





ZHCSFM8A - DECEMBER 2011 - REVISED OCTOBER 2016

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TPS53313 集成开关的高效 6A 降压稳压器

Technical

Documents

Sample &

Buy

1 特性

- 4.5V 至 16V 转换电压范围
- 可调节输出电压范围: 0.6V 至 0.7 × V_{IN}
- 6A 持续输出电流
- 支持所有多层陶瓷电容 (MLCC) 输出电容
- 可选跳跃模式或强制连续导通模式 (CCM)
- 可选软启动时间(1ms、3ms 或 6ms)
- 可选 4A-5A、6A 或 9A 峰值电流限值
- 优化了轻负载与重负载条件下的效率
- 电压模式控制
- 可编程开关频率范围: 250kHz 至 1.5MHz
- 同步至外部时钟
- 针对过零检测和过流保护提供 R_{DS(on)} 感测
- 软停止输出在禁用期间放电
- 在断续模式下提供过流、过压和欠压保护
- 过热保护
- 开漏电源正常指示
- 内部自举开关
- 4mm × 4mm 24 引脚超薄四方扁平无引线 (VQFN) 封装

- 2 应用
- 电压为 5V 的 负载点 (POL) 应用
- 12V 降压电压轨

Tools &

Software

3 说明

TPS53313 提供集成两个 N 沟道金属氧化物半导体场 效应晶体管 (MOSFET) 的 5V 或 12V 同步降压转换 器。由于低R_{DS (接通)}和TI私有的 SmoothPWM™跳跃 模式操作可优化轻载条件下的效率,同时不影响输出电 压纹波。

TPS53313 具有 可编程开关频率(250kHz 至 1.5MHz),可选择跳跃模式或强制 CCM 模式操作。 该器件提供预偏置启动、软停止、集成自举开关、电源 正常功能和 EN/输入电压锁定 (UVLO) 保护。该器件支 持 4.5V 至 16V 范围内的输入电压,无需额外使用偏 置电压。可调节输出电压范围: 0.6V 至 0.7 × V_{IN}。

TPS53313 采用 4mm × 4mm 24 VQFN 封装(绿色环保,符合 RoHS 标准并且无铅),额定运行温度范围为 -40°C 至 85°C。

器件信息⁽¹⁾

	相广 日心、	-
器件型号	封装	封装尺寸(标称值)
TPS53313	VQFN (24)	4.00mm x 4.00mm

(1) 要了解所有可用封装,请见数据表末尾的可订购产品附录。



典型应用电路





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4 修订历史记录

注: 之前版本的页码可能与当前版本有所不同。

Changes from Original (December 2011) to Revision A

•	已添加 ESD 额定值表	, 特性 描述部分,	器件功能模式,	应用和实施部分,	电源相关建议部分,	布局部分,	器件和文	
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•	已删除 订购信息表; i	请参见数据表末尾的	的 POA					1

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5 Pin Configuration and Functions



Pin Functions

PIN			DESCRIPTION		
NO.	NAME	IIFE''	DESCRIPTION		
1	EN	I	Enable pin		
2	PG	0	Power good output flag. Open drain output. Pull up to an external rail through a resistor.		
3	VIN	Р	Gate driver supply and power conversion voltage		
4	VIN	Р	Gate driver supply and power conversion voltage		
5	VIN	Р	Gate driver supply and power conversion voltage		
6	VIN	Р	Gate driver supply and power conversion voltage		
7	PGND	Р	Device power ground terminal		
8	PGND	Р	Device power ground terminal		
9	PGND	Р	Device power ground terminal		
10	PGND	Р	Device power ground terminal		
11	PGND	Р	Device power ground terminal		
12	PGND	Р	Device power ground terminal		
13	SW	0	Output inductor connection to integrated power devices		
14	SW	0	Output inductor connection to integrated power devices		
15	SW	0	Output inductor connection to integrated power devices		
16	SW	0	Output inductor connection to integrated power devices		
17	VBST	Р	Supply input for high-side MOSFET (bootstrap terminal). Connect capacitor from this pin to SW terminal.		
18	BP7	Р	Bias for internal circuitry and driver		
19	BP3	Р	Input bias supply for analog functions		
20	AGND	G	Device analog ground terminal		
21	RT/SYNC	I/O	Synchronized to external clock. Program the switching frequency by connecting with a resistor to GND.		

