



TPS61093-Q1 具有集成功率二极管和输入/输出隔离功能的 低输入升压转换器

1 特性

- 具有符合 AEC-Q100 的下列结果：
 - 器件温度 1 级：-40°C 至 125°C 结温工作温度范围
- 输入范围：1.6V 至 6V
- 集成功率二极管和隔离场效应晶体管 (FET)
- 具有 1.1A 电流的 20V 内部开关 FET
- 1.2MHz 固定开关频率
- 15V 输出时的效率高达 88%
- 过载和过压保护
- 可编程软启动
- 负载放电路径 (IC 关断后)
- 2.5 × 2.5 × 0.8mm 小外形无引线 (SON) 封装

2 应用

- 有机发光二极管 (OLED) 电源
- 3.3V 至 12V、5V 至 12V 升压转换器

3 说明

TPS61093-Q1 是一款兼具高集成度和高可靠性的 1.2MHz 固定频率升压转换器。该集成电路 (IC) 集成有 20V 电源开关、输入/输出隔离开关以及功率二极管。当输出电流超出过载限值时，IC 的隔离开关会断开，进而使输出与输入断开连接。这一断开功能可保护 IC 和输入电源。在关断期间，隔离开关也会使输出与输入断开连接，以便最大限度降低泄漏电流。当 IC 关断时，输出电容会通过内部二极管放电至低电压。其他保护特性包括逐周期 1.1A 峰值过流保护 (OCP)、输出过压保护 (OVP)、热关断以及欠压闭锁 (UVLO)。

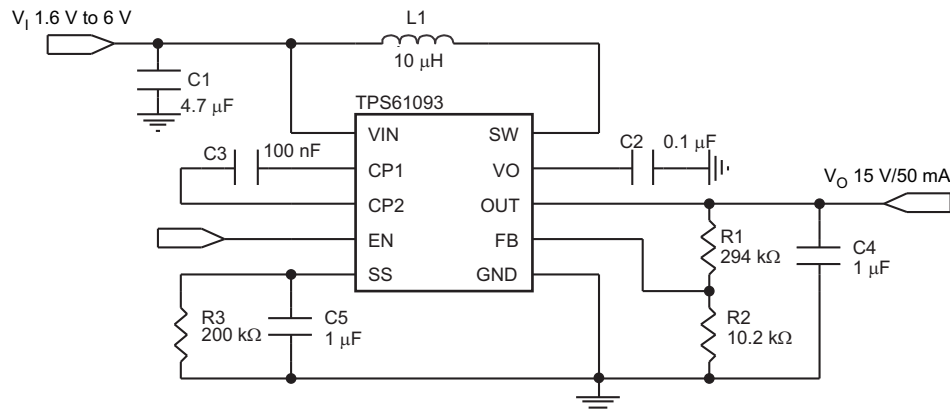
IC 的最低输入电压为 1.6V，可通过两个碱性电池、单个锂离子电池或者 3.3V 和 5V 稳压电源供电运行。输出电压最高可升压至 17V。TPS61093-Q1 采用带散热焊盘的 2.5mm × 2.5mm SON 封装。

器件信息⁽¹⁾

器件型号	封装	封装尺寸 (标称值)
TPS61093-Q1	SON (10)	2.50mm x 2.50mm

(1) 要了解所有可用封装，请见数据表末尾的可订购产品附录。

4 简化电路原理图



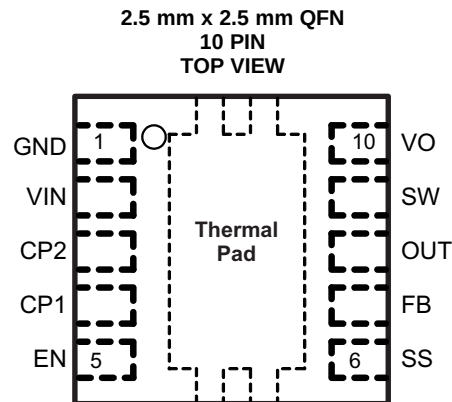
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5 修订历史记录

日期	修订版本	注释
2015 年 1 月	*	最初发布版本

6 Pin Configuration and Functions



Pin Functions

PIN		I/O	DESCRIPTION
NAME	NO.		
VIN	2	I	IC Supply voltage input.
VO	10	O	Output of the boost converter. When the output voltage exceeds the over voltage protection (OVP) threshold, the power switch turns off until VO drops below the over voltage protection hysteresis.
OUT	8	O	Isolation switch is between this pin and VO pin. Connect load to this pin for input/output isolation during IC shutdown. See Without Isolation FET for the tradeoff between isolation and efficiency.
GND	1	–	Ground of the IC.
CP1, CP2	3, 4		Connect to flying capacitor for internal charge pump.
EN	5	I	Enable pin (HIGH = enable). When the pin is pulled low for 1 ms, the IC turns off and consumes less than 1-μA current.
SS	6	I	Soft start pin. A RC network connecting to the SS pin programs soft start timing. See Start Up
FB	7	I	Voltage feedback pin for output regulation, 0.5-V regulated voltage. An external resistor divider connected to this pin programs the regulated output voltage.
SW	9	I	Switching node of the IC where the internal PWM switch operates.
Thermal Pad	–	–	It should be soldered to the ground plane. If possible, use thermal via to connect to ground plane for ideal power dissipation.

7 Specifications

7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)⁽¹⁾

	MIN	MAX	UNIT
Supply voltage on pin VIN ⁽²⁾	−0.3	7	V
Voltage on pins CP2, EN, and SS ⁽²⁾	−0.3	7	V
Voltage on pin CP1 and FB ⁽²⁾	−0.3	3	V
Voltage on pin SW, VO, and OUT ⁽²⁾	−0.3	20	V
Operating Junction Temperature Range	−40	150	°C
T _{stg} , Storage temperature range	−55	150	°C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions* is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) All voltage values are with respect to network ground terminal.

7.2 ESD Ratings

			VALUE	UNIT
V _(ESD)	Electrostatic discharge	Human body model (HBM), per AEC Q100-002 ⁽¹⁾	±2000	V
		Charged device model (CDM), per AEC Q100-011	Corner pins (1, 5, 6, and 10)	
			Other pins	
			±500	

- (1) AEC Q100-002 indicates HBM stressing is done in accordance with the ANSI/ESDA/JEDEC JS-001 specification.

7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
V _i	Input voltage range	1.6		6	V
V _o	Output voltage range at VO pin			17	V
L	Inductor ⁽¹⁾	2.2	4.7	10	μH
C _{in}	Input capacitor	4.7			μF
C _o	Output capacitor at OUT pin ⁽¹⁾	1		10	μF
C _{fly}	Flying capacitor at CP1 and CP2 pins	10			nF
T _j	Operating junction temperature	−40		125	°C
T _A	Operating ambient temperature	−40		125	°C

- (1) These values are recommended values that have been successfully tested in several applications. Other values may be acceptable in other applications but should be fully tested by the user.

