramic capacitor and a larger bulk capacitor rated for at least the VBB voltage
VCP	14	PWR	Charge pump output	Connect a 0.1-μF 16-V ceramic capacitor between VCP and VBB
CONTROL				
EN1	6	I	½-H bridge enable	Logic high enables ½-H bridge output; logic low puts the FETs in HI-Z; internal pull-down
EN2	2			
IN1	3	I	½-H bridge control	Logic high enables the high-side ½-H bridge FET; logic low enables the low side FET; internal pull-down
IN2	16			
nFAULT	1	O	Fault indication pin	Pulled logic low with fault condition; open-drain output requires an external pull-up. This output is indeterminate in sleep mode
nSLEEP	5	I	Device sleep mode	Pull logic low to put device into a low-power sleep mode; internal pull-down
OUTPUT				
OUT1	7	O	½-H bridge output	
OUT2	10	O	½-H bridge output	
SENSE	8	O	H-bridge low-side connect	Connect directly to GND or through a sense resistor to set OCP
VPROPI				
VPROPI	15	O	Current-proportional output	

**Table 1. External Components**

COMPONENT	PIN 1	PIN 2	RECOMMENDED
C <sub>VBB</sub>	VBB	GND	0.1-μF ceramic capacitor and a larger bulk capacitor rated for at least the VBB voltage
C <sub>VCP</sub>	VCP	VBB	0.1-μF 16-V ceramic capacitor
R <sub>nFAULT</sub>	VCC <sup>(1)</sup>	nFAULT	>1 kΩ resistor
R <sub>nSLEEP</sub>	VCC <sup>(1)</sup>	nSLEEP	If nSLEEP isn't actively controlled, use a pull-up resistor of less than 20 kΩ
R <sub>SENSE</sub>	SENSE	GND	Optional low-value resistor. If not used, connect SENSE pin directly to GND.

(1) VCC is not a pin on the DRV8816, but a VCC supply voltage pullup is required.

## 6 Specifications

### 6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	MAX	UNIT
V <sub>BB</sub>	Power supply voltage	−0.6	40	V
	Charge pump positive switching pin (CP2)	−0.6	V <sub>BB</sub> + 7	V
	Charge pump negative switching pin (CP1)	−0.6	V <sub>BB</sub>	V
	Digital pin voltage range (IN1, IN2, EN1, EN2, nSLEEP, nFAULT)	−0.3	7	V
	V <sub>BB</sub> to OUTx	−0.6	40	V
	OUTx to SENSE	−0.6	40	V
V <sub>(SENSE)</sub>	Sense voltage (SENSE) <sup>(2)</sup>	−0.5	1.0	V
	H-bridge output current (OUT1, OUT2, SENSE)	0	2.8	A
	V <sub>PROPI</sub> pin voltage range (V <sub>PROPI</sub> )	−0.3	3.6	V
T <sub>A</sub>	Operating ambient temperature	−40	85	°C
T <sub>J</sub>	Operating junction temperature	−40	190	°C
T <sub>stg</sub>	Storage temperature	−40	125	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) Transients of ±1 V for less than 25 ns are acceptable.

### 6.2 ESD Ratings

		VALUE	UNIT
V <sub>(ESD)</sub>	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000
		Charged-device model (CDM), per JEDEC specification JESD22-C101 <sup>(2)</sup>	±500

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

### 6.3 Recommended Operating Conditions

Power dissipation and thermal limits must be observed.

		MIN	MAX	UNIT
V <sub>BB</sub>	Power supply voltage	8	38	V
V <sub>I</sub>	Input pin voltage	0	5.5	V
f <sub>PWM</sub>	Applied PWM signal (IN1, IN2, EN1, EN2)		100	kHz
I <sub>OUT</sub>	H-bridge output current		2.8	A
T <sub>A</sub>	Ambient temperature	−40	85	°C

## 6.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		DRV8816	UNIT
		PWP (HTSSOP)	
		16 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance <sup>(2)</sup>	43.9	°C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance <sup>(3)</sup>	30.8	°C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance <sup>(4)</sup>	25.3	°C/W
ψ <sub>JT</sub>	Junction-to-top characterization parameter <sup>(5)</sup>	1.1	°C/W
ψ <sub>JB</sub>	Junction-to-board characterization parameter <sup>(6)</sup>	25	°C/W
R <sub>θJC(bot)</sub>	Junction-to-case (bottom) thermal resistance <sup>(7)</sup>	5.6	°C/W

- (1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, [SPRA953](#).
- (2) The junction-to-ambient thermal resistance under natural convection is obtained in a simulation on a JEDEC-standard, high-K board, as specified in JESD51-7, in an environment described in JESD51-2a.
- (3) The junction-to-case (top) thermal resistance is obtained by simulating a cold plate test on the package top. No specific JEDEC-standard test exists, but a close description can be found in the ANSI SEMI standard G30-88.
- (4) The junction-to-board thermal resistance is obtained by simulating in an environment with a ring cold plate fixture to control the PCB temperature, as described in JESD51-8.
- (5) The junction-to-top characterization parameter, ψ<sub>JT</sub>, estimates the junction temperature of a device in a real system and is extracted from the simulation data for obtaining θ<sub>JA</sub>, using a procedure described in JESD51-2a (sections 6 and 7).
- (6) The junction-to-board characterization parameter, ψ<sub>JB</sub>, estimates the junction temperature of a device in a real system and is extracted from the simulation data for obtaining θ<sub>JA</sub>, using a procedure described in JESD51-2a (sections 6 and 7).
- (7) The junction-to-case (bottom) thermal resistance is obtained by simulating a cold plate test on the exposed (power) pad. No specific JEDEC standard test exists, but a close description can be found in the ANSI SEMI standard G30-88.