(1) B = Bidirectional, G = Ground, I = Input, O = Output, P = Supply

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Pin Functions (continued)

	PIN		DESCRIPTION
NO.	NAME	ITPE''	DESCRIPTION
22	MODE/SS	I	Mode configuration pin. Connect with a resistor to GND sets different modes and soft-start time, parallel a capacitor (or no capacitor) with the resistor changes the current limit threshold. Shorting MODE/SS pin to supply inhibits the device; shorting MODE/SS pin to AGND is equivalent to 10-k Ω resistor setting is not recommended (see $\frac{1}{5}$ 1 and $\frac{1}{5}$ 2 for resistor and capacitor settings).
23	COMP	0	Error amplifier compensation terminal. Type III compensation method is generally recommended for stability.
24	FB	I	Voltage feedback pin. Use for OVP, UVP, and power good determination



6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) $^{(1)(2)(3)}$

			MIN	MAX	UNIT	
	VIN	VIN		20		
	VBST		-0.3	27		
	VBST to SW		-0.3	7		
		DC	-2	20		
input voitage	tr	transient < 20 ns	-3	20	V	
		V _{VIN} ≥ 17	-0.3	17		
	EN	V _{VIN} < 17	-0.3	V _{VIN} + 0.1		
	FB, MODE/SS		-0.3	3.6		
	COMP, RT/SYNC, BP3		-0.3	3.6		
VBST VBST to S VBST to S SW (bidire EN FB, MODE Output voltage BP7 PGD Ground pin (GND) Output current Operating temperature, T _J Storage temperature, T _{stg}	BP7	BP7 PGD		7	V	
	PGD			17	l	
Ground pin (GND)			-0.3	0.3	V	
Output current				6	А	
Operating temperature, T _J			-40	150	°C	
Storage temperature, T _{stq}			-55	150	°C	

(1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) All voltage values are with respect to the network ground terminal unless otherwise noted.

(3) Voltage values are with respect to the corresponding LL terminal.

6.2 ESD Ratings

			VALUE	UNIT
V	Electrostatic discharge Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾ Charged-device model (CDM), per JEDEC specification JESD22-C1	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	±2000	V
V(ESD)		Charged-device model (CDM), per JEDEC specification JESD22-C101 ⁽²⁾	±500	V

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)⁽¹⁾⁽²⁾

			MIN	MAX	UNIT
	VIN (main supply)		4.5	16	
	VBST		-0.1	22	
Input voltage	VBST to SW		-0.1	6.5	
	CIA/ (bidiractional)	dc	-1	18	V
	Sw (bidirectional)	transient < 20 ns	-2	18	
	EN		-0.1	V _{VIN} + 0.1	
	FB, MODE/SS		-0.1	3.5	
	COMP, RT/SYNC, BP3		-0.1	3.5	V
Output voltage	BP7		-0.1	6.5	
	PGD		-0.1	14	
Ground pin (GND)		-0.1	0.1	V	
T _A Ambient temperature	Ambient temperature		-40	85	°C
T _J Junction temperature			-40	125	°C

(1) Voltage values are with respect to the corresponding LL terminal.

(2) All voltage values are with respect to the network ground terminal unless otherwise noted.

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6.4 Thermal Information

		TPS53313	
	THERMAL METRIC ⁽¹⁾	RGE (VQFN)	UNIT
		24 PINS	
$R_{ heta JA}$	Junction-to-ambient thermal resistance	44.1	°C/W
R _{0JC(top)}	Junction-to-case (top) thermal resistance	35	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	19	°C/W
ΨJT	Junction-to-top characterization parameter	0.5	°C/W
Ψјв	Junction-to-board characterization parameter	18.8	°C/W
R _{0JC(bot)}	Junction-to-case (bottom) thermal resistance	8.9	°C/W

(1) For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.