7.4 Thermal Information

THERMAL METRIC ⁽¹⁾		TPS61093-Q1	UNIT
		DSK	
		10 PINS	
R _{θJA}	Junction-to-ambient thermal resistance	49.2	°C/W
R _{θJC(top)}	Junction-to-case (top) thermal resistance	63.3	
R _{θJB}	Junction-to-board thermal resistance	23.4	
Ψ _{JT}	Junction-to-top characterization parameter	1.1	
Ψ _{JB}	Junction-to-board characterization parameter	23.0	
R _{θJC(bot)}	Junction-to-case (bottom) thermal resistance	5.7	

- (1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, [SPRA953](#).

7.5 Electrical Characteristics

V_{IN} = 3.6 V, EN = V_{IN}, T_A = T_J = –40°C to 125°C, typical values are at T_A = 25°C (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY CURRENT						
V _{IN}	Input voltage range, V _{IN}		1.6		6	V
I _Q	Operating quiescent current into V _{IN}	Device PWM switching no load		0.9	1.5	mA
I _{SD}	Shutdown current	EN = GND, V _{IN} = 6 V			5	μA
UVLO	Undervoltage lockout threshold	V _{IN} falling		1.5	1.55	V
V _{hys}	Undervoltage lockout hysteresis			50		mV
ENABLE AND PWM CONTROL						
V _{ENH}	EN logic high voltage	V _{IN} = 1.6 V to 6 V	1.2			V
V _{ENL}	EN logic low voltage	V _{IN} = 1.6 V to 6 V			0.3	V
R _{EN}	EN pull down resistor		400	800	1600	kΩ
VOLTAGE CONTROL						
V _{REF}	Voltage feedback regulation voltage		0.49	0.5	0.51	V
I _{FB}	Voltage feedback input bias current				100	nA
f _S	Oscillator frequency		1.0	1.2	1.4	MHz
D _{max}	Maximum duty cycle	V _{FB} = 0.1 V	90%	93%		
POWER SWITCH, ISOLATION FET						
R _{DS(ON)N}	N-channel MOSFET on-resistance	V _{IN} = 3 V		0.25	0.4	Ω
R _{DS(ON)iso}	Isolation FET on-resistance	VO = 5 V		2.5	4	Ω
		VO = 3.5 V		4.5		
I _{LN_N}	N-channel leakage current	V _{DS} = 20 V			3	μA
I _{LN_iso}	Isolation FET leakage current	V _{DS} = 20 V			1	μA
V _F	Power diode forward voltage	Current = 500 mA		0.8		V
OC, ILIM, OVP SC AND SS						
I _{LIM}	N-Channel MOSFET current limit		0.9	1.1	1.6	A
V _{ovp}	Over voltage protection threshold	Measured on the VO pin	18	19		V
V _{ovp_hys}	Over voltage protection hysteresis			0.6		V
I _{OL}	Over load protection		200	300		mA
THERMAL SHUTDOWN						
T _{shutdown}	Thermal shutdown threshold			150		°C
T _{hysteresis}	Thermal shutdown hysteresis			15		°C

7.6 Timing Requirements

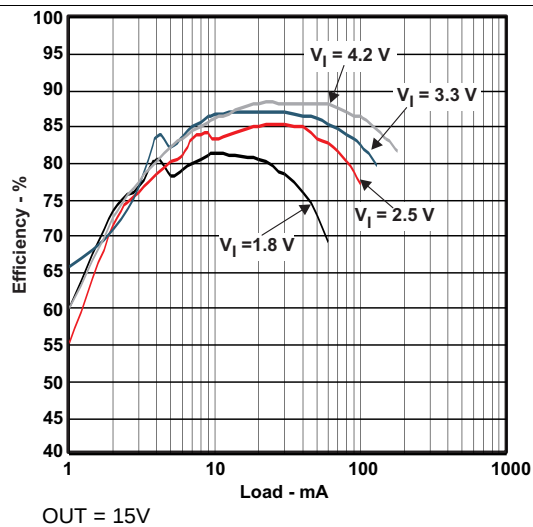
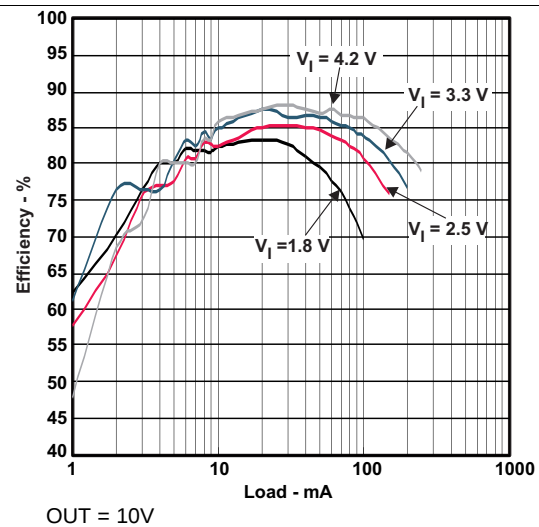
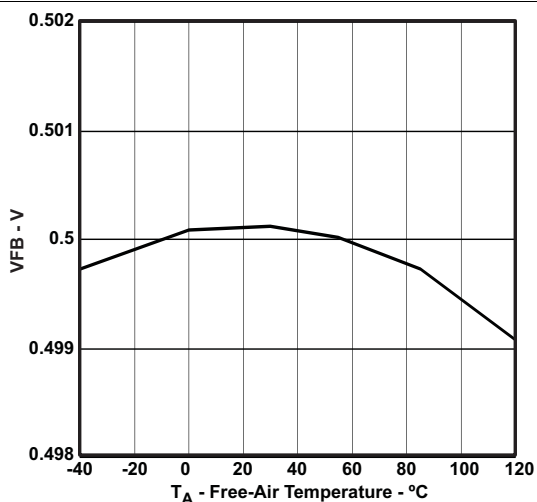
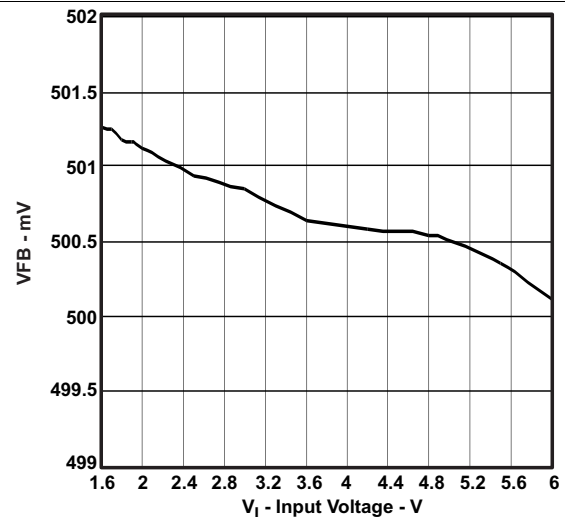
V_{IN} = 3.6 V, EN = V_{IN}, T_A = T_J = –40°C to 125°C, typical values are at T_A = 25°C (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
T _{off}	EN pulse width to shutdown EN high to low			1	ms
T _{min_on}	Minimum on pulse width		65		ns