## 6.5 Electrical Characteristics

over recommended operating conditions (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
<b>POWER SUPPLIES (VBB)</b>						
VBB	VBB operating voltage		8		38	V
I <sub>VBB</sub>	VBB operating supply current	f <sub>PWM</sub> < 50 kHz		6		mA
		Charge pump on, Outputs disabled		3.2		mA
I <sub>VBBQ</sub>	VBB sleep-mode supply current	nSLEEP = 0, T <sub>J</sub> = 25°C			10	μA
<b>CONTROL INPUTS (IN1, IN2, EN1, EN2, nSLEEP)</b>						
V <sub>IL</sub>	Input logic low voltage	IN1, IN2, EN1, EN2	0		0.8	V
V <sub>IH</sub>	Input logic high voltage	IN1, IN2, EN1, EN2	2		5.5	V
V <sub>IL</sub>	Input logic low voltage	nSLEEP	0		0.8	V
V <sub>IH</sub>	Input logic high voltage	nSLEEP	2.2		5.5	V
I <sub>IL</sub>	Input logic low current	IN1, IN2, EN2, nSLEEP		0		μA
I <sub>IH</sub>	Input logic high current	IN1, IN2, EN2, nSLEEP		25		μA
I <sub>IL</sub>	Input logic low current	EN1		0		μA
I <sub>IH</sub>	Input logic high current	EN1		100		μA
R <sub>PD</sub>	Pulldown resistance	IN1, IN2, EN2, nSLEEP		200		kΩ
		EN1		50		
<b>SERIAL AND CONTROL OUTPUT (nFAULT)</b>						
V <sub>OL</sub>	Output logic low voltage	I <sub>sink</sub> = 1 mA			0.4	V
<b>DMOS DRIVERS (OUT1, OUT2, SENSE)</b>						
R <sub>DS(on)</sub>	Output ON resistance	Source driver, I <sub>OUT</sub> = –2.8 A, T <sub>J</sub> = 25°C		0.48		Ω
		Source driver, I <sub>OUT</sub> = –2.8 A, T <sub>J</sub> = 125°C		0.74	0.85	
		Sink driver, I <sub>OUT</sub> = –2.8 A, T <sub>J</sub> = 25°C		0.35		
		Sink driver, I <sub>OUT</sub> = –2.8 A, T <sub>J</sub> = 125°C		0.52	0.7	
V <sub>TRIP</sub>	SENSE trip voltage	R <sub>SENSE</sub> between SENSE and GND		500		mV
V <sub>f</sub>	Body diode forward voltage	Source diode, I <sub>f</sub> = –2.8 A			1.4	V
		Sink diode, I <sub>f</sub> = 2.8 A			1.4	

## Electrical Characteristics (continued)

over recommended operating conditions (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
$t_{pd}$ OUTx propagation delay	From High-Z to High		70		ns
	From High-Z to Low		700 <sup>(1)</sup>		
	From High to High-Z		120		
	From High to Low		700		
	From Low to High-Z		350		
	From Low to High		350		
$t_{COD}$ Crossover delay			500		ns
DAGain VPROPI amplifier gain	Sense = 0.1 to 0.4 V		5		V/V
<b>PROTECTION CIRCUITS</b>					
$V_{UVLO}$ VBB UVLO	VBB rising		6.5	7.5	V
$V_{CPUV}$ VCP UVLO <sup>(2)</sup>	VBB rising; CPUV recovery		12	13.8	V
$I_{OCP}$ Overcurrent protection trip level		3			A
$t_{DEG}$ Overcurrent deglitch time			3.0		μs
$t_{OCP}$ Overcurrent retry time			1.6		ms
$T_{OTW}$ Thermal warning temperature	Die temperature $T_j$		160		°C
$T_{OTW\ HYS}$ Thermal warning hysteresis	Die temperature $T_j$		15		°C
$T_{OTS}$ Thermal shutdown temperature	Die temperature $T_j$		175		°C
$T_{OTS\ HYS}$ Thermal shutdown hysteresis	Die temperature $T_j$		15		°C

(1) If OUT2 is High, the typical time for OUT1 to go from High-Z to Low is 1700 ns.

(2) Whenever VCP is less than  $V_M + 10\text{ V}$ , a CPUV event occurs. This fault will be asserted whenever VBB is below 12 V. Note that the H-bridges will remain enabled until  $V_{BB} = V_{UVLO}$  even through nFAULT is pulled low.

## 6.6 Typical Characteristics

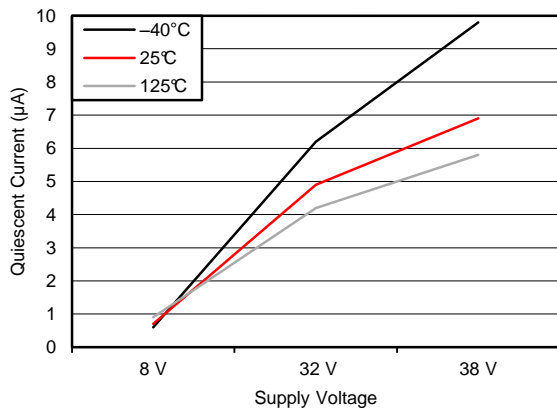


Figure 1.  $I_{VBBQ}$  vs VBB

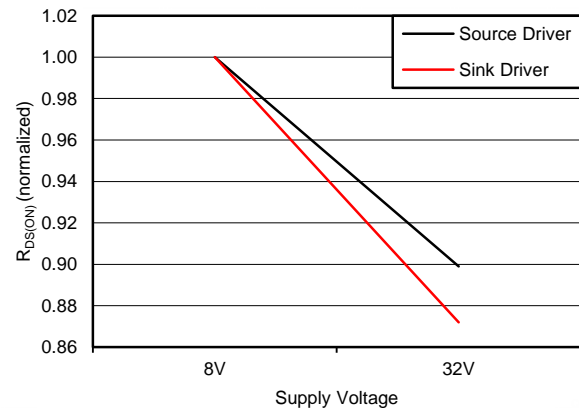
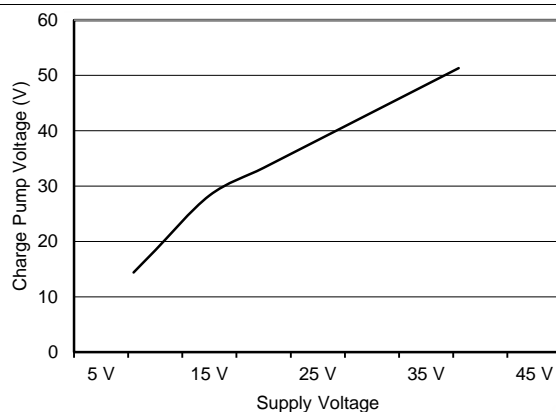


Figure 2.  $R_{DS(ON)}$  vs VBB (normalized to VBB = 8V)

