













Community

TPS1H100-Q1

ZHCSDD8D - OCTOBER 2014-REVISED DECEMBER 2019

# TPS1H100-Q1 40V、100m $\Omega$ 单通道智能高侧电源开关

## 特性

- 符合汽车类 应用要求
- 具有符合 AEC-Q100 标准的下列特性:
  - 器件温度等级 1: -40°C 至 125°C 的环境工作 温度范围
  - 器件 HBM ESD 分类等级 H3A
  - 器件 CDM ESD 分类等级 C4B
- 提供功能安全
  - 提供文档以帮助创建功能安全系统设计
- 具有全面诊断功能的单通道智能高侧电源开关
  - 版本 A: 开漏状态输出
  - 版本 B: 电流感应模拟输出
- 宽工作电压范围: 3.5V 至 40V
- 超低待机电流,低于 0.5µA
- 工作结温范围, -40°C 至 150°C
- 输入控制,兼容 3.3V 和 5V 逻辑
- 高精度电流感应,电流为 1A 时为 ±30mA, 电流为 5mA 时为 ±4mA
- 利用外部电阻器实现可编程电流限制(在 0.5A 时 为 ±20%)
- 用于对 MCU 模拟或数字接口进行多路复用的诊断 使能功能
- 测试符合 AECQ100-12 A 级标准, 经过 100 万次接地短路测试
- 通过 ISO7637-2 和 ISO16750-2 电瞬变抗扰度认证
- 保护
  - 过载和短路保护
  - 电感负载负电压钳位

- 欠压锁定 (UVLO) 保护
- 具备自恢复功能的热关断/热振荡
- 接地失效保护和失电保护
- 对外部电路提供反向电池保护
- 诊断
  - 开启和关闭状态输出的开路和电池短路检测
  - 过载和接地短路检测以及电流限制
  - 热关断/热振荡检测
- 14 引脚热增强型 PWP 封装

## 2 应用

- 适用于子模块的高侧电源开关
- 适用于低功率灯的电源开关
- 高侧继电器和电磁阀
- PLC 数字输出电源开关
- 一般阻性、感性和容性负载

## 3 说明

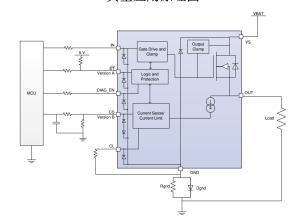
TPS1H100-Q1 是一款具有全方位保护的高侧电源开 关,它集成有 NMOS 功率 FET 和电荷泵,专用于对 各类阻性、感性和容性负载进行智能控制。精确的电流 检测和可编程电流限制 特性 使该器件从市场中脱颖而 出。

### 器件信息(1)

	HH 11 1H 10.	
器件型号	封装	封装尺寸 (标称值)
TPS1H100-Q1	HTSSOP (14)	4.40mm × 5.00mm

(1) 如需了解所有可用封装,请参阅产品说明书末尾的可订购产品 附录。

## 典型应用原理图





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# 4 修订历史记录

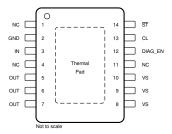
注: 之前版本的页码可能与当前版本有所不同。

Cr	hanges from Revision C (June 2018) to Revision D	Page
•	向特性部分添加了提供功能安全的链接	<u> 1</u>
Cr	hanges from Revision B (June 2015) to Revision C	Page
•	Changed the <i>Pin Functions</i> table to alphabetical order and created separate columns fo B devices	
	Added tablenotes to the <i>Electrical Characteristics</i> table	
Ch	hanges from Revision A (January 2015) to Revision B	Page
•	Updated Figure 6 and Figure 7	10
•	Updated Figure 38	25
•	Updated Figure 39	26
•	Updated Figure 40	27
<u>•</u>	添加了社区资源	
Ch	hanges from Original (October 2014) to Revision A	Page
•	将器件状态从预览更新为生产数据	1

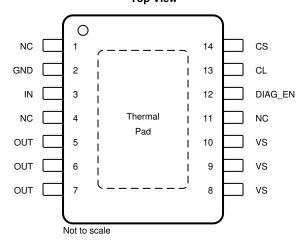


# **5 Pin Configuration and Functions**





#### PWP Package Version B 14-Pin HTSSOP Top View



### **Pin Functions**

	PIN		1/0	DESCRIPTION	
NAME	VER. A	VER. B	1/0	DESCRIPTION	
CL	13	13	0	Programmable current-limit pin. Connect to device GND if external current limit is not used.	
CS	_	14	0	Current-sense output. Leave floating if not used.	
DIAG_EN	12	12	I	Enable and disable pin for diagnostic functions. Connect to device GND if not used.	
GND	2	2	_	Ground pin	
IN	3	3	1	Input control for channel activation	
NC	1, 4, 11	1, 4, 11	_	No-connect pin; leave floating.	
OUT	5, 6, 7	5, 6, 7	0	Output, connected to load (NMOS source)	
ST	14	_	0	Open-drain diagnostic status output. Leave floating if not used.	
VS	8, 9, 10	8, 9, 10	I	Power supply; battery voltage	
Thermal pad	_	_	_	Thermal pad. Connect to device GND or leave floating.	