6.5 Electrical Characteristics

over operating free-air temperature range, V_{VIN} = 12 V, PGND = GND (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT	
INPUT SUPP	LY						
V _{VIN}	VIN supply voltage	Nominal input voltage range	4.5		16	V	
V _{POR}	VIN POR threshold	Ramp up, EN = HIGH	4	4.23	4.4	V	
V _{POR(hys)}	VIN POR hysteresis			200		mV	
I _{STBY}	Standby current	$EN = LOW, V_{IN} = 12 V$		58		μA	
R _{BOOT}	Bootstrap on-resistance			10		Ω	
REFERENCE							
V _{VREF}	Internal precision reference voltage			0.6		V	
TOLVREF	VREF tolerance		-1%		1%		
ERROR AMP	LIFIER						
UGBW ⁽¹⁾	Unity gain bandwidth		14			MHz	
A _{OL} ⁽¹⁾	Open loop gain		80			dB	
I _{FBINT}	FB input leakage current	Sourced from FB pin		50		nA	
I _{EA(max)}	Output sinking and sourcing current			5		mA	
SR ⁽¹⁾	Slew rate			5		V/µs	
ENABLE							
R _{ENPD} ⁽¹⁾	Enable pulldown resistor			800		kΩ	
V _{ENH}	EN logic high	V _{VIN} = 4.5 V	1.8			V	
V _{ENHYS}	EN hysteresis	$V_{VIN} = 4.5 V$			0.6	V	
		$V_{EN} = 0 V$			1		
I _{EN}	EN pin current	V _{EN} = 3.3 V		3.3	5	μA	
		V _{EN} = 14 V		17.8	27.5		
SOFT-START	-						
t _{SS_1}	Delay after EN asserts	EN = High		0.65		ms	
		0 V \leq V _{SS} \leq 0.6 V, 39-k Ω or no resistor to MODE/SS pin		1			
t _{SS_2}	Soft start ramp_up time	0 V ≤ V _{SS} ≤ 0.6 V, 20-k Ω or 160-k Ω resistor to MODE/SS pin		3		ms	
		$0 \text{ V} \le \text{V}_{SS} \le 0.6 \text{ V}$, $10\text{-}k\Omega$ or $82\text{-}k\Omega$ resistor to MODE/SS pin		6			
t _{PGDENDLY}	PGD startup delay time	V_{SS} = 0.6 \overline{V} to PGD (SSOK) going high, t_{SS} = 1 ms		0.2		ms	

(1) Ensured by design. Not production tested.



Electrical Characteristics (接下页)

over operating free-air temperature range, V_{VIN} = 12 V, PGND = GND (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
RAMP		-				
	_	$4.5 \text{ V} \le \text{V}_{\text{VIN}} \le 14.4 \text{ V}$		V _{VIN} /9		V
	Ramp amplitude	$14.4 \text{ V} \le \text{V}_{\text{VIN}} \le 16 \text{ V}$		1.6		
PWM		-			1	
t _{MIN(off)}	Minimum OFF time	f _{SW} = 1 MHz		150		ns
t _{MIN(on)}	Minimum ON time	No load			90	ns
D _{MAX}	Maximum duty cycle	f _{SW} = 1 MHz		80%		
SWITCHING I	FREQUENCY	+				
f _{SW}	Switching frequency tolerance	f _{SW} = 1 MHz, R _T = 45.3 kΩ	-10%		10%	
SOFT DISCH	ARGE					
R _{SFTDIS}	Soft-discharge transistor resistance	EN = Low, V _{IN} = 4.5 V, V _{OUT} = 0.6 V		120		Ω
OVERCURRE	INT AND ZERO CROSSING	L			1	
		When I _{OUT} exceeds this threshold for 4 consecutive cycles, 2.2-nF capacitor to MODE/SS pin		4.5		A
I _{OCPL}	Overcurrent limit on high-side FET (peak)	When I _{OUT} exceeds this threshold for 4 consecutive cycles, no capacitor to MODE/SS pin		6		А
		When I _{OUT} exceeds this threshold for 4 consecutive cycles, 10-nF capacitor to MODE/SS pin		9		
		Immediately shut down when sensed current reach this value, 2.2-nF capacitor to MODE/SS pin		4.5		A
I _{ОСРН}	One time overcurrent shut-off on the low-side FET (peak)	Immediately shut down when sensed current reach this value, no capacitor to MODE/SS pin		6		А
		Immediately shut down when sensed current reach this value, 10-nF capacitor to MODE/SS pin		9		
V _{ZXOFF}	Zero crossing comparator internal offset	SW – PGND, SKIP mode		-3		mV
POWER GOO	D					
V _{PGDL}	Power good low threshold	Measured at the FB pin w/r/t VREF	80%	83%	86%	
V _{PGDH}	Power good high threshold	Measured at the FB pin w/r/t VREF	114%	117%	120%	
V _{PG(hys)}	Power good hysteresis			2		
V _{IN(min_pg)}	Minimum Vin voltage for valid PG at startup.	Measured at V_{IN} with 1-mA (or 2-mA) sink current on PG pin at startup			1	V
V _{PG(pd)}	Power good pull-down voltage	Pull down voltage with 4-mA sink current		0.2	0.4	V
I _{PG(leak)}	Power good leakage current	Hi-Z leakage current, apply 3.3-V in off state		12	16.2	μA
OUTPUT OVE	ERVOLTAGE AND UNDERVOLTAG	SE PROTECTION				
T _{OVPDLY}	Overvoltage protection delay time	Time from FB out of +17% of VREF to OVP fault		2		μs
T _{UVPDLY}	Undervoltage protection delay time	Time from FB out of –17% of VREF to UVP fault		10		μs
THERMAL SH	IUTDOWN	·			1	
THSD ⁽¹⁾	Thermal shutdown	Shutdown controller, attempt soft-stop	130	140	150	°C
THSD _{HYST} ⁽¹⁾	Thermal shutdown hysteresis	Controller restarts after temperature drops		40		°C