## Typical Characteristics (continued)



**Figure 3. VCP vs VBB**

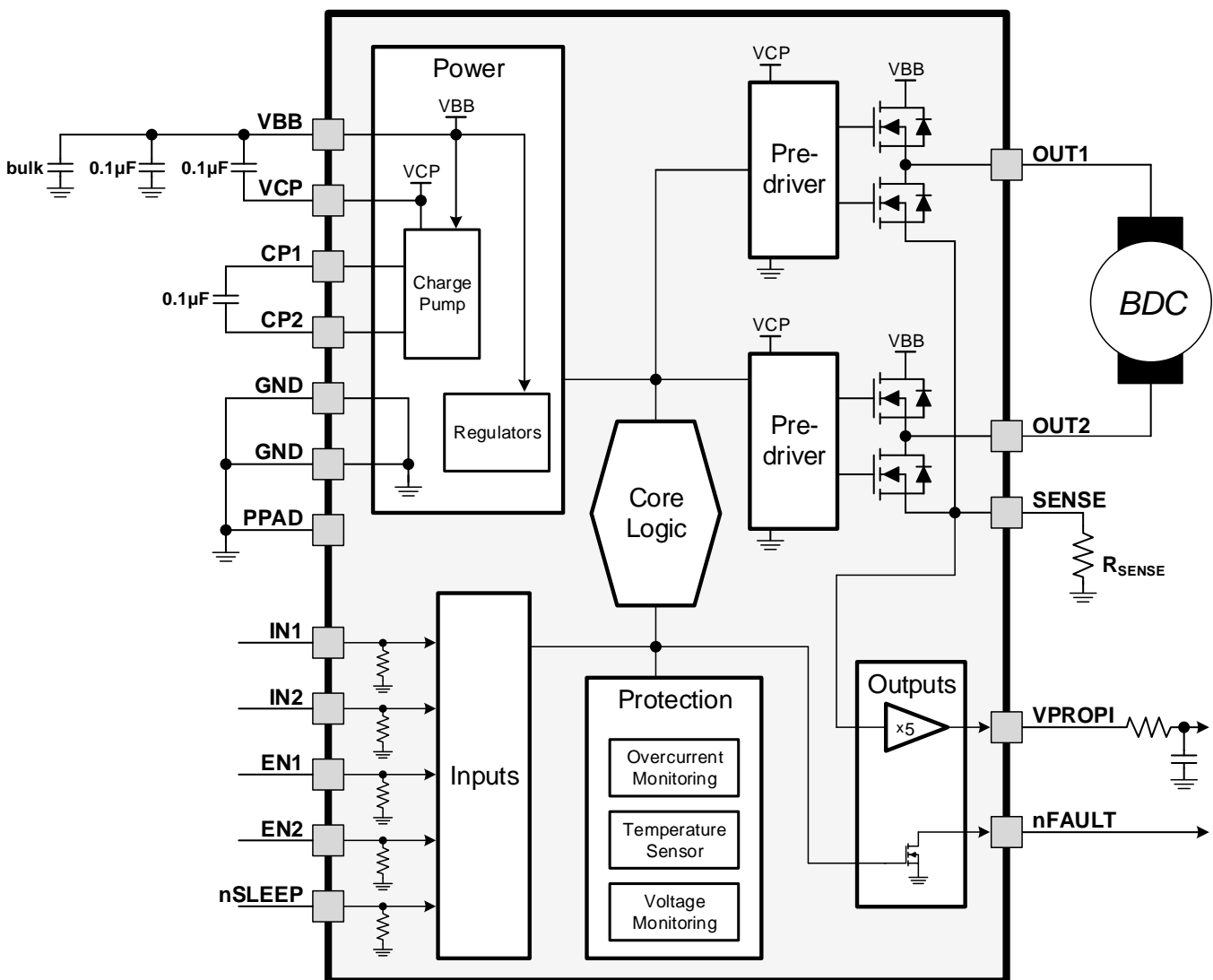
## 7 Detailed Description

### 7.1 Overview

The DRV8816 uses 4 CMOS inputs to control 2 high-voltage high-current outputs, while integrating protection features, fault reporting, a sleep mode, and current sensing. EN1 and IN1 control OUT1, and EN2 and IN2 control OUT2, according to Table 2. The device is designed to drive two independent loads or one brushed DC motor, as shown in Figure 4 and Table 3.

When an  $R_{SENSE}$  resistor is used, the DRV8816 will automatically disable itself if  $V_{SENSE}$  exceeds 500mV—this provides a user-programmable overcurrent threshold. The VPROPI output equals the sense voltage amplified by a factor of 5, and it can be used by a microcontroller to know the motor current, in order to Pulse-Width Modulate the DRV8816 inputs and regulate motor current.

### 7.2 Functional Block Diagram



### 7.3 Feature Description

#### 7.3.1 Bridge Control

The DRV8816 is controlled using separate enable and input pins for each ½-H-bridge.



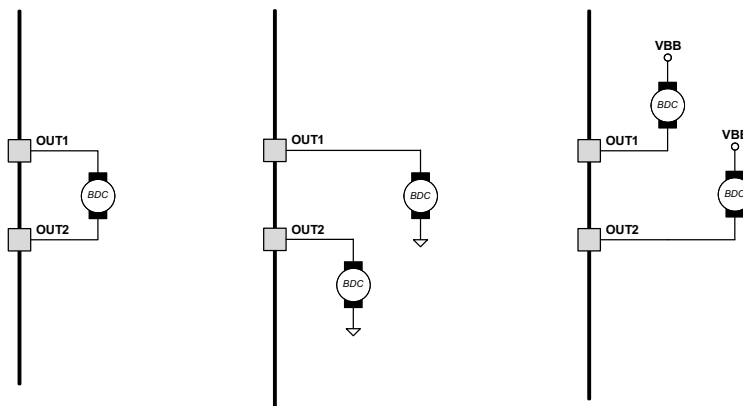
## Feature Description (continued)

Table 2 shows the logic for the DRV8816.

**Table 2. DRV8816 Logic**

ENx	INx	OUTx
0	X	Z
1	0	L
1	1	H

If a single DC motor is connected to the DRV8816, it is connected between the OUT1 and OUT2 pins as shown in Figure 4. Two DC motors may also be connected to the DRV8816. In this mode, it is not possible to reverse the direction of the motors; the motors will turn only in one direction. The connections are shown in Figure 4.



**Figure 4. Bridge Control**

Table 3 shows how motor operation for a single-brushed DC motor is controlled.

**Table 3. Motor Operation for a Single-Brushed DC Motor**

EN1	EN2	IN1	IN2	OUT1	OUT2	Operation
0	X	X	X	Z	X <sup>(1)</sup>	Off (coast)
X	0	X	X	X <sup>(1)</sup>	Z	Off (coast)
1	1	0	0	L	L	Brake
1	1	0	1	L	H	Reverse
1	1	1	0	H	L	Forward
1	1	1	1	H	H	Brake

(1) The Half-H bridges are independent; output state depends on ENx and INx.

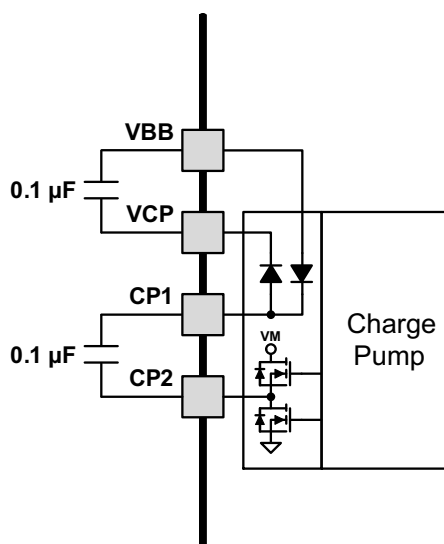
Table 4 shows how motor operation for dual-brushed DC motors is controlled.