7.7 Typical Characteristics

Table 1. Table Of Graphs

Figure 1, L = TOKO #A915_Y-100M, unless otherwise noted			FIGURE
η	Efficiency	vs Load current at OUT = 15 V	Figure 1
η	Efficiency	vs Load current at OUT = 10 V	Figure 2
V_{FB}	FB voltage	vs Free-air temperature	Figure 3
V_{FB}	FB voltage	vs Input voltage	Figure 4
I_{LIM}	Switch current limit	vs Free-air temperature	Figure 5
	Line transient response	VIN = 3.3 V to 3.6 V; Load = 50 mA	Figure 10
	Load transient response	VIN = 2.5 V; Load = 10 mA to 50 mA; Cff = 100 pF	Figure 11
	PWM control in CCM	VIN = 3.6 V; Load = 50 mA	Figure 12
	PWM control in DCM	VIN = 3.6 V; Load = 1 mA	Figure 13
	Pulse skip mode	VIN = 4.5 V; OUT = 10 V; No load	Figure 14
	Soft start-up	VIN = 3.6 V; Load = 50 mA	Figure 15


Figure 1. Efficiency vs. Load

Figure 2. Efficiency vs. Load

Figure 3. FB Voltage vs. Free-Air Temperature

Figure 4. FB Voltage vs. Input Voltage

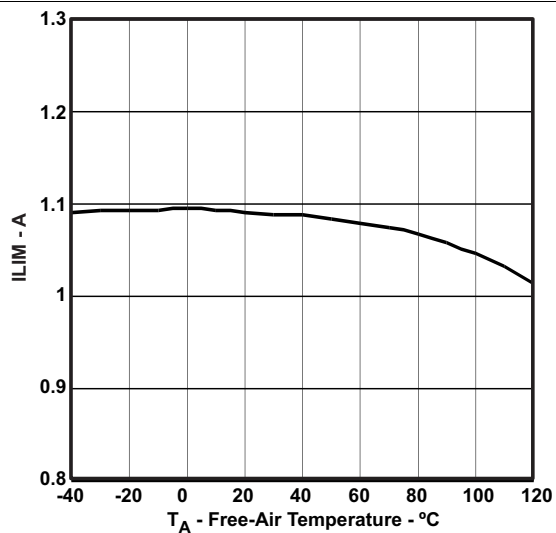


Figure 5. Switch Current Limit vs. Free-Air Temperature

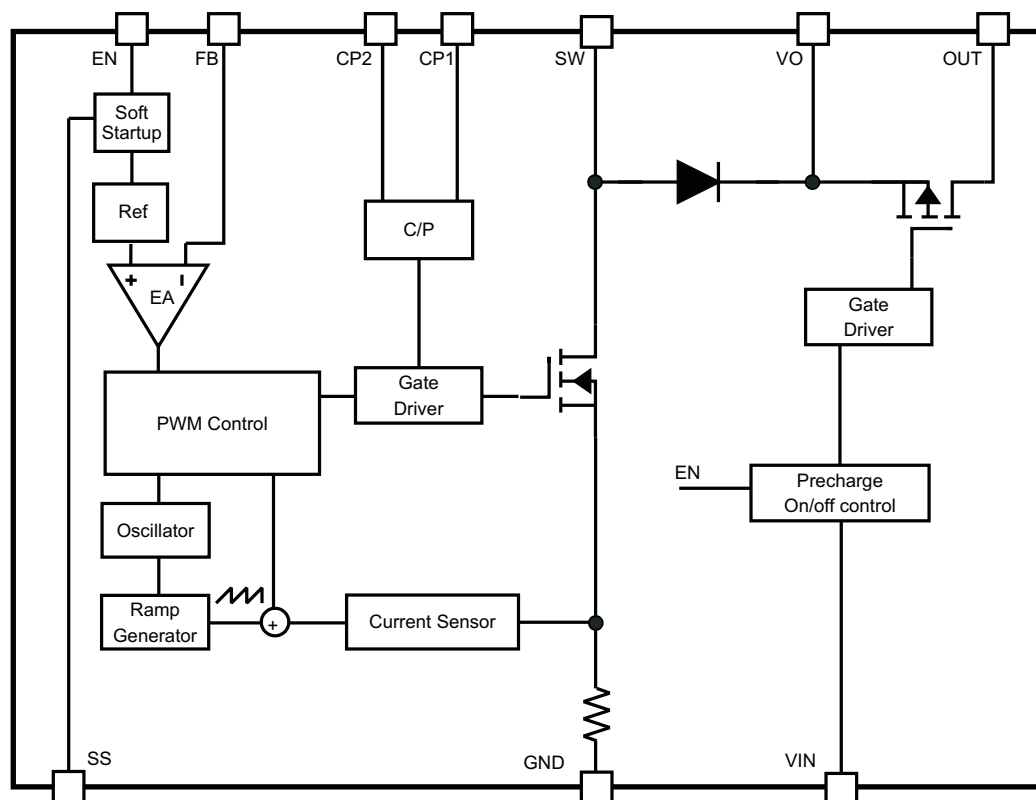
8 Detailed Description

8.1 Overview

The TPS61093-Q1 is a highly integrated boost regulator for up to 17-V output. In addition to the on-chip 1-A PWM switch and power diode, this IC also integrates an output-side isolation switch as shown in the functional block diagram. One common issue with conventional boost regulators is the conduction path from input to output even when the PWM switch is turned off. It creates three problems, which are inrush current during start-up, output leakage current during shutdown, and excessive over load current. In the TPS61093-Q1, the isolation switch turns off under shutdown-mode and over load conditions, thereby opening the current path. However, shorting the VO and OUT pins bypasses the isolation switch and enhances efficiency. Because the isolation switch is on the output side, the IC's VIN pin and power stage input power (up to 10 V) can be separated.

The TPS61093-Q1 adopts current-mode control with constant pulse-width-modulation (PWM) frequency. The switching frequency is fixed at 1.2-MHz typical. PWM operation turns on the PWM switch at the beginning of each switching cycle. The input voltage is applied across the inductor and the inductor current ramps up. In this mode, the output capacitor is discharged by the load current. When the inductor current hits the threshold set by the error amplifier output, the PWM switch is turned off, and the power diode is forward-biased. The inductor transfers its stored energy to replenish the output capacitor. This operation repeats in the next switching cycle. The error amplifier compares the FB-pin voltage with an internal reference, and its output determines the duty cycle of the PWM switching. This closed-loop system requires frequency compensation for stable operation. The device has a built-in compensation circuit that can accommodate a wide range of input and output voltages. To avoid the sub-harmonic oscillation intrinsic to current-mode control, the IC also integrates slope compensation, which adds an artificial slope to the current ramp.

8.2 Functional Block Diagram



8.3 Feature Description

8.3.1 Shutdown And Load Discharge

When the EN pin is pulled low for 1-ms, the IC stops the PWM switch and turns off the isolation switch, providing isolation between input and output. The internal current path consisting of the isolation switch's body diode and several parasitic diodes quickly discharges the output voltage to less than 3.3-V. Afterwards, the voltage is slowly discharged to zero by the leakage current. This protects the IC and the external components from high voltage in shutdown mode.

