

用于笔记本电脑显示器的白光 LED (WLED) 驱动器

查询样品: [TPS61181A](#)

特性

- **4.5V 至 24V** 输入电压
- **38V** 最大输出电压
- 集成型 **1.5A / 40V MOSFET**
- **1.0MHz** 开关频率
- 自适应升压输出至 **WLED** (白光LED) 电压
- 小型外部组件
- 集成环路补偿
- **6 个 30mA 电流源 (current sink)**
- 多达 **10 个** 串联的白光 **LED (WLED)**
- **1%** 的典型电流匹配及准确度
- 高达 **1000:1** 的 **PWM** 亮度调光
- 在 **PWM** 调光条件下实现了输出纹波的最小化
- 用于输入/输出隔离 **PFET** 的驱动器
- 真正的停机
- 具有过压保护功能
- 白光 **LED (WLED)** 开路/短路保护
- 内置软启动功能
- **16L 3mm x 3mm QFN** 封装

应用

- 笔记本电脑 **LCD** 显示器背光源
- **UMPC** (超级移动个人电脑) **LCD** 显示器背光源
- 媒体外形 (**Media Form Factor**) **LCD** 显示器的背光源

说明

TPS61181A IC 为媒体尺寸 LCD 背光照提供了高度集成的解决方案。这些器件具有一个内置的高效率升压型稳压器和集成型 1.5A / 40V 功率 MOSFET。6 个电流源稳压器提供了高精度的电流调节和匹配。该器件总共能够支持多达 60 个白光 LED。此外, 升压输出还可自动地将其电压调节至白光 LED 正向电压以改善效率。

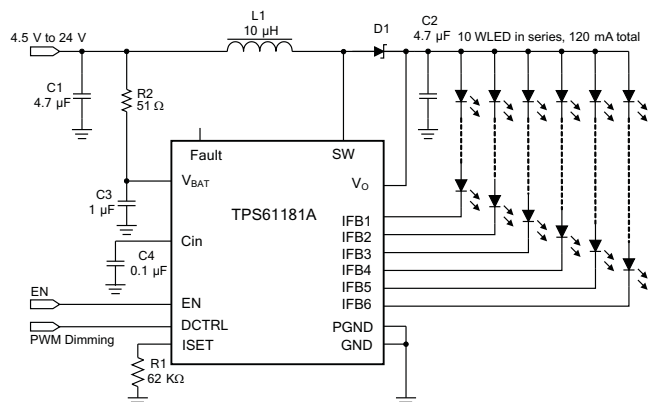
这些器件支持脉宽调制 (PWM) 亮度调光。在调光期间, 以由 DCRTL 引脚的 PWM 信号输入决定的占空比和频率来接通和关断白光 LED 电流。PWM 的一个潜在的问题是来陶瓷输出电容器的可听噪声。

TPS61181A 专为在宽阔的调光占空比和频率范围内实现该输出 AC 纹波的最小化而设计, 因而降低了这种可听噪声。

TPS61181A 为连接在输入和电感器之间的外部 PFET 提供了一个驱动器输出。在短路或过流情况下, 该 IC 将关断外部 PFET 并把电池与白光 LED 断开。在 IC 停机期间, PFET 也被关断 (从而实现了“真正的”停机), 以阻止电池产生任何漏电流。另外, 这款器件还集成了过压保护、软启动和热停机功能。

TPS61181A 具有一个用于提供 IC 电源的内置线性稳压器。该器件采用 3mm x 3mm QFN 封装。

TPS61181A 的典型应用



Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

ORDERING INFORMATION⁽¹⁾

| PACKAGE | PACKAGE MARKING |
|--------------|-----------------|
| TPS61181ARTE | QWF |

- (1) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at www.ti.com.

ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range (unless otherwise noted) ⁽¹⁾

| | | VALUE | | UNIT |
|--------------------------------------|----------------------------|-------------------------------|-----|------|
| | | MIN | MAX | |
| Voltage Range ⁽²⁾ | V _{BAT} and Fault | –0.3 | 24 | V |
| | C _{in} and ISET | –0.3 | 3.6 | |
| | SW and V _O | –0.3 | 40 | |
| | IFB1 to IFB6, EN and DCTRL | –0.3 | 20 | |
| ESD Rating ⁽³⁾ | Human Body Mode – (HBM) | | 3 | kV |
| | Machine Mode – (MM) | | 200 | V |
| | Charge Device Mode – (CDM) | | 1 | kV |
| Continuous power dissipation | | See Thermal Information Table | | |
| Operating junction temperature range | | –40 | 150 | °C |
| Storage temperature range | | –65 | 150 | |

- (1) Stresses beyond those listed under *absolute maximum ratings* may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under *recommended operating conditions* is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) All voltage values are with respect to network ground terminal.
- (3) ESD testing is performed according to the respective JEDEC standard.

THERMAL INFORMATION

| THERMAL METRIC ⁽¹⁾ | | TPS61181A | UNITS |
|-------------------------------|--|--------------|-------|
| | | QFN (16) PIN | |
| θ_{JA} | Junction-to-ambient thermal resistance | 43.1 | °C/W |
| θ_{JCTop} | Junction-to-case (top) thermal resistance | 38.3 | |
| θ_{JB} | Junction-to-board thermal resistance | 14.6 | |
| ψ_{JT} | Junction-to-top characterization parameter | 0.4 | |
| ψ_{JB} | Junction-to-board characterization parameter | 14.4 | |
| θ_{JCbott} | Junction-to-case (bottom) thermal resistance | 3.6 | |

- (1) 有关传统和新的热度的更多信息，请参阅 IC 封装热量量 应用报告 [SPRA953](#)。

RECOMMENDED OPERATING CONDITIONS

| | | MIN | TYP | MAX | UNIT |
|------------------|--|-----------------|-----|-----|------|
| V _{bat} | Battery input voltage range | 4.5 | | 24 | V |
| V _O | Output voltage range | V _{in} | | 38 | V |
| L | Inductor | 4.7 | | 10 | μH |
| C _O | Output capacitor | 2.2 | | 10 | μF |
| F _{PWM} | PWM dimming frequency at D _{PWM} ≥ 1% | 0.1 | | 1 | kHz |
| | PWM dimming frequency at D _{PWM} ≥ 5% | 1 | | 5 | |
| T _A | Operating ambient temperature | –40 | | 85 | °C |
| T _J | Operating junction temperature | –40 | | 125 | °C |

ELECTRICAL CHARACTERISTICS

$V_{BAT} = 10.8\text{ V}$, $0.1\text{ }\mu\text{F}$ at C_{in} , $EN = \text{Logic High}$, IFB current = 20 mA , IFB voltage = 500 mV , $T_A = -40^{\circ}\text{C}$ to 85°C , typical values are at $T_A = 25^{\circ}\text{C}$ (unless otherwise noted)

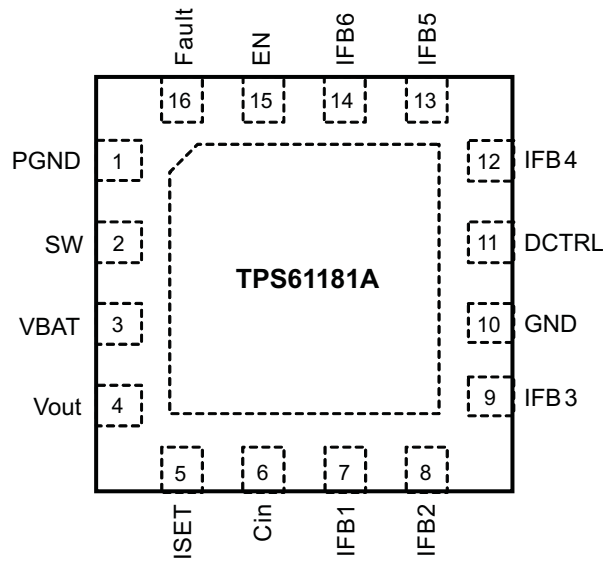
| PARAMETER | | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
|--------------------------------|--|--|-------|-------|-------|---------------|
| SUPPLY CURRENT | | | | | | |
| V_{BAT} | Battery input voltage range | | 4.5 | | 24 | V |
| V_{cin} | C_{in} pin output voltage | | 2.7 | 3.15 | 3.6 | V |
| I_{q_bat} | Operating quiescent current into V_{BAT} | Device enable, switching no load, $V_{in} = 24\text{ V}$ | | | 3 | mA |
| I_{Q_sw} | Operating quiescent current into V_O | $V_O = 35\text{V}$ | | | 60 | μA |
| I_{SD} | Shutdown current | $EN = \text{GND}$ | | 2 | 18 | μA |
| V_{bat_UVLO} | V_{BAT} under-voltage lockout threshold | V_{BAT} rising | | | 4.45 | V |
| | | V_{BAT} falling | 3.9 | | | |
| V_{bat_hys} | V_{BAT} under-voltage lockout hysteresis | V_{BAT} rising – V_{BAT} falling | | 220 | | mV |
| EN AND DCTRL | | | | | | |
| V_H | EN pin logic high voltage | | 2.0 | | | V |
| V_L | EN pin logic low voltage | | | | 0.8 | V |
| V_H | DCTRL pin logic high voltage | | 2.0 | | | V |
| V_L | DCTRL pin logic low voltage | | | | 0.8 | V |
| R_{PD} | Pull down resistor on both pins | $V_{EN, DCTRL} = 2\text{V}$ | 400 | 800 | 1600 | k Ω |
| CURRENT REGULATION | | | | | | |
| V_{ISET} | ISET pin voltage | | 1.204 | 1.229 | 1.253 | V |
| K_{ISET} | Current multiple I_{out}/I_{SET} | ISET current = $20\text{ }\mu\text{A}$ | 970 | 1000 | 1030 | |
| IFB | Current accuracy | ISET current = $20\text{ }\mu\text{A}$ | 19.4 | 20 | 20.6 | mA |
| K_m | $(I_{max} - I_{min})/I_{AVG}$ | ISET current = $20\text{ }\mu\text{A}$ | | 1 | 2.5 | % |
| I_{leak} | IFB pin leakage current | IFB voltage = 20 V on all pins | | | 3 | μA |
| I_{IFB_MAX} | Current sink max output current | IFB = 500 mV | 30 | | | mA |
| BOOST OUTPUT REGULATION | | | | | | |
| V_{IFB_L} | V_O dial up threshold | ISET current = $20\text{ }\mu\text{A}$ | | 400 | | mV |
| V_{IFB_H} | V_O dial down threshold | ISET current = $20\text{ }\mu\text{A}$ | | 700 | | mV |
| V_{reg_L} | Min V_{out} regulation voltage | | | | 16 | V |
| V_{o_step} | V_O stepping voltage | | | 100 | 150 | mV |
| POWER SWITCH | | | | | | |
| R_{PWM_SW} | PWM FET on-resistance | | | 0.2 | 0.45 | Ω |
| R_{start} | Start up charging resistance | $V_O = 0\text{ V}$ | 100 | | 300 | Ω |
| V_{start_r} | Isolation FET start up threshold | $V_{IN} - V_O$, V_O ramp up | | 1.2 | 2 | V |
| I_{LN_NFET} | PWM FET leakage current | $V_{SW} = 35\text{ V}$, $T_A = 25^{\circ}\text{C}$ | | | 1 | μA |