**Table 4. Motor Operation for a Dual-Brushed DC Motor**

Motor connected to GND	ENx	INx	OUTx	Operation
	0	X	Z	Off (coast)
	1	0	L	Brake
	1	1	H	Forward
Motor connected to VBB	ENx	INx	OUTx	Operation
	0	X	Z	Off (coast)
	1	0	L	Forward
	1	1	H	Brake

### 7.3.2 Charge Pump

The charge pump is used to generate a supply above VBB to drive the source-side DMOS gates. A 0.1-μF ceramic monolithic capacitor should be connected between CP1 and CP2 for pumping purposes. A 0.1-μF ceramic monolithic capacitor should be connected between VCP and VBB to act as a reservoir to run the high-side DMOS devices. The VCP voltage level is internally monitored, and in the case of a fault condition, the outputs of the device are disabled.



**Figure 5. Charge Pump**

### 7.3.3 VPROPI

The VPROPI output is equal to approximately 5× the voltage present on the SENSE pin. VPROPI is meaningful only if there is a resistor connected to the SENSE pin; if SENSE is connected to ground, VPROPI measures 0 V. Also note that during slow decay (brake), VPROPI measures 0 V. VPROPI can output a maximum of 2.5 V, because at 500 mV on SENSE, the H-bridge is disabled.

### 7.3.4 Protection Circuits

The DRV8816 is fully protected against VBB undervoltage, charge pump undervoltage, overcurrent, and overtemperature events.

#### 7.3.4.1 VBB UVLO

If at any time the voltage on the VBB pin falls below the UVLO threshold voltage, all FETs in the H-bridge will be disabled and the charge pump will be disabled. Operation will resume when VBB rises above the UVLO threshold. Note that nFAULT does not indicate a UVLO because the CPUV fault is always asserted below VBB = 12 V.

#### 7.3.4.2 VCP UVLO (CPUV)

During a CPUV event, the VCP voltage is measured to be below VCP + 10 V. If at any time the voltage on the VCP pin falls below the UVLO threshold voltage, the nFAULT pin is driven low. The nFAULT pin is released after operation has resumed. Note that this fault does not disable the output FETs and allows the device to continue operating. When VBB is below 12 V, this fault condition is always asserted and nFAULT is pulled low.

### 7.3.4.3 OCP

The current flowing through the high-side and low-side drivers is monitored to ensure that the motor lead is not shorted to supply or ground. If a short is detected, all FETs in the H-bridge are disabled, nFAULT is driven low, and a  $t_{OCP}$  fault timer is started. After this period,  $t_{OCP}$ , the device is then allowed to follow the input commands and another turn-on is attempted (nFAULT becomes high again during this attempt). If there is still a fault condition, the cycle repeats. If after  $t_{OCP}$  expires it is determined the short condition is not present, normal operation resumes and nFAULT is released.

### 7.3.4.4 OTW

If the die temperature increases past the thermal warning threshold, the nFAULT pin is driven low. After the die temperature has fallen below the hysteresis level, the nFAULT pin is released. If the die temperature continues to increase, the device enters overtemperature shutdown as described in [OTS](#).

### 7.3.4.5 OTS

If the die temperature exceeds safe limits, all FETs in the H-bridge are disabled and the charge pump is shut down. After the die temperature has fallen to a safe level, operation automatically resumes.

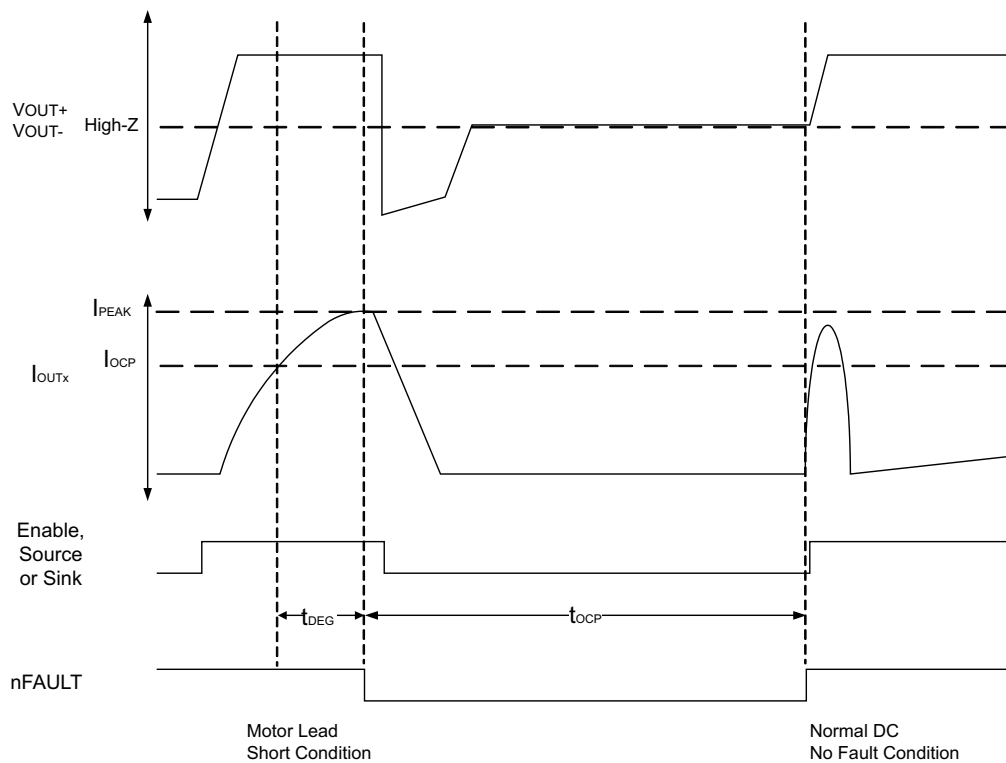
## 7.4 Device Functional Modes

### 7.4.1 SENSE

A low-value resistor can be placed between the SENSE pin and ground for current-sensing purposes. The PCB should be designed with wide metal paths on each side of the resistor, to minimize IR drop that would decrease sense accuracy. Likewise, the distance from the sense resistor to the DRV8816 and bulk capacitor should be minimized.

To set a manual overcurrent trip threshold, place a resistor between the SENSE pin and GND. When the SENSE pin rises above 500 mV, the H-bridge output is disabled (High-Z). The device will automatically retry with a period of  $t_{OCP}$ . The overcurrent trip threshold can be calculated using  $I_{TRIP} = 500 \text{ mV}/\Omega$ . The overcurrent trip level selected cannot be greater than  $I_{OCP}$ .

If a sense resistor is not used, tie the SENSE pin directly to GND; in that case, the  $I_{OCP}$  detection of current through the internal FETs still functions.