In shutdown mode, less than 5- μ A of input current is consumed by the IC.

8.3.2 Over Load And Over Voltage Protection

If the over load current passing through the isolation switch is above the over load limit (I_{OL}) for 3- μ s (typ), the TPS61093-Q1 is switched off until the fault is cleared and the EN pin toggles. The function only is triggered 52-ms after the IC is enabled.

To prevent the PWM switch and the output capacitor from exceeding maximum voltage ratings, an over voltage protection circuit turns off the boost switch as soon as the output voltage at the VO pin exceeds the OVP threshold. Simultaneously, the IC opens the isolation switch. The regulator resumes PWM switching after the VO pin voltage falls 0.6-V below the threshold.

8.3.3 Under Voltage Lockout (UVLO)

An under voltage lockout prevents improper operation of the device for input voltages below 1.55-V. When the input voltage is below the under voltage threshold, the entire device, including the PWM and isolation switches, remains off.

8.3.4 Thermal Shutdown

An internal thermal shutdown turns off the isolation and PWM switches when the typical junction temperature of 150°C is exceeded. The thermal shutdown has a hysteresis of 15°C, typical.

8.4 Device Functional Modes

The converter operates in continuous conduction mode (CCM) as soon as the input current increases above half the ripple current in the inductor, for lower load currents it switches into discontinuous conduction mode (DCM). If the load is further reduced, the part starts to skip pulses to maintain the output voltage.

9 Application and Implementation

9.1 Application Information

The following section provides a step-by-step design approach for configuring the TPS61093-Q1 as a voltage regulating boost converter, as shown in Figure 6.

9.2 Typical Applications

9.2.1 15V Output Boost Converter

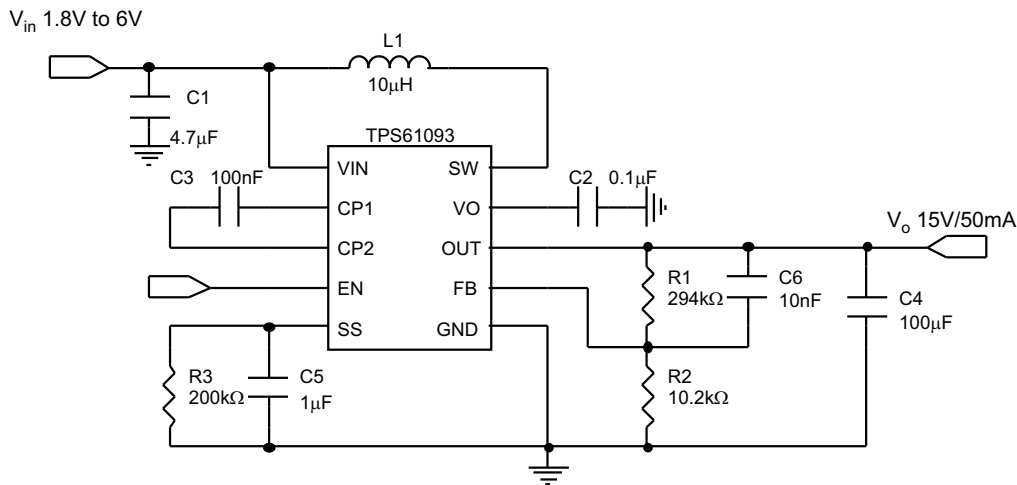


Figure 6. 15V Boost Converter with 100µF Output Capacitor

9.2.1.1 Design Requirements

Table 2. Design Parameters

PARAMETERS	VALUES
Input voltage	4.2 V
Output voltage	15 V
Operating frequency	1.2 MHz

9.2.1.2 Detailed Design Procedure

9.2.1.2.1 Output Program

To program the output voltage, select the values of R1 and R2 (see Figure 7) according to Equation 1.

$$V_{out} = 0.5 \text{ V} \times \left(\frac{R1}{R2} + 1 \right)$$

$$R1 = R2 \times \left(\frac{V_{out}}{0.5 \text{ V}} - 1 \right) \quad (1)$$

A recommended value for R2 is approximately 10-kΩ which sets the current in the resistor divider chain to 0.5V/10kΩ = 50-μA. The output voltage tolerance depends on the VFB accuracy and the resistor divider.

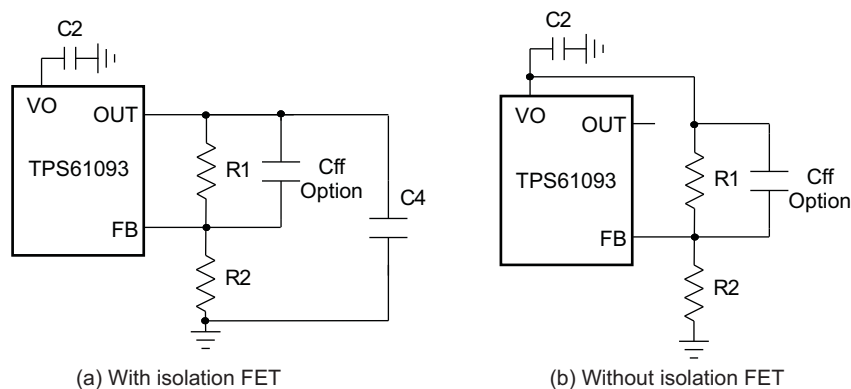


Figure 7. Resistor Divider to Program Output Voltage

9.2.1.2.2 Without Isolation FET

The efficiency of the TPS61093-Q1 can be improved by connecting the load to the VO pin instead of the OUT pin. The power loss in the isolation FET is then negligible, as shown in Figure 8. The tradeoffs when bypassing the isolation FET are:

- Leakage path between input and output causes the output to be a diode drop below the input voltage when the IC is in shutdown
- No overload circuit protection

When the load is connected to the VO pin, the output capacitor on the VO pin should be above 1-μF.

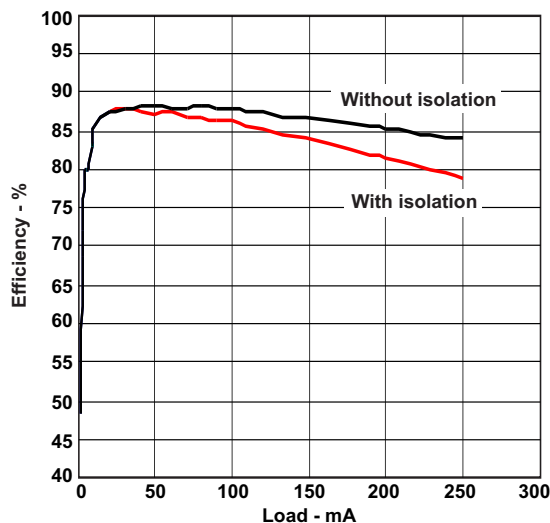


Figure 8. Efficiency vs. Load

9.2.1.2.3 Start Up

The TPS61093-Q1 turns on the isolation FET and PWM switch when the EN pin is pulled high. During the soft start period, the R and C network on the SS pin is charged by an internal bias current of 5-μA (typ). The RC network sets the reference voltage ramp up slope. Since the output voltage follows the reference voltage via the FB pin, the output voltage rise time follows the SS pin voltage until the SS pin voltage reaches 0.5-V. The soft start time is given by [Equation 2](#).

$$t_{ss} = \frac{0.5 \text{ V} \times C5}{5 \mu\text{A}}$$

where

- C5 is the capacitor connected to the SS pin (2)

When the EN pin is pulled low to switch the IC off, the SS pin voltage is discharged to zero by the resistor R3. The discharge period depends on the RC time constant. Note that if the SS pin voltage is not discharged to zero before the IC is enabled again, the soft start circuit may not slow the output voltage startup and may not reduce the startup inrush current.