## **Specifications**

### 6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) (1)(2)(3)

	MIN	MAX	UNIT
Supply voltage <sup>(4)</sup> , t < 400 ms		48	V
Reverse polarity voltage <sup>(5)</sup>	-18		V
Continuous drain current	Internall	y limited	А
Reverse current on GND	-50	20	mA
Reverse current on GND, t < 120 s	-250	20	mA
Voltage on IN/DIAG_EN pin	-0.3	7	V
Current on IN /DIAG_EN pin	-30	2	mA
Voltage on ST pin	-0.3	7	V
Current on ST pin	-30	10	mA
IN pin PWM frequency		2	KHz
Voltage on CL pin	-0.3	7	V
Current on CL pin	-2	30	mA
Voltage on CS pin	-2.7	6.5	V
Current on CS pin	-2	30	mA
Inductive load switch-off energy dissipation, single pulse (6)		70	mJ
Operating ambient temperature	-40	125	°C
Operating junction temperature	-40	150	°C
Storage temperature, T <sub>stg</sub>	-65	150	°C

<sup>(1)</sup> Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

- All voltage values are with respect to GND.
- Absolute negative voltage on these terminals is not to go below -0.3 V.
- Absolute maximum voltage, withstand 48-V load dump voltage for 400 ms.
- Reverse polarity condition: t < 60 s, reverse current < Irev1, GND pin 1-k $\Omega$  resistor in parallel with diode. Test condition:  $V_S = 13.5$  V, L = 8 mH, R = 0  $\Omega$ ,  $T_J = 150^{\circ}$ C. FR4 2s2p board, 2- × 70- $\mu$ m Cu, 2- × 35- $\mu$ m Cu. 600-mm<sup>2</sup> thermal pad copper area.

### 6.2 ESD Ratings

				VALUE	UNIT
		Human body model (HBM) AEC-Q100 Classification Level H3A <sup>(1)</sup>	VS, OUT, GND	±5000	
$V_{(ESD)}$	Electrostatic discharge	Human body model (HBM) AEC-Q100 Classification Level H2 <sup>(1)</sup>	Other pins	±4000	V
	alconargo	Charged device model (CDM), per AEC Q100-011 (2)		±750	

- The human-body model is a 107-pF capacitor discharged through a 1.5-k $\Omega$  resistor into each terminal.
- The charged-device model is tested according to AEC\_Q100-011C.

### 6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

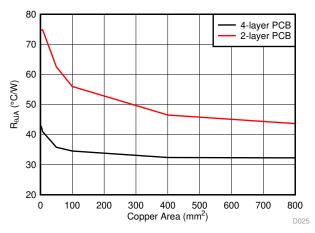
		MIN	MAX	UNIT
Vs	Operating voltage	5	40	V
	Voltage on IN/DIAG_EN pin	0	5	V
	Voltage on ST pin	0	5	V
$I_{o,nom}$	Nominal DC load current	0	4	Α
$T_J$	Operating junction temperature range	-40	150	°C



### 6.4 Thermal Information

		TPS1H100-Q1	
	THERMAL METRIC <sup>(1)</sup>	PWP (HTSSOP)	UNIT
		14 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance (2)	41	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	29.7	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	25.1	°C/W
ΨЈТ	Junction-to-top characterization parameter	0.9	°C/W
ΨЈВ	Junction-to-board characterization parameter	24.8	°C/W
$R_{\theta JC(bot)}$	Junction-to-case (bottom) thermal resistance	2.7	°C/W

- For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.
- (2) The thermal data is based on JEDEC standard high-K profile JESD 51-7. The copper pad is soldered to the thermal land pattern. Also, correct attachment procedure must be incorporated.



- (1) 4-layer board: FR4 2s2p board, 2.8-mil copper (top/bottom), 1.4-mil copper (internal layers). 76.4- x 114.3- x 1.5-mm board size.
- (2) 2-layer board: FR4 2s0p board, 2.8-mil copper (top/bottom). 76.4- x 114.3- x 1.5-mm board size.

Figure 1. R<sub>0JA</sub> Value vs Copper Area



## 6.5 Electrical Characteristics

 $5 \text{ V} < \text{V}_{c} < 40 \text{ V}$ :  $-40^{\circ}\text{C} < \text{T}_{c} < 150^{\circ}\text{C}$  unless otherwise specified