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6.6 Typical Characteristics





Typical Characteristics (接下页)



7 Detailed Description

7.1 Overview

The TPS53313 is a high-efficiency switching regulator with two integrated N-channel MOSFETs and is capable of delivering up to 6 A of load current. The TPS53316 provides output voltage from 0.6 V up to 0.7 × V_{IN} from 4.5-V to 16-V wide input voltage range. The output voltage accuracy is better than ±1% over load, line, and temperature.

This device can operate in either forced continuous conduction mode (FCCM) or skip mode with selectable softstart time to fit various application needs. Skip mode operation provides reduced power loss and increases the efficiency at light load. The unique, patented PWM modulator enables smooth light load to heavy load transition while maintaining fast load transient.

7.2 Functional Block Diagram



7.3 Feature Description

7.3.1 Soft-Start Operation

The soft-start operation reduces the inrush current during the start-up time. A slow rising reference is generated by the soft-start circuitry and sent to the input of the error amplifier. When the soft-start ramp voltage is less than 600 mV, the error amplifier uses this ramp voltage as the reference. When the ramp voltage reaches 600 mV, a fixed 600-mV reference voltage is used for the error amplifier. The soft-start time has selectable values of 1 ms, 3 ms, and 6 ms.



Feature Description (接下页)

The TPS53313 monitors the output voltage through the FB pin. If the FB voltage is within 117% and 83% of the reference voltage, the power good signal remains high. If the FB voltage is outside of this range, the PG pin pin is pulled low by the internal open drain output.

During start up, the power good signal has a 200-µs delay after the FB voltage falls into the power good range limit when the soft-start time is set to 1 ms. There is also 10-µs delay during shut down.

7.3.3 UVLO Function

The TPS53313 provides UVLO protection for input voltage, VIN. If the input voltage is lower than UVLO threshold voltage minus the hysteresis, the device shut off. When the voltage rises above the threshold voltage, the device restarts. The typical UVLO rising threshold is 4.23 V. Hysteresis of 200 mV for input voltage is provided to prevent glitch.

7.3.4 Overcurrent (OC) Protection

The TPS53313 provides peak current protection and continuously monitors the current flowing through high-side and low-side MOSFETs. If the current through the high-side FET exceeds the current limit threshold, the high-side FET turns off and the low-side FET turns on. An overcurrent (OC) counter starts to increment every switching cycle to count the occurrence of the overcurrent events. The converter shuts down immediately when the OC counter reaches 4. The OC counter resets if the detected current is less than 6 A (with 6-A OC setting) after an OC event.