9.2.1.2.4 Switch Duty Cycle

The maximum switch duty cycle (D) of the TPS61093-Q1 is 90% (minimum). The duty cycle of a boost converter under continuous conduction mode (CCM) is given by:

$$D = \frac{V_{out} + 0.8 \text{ V} - V_{in}}{V_{out} + 0.8 \text{ V}} \quad (3)$$

The duty cycle must be lower than the specification in the application; otherwise the output voltage cannot be regulated.

The TPS61093-Q1 has a minimum ON pulse width once the PWM switch is turned on. As the output current drops, the device enters discontinuous conduction mode (DCM). If the output current drops extremely low, causing the ON time to be reduced to the minimum ON time, the TPS61093-Q1 enters pulse-skipping mode. In this mode, the device keeps the power switch off for several switching cycles to keep the output voltage in regulation. See [Figure 14](#). The output current when the IC enters skipping mode is calculated with [Equation 4](#).

$$I_{out_skip} = \frac{V_{in}^2 \times T_{min_on}^2 \times f_{sw}}{2 \times (V_{out} + 0.8 \text{ V} - V_{in}) \times L}$$

where

- T_{min_on} = Minimum ON pulse width specification (typically 65-ns);
- L = Selected inductor value;
- f_{sw} = Converter switching frequency (typically 1.2-MHz) (4)

9.2.1.2.5 Inductor Selection

Because the selection of the inductor affects steady state operation, transient behavior, and loop stability, the inductor is the most important component in power regulator design. There are three important inductor specifications, inductor value, saturation current, and dc resistance. Considering inductor value alone is not enough.

The saturation current of the inductor should be higher than the peak switch current as calculated in [Equation 5](#).

$$I_{L_peak} = I_{L_DC} + \frac{\Delta I_L}{2}$$

$$I_{L_DC} = \frac{V_{out} \times I_{out}}{V_{in} \times \eta}$$

$$\Delta I_L = \frac{1}{L \times f_{sw} \times \left(\frac{1}{V_{out} + 0.8 V - V_{IN}} + \frac{1}{V_{IN}} \right)}$$

where

- I_{L_peak} = Peak switch current
- I_{L_DC} = Inductor average current
- ΔI_L = Inductor peak to peak current
- η = Estimated converter efficiency

(5)

Normally, it is advisable to work with an inductor peak-to-peak current of less than 30% of the average inductor current. A smaller ripple from a larger valued inductor reduces the magnetic hysteresis losses in the inductor and EMI. But in the same way, load transient response time is increased. Also, the inductor value should not be outside the 2.2-μH to 10-μH range in the recommended operating conditions table. Otherwise, the internal slope compensation and loop compensation components are unable to maintain small signal control loop stability over the entire load range. [Table 3](#) lists the recommended inductor for the TPS61093-Q1.

Table 3. Recommended Inductors for the TPS61093-Q1

Part Number	L (μH)	DCR Max (mΩ)	Saturation Current (A)	Size (L×W×H mm)	Vendor
#A915_Y-4R7M	4.7	45	1.5	5.2x5.2x3.0	Toko
#A915_Y-100M	10	90	1.09	5.2x5.2x3.0	Toko
VLS4012-4R7M	4.7	132	1.1	4.0x4.0x1.2	TDK
VLS4012-100M	10	240	0.82	4.0x4.0x1.2	TDK
CDRH3D23/HP	10	198	1.02	4.0x4.0x2.5	Sumida
LPS5030-103ML	10	127	1.4	5.0x5.0x3.0	Coilcraft

9.2.1.2.6 Input And Output Capacitor Selection

The output capacitor is mainly selected to meet the requirements for output ripple and loop stability. This ripple voltage is related to the capacitor's capacitance and its equivalent series resistance (ESR). Assuming a ceramic capacitor with zero ESR, the minimum capacitance needed for a given ripple can be calculated by:

$$C_{out} = \frac{D \times I_{out}}{F_s \times V_{ripple}}$$

where

- V_{ripple} = peak to peak output ripple

(6)

The ESR impact on the output ripple must be considered if tantalum or electrolytic capacitors are used.

Care must be taken when evaluating a ceramic capacitor's derating under dc bias, aging, and ac signal. For example, larger form factor capacitors (in 1206 size) have their self resonant frequencies in the range of the switching frequency. So the effective capacitance is significantly lower. The dc bias can also significantly reduce capacitance. A ceramic capacitor can lose as much as 50% of its capacitance at its rated voltage. Therefore, always leave margin on the voltage rating to ensure adequate capacitance at the required output voltage.

A 4.7- μ F (minimum) input capacitor is recommended. The output requires a capacitor in the range of 1 μ F to 10 μ F. The output capacitor affects the small signal control loop stability of the boost regulator. If the output capacitor is below the range, the boost regulator can potentially become unstable.

The popular vendors for high value ceramic capacitors are:

- TDK (<http://www.component.tdk.com/components.php>)
- Murata (<http://www.murata.com/cap/index.html>)

9.2.1.2.7 Small Signal Stability

The TPS61093-Q1 integrates slope compensation and the RC compensation network for the internal error amplifier. Most applications will be control loop stable if the recommended inductor and input/output capacitors are used. For those few applications that require components outside the recommended values, the internal error amplifier's gain and phase are presented in [Figure 9](#).