**Device Functional Modes (continued)**

**Figure 6. Overcurrent Threshold**

## 8 Application and Implementation

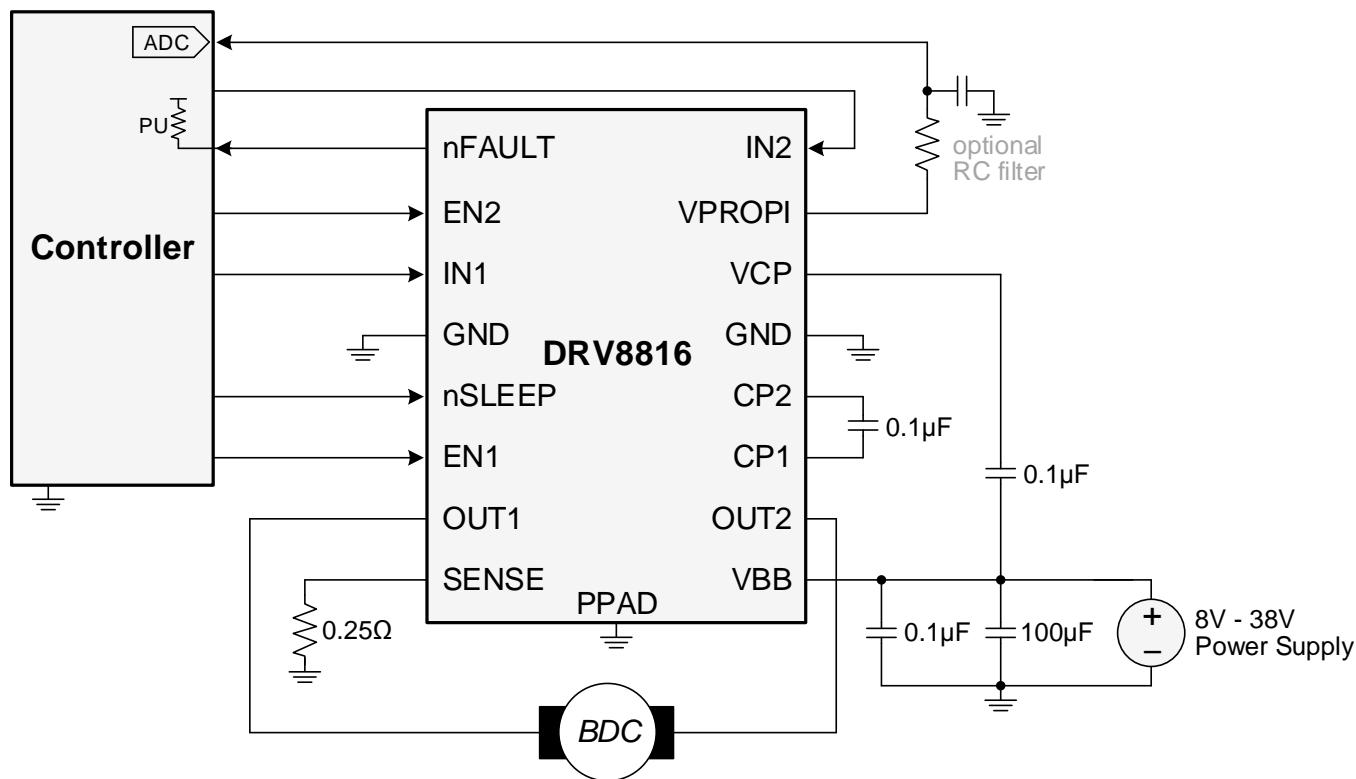
### NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 8.1 Application Information

The DRV8816 is typically used to drive a brushed DC motor.

### 8.2 Typical Application



**Figure 7. Typical Application**

#### 8.2.1 Design Requirements

Table 5 shows parameters to consider when designing.

**Table 5. Design Parameters**

DESIGN PARAMETER	REFERENCE	EXAMPLE VALUE
Motor voltage	$V_{BB}$	24 V
Motor RMS current	$I_{RMS}$	0.8 A
Motor startup current	$I_{START}$	2 A
Motor current trip point	$I_{TRIP}$	2.5 A

## 8.2.2 Detailed Design Procedure

### 8.2.2.1 Motor Voltage

The motor voltage to use will depend on the ratings of the motor selected and the desired RPM. A higher voltage spins a brushed DC motor faster with the same PWM duty cycle applied to the power FETs. A higher voltage also increases the rate of current change through the inductive motor windings.

### 8.2.2.2 Power Dissipation

The power dissipation of the DRV8816 is a function of RMS motor current and the each output's FET resistance ( $R_{DS(ON)}$ ).

$$\text{Power} \approx I_{RMS}^2 \times (\text{High-Side } R_{DS(ON)} + \text{Low-Side } R_{DS(ON)}) \quad (1)$$

For this example, the ambient temperature is 35°C, and the junction temperature reaches 65°C. At 65°C, the sum of  $R_{DS(ON)}$  is about 1Ω. With an example motor current of 0.8A, the dissipated power in the form of heat will be  $0.8A^2 \times 1\Omega = 0.64W$ .

The temperature that the DRV8816 reaches will depend on the thermal resistance to the air and PCB. It is important to solder the device PowerPAD to the PCB ground plane, with vias to the top and bottom board layers, in order dissipate heat into the PCB and reduce the device temperature. In the example used here, the DRV8816 had an effective thermal resistance  $R_{\theta JA}$  of 47°C/W, and:

$$T_J = T_A + (P_D \times R_{\theta JA}) = 35^\circ\text{C} + (0.64W \times 47^\circ\text{C/W}) = 65^\circ\text{C} \quad (2)$$

### 8.2.2.3 Motor Current Trip Point

When the voltage on pin SENSE exceeds  $V_{TRIP}$  (0.5V), overcurrent is detected. The  $R_{SENSE}$  resistor should be sized to set the desired  $I_{TRIP}$  level.

$$R_{SENSE} = 0.5V / I_{TRIP} \quad (3)$$

To set  $I_{TRIP}$  to 2A,  $R_{SENSE} = 0.5V / 2A = 0.25\Omega$ .

To prevent false trips,  $I_{TRIP}$  must be higher than regular operating current. Motor current during startup is typically much higher than steady-state spinning, because the initial load torque is higher, and the absence of back-EMF causes a higher voltage and extra current across the motor windings.

It can be beneficial to limit startup current by using series inductors on the DRV8816 output, as that allows  $I_{TRIP}$  to be lower, and it may decrease the system's required bulk capacitance. Startup current can also be limited by ramping the forward drive duty cycle.