Another set of overcurrent circuitry monitors the current through low-side FET. If the current through the low-side FET exceeds 6 A (with 6-A OC setting), the overcurrent protection is engaged and turns off both high-side and low-side FETs immediately.

Therefore, the device is fully protected against overcurrent during both on-time and off-time. Also, the OC threshold is selectable and can be set to 4.5 A, 6 A, or 9 A by connecting different capacitor in parallel with MODE/SS pin. After OC events, the device stops switching and enters hiccup mode. A re-start is attempted after a hiccup waiting time. If the fault condition is not cleared, hiccup mode operation may continue indefinitely

7.3.5 Overvoltage and Undervoltage Protection

The TPS53313 monitors the voltage divided feedback voltage to detect the overvoltage and undervoltage conditions. When the feedback voltage is greater than 117% of the reference, overvoltage protection is triggered, the high-side MOSFET turns off and the low-side MOSFET turns on. Then the output voltage drops and the FB voltage reaches the undervoltage threshold. At that point the low-side MOSFET turns off and the device goes into tri-state logic.

When the feedback voltage is lower than 83% of the reference voltage, the undervoltage protection counter starts. If the feedback voltage remains lower than the undervoltage threshold voltage after 10 μ s, the device turns off both the high-side and low-side MOSFETs and then goes into tri-state logic.

After the undervoltage events, the device stops switching and enters hiccup mode. A restart is attempted after a hiccup waiting time. If the fault condition is not cleared, hiccup mode operation may continue indefinitely.

7.3.6 Overtemperature Protection

The TPS53313 continuously monitors the die temperature. If the die temperature exceeds the threshold value (140°C typical), the device shuts off. When the device is cooled to 40°C below the overtemperature threshold, it restarts and returns to normal operation.

7.3.7 Output Discharge

When the EN pin is low, the TPS53313 discharges the output capacitors through an internal MOSFET switch between SW and GND while the high-side and low-side MOSFETs are maintained in the OFF state. The typical discharge switch on resistance is 120 Ω . This function is disabled when V_{VIN} is less than 1 V.

Feature Description (接下页)

7.3.8 Switching Frequency Setting and Synchronization

The clock frequency is programmed by the value of the resistor connected from the RT/SYNC pin to GND. The switching frequency is programmable between 250 kHz and 1.5 MHz.

Also, TPS53313 is able to synchronize to external clock. The synchronization is fulfilled by connecting the RT/SYNC pin to external clock source. If no external pulse is received from RT/SYNC pin, the device continues to operate the internal clock.

7.4 Device Functional Modes

7.4.1 Operation Mode

The TPS53313 has 6 operation modes determined by the MODE/SS pin connection as listed in $\frac{1}{5}$ 1. The current limit thresholds and associated capacitance selections are shown in $\frac{1}{5}$ 2.

MODE/SS PIN CONNECTION	OPERATION MODE	t _{SS} SOFT-START TIME (ms)
10 kΩ to GND	FCCM	6
20 kΩ to GND	FCCM	3
39 kΩ to GND	FCCM	1
82 kΩ to GND	Skip mode	6
160 k Ω to GND	Skip mode	3
Floating	Skip mode	1

表 1. Operation Mode Selection

MODE/SS PIN SETTING (nF)	CURRENT LIMIT THRESHOLD (A)
No capacitor	6
2.2	4.5
10	9

表 2. Capacitor Selection

In forced continuous conduction mode (FCCM), the high-side FET is ON during the on-time and low-side FET is ON during the off-time. The switching is synchronized to the internal clock thus the switching frequency is fixed.

In this mode, the switching frequency remains constant over the entire load range which is suitable for applications that need tight control of switching frequency.

In skip mode, the high-side FET is on during the on-time and low-side FET is on during the off-time until the inductor current reaches zero. An internal zero-crossing comparator detects the zero crossing of inductor current from positive to negative. When the inductor current reaches zero, the comparator sends a signal to the logic control and turns off the low-side FET. The on-pulse in skip mode is designed to be 25% higher than CCM to provide hysteresis to avoid chattering between CCM and skip mode.