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
OPERATI	NG VOLTAGE					
$V_{S,nom}$	Nominal operating voltage		5		40	V
$V_{S,op}$	Extended operating voltage	R <sub>DS(on)</sub> value increases maximum 20%, compared to 5 V, see R <sub>DS(on)</sub> parameter	3.5		5	V
$V_{S,UVR}$	Undervoltage restart	$V_S$ rises up, $V_S > V_{S,UVR}$ , device turn on	3.5	3.7	4	V
$V_{S,UVF}$	Undervoltage shutdown	$V_S$ falls down, $V_S < V_{S,UVF}$ , device shuts off	3	3.2	3.5	V
$V_{\rm UV,hys}$	Undervoltage shutdown, hysteresis			0.5		V
<b>OPERATI</b>	NG CURRENT					
l,	Nominal operating current	$V_{IN} = 5 \text{ V}, V_{DIAG\_EN} = 0 \text{ V}, \text{ no load}$			5	mA
I <sub>nom</sub>	Nominal operating current	$V_{IN} = 5 \text{ V}, V_{DIAG\_EN} = 0 \text{ V}, 10-\Omega \text{ load}$			10	mA
I <sub>off</sub>	Standby current	$V_S = 13.5 \text{ V}, V_{IN} = V_{DIAG\_EN} = V_{CS} = V_{CL} = V_{OUTPUT} = 0 \text{ V}, T_J = 25^{\circ}C$			0.5	μΑ
·on	Startasy surroin	$V_S = 13.5 \text{ V}, V_{IN} = V_{DIAG\_EN} = V_{CS} = V_{CL} = V_{OUTPUT} = 0 \text{ V}, T_J = 125 ^{\circ}\text{C}$			5	μΑ
I <sub>off,diag</sub>	Standby current with diagnostic enabled	$V_{IN} = 0 \text{ V}, V_{DIAG\_EN} = 5 \text{ V}$			1.2	mΑ
t <sub>off,deg</sub>	Standby mode deglitch time (1)	IN from high to low, if deglitch time > t <sub>off,deg</sub> , enters into standby mode.		2		ms
	Off state output lookage ourrent	$V_S = 13.5 \text{ V}, V_{IN} = V_{OUTPUT} = 0, T_J = 25^{\circ}\text{C}$			0.5	μΑ
Ileak,out	Off-state output leakage current	$V_S = 13.5 \text{ V}, V_{IN} = V_{OUTPUT} = 0, T_J = 125^{\circ}\text{C}$			3	μΑ
POWER S	STAGE					
		$V_S > 5 \text{ V}, T_J = 25^{\circ}\text{C}$		80	100	$m\Omega$
$R_{DS-ON}$	On-state resistance	$V_S > 5 \text{ V}, T_J = 150^{\circ}\text{C}$			166	$m\Omega$
		$V_S = 3.5 \text{ V}, T_J = 25^{\circ}\text{C}$			120	$m\Omega$
$I_{lim,nom}$	Internal current limit		7		13	Α
		Internal current limit, thermal cycling condition		5		Α
II <sub>im,tsd</sub>	Current limit during thermal shutdown	External current limit, thermal cycling condition; Percentage of current limit set value		50%		
$V_{DS}$	Clamp drain-to-source voltage internally clamped		50		70	V
OUTPUT	DIODE CHARACTERISTICS	,				
$V_{F}$	Drain-to-source diode voltage	$V_{IN} = 0$ , $I_{OUT} = -0.2$ A		0.7		V
I <sub>rev1</sub>	Continuous reverse current when reverse polarity (2)	$t$ < 60 s, $V_S$ = 13.5 V, GND pin 1-k $\Omega$ resistor in parallel with diode. $T_J$ = 25°C. See $I_{rev1}$ test condition (Figure 6).		4		Α
I <sub>rev2</sub>	Continuous reverse current when $V_{OUT} > V_{S} + V_{diode}^{(2)}$	$t < 60 \text{ s}, V_S = 13.5 \text{ V}. T_J = 25^{\circ}\text{C}. \text{ See } I_{rev2}$ test condition (Figure 7).		2		Α
LOGIC IN	PUT (IN AND DIAG_EN)					
V <sub>logic,h</sub>	Input or DIAG_EN high-level voltage		2			V
V <sub>logic,I</sub>	Input or DIAG_EN low-level voltage				0.8	V
V <sub>logic,hys</sub>	Input or DIAG_EN hysteresis voltage			250		mV
R <sub>pd,in</sub>	Input pulldown resistor			500		kΩ
R <sub>pd,diag</sub>	Diag pulldown resistor			150		kΩ

<sup>(1)</sup> Value is specified by design, not subject to production test.(2) Value is based on the minimum value of the 10 pcs/3 lots samples.



# **Electrical Characteristics (continued)**

5 V <  $V_S$  < 40 V; -40°C <  $T_J$  < 150°C unless otherwise specified

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
DIAGNOS	TICS					
I <sub>loss,gnd</sub>	Loss-of-ground output leakage current				100	μΑ
$V_{ol,off}$	Open-load detection threshold in off- state	$V_{\rm IN} = 0$ V, When $V_{\rm S} - V_{\rm OUT} < V_{\rm ol,off}$ , duration longer than $t_{\rm ol,off}$ . Open load detected.	1.4	1.8	2.6	٧
I <sub>ol,off</sub>	Off-state output sink current with open load	V <sub>IN</sub> = 0 V, V <sub>S</sub> = V <sub>OUT</sub> = 13.5 V, T <sub>J</sub> = 125°C.			-50	μΑ
$t_{ol,off}$	Open-load detection-threshold deglitch time in off state	$V_{IN} = 0$ V, When $V_S - V_{OUT} < V_{ol,off}$ , duration longer than $t_{ol,off}$ . Open load detected.		600		μs
I <sub>ol,on</sub>	Open-load detection threshold in on state	V <sub>IN</sub> = 5 V, when I <sub>OUT</sub> < I <sub>ol,on</sub> , duration longer than t <sub>ol,on</sub> . Open load detected.  Version A only	2	6	10	mA
t <sub>ol,on</sub>	Open-load detection-threshold deglitch time in on-state	V <sub>IN</sub> = 5 V, when I <sub>OUT</sub> < I <sub>ol,on</sub> , duration longer than t <sub>ol,on</sub> . Open load detected. Version A only		700		μs
V <sub>ST</sub>	Status low output voltage	I <sub>ST</sub> = 2 mA Version A only			0.4	V
T <sub>SD</sub>	Thermal shutdown threshold			175		
T <sub>SD,rst</sub>	Thermal shutdown status reset			155		
T <sub>sw</sub>	Thermal swing shutdown threshold			60		°C
T <sub>hys</sub>	Hysteresis for resetting the thermal shutdown and swing		10			
CURRENT	SENSE (VERSION B) AND CURRENT L	MIT				
K	Current sense current ratio			500		
K <sub>CL</sub>	Current limit current ratio			2000		
		I <sub>load</sub> ≥ 5 mA	-80		80	
		I <sub>load</sub> ≥ 25 mA	-10		10	1
dK/K	Current-sense accuracy	I <sub>load</sub> ≥ 50 mA	-7		7	%
		I <sub>load</sub> ≥ 0.1 A	-5		5	
		I <sub>load</sub> ≥ 1 A	-3		3	
		I <sub>limit</sub> ≥ 0.5 A	-20		20	
dK <sub>CL</sub> /K <sub>CL</sub>	External current-limit accuracy (3) (4)	I <sub>limit</sub> ≥ 1.6 A	-14		14	%
$V_{CS,lin}$	Linear current sense voltage range <sup>(1)</sup>	V <sub>S</sub> ≥ 5 V	0		4	V
I <sub>OUT,lin</sub>	Linear output current range <sup>(1)</sup>	V <sub>S</sub> ≥ 5 V, V <sub>CS,lin</sub> ≤ 4 V	0		4	Α
·		V <sub>S</sub> ≥ 7 V	4.3	4.75	4.9	
$V_{\text{CS},H}$	Current-sense fault high voltage	V <sub>S</sub> ≥ 5 V	Min(V <sub>S</sub> – 0.8, 4.3)		4.9	V
I <sub>CS,H</sub>	Current sense fault condition current	V <sub>CS</sub> = 4.3 V, V <sub>S</sub> > 7 V	10			mA
$V_{CL,th}$	Current limit internal threshold voltage (1)			1.233		V
I <sub>CS,leak</sub>	Current sense leakage current in	$V_{IN}$ = 5 V, $R_{load}$ = 10 $\Omega$ , $V_{DIAG\_EN}$ = 0 V, $T_{J}$ = 125°C			1	μΑ
Jojioan	disabled mode	V <sub>IN</sub> = 0 V, V <sub>DIAG EN</sub> = 0 V, T <sub>J</sub> = 125°C			1	μA