### 8.2.2.4 Sense Resistor Selection

For optimal performance, it is important for the sense resistor to be:

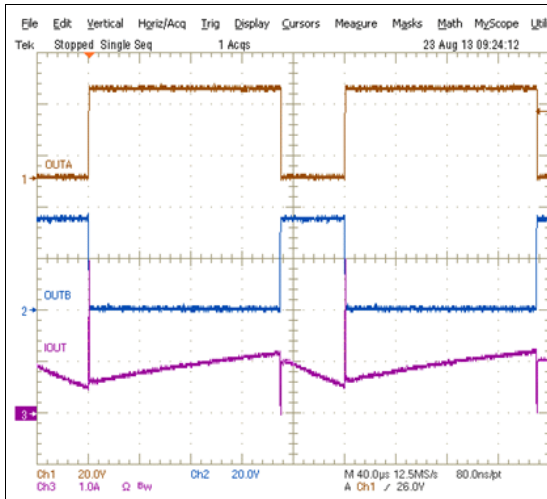
- Surface-mount
- Low inductance
- Rated for high enough power
- Placed closely to the motor driver

The power dissipated by the sense resistor equals  $I_{RMS}^2 \times R$ . For example, if peak motor current is 3A, RMS motor current is 2A, and a 0.05Ω sense resistor is used, the resistor will dissipate  $2A^2 \times 0.05\Omega = 0.2W$ . The power quickly increases with higher current levels.

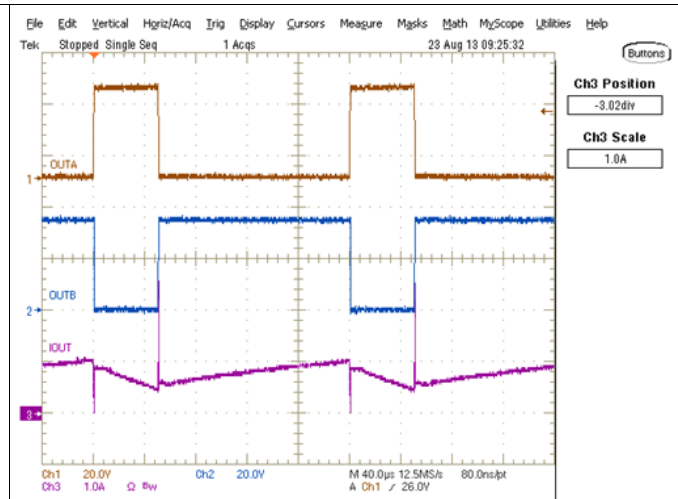
Resistors typically have a rated power within some ambient temperature range, along with a de-rated power curve for high ambient temperatures. When a PCB is shared with other components generating heat, margin should be added. It is always best to measure the actual sense resistor temperature in a final system, along with the power MOSFETs, as those are often the hottest components.

Because power resistors are larger and more expensive than standard resistors, it is common practice to use multiple standard resistors in parallel, between the sense node and ground. This distributes the current and heat dissipation.

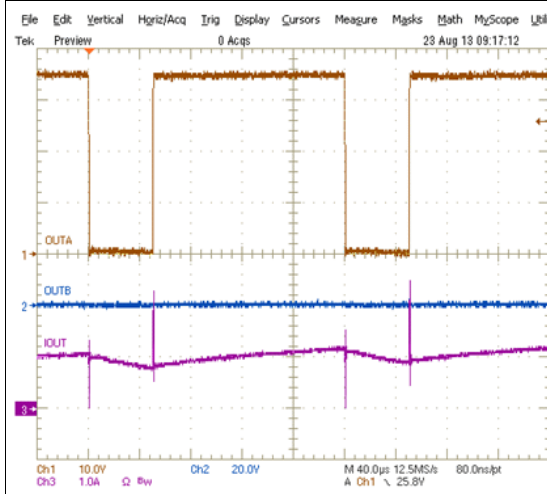
## 8.2.3 Application Curves



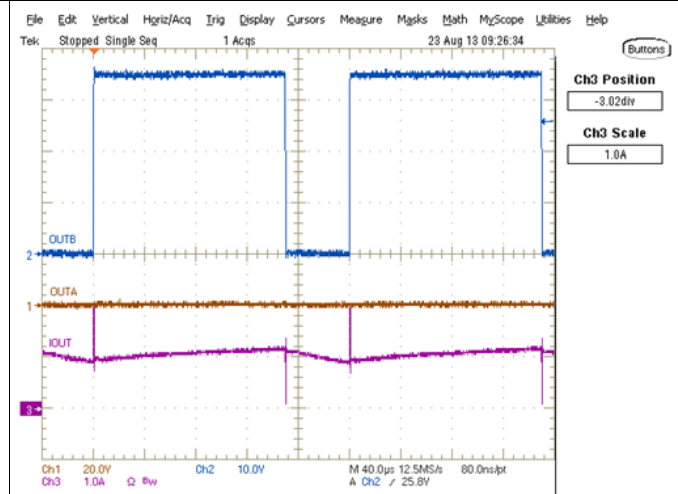
**Figure 8. Forward Drive, Fast Decay**



**Figure 9. Reverse Drive, Fast Decay**



**Figure 10. Forward Drive, Slow Decay**



**Figure 11. Reverse Drive, Slow Decay**

## 9 Power Supply Recommendations

### 9.1 Bulk Capacitance

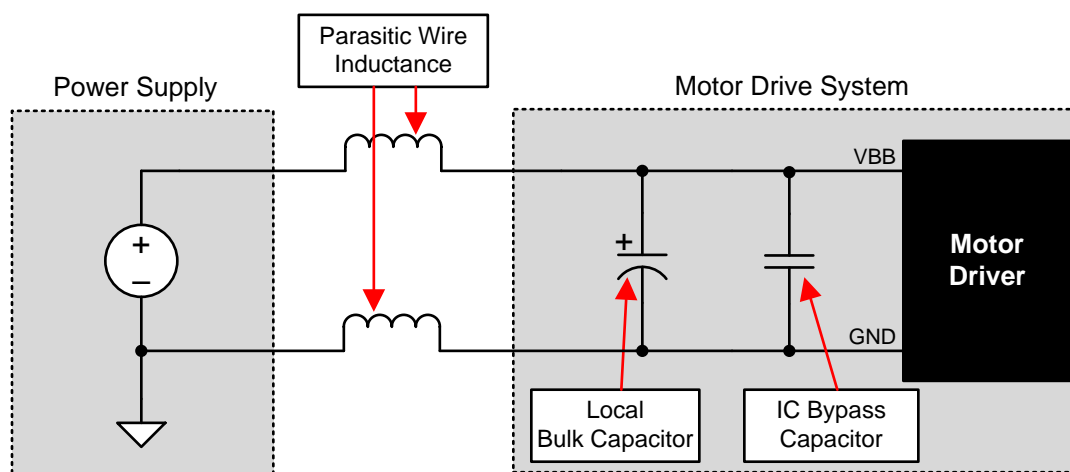
Having appropriate local bulk capacitance is an important factor in motor drive system design. It is generally beneficial to have more bulk capacitance, while the disadvantages are increased cost and physical size.