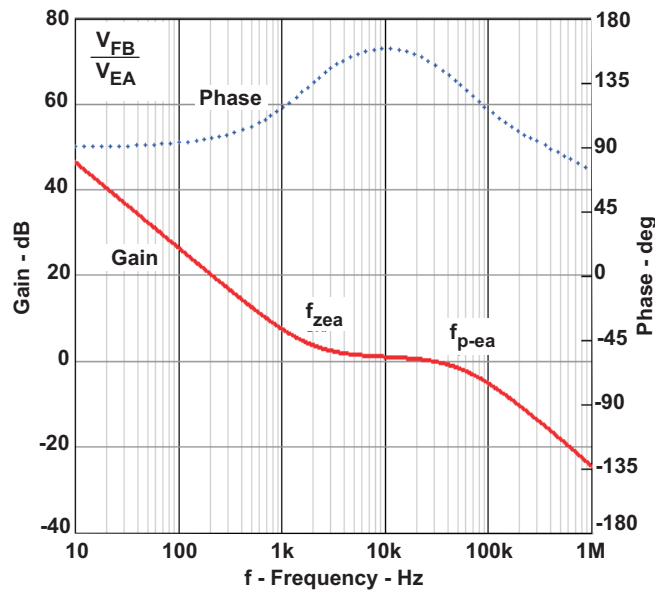


Figure 9. Bode Plot of Error Amplifier Gain and Phase

The RC compensation network generates a pole f_{p-ea} of 57-kHz and a zero f_{z-ea} of 1.9-kHz, shown in [Figure 9](#). Use [Equation 7](#) to calculate the output pole, f_p , of the boost converter. If $f_p \ll f_{z-ea}$, due to a large capacitor beyond 10 μ F, for example, a feed forward capacitor on the resistor divider, as shown in [Figure 9](#), is necessary to generate an additional zero f_{z-f} to improve the loop phase margin and improve the load transient response. The low frequency pole f_{p-f} and zero f_{z-f} generated by the feed forward capacitor are given by [Equation 8](#) and [Equation 9](#):

$$f_p = \frac{1}{\pi \times R_o \times C_o} \quad (a) \quad (7)$$

$$f_{p-f} = \frac{1}{2\pi \times R2 \times C_{ff}} \quad (b) \quad (8)$$

$$f_{z-f} = \frac{1}{2\pi \times R1 \times C_{ff}} \quad (c) \quad (9)$$

where

- C_{ff} = the feed-forward capacitor

For example, in the typical application circuitry (see [Figure 7](#)), the output pole f_p is approximately 1-kHz. When the output capacitor is increased to 100- μ F, then the f_p is reduced to 10-Hz. Therefore, a feed-forward capacitor of 10-nF compensates for the low frequency pole.

A feed forward capacitor that sets f_{z-f} near 10-kHz improves the load transient response in most applications, as shown in [Figure 11](#).

9.2.1.3 Application Curves

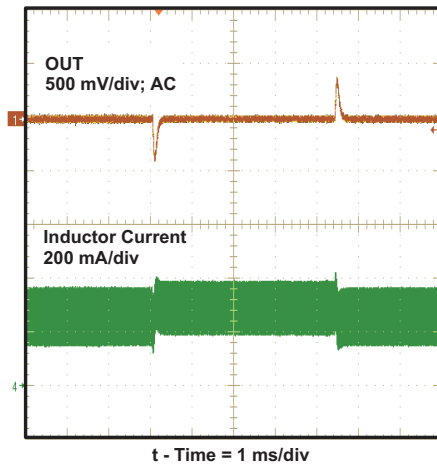


Figure 10. 3.3V to 3.6V Line Transient Response

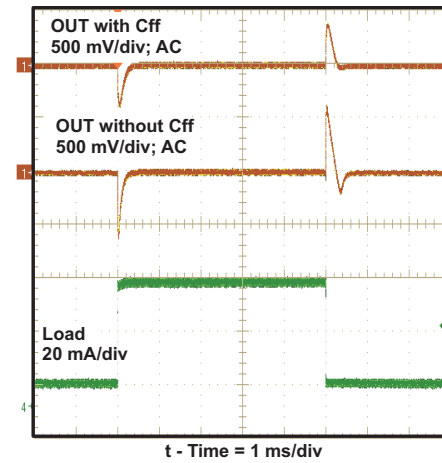


Figure 11. 10mA to 50mA Load Transient Response

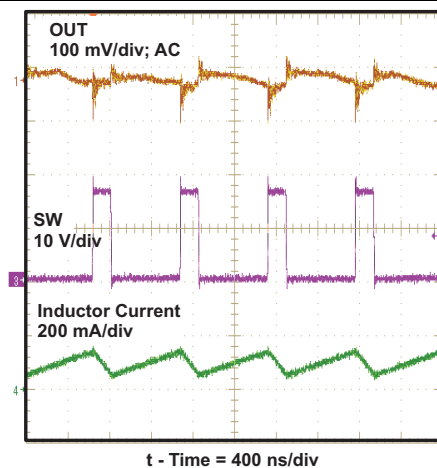


Figure 12. PWM Control in CCM

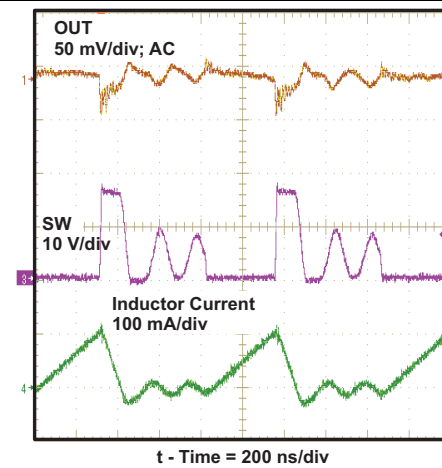


Figure 13. PWM Control in DCM

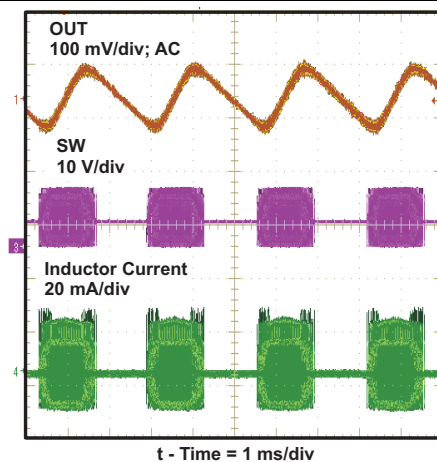


Figure 14. Pulse Skip Mode at Light Load

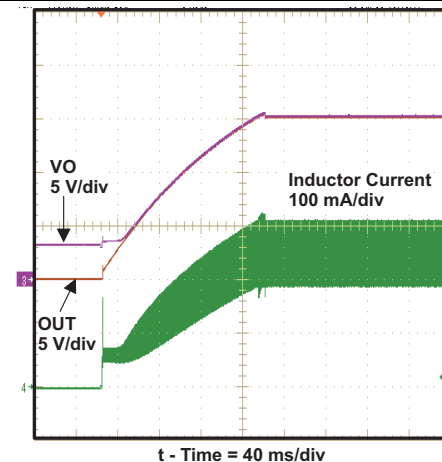
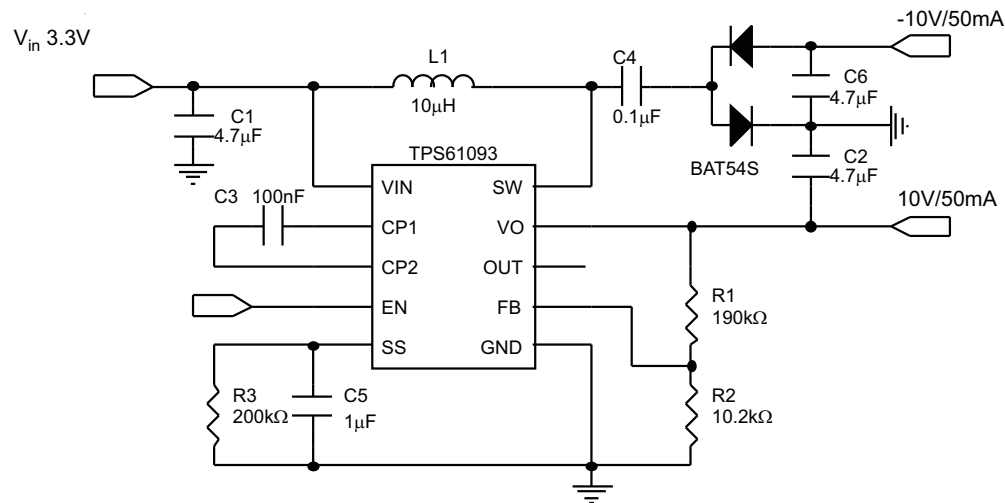