External current-limit accuracy is only applicable to overload conditions greater than 1.5x the current-limit setting. External current-limit setting is recommended to be higher than 500 mA.



# 6.6 Timing Requirements – Current Sense Characteristics (1)

			MIN	NOM	MAX	UNIT
t <sub>CS,off1</sub>	CS settling time from DIAG disabled	$V_{IN} = 5 \text{ V}$ , $I_{load} \ge 5 \text{ mA}$ . $V_{DIAG\_EN}$ from 5 to 0 V. CS to 10% of sense value.			10	μs
t <sub>CS,on1</sub>	CS settling time from DIAG enabled	$V_{IN} = 5 \text{ V}$ , $I_{load} \ge 5 \text{ mA}$ . $V_{DIAG\_EN}$ from 0 to 5 V. CS to 90% of sense value.			10	μs
t <sub>CS.off2</sub>	CS settling time	$V_{DIAG\_EN} = 5 \text{ V}, I_{load} \ge 5 \text{ mA}. \text{ IN from 5 to 0 V. CS to 10\% of sense value.}$		10		μs
00,02	from IN falling edge	V <sub>DIAG_EN</sub> = 5 V, I <sub>load</sub> ≥ 5 mA. IN from 5 to 0 V. Current limit triggered.			180	μs
t <sub>CS,on2</sub>	CS settling time from IN rising edge	$V_{VS}$ = 13.5 V, $V_{DIAG\_EN}$ = 5 V, $I_{load}$ $\ge$ 100 mA. $V_{IN}$ from 0 to 5 V. CS to 90% of sense value.			150	μs

(1) Value specified by design, not subject to production test.

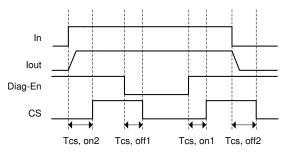


Figure 2. CS Delay Characteristics

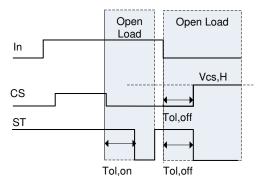


Figure 3. Open-Load Blanking Time Characteristics

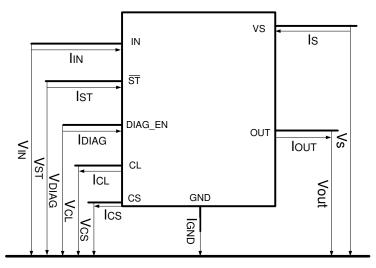


Figure 4. Pin Current and Voltage Conventions



## 6.7 Switching Characteristics

 $V_{VS}$  = 13.5 V,  $R_{load}$  = 10  $\Omega$ , over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

	PARAMETER	TEST CONDITIONS	MIN	TYP MAX	UNIT
$t_{d,ON}$	Turn-on delay time	IN rising edge to V <sub>OUT</sub> = 10%, DIAG_EN high	20	50	μs
$t_{d,OFF}$	Turn-off delay time	IN falling edge to V <sub>OUT</sub> = 90%, DIAG_EN high	20	50	μs
dV/dt <sub>ON</sub>	Slew rate on	V <sub>OUT</sub> = 10% to 90%, DIAG_EN high	0.1	0.5	V/µs
dV/dt <sub>OFF</sub>	Slew rate off	V <sub>OUT</sub> = 90% to 10%, DIAG_EN high	0.1	0.5	V/µs
	Slew rate on and off matching		-0.15	0.15	V/µs

(1) Value specified by design, not subject to production test.