ELECTRICAL CHARACTERISTICS (continued)

$V_{BAT} = 10.8\text{ V}$, $0.1\text{ }\mu\text{F}$ at C_{in} , $EN = \text{Logic High}$, IFB current = 20 mA , IFB voltage = 500 mV , $T_A = -40^\circ\text{C}$ to 85°C , typical values are at $T_A = 25^\circ\text{C}$ (unless otherwise noted)

| PARAMETER | | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
|---------------------------|---|---|-----|-----|-----|------------------|
| OSCILLATOR | | | | | | |
| f_S | Oscillator frequency | | 0.9 | 1.0 | 1.2 | MHz |
| D_{max} | Maximum duty cycle | $IFB = 0\text{ V}$ | | 94 | | % |
| D_{min} | Minimum duty cycle | | | | 7 | % |
| OS, SC, OVP AND SS | | | | | | |
| I_{LIM} | N-Channel MOSFET current limit | $D = D_{max}$ | 1.5 | | 3 | A |
| V_{ovp} | V_O overvoltage threshold | Measured on the V_O pin | 38 | 39 | 40 | V |
| V_{ovp_IFB} | IFB overvoltage threshold | Measured on the $IFBx$ pin | 15 | 17 | 20 | V |
| V_{sc} | Short circuit detection threshold | $V_{IN}-V_O$, V_O ramp down | | 1.7 | 2.5 | V |
| V_{sc_dly} | Short circuit detection delay during start up | | | 32 | | ms |
| Fault OUTPUT | | | | | | |
| V_{fault_high} | Fault high voltage | Measured as $V_{BAT}-V_{Fault}$ | | 0.1 | | V |
| V_{fault_low} | Fault low voltage | Measured as $V_{BAT}-V_{Fault}$, sink 0.1 mA , $V_{in} = 15\text{ V}$ | 6 | 8 | 10 | V |
| THERMAL SHUTDOWN | | | | | | |
| $T_{shutdown}$ | Thermal shutdown threshold | | | 160 | | $^\circ\text{C}$ |
| $T_{hysteresis}$ | Thermal shutdown threshold hysteresis | | | 15 | | $^\circ\text{C}$ |

PINOUT



PIN ASSIGNMENTS

| PIN NO. | PIN NAME | I/O | DESCRIPTION |
|-----------------------|------------------------|-----|---|
| 1 | PGND | I | Power ground of the IC. Internally, it connects to the source of the PWM switch. |
| 2 | SW | I | This pin connects to the drain of the internal PWM switch, external Schottky diode and inductor. |
| 3 | V _{BAT} | I | This pin is connected to the battery supply. It provides the pull-up voltage for the Fault pin and battery voltage signal. This is also the input to the internal LDO. |
| 4 | V _O | O | This pin monitors the output of the boost regulator. Connect this pin to the anode of the WLED strings. |
| 5 | ISET | I | The resistor on this pin programs the WLED output current. |
| 6 | Cin | I | Supply voltage of the IC. It is the output of the internal LDO. Connect 0.1 μ F bypass capacitor to this pin. |
| 7, 8, 9 12, 13, 14 | IFB1-IFB3 IFB4-IFB6 | I | Current sink regulation inputs. They are connected to the cathode of WLEDs. The PWM loop regulates the lowest V _{IFB} to 400 mV. Each channel is limited to 30 mA current. |
| 10 | GND | I | Signal ground of the IC. |
| 11 | DCTRL | I | Dimming control logic input. The dimming frequency range is 100 Hz to 1 kHz. |
| 15 | EN | I | The enable pin to the IC. A logic high signal turns on the internal LDO and enables the IC. Therefore, do not connect the EN pin to the Cin pin. |
| 16 | Fault | I | Gate driver output for an external PFET used for fault protection. It can also be used as signal output for system fault report. |

TYPICAL CHARACTERISTICS

Table of Graphs

| Description (Reference to application circuit in Figure 15) | | Figure |
|--|--|---------------------------|
| DC Load Efficiency | $V_{bat} = 5V, 10.8V, 19V; V_O = 28.6V, 9LEDs; L = 10\mu H$ | Figure 1 |
| DC Load Efficiency | $V_{bat} = 5V, 10.8V, 19V; V_O = 31.7V, 10LEDs; L = 10\mu H$ | Figure 2 |
| PWM Dimming Efficiency | $V_{bat} = 5V, 10.8V$ and $19V; V_O = 25.5V, 8LEDs; PWM\ Freq = 1kHz$ | Figure 3 |
| PWM Dimming Efficiency | $V_{bat} = 5V, 10.8V$ and $19V; V_O = 28.6V, 9LEDs; PWM\ Freq = 1kHz$ | Figure 4 |
| PWM Dimming Efficiency | $V_{bat} = 5V, 10.8V$ and $19V; V_O = 31.7V, 10LEDs; PWM\ Freq = 1kHz$ | Figure 5 |
| PWM Dimming Efficiency | $V_{bat} = 5V, 10.8V$ and $19V; V_O = 34.8V, 11LEDs; PWM\ Freq = 1kHz$ | Figure 6 |
| Dimming Linearity | $V_{bat} = 10.8V; V_O = 28.6V, 9LEDs; I_{set} = 20\mu A; PWM\ Freq = 1kHz$ | Figure 7 |
| Dimming Linearity | $V_{bat} = 10.8V; V_O = 28.6V, 9LEDs; I_{set} = 20\mu A; PWM\ Freq = 200Hz$ | Figure 8 |
| Output Ripple | $V_O = 28.6V; I_{set} = 20\mu A; PWM\ Freq = 200Hz; Duty = 50\%$ | Figure 9 |
| Switching Waveform | $V_{bat} = 10.8V; I_{set} = 20\mu A$ | Figure 10 |
| Output Ripple at PWM Dimming | $V_{bat} = 10.8V; I_{set} = 20\mu A; PWM\ Freq = 200Hz; Duty = 50\%; C_O = 4.7\mu F$ | Figure 11 |
| Short Circuit Protection | $V_{bat} = 10.8V; I_{set} = 20\mu A$ | Figure 12 |
| Open WLED Protection | $V_{bat} = 10.8V; I_{set} = 20\mu A$ | Figure 13 |
| Startup Waveform | $V_{bat} = 10.8V; I_{set} = 20\mu A$ | Figure 14 |

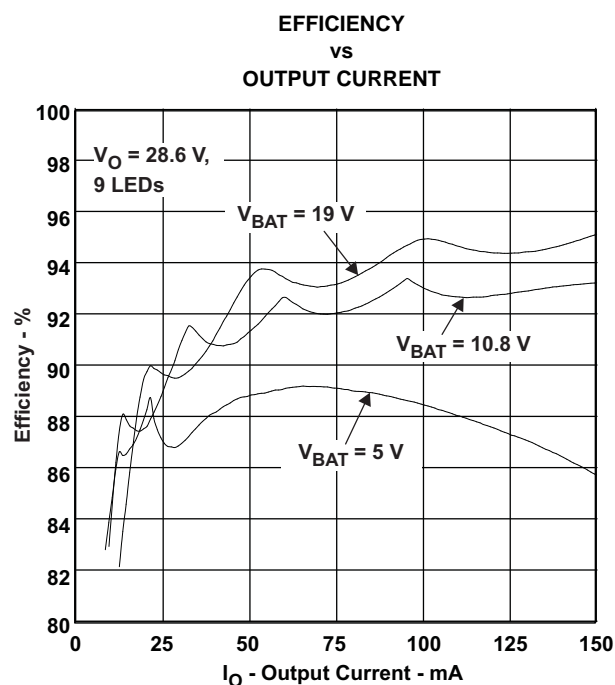


Figure 1.

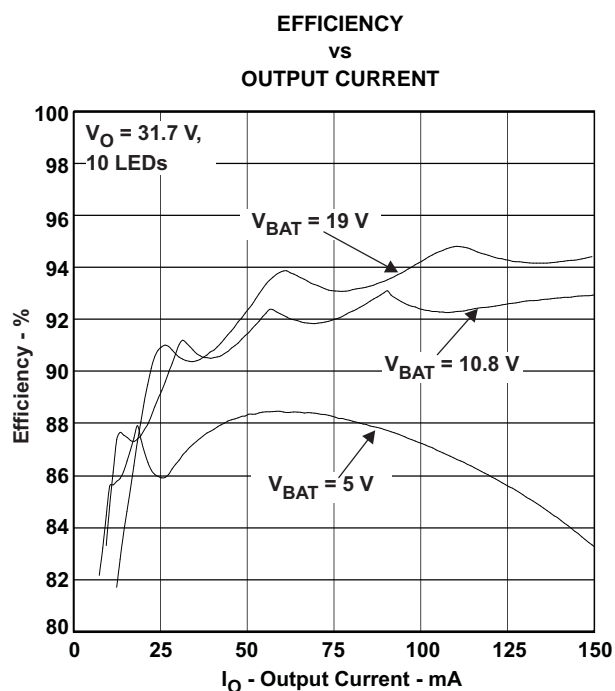


Figure 2.