The amount of local capacitance needed depends on a variety of factors, including:

- The highest current required by the motor system.
- The power supply's capacitance and ability to source current.
- The amount of parasitic inductance between the power supply and motor systems.
- The acceptable voltage ripple.
- The type of motor used (Brushed DC, Brushless DC, Stepper).
- The motor braking method.

The inductance between the power supply and motor drive system will limit the rate current can change from the power supply. If the local bulk capacitance is too small, the system will respond to excessive current demands or dumps from the motor with a change in voltage. When adequate bulk capacitance is used, the motor voltage remains stable and high current can be quickly supplied.

The datasheet generally provides a recommended value, but system-level testing is required to determine the appropriate sized bulk capacitor.



**Figure 12. Example Setup of Motor Drive System with External Power Supply**

### 9.2 Power Supervisor

Control input nSLEEP is used to minimize power consumption when the DRV8816 is not in use. This disables much of the internal circuitry, including the internal voltage rails and charge pump. nSLEEP is asserted low. A logic high on this input pin results in normal operation. When switching from low to high, the user should allow a 1-ms delay before applying PWM signals. This time is needed for the charge pump to stabilize.



## 10 Layout

### 10.1 Layout Guidelines

The printed circuit board (PCB) should use a heavy ground plane. For optimum electrical and thermal performance, the DRV8816 must be soldered directly onto the board. On the underside of the DRV8816 is a thermal pad, which provides a path for enhanced thermal dissipation. The thermal pad should be soldered directly to an exposed surface on the PCB. Thermal vias are used to transfer heat to other layers of the PCB.

The load supply pin, VBB, should be decoupled with an electrolytic capacitor (typically 100 µF) in parallel with a ceramic capacitor placed as close as possible to the device. The ceramic capacitors between VCP and VBB, connected to VREG, and between CP1 and CP2 should be as close to the pins of the device as possible, in order to minimize lead inductance.

$$P_{TOT} = R_{DS(ON)} \times (I_{OUT(RMS)})^2$$

where

- $P_{TOT}$  is the total power dissipation.
- $R_{DS(ON)}$  is the resistance of the HS plus LS FETS.
- $I_{OUT(RMS)}$  is the RMS output current being applied to each winding. (4)

The voltage rating for bulk capacitors should be higher than the operating voltage, to provide margin for cases when the motor transfers energy to the supply.

$I_{OUT(RMS)}$  is equal to approximately 0.7× the full-scale output current setting.

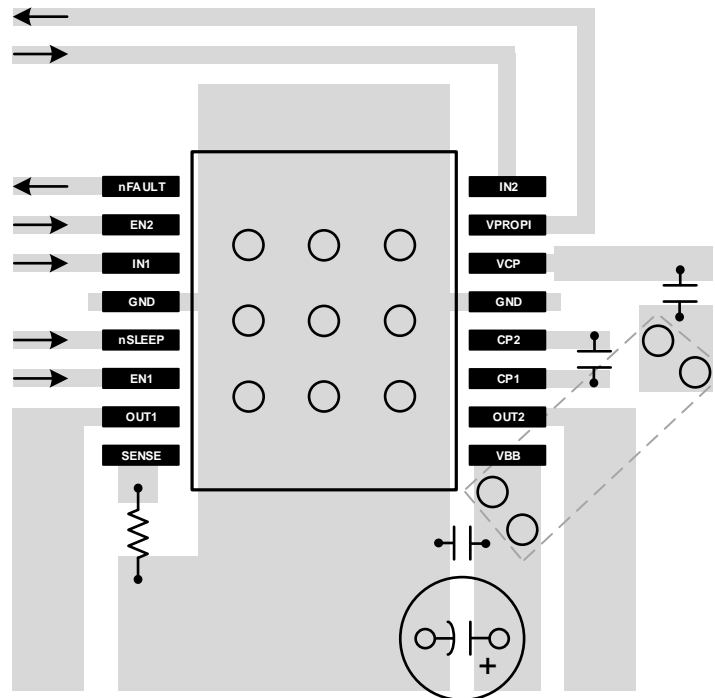
The maximum amount of power that can be dissipated in the device is dependent on ambient temperature and heatsinking.

Note that  $R_{DS(ON)}$  increases with temperature, so as the device heats, the power dissipation increases.

#### 10.1.1 Ground

A ground power plane should be located as close to DRV8816 as possible. The copper ground plane directly under the thermal pad makes a good location. This pad can then be connected to ground for this purpose.

## 10.2 Layout Example



**Figure 13. DRV8816 Layout Example**

## 10.3 Thermal Protection

If the die temperature exceeds approximately 150°C, the device is disabled until the temperature drops to a safe level. Any tendency of the device to enter thermal shutdown is an indication of either excessive power dissipation, insufficient heatsinking, or too high an ambient temperature.

## 11 Device and Documentation Support

### 11.1 Documentation Support

#### 11.1.1 Related Documentation

For related documentation see the following:

- *DRV8816 Evaluation Module*, [SLVU971](#)
- *Shelf-Life Evaluation of Lead-Free Component Finishes*, [SZZA046](#)

### 11.2 Community Resource

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's [Terms of Use](#).

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**Design Support** *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

### 11.3 Trademarks

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### 11.4 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### 11.5 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

## 12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

## PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package   Pins	Package qty   Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
<a href="#">DRV8816PWP</a>	Obsolete	Production	HTSSOP (PWP)   16	-	-	Call TI	Call TI	-40 to 85	DRV8816
<a href="#">DRV8816PWPR</a>	Active	Production	HTSSOP (PWP)   16	2000   LARGE T&R	Yes	NIPDAU	Level-3-260C-168 HR	-40 to 85	DRV8816
DRV8816PWPR.A	Active	Production	HTSSOP (PWP)   16	2000   LARGE T&R	Yes	NIPDAU	Level-3-260C-168 HR	-40 to 85	DRV8816

<sup>(1)</sup> **Status:** For more details on status, see our [product life cycle](#).

<sup>(2)</sup> **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

<sup>(3)</sup> **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

<sup>(4)</sup> **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

<sup>(5)</sup> **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

<sup>(6)</sup> **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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## TAPE AND REEL INFORMATION



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
DRV8816PWPR	HTSSOP	PWP	16	2000	330.0	12.4	6.9	5.6	1.6	8.0	12.0	Q1

## TAPE AND REEL BOX DIMENSIONS



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
DRV8816PWPR	HTSSOP	PWP	16	2000	350.0	350.0	43.0



Images above are just a representation of the package family, actual package may vary.  
Refer to the product data sheet for package details.