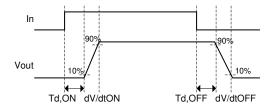


Figure 5. Switching Characteristics Diagram



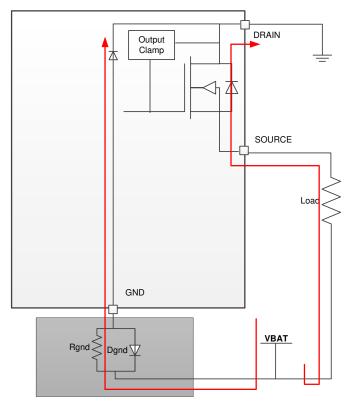


Figure 6.  $I_{rev1}$  Test Condition

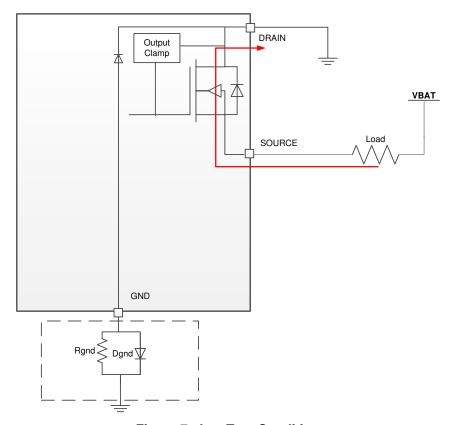
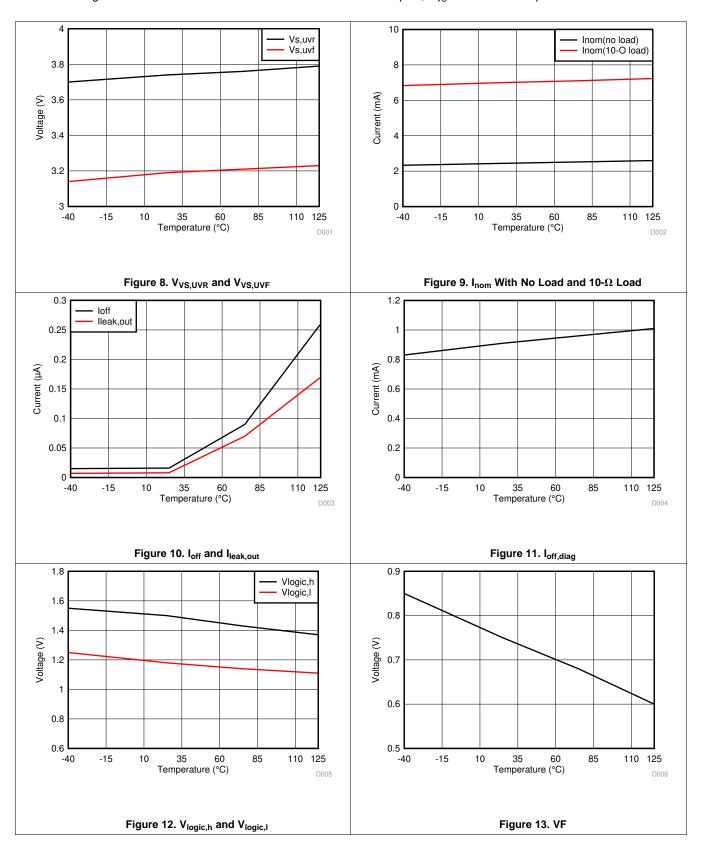


Figure 7.  $I_{rev2}$  Test Condition



## 6.8 Typical Characteristics

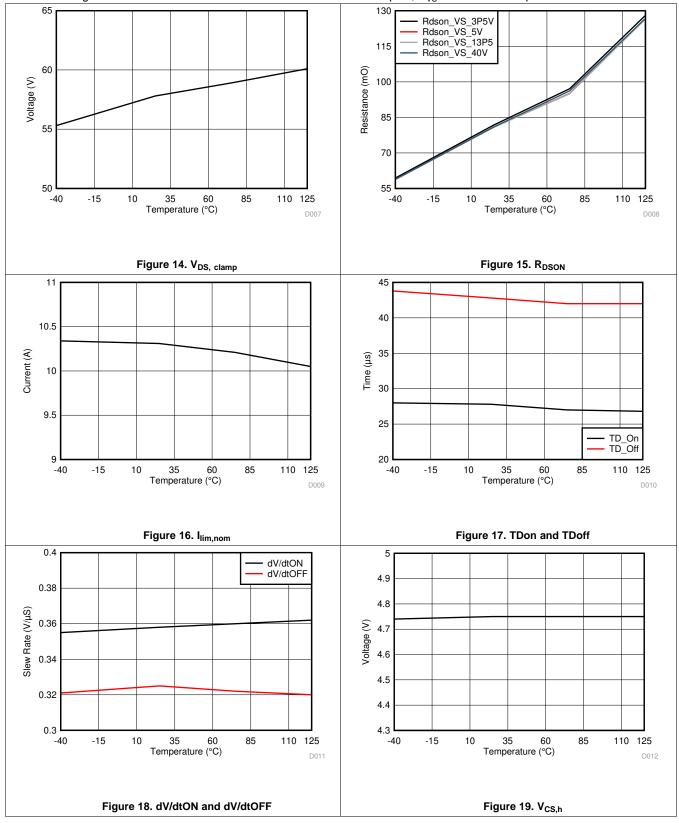
All the following data are based on the mean value of the three lots samples,  $V_{VS}$  = 13.5 V if not specified.