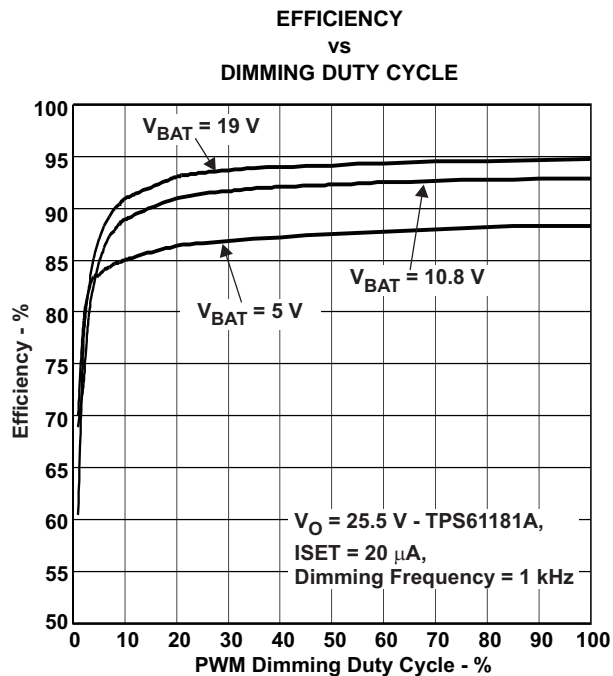


Figure 3.

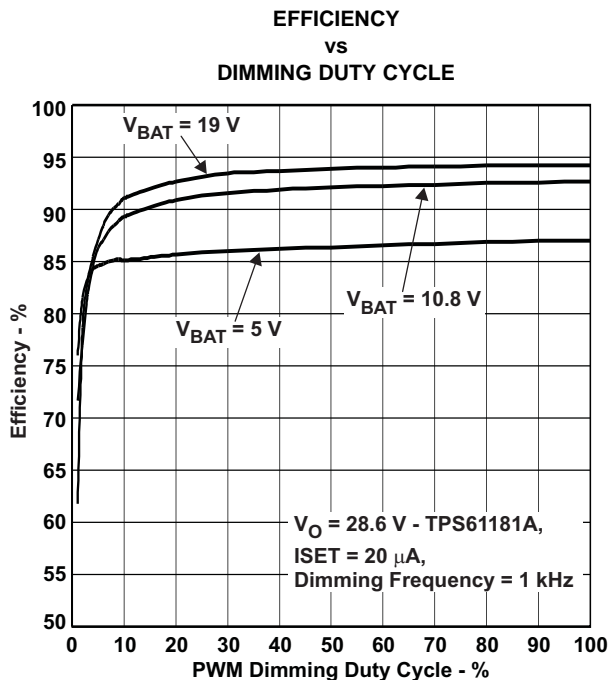


Figure 4.

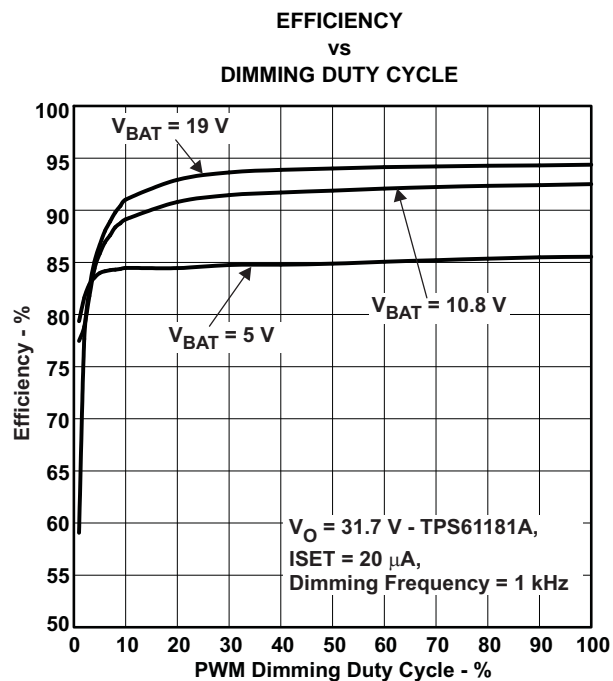


Figure 5.

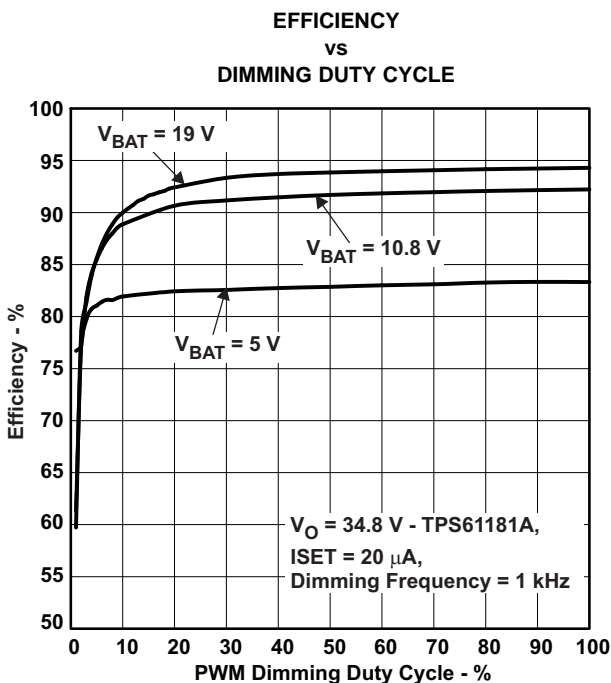


Figure 6.

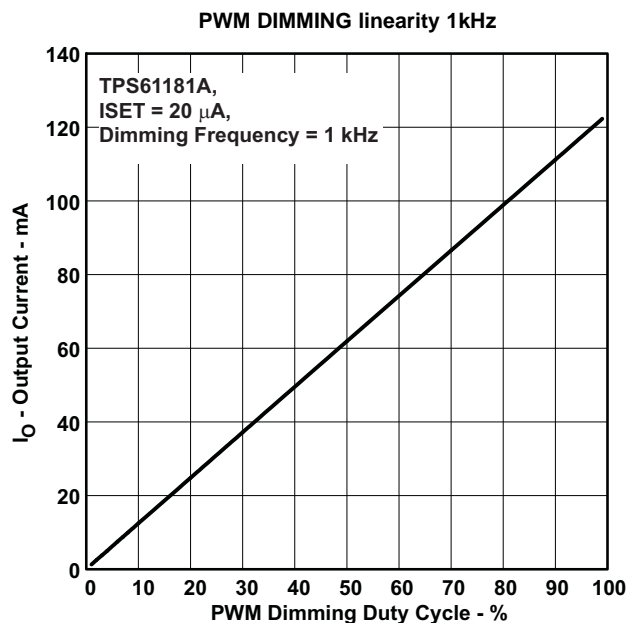


Figure 7.

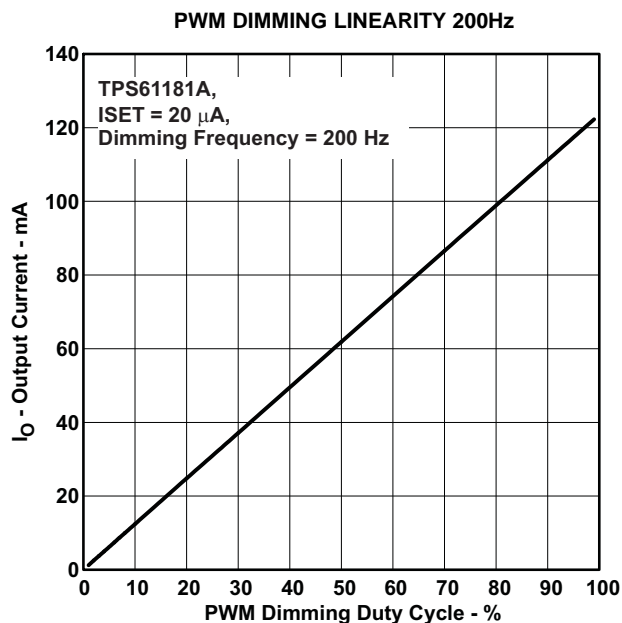


Figure 8.

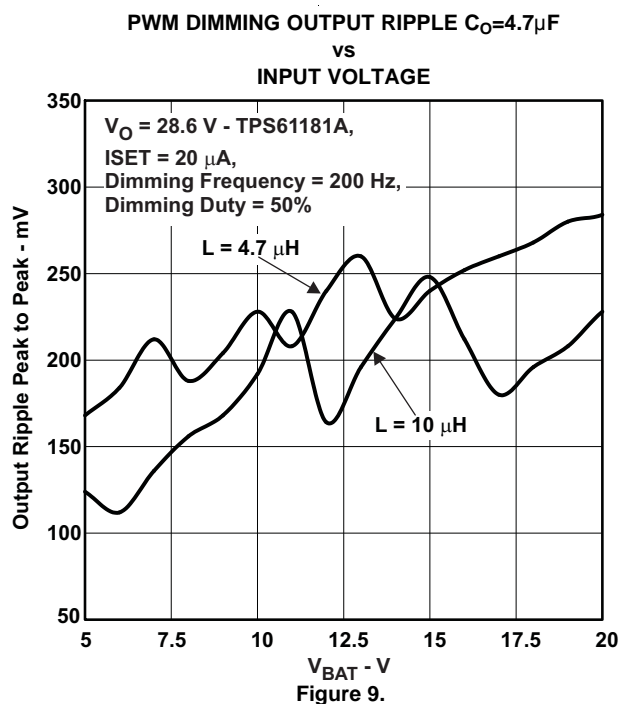


Figure 9.

SWITCHING WAVEFORM

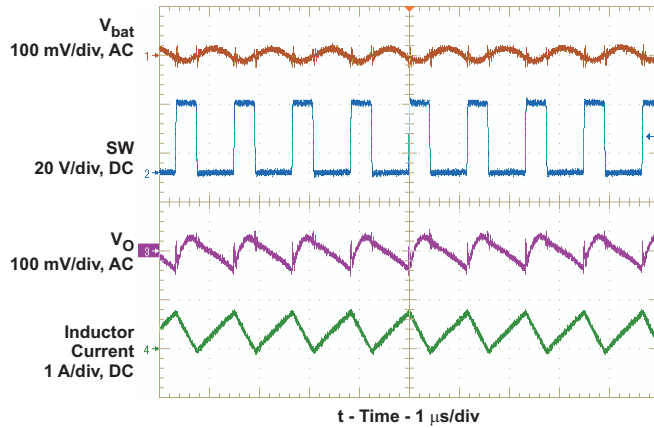


Figure 10.