Also, the overcurrent protection threshold can be set to 4.5 A, 6 A or 9 A by changing the capacitor that is in parallel with MODE/SS pin. Specifically, a 6-A current limit threshold is set without an external capacitor, the 4.5 A current limit threshold is set with a 2.2-nF capacitor, and the 9-A current limit threshold is set when a 10-nF capacitor is in parallel with MODE/SS pin.

7.4.2 Light Load Operation

In skip mode, when the load current is less than half of inductor ripple current, the inductor current reaches zero by the end of OFF-Time. The light load control scheme then turns off the low-side MOSFET when inductor current reaches zero. Since there is no negative inductor current, the energy delivered to the load per switching cycle is increased compared to the normal PWM mode operation. The controller then reduces the switching frequency to maintain the output voltage regulation. The switching loss is reduced and thus efficiency is improved.



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In skip mode, when the load current decreases, the switching frequency also decreases continuously in discontinuous conduction mode (DCM). When the load current is 0 A, the minimum switching frequency is reached. It is also required that the difference between V_{VBST} and V_{SW} to be higher than 3.3 V to ensure the supply for high-side gate driver.



图 12. TPS53313 Operation Modes in Light and Heavy Load Conditions

7.4.3 Forced Continuous Conduction Mode

When choosing FCCM, the TPS53313 is operating in continuous conduction mode in both light and heavy load condition. In this mode, the switching frequency remains constant over the entire load range which is suitable for applications need tight control of switching frequency at a cost of lower efficiency at light load.



8 Application and Implementation

注

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

8.1 Application Information

The TPS53313 device is a high-efficiency synchronous-buck converter. The device suits low output voltage point-of-load applications with 6-A or lower output current in computing and similar digital consumer applications.

8.2 Typical Application

This design example describes a voltage-mode, 6-A synchronous buck converter with integrated MOSFETs. The device provides a fixed 1.2-V output at up to 6-A from a 12-V input bus.



图 13. Typical Application Schematic



Typical Application (接下页)

8.2.1 Design Requirements

This design example illustrates the design process and component selection for a single-output synchronous buck converter using the TPS53313. The design example schematic of a is shown in \mathbb{E} 13. The specification of the converter is listed in $\frac{1}{5}$ 3.

表	3.	Design	Example	Converter	Specifications
---	----	--------	---------	-----------	----------------

	PARAMETER	TEST CONDITION	MIN	TYP MAX	UNIT
V _{IN}	Input voltage		10.8	12 13.2	V
V _{OUT}	Output voltage			1.2	V
V _{RIPPLE}	Output ripple	I _{OUT} = 6 A		1% of V _{OUT}	V
I _{OUT}	Output current			6	А
f _{SW}	Switching frequency			600	kHz

8.2.2 Detailed Design Procedure

8.2.2.1 Output Inductor Selection

The inductance value should be determined to give the ripple current of approximately 20% to 40% of maximum output current. The inductor ripple current is determined by $\Delta \pm 1$.

$$I_{L(ripple)} = \frac{1}{L \times f_{SW}} \times \frac{(V_{IN} - V_{OUT}) \times V_{OUT}}{V_{IN}}$$
(1)

The inductor also requires a low DCR to achieve good efficiency, as well as enough room above peak inductor current before saturation.

8.2.2.2 Output Capacitor Selection

The output capacitor selection is determined by output ripple and transient requirement. When operating in CCM, the output ripple has three components:

$$V_{\text{RIPPLE}} = V_{\text{RIPPLE}(C)} + V_{\text{RIPPLE}(\text{ESR})} + V_{\text{RIPPLE}(\text{ESL})}$$
(2)

$$V_{\text{RIPPLE}(C)} = \frac{I_{\text{L(ripple)}}}{8 \times C_{\text{OUT}} \times f_{\text{SW}}}$$
(3)

 $V_{RIPPLE(ESR)} = I_{L(ripple)} \times ESR$

$$V_{\mathsf{RIPPLE}(\mathsf{ESL})} = \frac{V_{\mathsf{IN}} \times \mathsf{ESL}}{\mathsf{L}}$$
(5)

When ceramic output capacitor is chosen, the ESL component is usually negligible. In the case when multiple output capacitors are used, the total ESR and ESL should be the equivalent of the all output capacitors in parallel.