## PowerPAD™ TSSOP - 1.2 mm max height

6.6  
6.2 TYP

PIN 1 ID AREA

16

14X 0.65

2X 4.55

16X 0.30  
0.19

5.1  
4.9  
NOTE 3

8

4.5  
4.3

9

SEATING PLANE

0.1 C

0.1 M C A S B S

(0.15) TYP

SEE DETAIL A

2X 0.95 MAX  
NOTE 5

4X 0.15 MAX  
NOTE 5

THERMAL PAD

3.0  
2.4

0.25

GAGE PLANE

0° - 8°

0.75  
0.50

1.2 MAX

0.15  
0.05

DETAIL A  
TYPICAL

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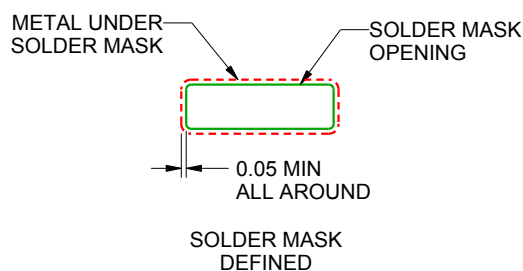
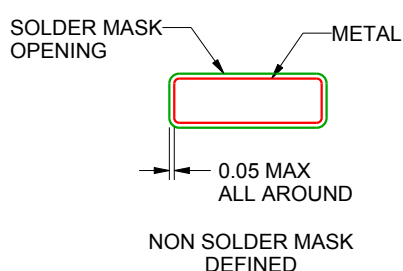
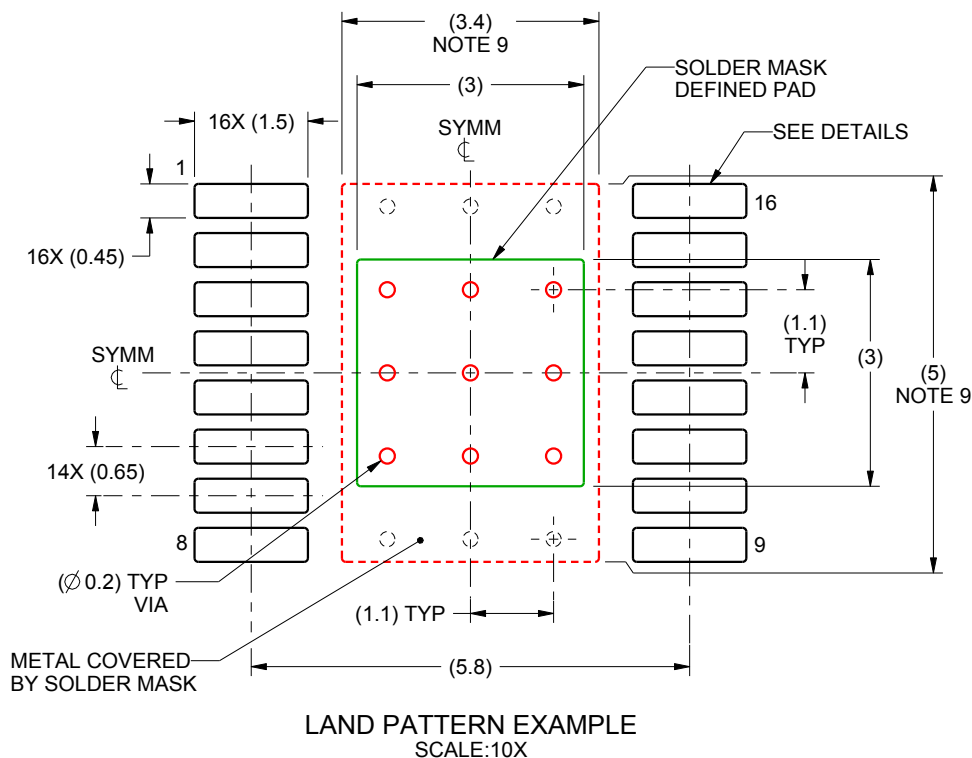


# EXAMPLE BOARD LAYOUT

PWP0016B

PowerPAD™ TSSOP - 1.2 mm max height

PLASTIC SMALL OUTLINE



SOLDER MASK DETAILS  
PADS 1-16

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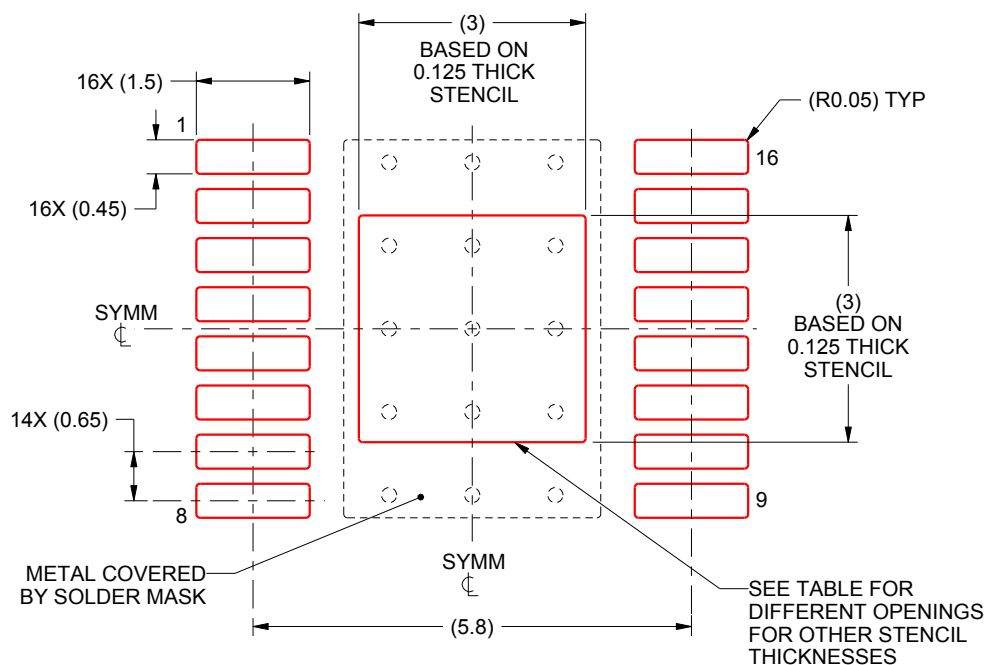
NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
8. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature numbers SLMA002 ([www.ti.com/lit/slma002](http://www.ti.com/lit/slma002)) and SLMA004 ([www.ti.com/lit/slma004](http://www.ti.com/lit/slma004)).
9. Size of metal pad may vary due to creepage requirement.

**PWP0016B**

## PowerPAD™ TSSOP - 1.2 mm max height

## PLASTIC SMALL OUTLINE



SOLDER PASTE EXAMPLE  
EXPOSED PAD  
100% PRINTED SOLDER COVERAGE BY AREA  
SCALE:10X

STENCIL THICKNESS	SOLDER STENCIL OPENING
0.1	3.35 X 3.35
0.125	3 X 3 (SHOWN)
0.15	2.74 X 2.74
0.175	2.54 X 2.54

4218971/A 01/2016

NOTES: (continued)

10. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
11. Board assembly site may have different recommendations for stencil design.

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