OUTPUT RIPPLE AT PWM DIMMING $C_O=4.7\mu\text{F}$

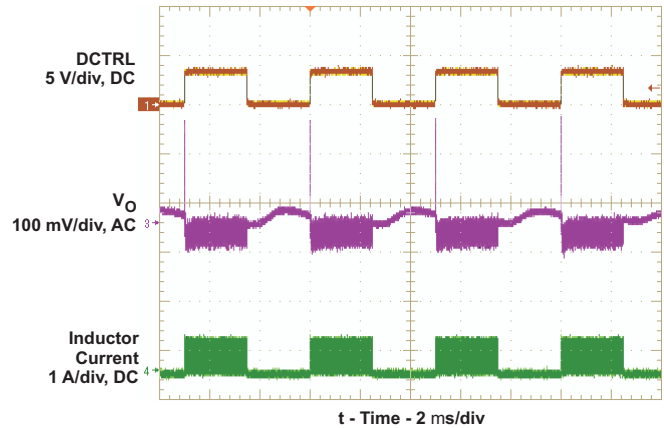


Figure 11.

OUTPUT SHORT PROTECTION

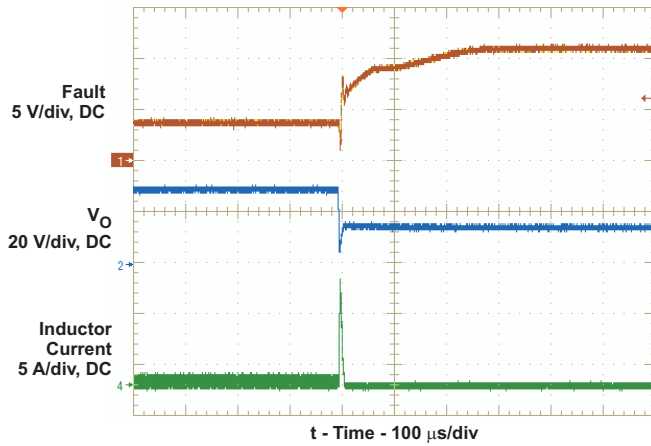


Figure 12.

OPEN WLED PROTECTION

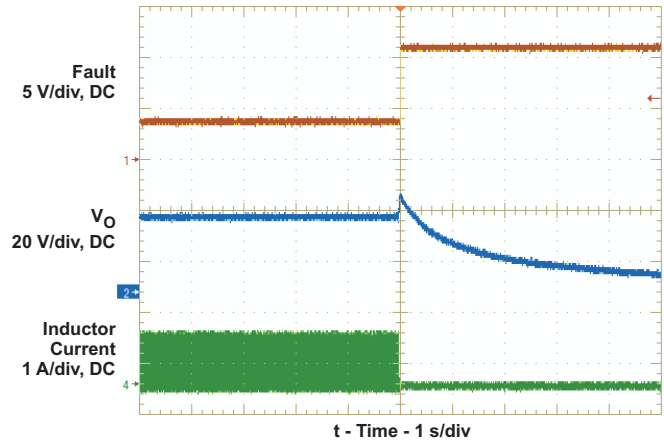


Figure 13.

STARTUP WAVEFORM

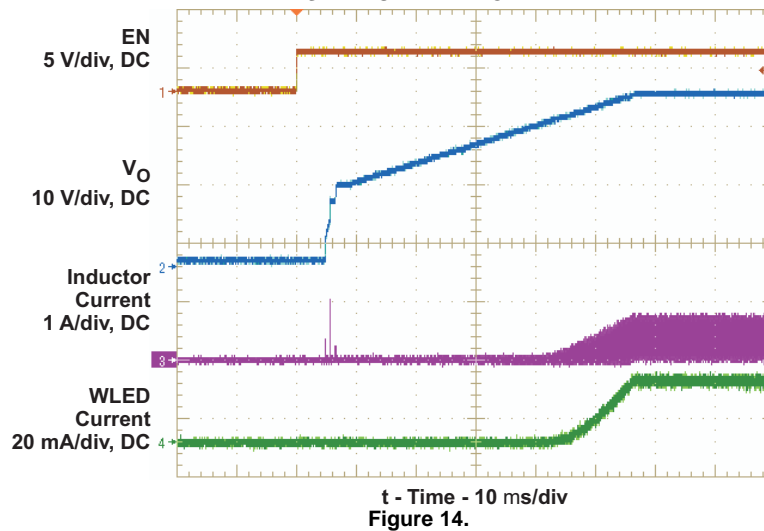
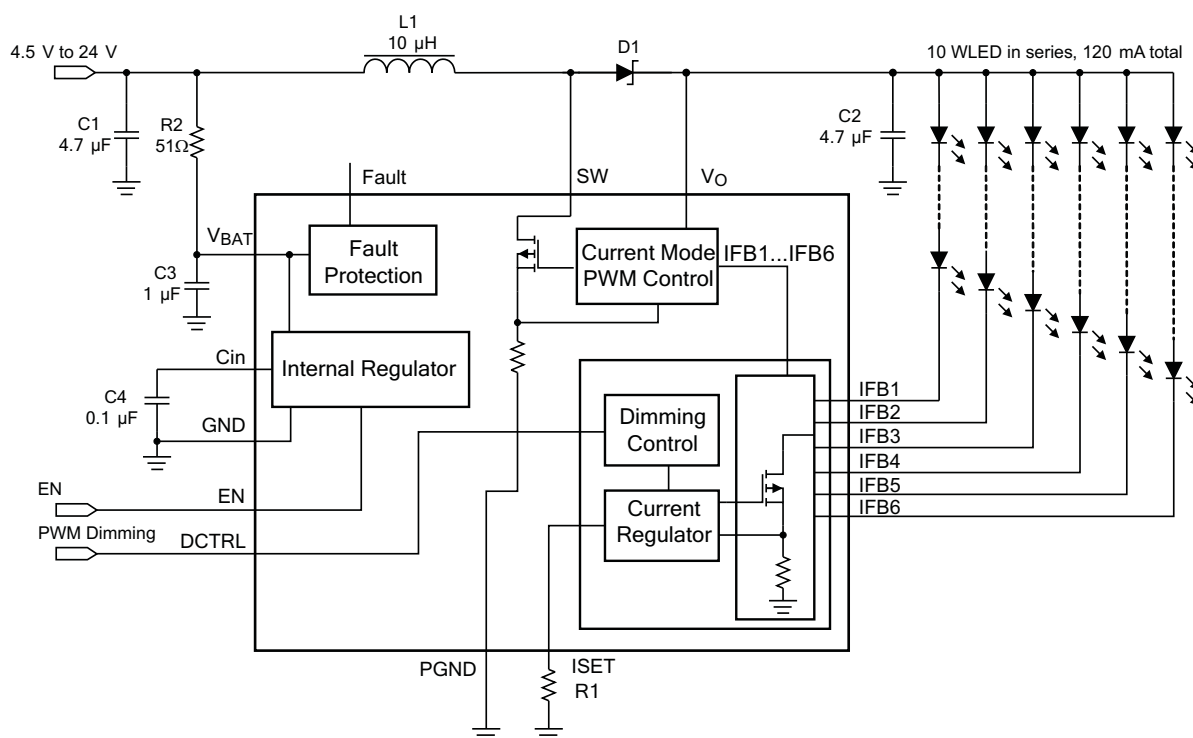


Figure 14.

FUNCTIONAL BLOCK DIAGRAM

DETAILED DESCRIPTION

Recently, WLEDs have gained popularity as an alternative to CCFL for backlighting media size LCD displays. The advantages of WLEDs are power efficiency and low profile design. Due to the large number of WLEDs, they are often arranged in series and parallel, and powered by a boost regulator with multiple current sink regulators. Having more WLEDs in series reduces the number of parallel strings and therefore improves overall current matching. However, the efficiency of the boost regulator declines due to the need for high output voltage. Also, there have to be enough WLEDs in series to ensure the output voltage stays above the input voltage range. Otherwise, a buck-boost (for example, SEPIC) power converter has to be adopted which could be more expensive and complicated.

The TPS61181A IC has integrated all the key function blocks to power and control up to 60 WLEDs. The devices include a 40V/1.5A boost regulator, six 30mA current sink regulators and protection circuit for over-current, over-voltage and short circuit failures. The key advantages of the devices are small solution size, low output AC ripple during PWM dimming control, and the capability to isolate the input and output during fault conditions.

SUPPLY VOLTAGE

The TPS61181A has built-in LDO linear regulator to supply the IC analog and logic circuits. The LDO is powered up when the EN pin is high. The output of the LDO is connected to the Cin pin. A 0.1 μ F bypass capacitor is required for LDO's stable operation. Do not connect the Cin pin to the EN pin because this prevents the IC from starting up. In addition, avoid connecting the Cin pin to any other circuit as this could introduce noise into the IC supply voltage.

The V_{BAT} connects to the input of the internal LDO, and powers the IC. The voltage on the V_{BAT} pin is also the reference for the pull-up circuit of the Fault pin. In addition, it serves as the input signal to the short circuit protection. There is an under-voltage lockout on the V_{BAT} pin which disables the IC when its voltage reduces to 4.2V (Typical). The IC restarts when the V_{BAT} pin voltage recovers by 220mV.

BOOST REGULATOR

The boost regulator is controlled by current mode PWM, and loop compensation is integrated inside the IC. The internal compensation ensures stable output over the full input and output voltage range. The TPS61181A switches at 1.0MHz which optimize boost converter efficiency and voltage ripple with a small form factor inductor and output capacitor.

The output voltage of the boost regulator is automatically set by the IC to minimize the voltage drop across the IFB pins. The IC automatically regulates the lowest IFB pin to 400mV, and consistently adjusts the boost output voltage to account for any changes of the LED forward voltages.

When the output voltage is too close to the input, the boost regulator may not be able to regulate the output due to the limitation of minimum duty cycle. In this case, increase the number of WLED in series or include series ballast resistors in order to provide enough headroom for the boost operation.

The TPS61181A boost regulator cannot regulate its output to voltages below 15V.