When operating in DCM, the output ripple is dominated by the component determined by capacitance. It also varies with load current and can be expressed as shown in $\Delta \pm 6$.

$$V_{\text{RIPPLE}(\text{DCM})} = \frac{\left(\alpha \times I_{\text{L(ripple)}} - I_{\text{OUT}}\right)^{2}}{2 \times f_{\text{SW}} \times C_{\text{OUT}} \times I_{\text{L(ripple)}}}$$

where

•
$$\alpha$$
 is the DCM on-time coefficient and can be expressed as shown in $\Delta \pm 7$. (6)

$$\alpha = \frac{t_{ON(DCM)}}{t_{ON(CCM)}}$$
⁽⁷⁾

(4)



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lout.

8.2.2.3 Input Capacitor Selection

The selection of input capacitor should be determined by the ripple current requirement. The ripple current generated by the converter needs to be absorbed by the input capacitors as well as the input source. The RMS ripple current from the converter can be expressed as shown in $\Delta \pm 8$.

αхΤ

图 14. DCM Output Voltage Ripple

$$I_{IN(ripple)} = I_{OUT} \times \sqrt{D \times (1 - D)}$$

where

• D is the duty cycle and can be expressed as shown in 公式 9.

$$\mathsf{D} = \frac{\mathsf{V}_{\mathsf{OUT}}}{\mathsf{V}_{\mathsf{IN}}} \tag{9}$$

To minimize the ripple current drawn from the input source, sufficient input decoupling capacitors should be placed close to the device. The ceramic capacitor is recommended due to its low ESR and low ESL. The input voltage ripple can be calculated as below when the total input capacitance is determined by $\Delta \pm 10$.

$$V_{IN(ripple)} = \frac{I_{OUT} \times D}{f_{SW} \times C_{IN}}$$
(10)

8.2.2.4 Output Voltage Setting Resistors Selection

The output voltage is programmed by the voltage-divider resistor, R1 and R2 shown in $\Delta \pm 11$. R1 is connected between VFB pin and the output, and R2 is connected between the VFB pin and GND. Recommended value for R1 is from 1k to 5k. Determine R2 using $\Delta \pm 11$.

$$R2 = \frac{0.6}{V_{OUT} - 0.6} \times R1$$
(11)

8.2.2.5 Compensation Design

The TPS53313 employs voltage mode control. To effectively compensate the power stage and ensure fast transient response, Type III compensation is typically used. $1+s \times Court \times FSR$

$$G_{CO} = 4 \times \frac{1 + s \times G_{OUT} \times 2s \times 1}{1 + s \times \left(\frac{L}{DCR + R_{LOAD}} + C_{OUT} \times (ESR + DCR)\right) + s^2 \times L \times C_{OUT}}$$
(12)

The output LC filter introduces a double pole which can be calculated as shown in 公式 13.



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,

(8)



$$f_{DP} = \frac{1}{2 \times \pi \times \sqrt{L \times C_{OUT}}}$$
(13)

The ESR zero of can be calculated as shown in 公式 14.

$$f_{ESR} = \frac{1}{2 \times \pi \times ESR \times C_{OUT}}$$
(14)

图 15 and 图 16 shows the configuration of Type III compensation and typical pole and zero locations. 公式 15 through 公式 17 describe the compensator transfer function and poles and zeros of the Type III network.

$$G_{\mathsf{EA}} = \frac{(1+s\times\mathsf{C1}\times(\mathsf{R1}+\mathsf{R3}))(1+s\times\mathsf{R4}\times\mathsf{C2})}{(s\times\mathsf{R1}\times(\mathsf{C2}+\mathsf{C3}))\times(1+s\times\mathsf{C1}\times\mathsf{R3})\times(1+s\times\mathsf{R4}\frac{\mathsf{C2}\times\mathsf{C3}}{\mathsf{C2}+\mathsf{C3}})}$$
(15)

$$f_{Z1} = \frac{1}{2 \times \pi \times R4 \times C2}$$
(16)



The two zeros can be placed near the double pole frequency to cancel the response from the double pole. One pole can be used to cancel ESR zero, and the other non-zero pole can be placed at half switching frequency to attenuate the high frequency noise and switching ripple. Suitable values can be selected to achieve a compromise between high phase margin and fast response. A phase margin higher than 45° is required for stable operation.