## **Typical Characteristics (continued)**

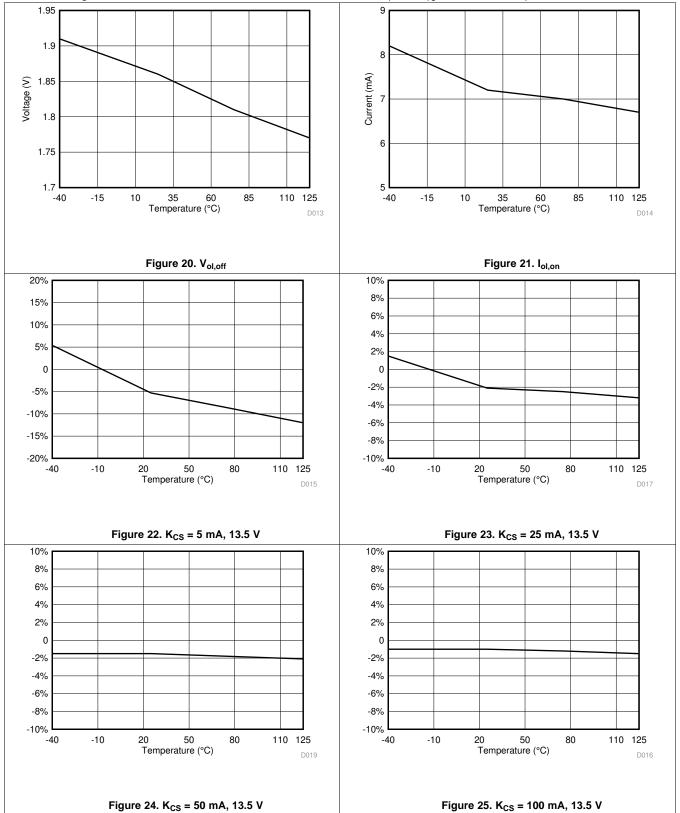
All the following data are based on the mean value of the three lots samples,  $V_{VS}$  = 13.5 V if not specified.





## **Typical Characteristics (continued)**

All the following data are based on the mean value of the three lots samples,  $V_{VS}$  = 13.5 V if not specified.





## **Typical Characteristics (continued)**

All the following data are based on the mean value of the three lots samples,  $V_{VS}$  = 13.5 V if not specified.

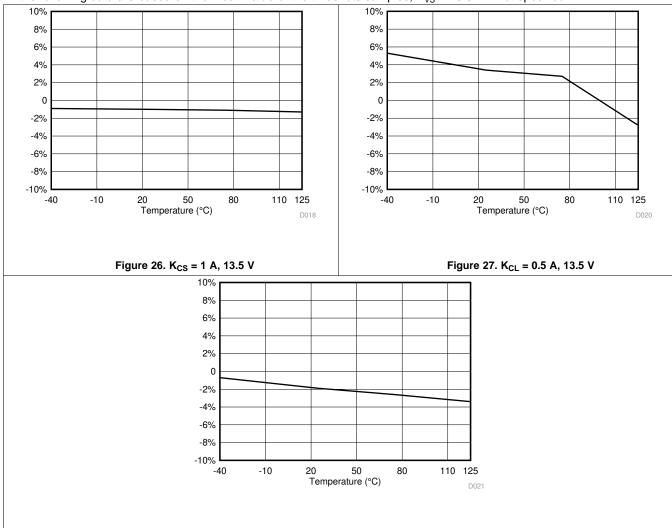


Figure 28.  $K_{CL} = 1.6 A, 13.5 V$ 



## 7 Detailed Description

#### 7.1 Overview

The TPS1H100-Q1 is a single-channel, fully-protected, high-side power switch with an integrated NMOS power FET and charge pump. Full diagnostics and high-accuracy current-sense features enable intelligent control of the load. A programmable current-limit function greatly improves the reliability of the whole system. The device diagnostic reporting has two versions to support both digital status and analog current-sense output, both of which can be set to the high-impedance state when diagnostics are disabled, for multiplexing the MCU analog or digital interface among devices.

For version A, the digital status report is implemented with an open-drain structure. When a fault condition occurs, it pulls down to GND. A 3.3- or 5-V external pullup is required to match the microcontroller supply level. For version B, high-accuracy current sensing allows a better real-time monitoring effect and more-accurate diagnostics without further calibration. A current mirror is used to source 1 / K of the load current, which is reflected as voltage on the CS pin. K is a constant value across the temperature and supply voltage. The current-sensing function operates normally within a wide linear region from 0 to 4 V. The CS pin can also report a fault by pulling up the voltage of  $V_{CS,h}$ .

The external high-accuracy current limit allows setting the current limit value by application. It highly improves the reliability of the system by clamping the inrush current effectively under start-up or short-circuit conditions. Also, it can save system costs by reducing PCB trace, connector size, and the preceding power-stage capacity. An internal current limit is also implemented in this device. The lower value of the external or internal current-limit value is applied.

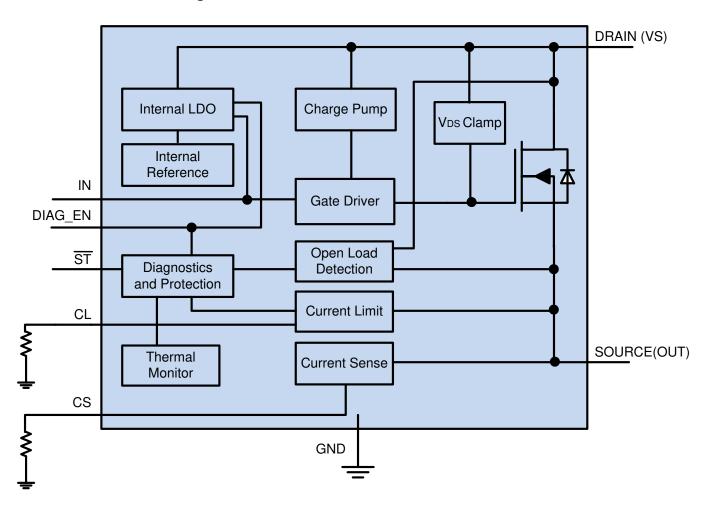
An active drain and source voltage clamp is built in to address switching off the energy of inductive loads, such as relays, solenoids, pumps, motors, and so forth. During the inductive switching-off cycle, both the energy of the power supply ( $E_{BAT}$ ) and the load ( $E_{LOAD}$ ) are dissipated on the high-side power switch itself. With the benefits of process technology and excellent IC layout, the TPS1H100-Q1 device can achieve excellent power dissipation capacity, which can help save the external free-wheeling circuitry in most cases. See *Inductive-Load Switching-Off Clamp* for more details.