CURRENT PROGRAM AND PWM DIMMING

The six current sink regulators can each provide a maximum of 30mA. The IFB current must be programmed to maximum WLED current using the ISET pin resistor and the following Equation 1.

$$I_{FB} = K_{ISET} \frac{V_{ISET}}{R_{ISET}} \quad (1)$$

Where

K_{ISET} = Current multiple (1000 typical)

V_{ISET} = ISET pin voltage (1.229 V typical)

R_{ISET} = ISET pin resistor

The TPS61181A has six built-in precise current sink regulators. The current matching among the current sinks at 20mA current through is below 2.5%. This means the differential value between the maximum and minimum current of the six current sinks divided by the average current of the six is less than 2.5%.

The WLED brightness is controlled by the PWM signal on the DCTRL pin. The frequency and duty cycle of the DCTRL signal is replicated on the IFB pin current. Keep the dimming frequency in the range of 100Hz to 1kHz to avoid screen flickering and maintain dimming linearity. Screen flickering may occur if the dimming frequency is below the range. The minimum achievable duty cycle increases with the dimming frequency. For example, while a 0.1% dimming duty cycle, giving a 1000:1 dimming range, is achievable at 100 Hz dimming frequency, only 1% duty cycle, giving a 100:1 dimming range, is achievable with a 1 KHz dimming frequency, and 5% dimming duty cycle is achievable with 5KHz dimming frequency. The device could work at high dimming frequency like 20 KHz, but then only 15% duty cycle could be achievable. The TPS61181A is designed to minimize the AC ripple on the output capacitor during PWM dimming. Careful passive component selection is also critical to minimize AC ripple on the output capacitor. See APPLICATION INFORMATION for more information.

ENABLE AND START UP

A logic high signal on the EN pin turns on the IC. For the TPS61181A, taking EN high turns on the internal LDO linear regulator which provides supply to the IC current. Then, an internal resistor, R_{start} (start up charging resistor) is connected between the V_{BAT} pin and V_O pin to charge the output capacitor toward the V_{BAT} pin voltage. The Fault pin outputs high during this time, and thus the external isolation PFET is turned off. Once the V_O pin voltage is within 2 V (isolation FET start up threshold) of the V_{BAT} pin voltage, R_{start} is open, and the Fault pin pulls down the gate of the PFET and connects the V_{BAT} voltage to the boost regulator. This operation is to prevent the in-rush current due to charging the output capacitor.

Once the isolation FET is turned on, the IC starts PWM switching to raise the output voltage above V_{BAT} . Soft-start is implemented by gradually ramping up the reference voltage of the error amplifier to prevent voltage over-shoot and in-rush current. See the start-up waveform of a typical example, Figure 14.

Pulling the EN pin low immediately shuts down the IC, resulting in the IC consuming less than 50µA in the shutdown mode.

OVER-CURRENT, OVER-VOLTAGE AND SHORT-CIRCUIT PROTECTION

The TPS61181A has pulse-by-pulse over-current limit of 1.5A (min). The PWM switch turns off when the inductor current reaches this current threshold. The PWM switch remains off until the beginning of the next switching cycle. This protects the IC and external components under over-load conditions. When there is sustained over-current condition for more than 16ms (under 100% dimming duty cycle), the IC turns off and requires POR or the EN pin toggling to restart.

Under severe over-load and/or short circuit conditions, the V_O pin can be pulled below the input (V_{BAT} pin). Under this condition, the current can flow directly from V_{BAT} to the WLED through the inductor and schottky diode. Turning off the PWM switch alone does not limit current anymore. In this case, the TPS61181A detects the output voltage is 1.7V (V_{sc} , short circuit detection threshold) below the input voltage, turns off the isolation FET, and shuts down the IC. The IC restarts after input power-on reset (V_{BAT} POR) or EN pin logic toggling.

During IC start up, if there is short circuit condition on the boost converter output, the output capacitor will not be charged to within 2V of V_{BAT} through R_{start} . After 32ms (V_{sc_dly} , short circuit detection delay during start up), the TPS61181A shuts down and does not restart until there is V_{BAT} POR or EN pin toggling. The isolation FET is never turned on under the condition.

If one of the WLED strings is open, the boost output rises to over-voltage threshold (39V typical). The TPS61181A detects the open WLED string by sensing no current in the corresponding IFB pin. As a result, the IC removes the open IFB pin from the voltage feedback loop. Subsequently, the output voltage drops down and is regulated to a voltage for the connected WLED strings. The IFB current of the connected WLED strings keep in regulation during the whole transition. The IC only shuts down if it detects that all of the WLED strings are open.

If the over-voltage threshold is reached, but the current sensed on the IFB pin is below the regulation target, the IC regulates the boost output at the over-voltage threshold. This operation could occur when the WLED is turned on under cold temperature, and the forward voltages of the WLEDs exceed the over-voltage threshold. Maintaining the WLED current allows the WLED to warm up and their forward voltages to drop below the over-voltage threshold.

If any IFB pin voltage exceeds IFB over-voltage threshold (17V typical), the IC turns off the corresponding current sink and removes this IFB pin from V_O regulation loop. The remaining IFB pins' current regulation is not affected. This condition often occurs when there are several shorted WLEDs in one string. WLED mismatch typically does not create such large voltage difference among WLED strings.

IFB PIN UNUSED

If the application requires less than 6 WLED strings, one can easily disable unused IFB pins. The TPS61181A simply requires leaving the unused IFB pin open or shorting it to ground. If the IFB pin is open, the boost output voltage ramps up to V_O over-voltage threshold during start up. The IC then detects the zero current string, and removes it from the feedback loop. If the IFB pin is shorted to ground, the IC detects the short immediately after IC enable, and the boost output voltage does not go up to V_O over-voltage threshold. Instead, it ramps to the regulation voltage after soft start.

APPLICATION INFORMATION

INDUCTOR SELECTION

Because the selection of the inductor affects a power supply's steady state operation, transient behavior and loop stability, the inductor is the most important component in switching power regulator design. There are three specifications most important to the performance of the inductor: inductor value, DC resistance and saturation current. The TPS61181A ICs are designed to work with inductor values between 4.7μH and 10μH. A 4.7μH inductor may be available in a smaller or lower profile package, while 10μH may produce higher efficiency due to lower inductor ripple. If the boost output current is limited by the over-current protection of the IC, using a 10μH inductor can offer higher output current.

The internal loop compensation for the PWM control is optimized for the recommended component values, including typical tolerances. Inductor values can have ±20% tolerance with no current bias. When the inductor current approaches saturation level, its inductance can decrease 20 to 35% from the zero current value depending on how the inductor vendor defines saturation

In a boost regulator, the inductor DC current can be calculated as

$$I_{dc} = \frac{V_O \times I_O}{V_{in} \times \eta} \quad (2)$$

Where

V_O = boost output voltage

I_O = boost output current

V_{in} = boost input voltage

η = power conversion efficiency, use 90% for TPS61181A applications

The inductor current peak to peak ripple can be calculated as

$$I_{pp} = \frac{1}{L \times \left(\frac{1}{V_O - V_{bat}} + \frac{1}{V_{bat}} \right) \times F_S} \quad (3)$$

Where

I_{pp} = inductor peak to peak ripple

L = inductor value

F_S = Switching frequency

V_{bat} = boost input voltage

Therefore, the peak current seen by the inductor is

$$I_p = I_{dc} + \frac{I_{pp}}{2} \quad (4)$$

Select the inductor with saturation current at least 25% higher than the calculated peak current. To calculate the worse case inductor peak current, use minimum input voltage, maximum output voltage and maximum load current.

Regulator efficiency is dependent on the resistance of its high current path, switching losses associated with the PWM switch and power diode. Although the TPS61181A ICs have optimized the internal switch resistance, the overall efficiency still relies on the DC resistance (DCR) of the inductor; lower DCR improves efficiency. However, there is a trade off between DCR and inductor footprint. Furthermore, shielded inductors typically have a higher DCR than unshielded ones. [Table 1](#) lists recommended inductor models.

Table 1. Recommended Inductor for TPS61181A

| | L (μ H) | DCR Typ (m Ω) | I_{sat} (A) | Size (LXWXH mm) |
|------------------|------------------------|---------------------------------|-------------------------------|---------------------------|
| TOKO | | | | |
| A915AY-4R7M | 4.7 | 38 | 1.87 | 5.2x5.2x3.0 |
| A915AY-100M | 10 | 75 | 1.24 | 5.2x5.2x3.0 |
| TDK | | | | |
| SLF6028T-4R7M1R6 | 4.7 | 28.4 | 1.6 | 6.0x6.0x2.8 |
| SLF6028T-100M1R3 | 10 | 53.2 | 1.3 | 6.0x6.0x2.8 |

OUTPUT CAPACITOR SELECTION

During PWM brightness dimming, the load transient causes voltage ripple on the output capacitor. Since the PWM dimming frequency is in the audible frequency range, the ripple can produce audible noises on the output ceramic capacitor. There are two ways to reduce or eliminate this audible noise. The first option is to select PWM dimming frequency outside the audible range. This means the dimming frequency needs be to lower than 200Hz or higher than 30KHz. The potential issue with a very low dimming frequency is that WLED on/off can become visible and thus cause a flickering effect on the display. On the other hand, high dimming frequency can compromise the dimming range since the LED current accuracy and current match are difficult to maintain at low dimming duty cycle. The second option is to reduce the amount of the output ripple, and therefore minimize the audible noise.

The TPS61181A adopts a patented technology to limit output ripple even with small output capacitance. In a typical application, the output ripple is less than 200mV during PWM dimming with a 4.7 μ F output capacitor, and the audible noise is not noticeable. The devices are designed to be stable with output capacitor down to 1.0 μ F. However, the output ripple will increase with lower output capacitor.

Care must be taken when evaluating a ceramic capacitor's derating due to applied dc voltage, aging and over frequency. For example, larger form factor capacitors (in 1206 size) have their self resonant frequencies in the switching frequency range of the TPS61181A. So the effective capacitance is significantly lower. Therefore, it may be necessary to use small capacitors in parallel instead of one large capacitor.

AUDIBLE NOISE REDUCTION

Ceramic capacitors can produce audible noise if the frequency of its AC voltage ripple is in the audible frequency range. In TPS61181A applications, both input and output capacitors are subject to AC voltage ripple during PWM brightness dimming. The ICs integrate a patented technology to minimize the ripple voltage, and thus audible noises.