For DCM operation, a capacitor with a value between 100 pF and 220 pF is recommended for C3 when the output capacitance is between 22 μ F and 220 μ F.

TEXAS INSTRUMENTS

TPS53313 ZHCSFM8A – DECEMBER 2011–REVISED OCTOBER 2016

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8.2.3 Application Curves





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9 Power Supply Recommendations

The devices are designed to operate from an input voltage supply range from 4.5 V to 16 V. This input supply must be well regulated. Proper bypassing of input supplies and internal regulators is also critical for noise performance, as is PCB layout and grounding scheme (see recommendations in *Layout*).

10 Layout

10.1 Layout Guidelines

Good layout is essential for stable power supply operation. Follow these guidelines for an efficient PCB layout:

- Separate the power ground and analog ground planes. Connect them together at one location.
- Use 6 vias to connect the thermal pad to power ground.
- Place VIN, BP7 and BP3 decoupling capacitors as close to the device as possible.
- Use wide traces for VIN, PGND and SW. These nodes carry high-current and also serve as heat sinks.
- Place feedback and compensation components as close to the device as possible.
- Keep analog signals (FB, COMP) away from noisy signals (SW, VBST).

10.2 Layout Example



图 26. TPS53313 Layout Example



11 器件和文档支持

11.1 接收文档更新通知

如需接收文档更新通知,请访问 www.ti.com.cn 网站上的器件产品文件夹。点击右上角的提醒我 (Alert me) 注册 后,即可每周定期收到已更改的产品信息。有关更改的详细信息,请查阅已修订文档中包含的修订历史记录。

11.2 社区资源

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11.4 静电放电警告



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11.5 Glossary

SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.

12 机械、封装和可订购信息

以下页中包括机械、封装和可订购信息。这些信息是针对指定器件可提供的最新数据。这些数据会在无通知且不对 本文档进行修订的情况下发生改变。欲获得该数据表的浏览器版本,请查阅左侧的导航栏



PACKAGING INFORMATION

Orderable part number	Status	Material type	Package Pins	Package qty Carrier	RoHS	Lead finish/	MSL rating/	Op temp (°C)	Part marking
	(1)	(2)			(3)	Ball material	Peak reflow		(6)
						(4)	(5)		
TPS53313RGER	Active	Production	VQFN (RGE) 24	3000 LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 85	TPS
									53313
TPS53313RGER.A	Active	Production	VQFN (RGE) 24	3000 LARGE T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 85	TPS
									53313
TPS53313RGET	Active	Production	VQFN (RGE) 24	250 SMALL T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 85	TPS
			. , , ,						53313
TPS53313RGET.A	Active	Production	VQFN (RGE) 24	250 SMALL T&R	Yes	NIPDAU	Level-2-260C-1 YEAR	-40 to 85	TPS
			. , , ,						53313

⁽¹⁾ **Status:** For more details on status, see our product life cycle.

⁽²⁾ **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

⁽³⁾ RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

⁽⁴⁾ Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

⁽⁵⁾ MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

⁽⁶⁾ Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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PACKAGE OPTION ADDENDUM

23-May-2025



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TAPE AND REEL INFORMATION





QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*	All dimensions are nominal												
	Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
	TPS53313RGER	VQFN	RGE	24	3000	330.0	12.4	4.25	4.25	1.15	8.0	12.0	Q2
Ĩ	TPS53313RGET	VQFN	RGE	24	250	180.0	12.4	4.25	4.25	1.15	8.0	12.0	Q2

Pack Materials-Page 1



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PACKAGE MATERIALS INFORMATION

20-Apr-2023



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS53313RGER	VQFN	RGE	24	3000	346.0	346.0	33.0
TPS53313RGET	VQFN	RGE	24	250	210.0	185.0	35.0

GENERIC PACKAGE VIEW

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



Images above are just a representation of the package family, actual package may vary. Refer to the product data sheet for package details.



RGE0024B



PACKAGE OUTLINE

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M. 2. This drawing is subject to change without notice.
- 3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.



RGE0024B

EXAMPLE BOARD LAYOUT

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



 This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).

5. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.



RGE0024B

EXAMPLE STENCIL DESIGN

VQFN - 1 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.



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