Figure 15. Soft Start-Up

9.2.2 10 V, -10 V Dual Output Boost Converter



9.2.2.1 Design Requirements

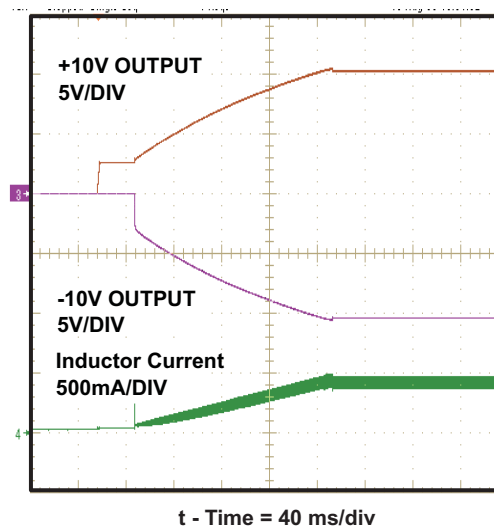
Table 4. Design Parameters

PARAMETERS	VALUES
Input voltage	3.3 V
Output voltage	10 V/-10 V
Operating frequency	1.2 MHz

9.2.2.2 Detailed Design Procedure

Refer to [Detailed Design Procedure](#) for the 15V Output Boost Converter.

9.2.2.3 Application Curves


Figure 16. Soft Startup Waveform, 10 V, -10 V Dual Output Boost Converter

10 Power Supply Recommendations

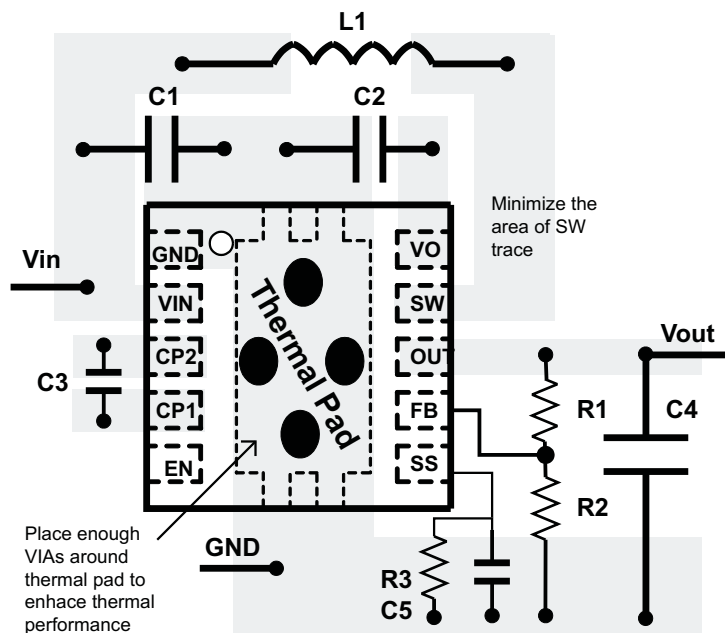
The device is designed to operate from an input voltage supply range between 1.6 V to 6 V. The input power supply's output current needs to be rated according to the supply voltage, output voltage and output current of the TPS61093-Q1.

11 Layout

11.1 Layout Guidelines

As for all switching power supplies, especially those running at high switching frequency and high currents, layout is an important design step. If layout is not carefully done, the regulator could suffer from instability as well as noise problems. To maximize efficiency, switch rise and fall times are very fast. To prevent radiation of high frequency noise (e.g., EMI), proper layout of the high frequency switching path is essential. Minimize the length and area of all traces connected to the SW pin and always use a ground plane under the switching regulator to minimize interplane coupling. The high current path including the switch and output capacitor contains nanosecond rise and fall times and should be kept as short as possible. The input capacitor needs not only to be close to the VIN pin, but also to the GND pin in order to reduce input supply ripple.

11.2 Layout Example



11.3 Thermal Considerations

The maximum IC junction temperature should be restricted to 125°C under normal operating conditions. This restriction limits the power dissipation of the TPS61093-Q1. Calculate the maximum allowable dissipation, $P_{D(max)}$, and keep the actual dissipation less than or equal to $P_{D(max)}$. The maximum-power-dissipation limit is determined using the following equation:

$$P_{D(max)} = \frac{125^{\circ}\text{C} - T_A}{R_{\theta JA}}$$

where

- T_A is the maximum ambient temperature for the application
- $R_{\theta JA}$ is the thermal resistance junction-toambient given in Power Dissipation Table (10)

The TPS61093-Q1 comes in a thermally enhanced SON package. This package includes a thermal pad that improves the thermal capabilities of the package. The $R_{\theta JA}$ of the SON package greatly depends on the PCB layout and thermal pad connection. The thermal pad must be soldered to the analog ground on the PCB. Using thermal vias underneath the thermal pad.

12 器件和文档支持

12.1 商标

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12.2 静电放电警告



ESD 可能会损坏该集成电路。德州仪器 (TI) 建议通过适当的预防措施处理所有集成电路。如果不遵守正确的处理措施和安装程序，可能会损坏集成电路。

ESD 的损坏小至导致微小的性能降级，大至整个器件故障。精密的集成电路可能更容易受到损坏，这是因为非常细微的参数更改都可能会导致器件与其发布的规格不相符。

12.3 术语表

[SLYZ022](#) — TI 术语表。

这份术语表列出并解释术语、首字母缩略词和定义。

13 机械封装和可订购信息

以下页中包括机械封装和可订购信息。 这些信息是针对指定器件可提供的最新数据。 这些数据会在无通知且不对本文档进行修订的情况下发生改变。 欲获得该数据表的浏览器版本，请查阅左侧的导航栏。

PACKAGING INFORMATION

Orderable part number	Status (1)	Material type (2)	Package Pins	Package qty Carrier	RoHS (3)	Lead finish/ Ball material (4)	MSL rating/ Peak reflow (5)	Op temp (°C)	Part marking (6)
TPS61093QDSKRQ1	Active	Production	SON (DSK) 10	3000 LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	093Q
TPS61093QDSKRQ1.A	Active	Production	SON (DSK) 10	3000 LARGE T&R	Yes	NIPDAU	Level-1-260C-UNLIM	-40 to 125	093Q

⁽¹⁾ **Status:** For more details on status, see our [product life cycle](#).