To further reduce the audible noise, one effective way is to use two or three small size capacitors in parallel instead of one large capacitor. The application circuit in [Figure 15](#) uses two 2.2- μ F/25V ceramic capacitors at the input and two 1- μ F/50V ceramic capacitors at the output. All of the capacitors are in 0805 package. Although the output ripple during PWM dimming is higher than with one 4.7 μ F in a 1206 package, the overall audible noise is lower.

In addition, connecting a 10-nF/50V ceramic capacitor between the V_O pin and IFB1 pin can further reduce the output AC ripple during the PWM dimming. Since this capacitor is subject to large AC ripple, choose a small package such as 0402 to prevent it from producing noise.

ISOLATION MOSFET SELECTION

The TPS61181A provides a gate driver to an external P-channel MOSFET which can be turned off during device shutdown or fault condition. This MOSFET can provide a true shutdown function, and also protect the battery from output short circuit conditions. The source of the PMOS should be connected to the input, and a pull up resistor is required between the source and gate of the FET to keep the FET off during IC shutdown. To turn on the isolation FET, the Fault pin is pulled low, and clamped at 8 V below the V_{BAT} pin voltage.

During device shutdown or fault condition, the isolation FET is turned off, and the input voltage is applied on the

isolation MOSFET. During a short circuit condition, the catch diode (D2 in typical application circuit) is forward biased when the isolation FET is turned off. The drain of the isolation FET swings below ground. The voltage across the isolation FET can be momentarily greater than the input voltage. Therefore, select a 30V MOSFET for a 24V maximum input. The on resistance of the FET has a large impact on power conversion efficiency since the FET carries the input voltage. Select a MOSFET with $R_{ds(on)}$ less than 100m Ω to limit the power losses.

LAYOUT CONSIDERATION

As for all switching power supplies, especially those providing high current and using high switching frequencies, layout is an important design step. If layout is not carefully done, the regulator could show instability as well as EMI problems. Therefore, use wide and short traces for high current paths. The input capacitor, C3 in the typical application circuit, needs not only to be close to the V_{BAT} pin, but also to the GND pin in order to reduce the input ripple seen by the IC. The input capacitor, C1 in the typical application circuit, should be placed close to the inductor. The SW pin carries high current with fast rising and falling edges. Therefore, the connection between the pin to the inductor and Schottky should be kept as short and wide as possible. It is also beneficial to have the ground of the output capacitor C2 close to the PGND pin since there is large ground return current flowing between them. When laying out signal ground, it is recommended to use short traces separated from power ground traces, and connect them together at a single point, for example on the thermal pad.

Thermal pad needs to be soldered on to the PCB and connected to the GND pin of the IC. Additional thermal via can significantly improve power dissipation of the IC.