Short-circuit reliability is critical for smart high-side power-switch devices. The standard of AEC-Q100-012 is to determine the reliability of the devices when operating in a continuous short-circuit condition. Different grade levels are specified according to the pass cycles. This device is qualified with the highest level, Grade A, 1 million times short-to-GND certification.

The TPS1H100-Q1 device can be used as a high-side power switch for a wide variety of resistive, inductive, and capacitive loads, including the low-wattage bulbs, LEDs, relays, solenoids, and heaters.



### 7.2 Functional Block Diagram



## 7.3 Feature Description

#### 7.3.1 Accurate Current Sense

For version B, the high-accuracy current-sense function is internally implemented, which allows a better real-time monitoring effect and more-accurate diagnostics without further calibration. A current mirror is used to source 1 / K of the load current, flowing out to the external resistor between the CS pin and GND, and reflected as voltage on the CS pin.

K is the ratio of the output current and the sense current. It is a constant value across the temperature and supply voltage. Each device was internally calibrated while in production, so post-calibration by users is not required in most cases.



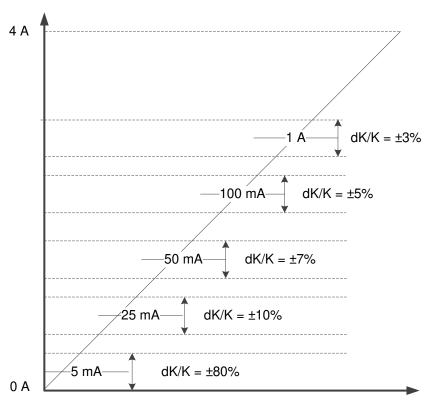


Figure 29. Current-Sense Accuracy

Ensure the CS voltage is in the linear region (0 to 4 V) during normal operation. Calculate R<sub>CS</sub> with Equation 1.

$$R_{CS} = \frac{V_{CS}}{I_{CS}} = \frac{V_{CS} \times K}{I_{out}}$$
 (1)

Also, when a fault condition occurs, CS works as a diagnostics report pin. When an open load or short to battery occurs in the on-state,  $V_{CS}$  almost equals 0. When current limit, thermal shutdown/swing, open load, or short to battery in the off-state occurs, the voltage is pulled up to  $V_{CS,h}$ . Figure 30 shows a typical current-sense voltage according to the operating conditions, including fault conditions.

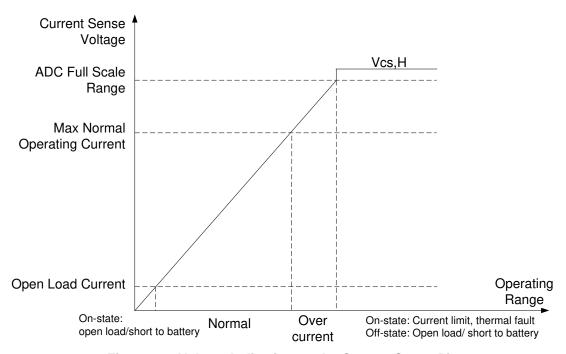


Figure 30. Voltage Indication on the Current-Sense Pin

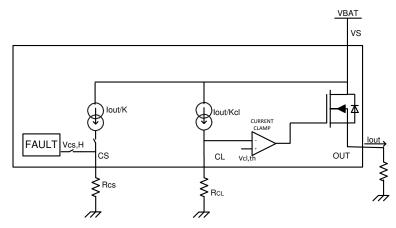


Figure 31. Current-Sense and Current-Limit Block Diagram

### 7.3.2 Programmable Current Limit

A high-accuracy current limit allows higher reliability, which protects the power supply during short circuit or power up. Also, it can save system costs by reducing PCB traces, connector size, and the capacity of the preceding power stage.

Current limit offers protection from overstressing to the load and integrated power FET. Current limit holds the current at the set value, and pulls up the CS pin to  $V_{CS,h}$  as a diagnostic report. The two current-limit thresholds are:

External programmable current limit -- An external resistor is used to convert a proportional load current into a voltage, which is compared with an internal reference voltage, V<sub>th,cl</sub>. When the voltage on the CL pin exceeds V<sub>th,cl</sub>, a closed loop steps in immediately. V<sub>GS</sub> voltage regulates accordingly, leading to the V<sub>ds</sub> voltage regulation. When the closed loop is set up, the current is clamped at the set value. The external programmable current limit provides the capability to set the current-limit value by application.



• Internal current limit -- The internal current limit is fixed and typically 10 A. To use the internal current limit for large-current applications, tie the CL pin directly to the device GND.

Both the internal current limit ( $I_{lim,nom}$ ) and external programmable current limit are always active when  $V_{VS}$  is powered and IN is high. The lower one (of  $I_{lim,nom}$  and the external programmable current limit) is applied as the actual current limit.