⁽²⁾ **Material type:** When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

⁽³⁾ **RoHS values:** Yes, No, RoHS Exempt. See the [TI RoHS Statement](#) for additional information and value definition.

⁽⁴⁾ **Lead finish/Ball material:** Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

⁽⁵⁾ **MSL rating/Peak reflow:** The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

⁽⁶⁾ **Part marking:** There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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OTHER QUALIFIED VERSIONS OF TPS61093-Q1 :

- Catalog : [TPS61093](#)

NOTE: Qualified Version Definitions:

- Catalog - TI's standard catalog product

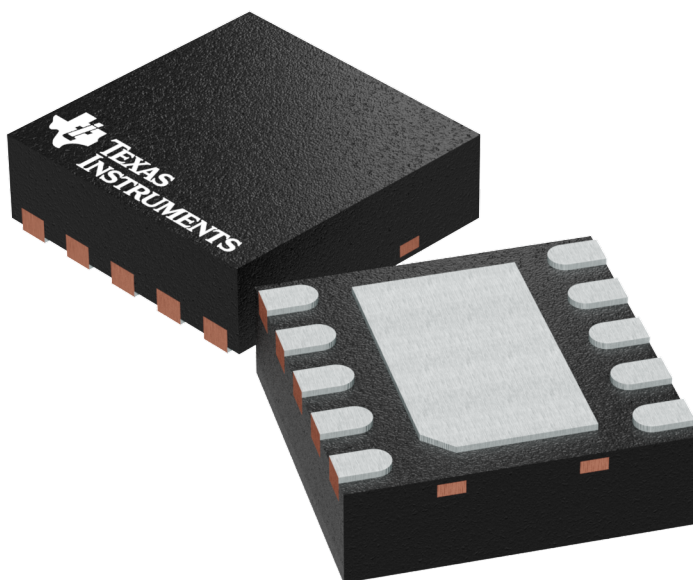
GENERIC PACKAGE VIEW

DSK 10

WSON - 0.8 mm max height

2.5 x 2.5 mm, 0.5 mm pitch

PLASTIC SMALL OUTLINE - NO LEAD



Images above are just a representation of the package family, actual package may vary.
Refer to the product data sheet for package details.

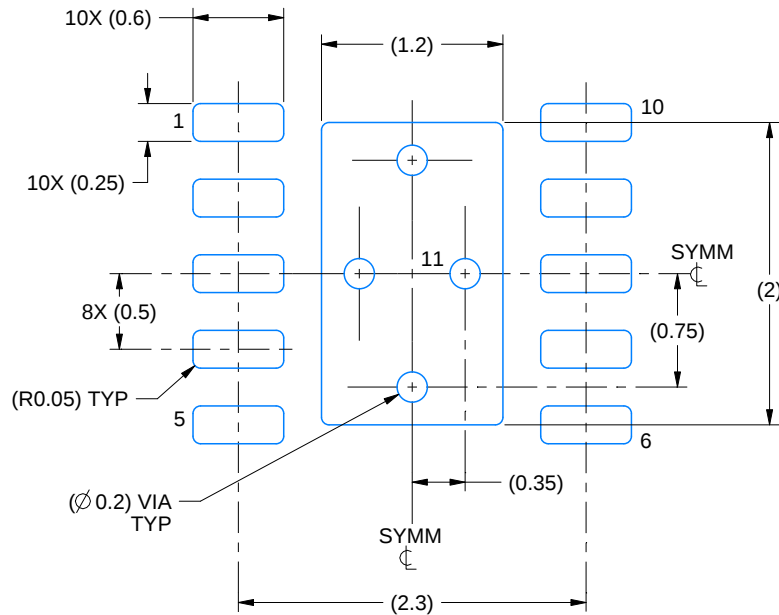
4225304/A

EXAMPLE BOARD LAYOUT

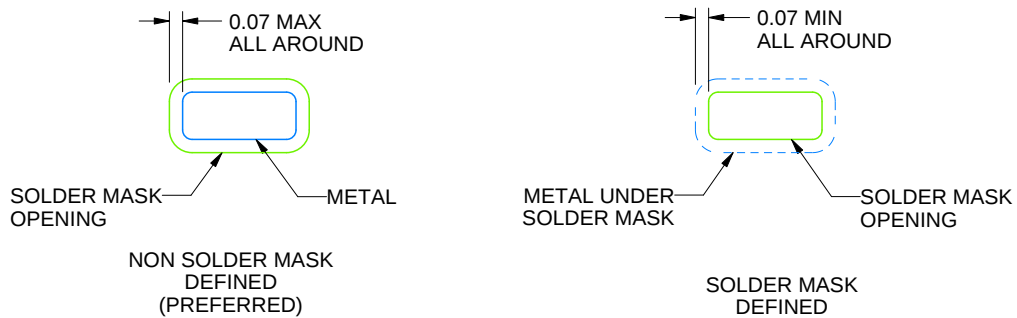
DSK0010A

WSN - 0.8 mm max height

PLASTIC SMALL OUTLINE - NO LEAD



LAND PATTERN EXAMPLE
SCALE:20X



SOLDER MASK DETAILS

4218903/B 10/2020

NOTES: (continued)

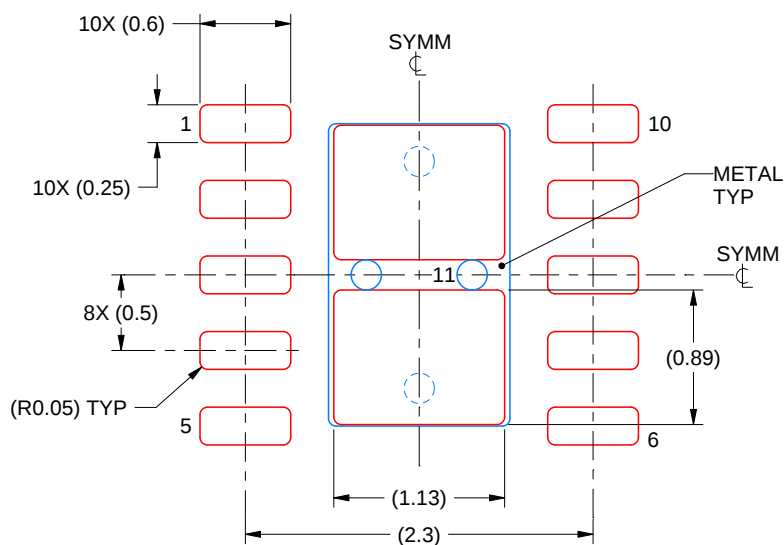
4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slue271).
5. Vias are optional depending on application, refer to device data sheet. If some or all are implemented, recommended via locations are shown.

EXAMPLE STENCIL DESIGN

DSK0010A

WSN - 0.8 mm max height

PLASTIC SMALL OUTLINE - NO LEAD



SOLDER PASTE EXAMPLE
BASED ON 0.125 mm THICK STENCIL

EXPOSED PAD 11
84% PRINTED SOLDER COVERAGE BY AREA
SCALE:20X

4218903/B 10/2020

NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

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