ADDITIONAL APPLICATION CIRCUITS

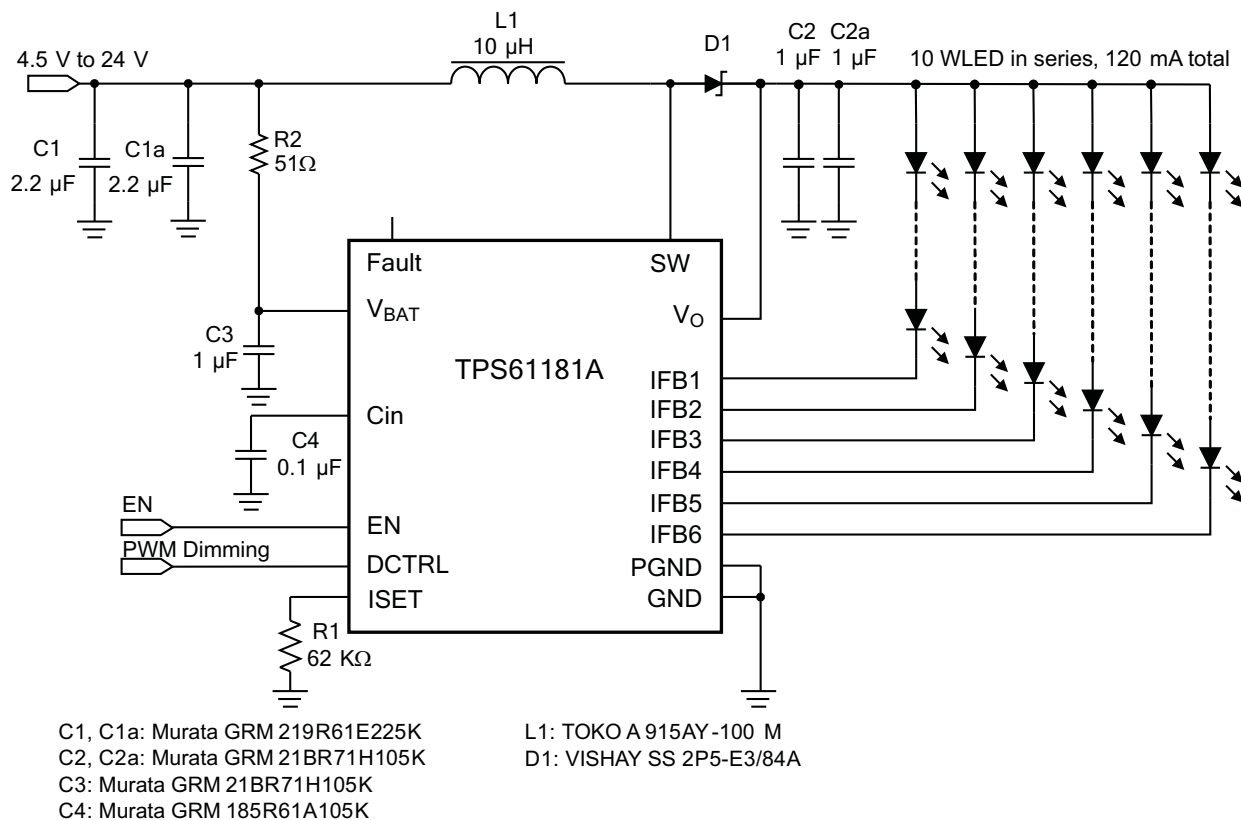


Figure 15. Audible Noise Reduction Circuit

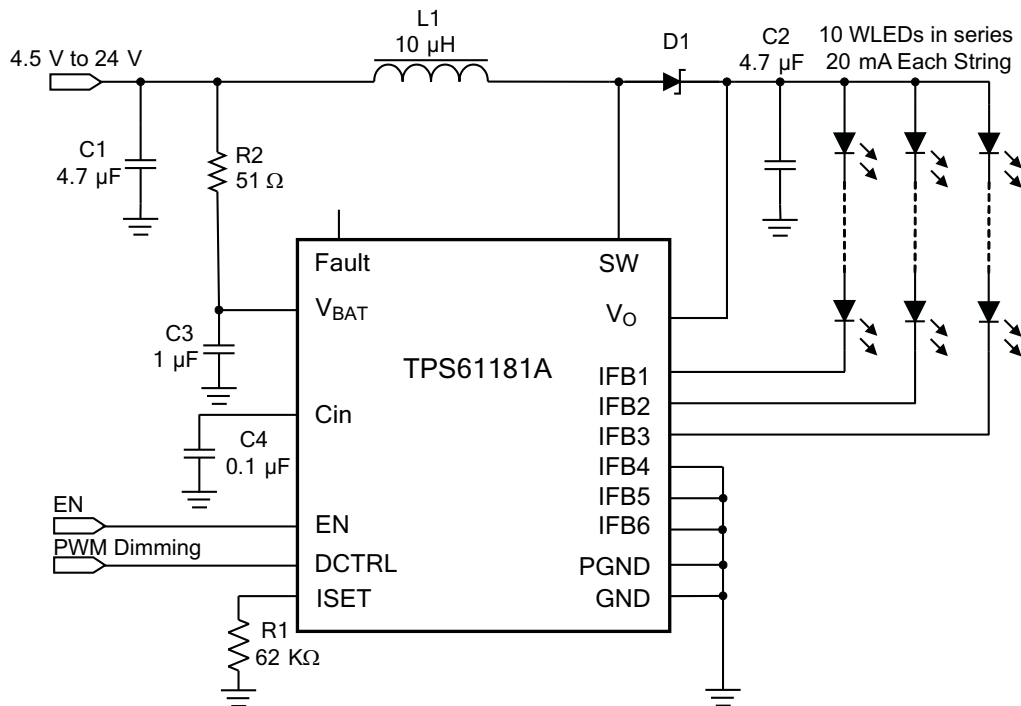


Figure 16. TPS61181A for Three Strings of LEDs

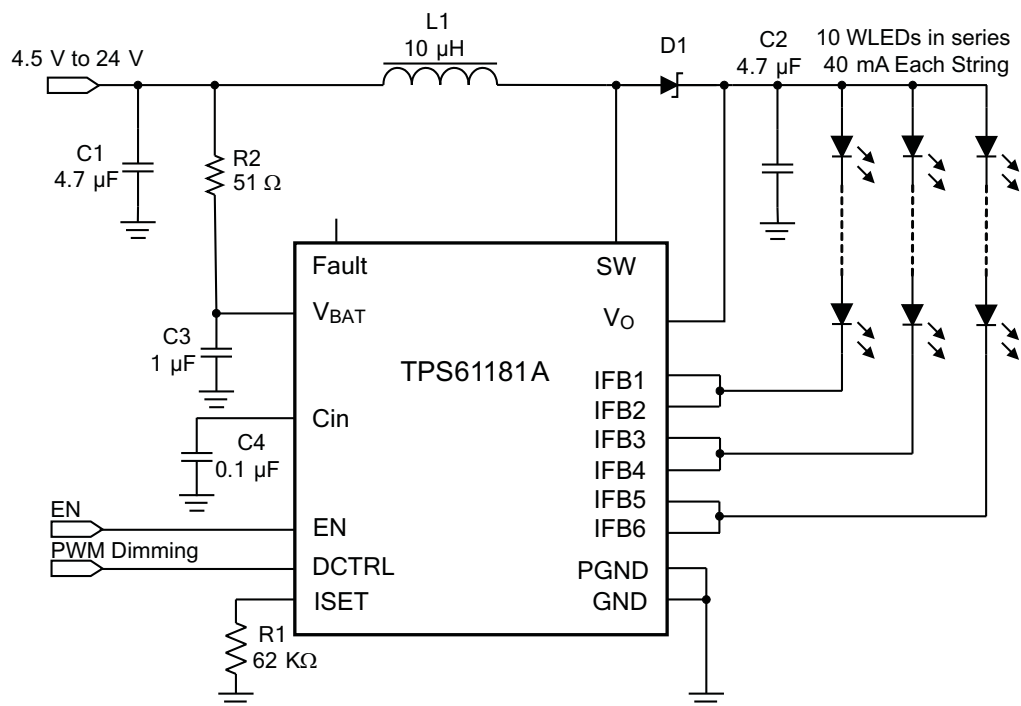


Figure 17. TSP61181A for Three Strings of LEDs with Double Current

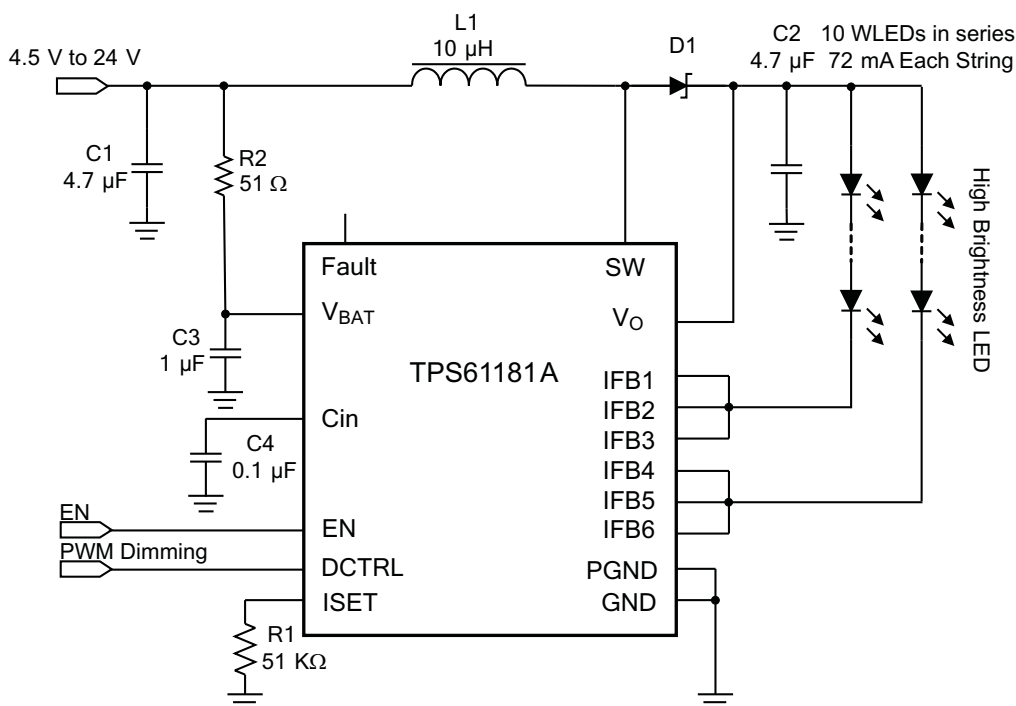


Figure 18. TSP61181A for Two Strings High Brightness LEDs Application

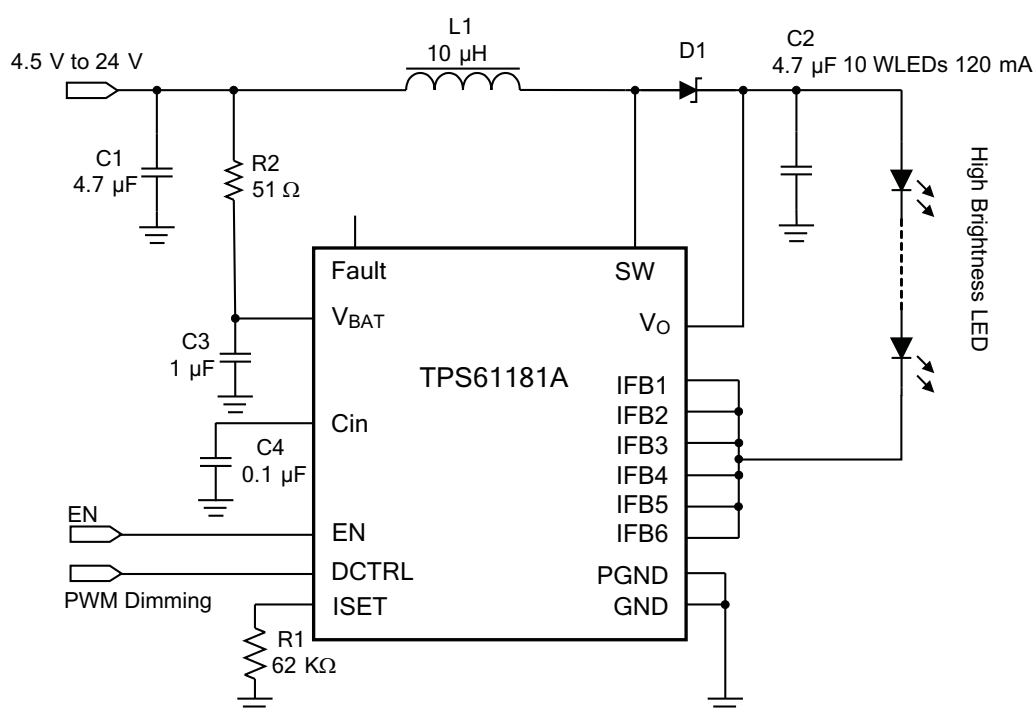


Figure 19. TSP61181A for One String High Brightness LEDs Application

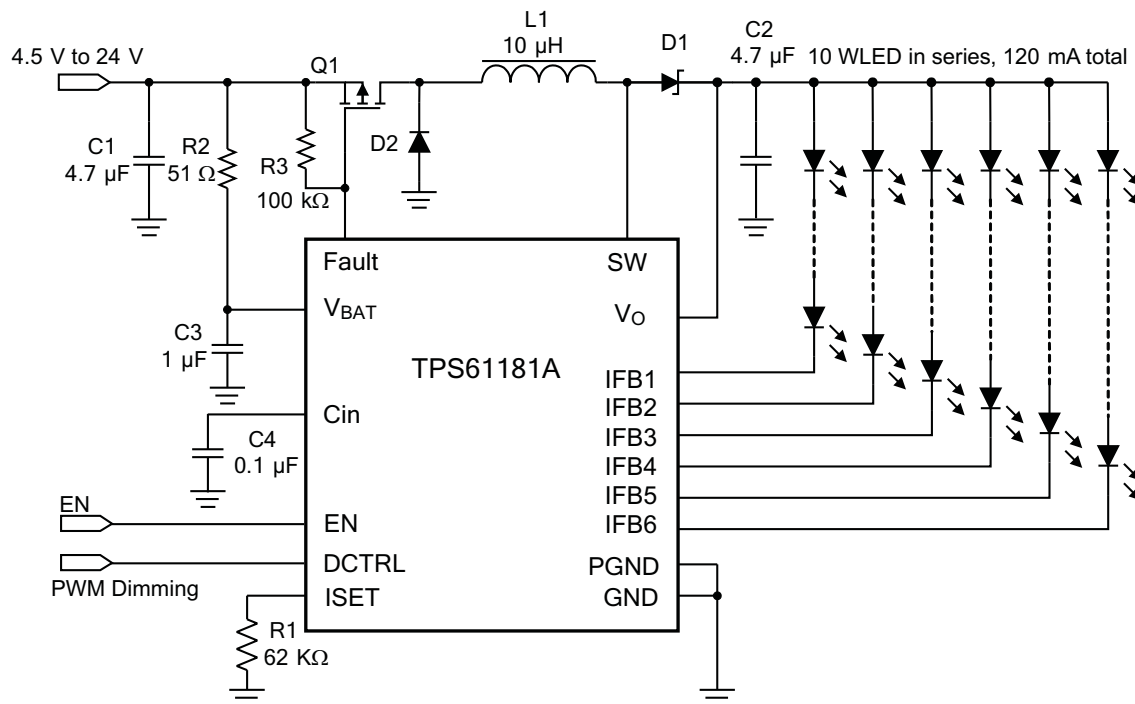


Figure 20. TPS61181A Driving External PFET for True Shutdown Application

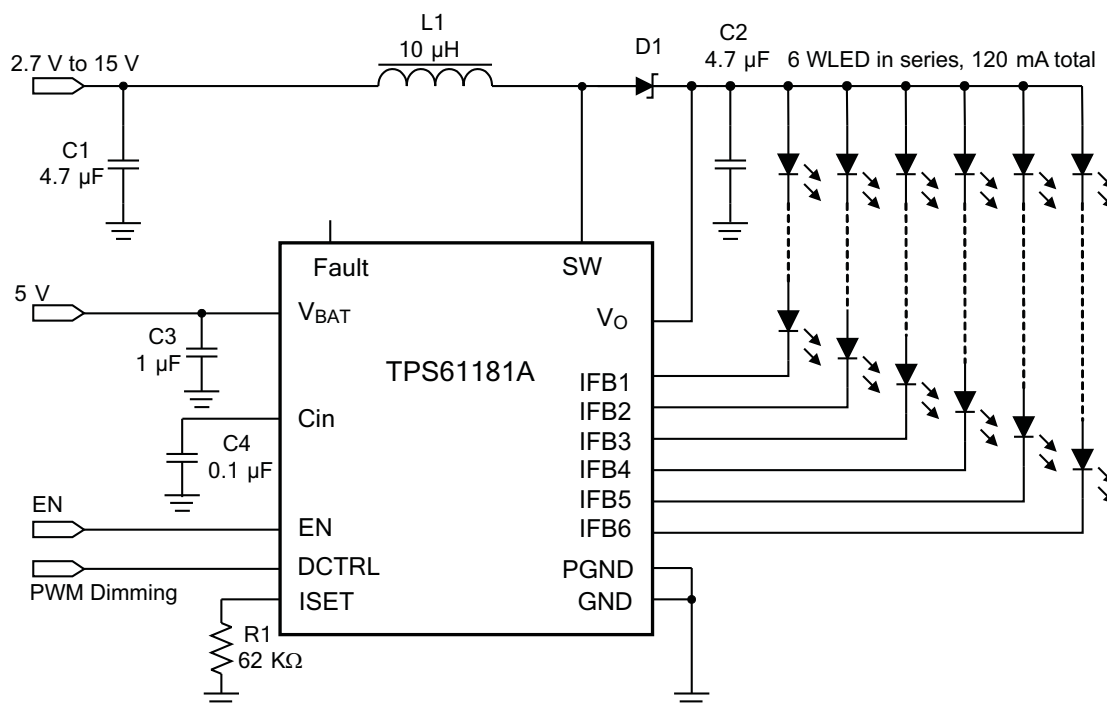
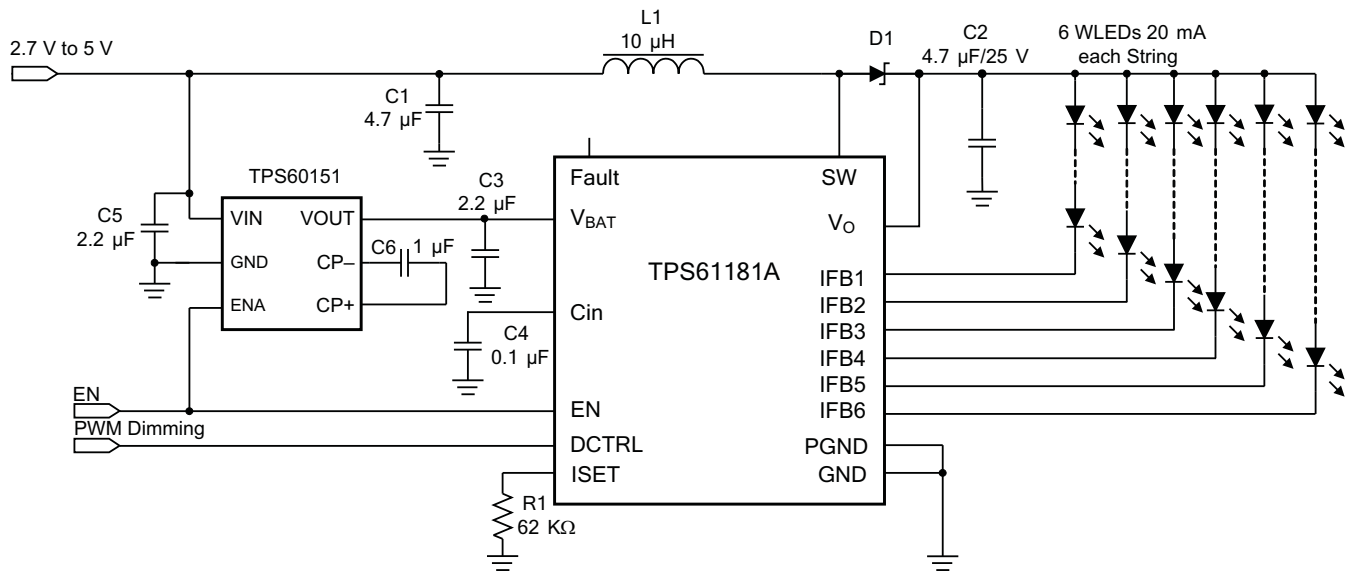


Figure 21. TPS61181A with Separate V_{BAT} Power for Low Voltage Input Application



REVISION HISTORY

Note: Page numbers of current version may differ from previous version.

| Changes from Original (February) to Revision A | Page |
|--|-------------------|
| • Deleted Voltage Range spec for "all other pins" in the Absolute Maximum Ratings table. | 2 |
| • Added F_{PWM} spec. for PWM dimming frequency at $D_{PWM} \geq 1\%$ and $D_{PWM} \geq 5\%$ | 2 |

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PACKAGING INFORMATION

| Orderable part number | Status (1) | Material type (2) | Package Pins | Package qty Carrier | RoHS (3) | Lead finish/ Ball material (4) | MSL rating/ Peak reflow (5) | Op temp (°C) | Part marking (6) |
|-------------------------------|---------------|----------------------|-----------------|-----------------------|-------------|--------------------------------------|-----------------------------------|--------------|---------------------|
| TPS61181ARTER | Active | Production | WQFN (RTE) 16 | 3000 LARGE T&R | Yes | NIPDAU | Level-2-260C-1 YEAR | -40 to 85 | QWF |
| TPS61181ARTER.B | Active | Production | WQFN (RTE) 16 | 3000 LARGE T&R | Yes | NIPDAU | Level-2-260C-1 YEAR | -40 to 85 | QWF |
| TPS61181ARTET | Active | Production | WQFN (RTE) 16 | 250 SMALL T&R | Yes | NIPDAU | Level-2-260C-1 YEAR | -40 to 85 | QWF |
| TPS61181ARTET.B | Active | Production | WQFN (RTE) 16 | 250 SMALL T&R | Yes | NIPDAU | Level-2-260C-1 YEAR | -40 to 85 | QWF |

⁽¹⁾ **Status:** For more details on status, see our [product life cycle](#).

⁽²⁾ **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

⁽³⁾ **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

⁽⁴⁾ **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

⁽⁵⁾ **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

⁽⁶⁾ **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

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TAPE AND REEL INFORMATION



*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Reel Diameter (mm) | Reel Width W1 (mm) | A0 (mm) | B0 (mm) | K0 (mm) | P1 (mm) | W (mm) | Pin1 Quadrant |
|---------------|--------------|-----------------|------|------|--------------------|--------------------|---------|---------|---------|---------|--------|---------------|
| TPS61181ARTER | WQFN | RTE | 16 | 3000 | 330.0 | 12.4 | 3.3 | 3.3 | 1.1 | 8.0 | 12.0 | Q2 |
| TPS61181ARTET | WQFN | RTE | 16 | 250 | 180.0 | 12.4 | 3.3 | 3.3 | 1.1 | 8.0 | 12.0 | Q2 |

TAPE AND REEL BOX DIMENSIONS



*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Length (mm) | Width (mm) | Height (mm) |
|---------------|--------------|-----------------|------|------|-------------|------------|-------------|
| TPS61181ARTER | WQFN | RTE | 16 | 3000 | 353.0 | 353.0 | 32.0 |
| TPS61181ARTET | WQFN | RTE | 16 | 250 | 213.0 | 191.0 | 35.0 |

GENERIC PACKAGE VIEW

RTE 16

WQFN - 0.8 mm max height

3 x 3, 0.5 mm pitch

PLASTIC QUAD FLATPACK - NO LEAD

This image is a representation of the package family, actual package may vary.
Refer to the product data sheet for package details.



4225944/A



4219117/B 04/2022

NOTES:

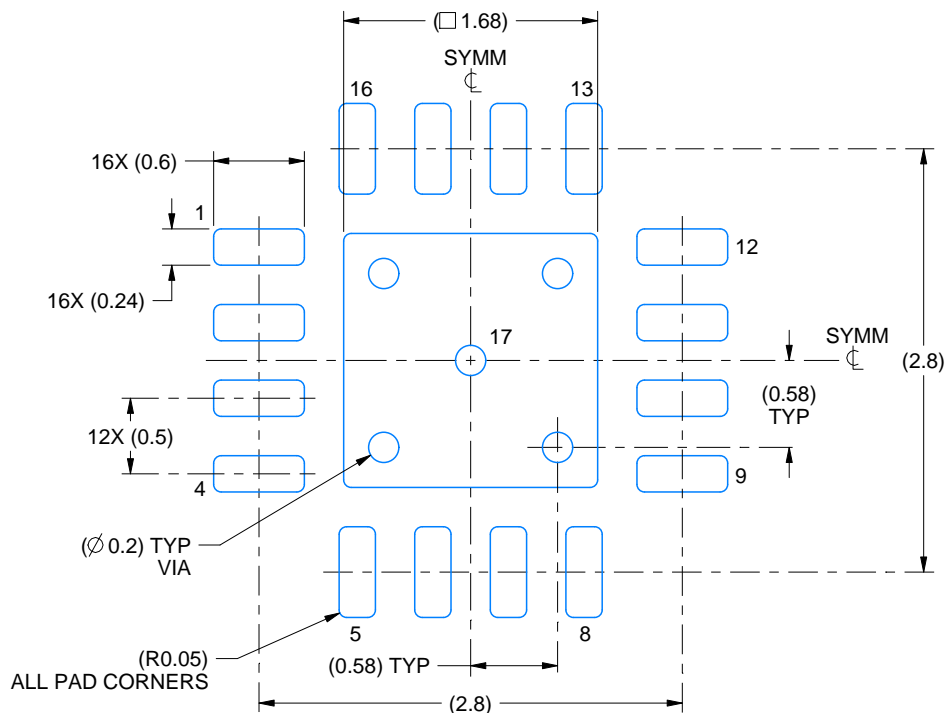
1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.

EXAMPLE BOARD LAYOUT

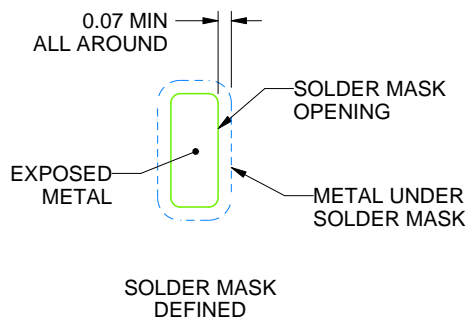
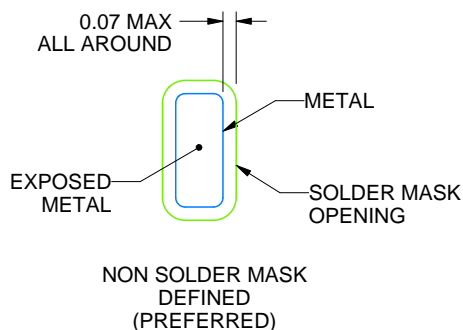
RTE0016C

WQFN - 0.8 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



LAND PATTERN EXAMPLE
EXPOSED METAL SHOWN
SCALE:20X



SOLDER MASK DETAILS

4219117/B 04/2022

NOTES: (continued)

- This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/sluea271).
- Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.

RTE0016C

WQFN - 0.8 mm max height

PLASTIC QUAD FLATPACK - NO LEAD



SOLDER PASTE EXAMPLE BASED ON 0.125 mm THICK STENCIL

EXPOSED PAD 17:
85% PRINTED SOLDER COVERAGE BY AREA UNDER PACKAGE
SCALE:25X

4219117/B 04/2022

NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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