Note that if a GND network is used (which leads to the level shift between the device GND and board GND), the CL pin must be connected with device GND. Calculate  $R_{CL}$  with Equation 2.

$$I_{CL} = \frac{V_{CL,th}}{R_{CL}} = \frac{I_{out}}{K_{CL}} \rightarrow R_{CL} = \frac{V_{CL,th} \times K_{CL}}{I_{out}}$$
(2)

For better protection from a hard short-to-GND condition (when  $V_S$  and input are high and a short to GND happens suddenly), an open-loop fast-response behavior is set to turn off the channel, before the current-limit closed loop is set up. The open-loop response time is around 1  $\mu s$ . With this fast response, the device can achieve better inrush-suppression performance.

### 7.3.3 Inductive-Load Switching-Off Clamp

When an inductive load is switching off, the output voltage is pulled down to negative, due to the inductance characteristics. The power FET may break down if the voltage is not clamped during the current-decay period. To protect the power FET in this situation, internally clamp the drain-to-source voltage, namely  $V_{DS,clamp}$ , the clamp diode between the drain and gate.

$$V_{DS,clamp} = V_{BAT} - V_{OUT}$$
(3)

During the current-decay period ( $T_{DECAY}$ ), the power FET is turned on for inductance-energy dissipation. Both the energy of the power supply ( $E_{BAT}$ ) and the load ( $E_{LOAD}$ ) are dissipated on the high-side power switch itself, which is called  $E_{HSD}$ . If resistance is in series with inductance, some of the load energy is dissipated in the resistance.

$$E_{HSD} = E_{BAT} + E_{LOAD} = E_{BAT} + E_{L} - E_{R}$$
(4)

From the high-side power switch's view, E<sub>HSD</sub> equals the integration value during the current-decay period.

$$E_{HSD} = \int_{0}^{T_{DECAY}} V_{DS,clamp} \times I_{OUT}(t) dt$$
 (5)

$$T_{DECAY} = \frac{L}{R} \times \ln \left( \frac{R \times I_{OUT(MAX)} + |V_{OUT}|}{|V_{OUT}|} \right)$$
(6)

$$E_{HSD} = L \times \frac{V_{BAT} + \left| V_{OUT} \right|}{R^2} \times \left[ R \times I_{OUT(MAX)} - \left| V_{OUT} \right| In \left( \frac{R \times I_{OUT(MAX)} + \left| V_{OUT} \right|}{\left| V_{OUT} \right|} \right) \right]$$
(7)

When R approximately equals 0,  $E_{\mbox{\scriptsize HSD}}$  can be given simply as:

$$E_{HSD} = \frac{1}{2} \times L \times I_{OUT(MAX)}^2 \frac{V_{BAT} + |V_{OUT}|}{R^2}$$
(8)



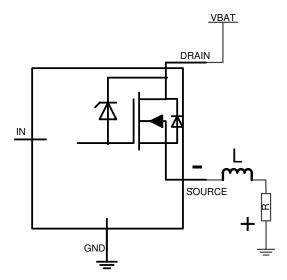


Figure 32. Driving Inductive Load

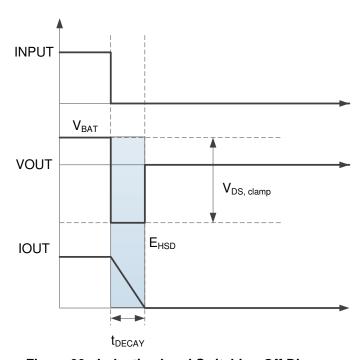


Figure 33. Inductive-Load Switching-Off Diagram

As discussed previously, when switching off, battery energy and load energy are dissipated on the high-side power switch, which leads to the large thermal variation. For each high-side power switch, the upper limit of the maximum safe power dissipation depends on the device intrinsic capacity, ambient temperature, and board dissipation condition. TI provides the upper limit of single-pulse energy that devices can tolerate under the test condition:  $V_{VS} = 13.5 \text{ V}$ , inductance from 0.1 mH to 400 mH,  $R = 0 \Omega$ , FR4 2s2p board, 2- × 70- $\mu$ m copper, 2- × 35- $\mu$ m copper, thermal pad copper area 600 mm<sup>2</sup>.

For one dedicated inductance, see Figure 34. If the maximum switching-off current is lower than the current value shown on the curve, the internal clamp function can be used for the demagnetization energy dissipation. If not, external free-wheeling circuitry is necessary for device protection.



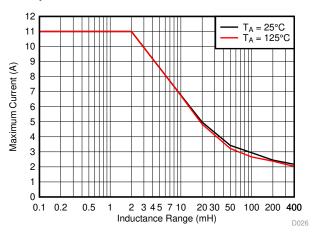


Figure 34. Maximum Current vs Inductance Range

## 7.3.4 Full Protections and Diagnostics

Table 1 is when DIAG\_EN enabled. When DIAG\_EN is low, current sense or ST is disabled accordingly. The output is in high-impedance mode. Refer to Table 2 for details.

**Table 1. Fault Table** 

CONDITIONS	IN	OUT	CRITERION	ST (Version A)	CS (Version B)	Diagnostics Recovery
Normal	L L			Н	0	
Normal	Н	Н		Н	In linear region	
Short to GND	Н	L	Current limit triggered.	L	V <sub>CS,h</sub>	AUTO
Open load <sup>(1)</sup> Short to battery	Н	Н	Version A: Output current < I <sub>ol,on</sub> Version B: Judged by users	L (deglitch)	Almost 0	AUTO
Reverse polarity	L	Н	$V_{VS} - V_{OUT} < V_{ol,off}$	L (deglitch)	V <sub>CS,h</sub> (deglitch)	AUTO
Thermal shutdown	Н		TSD triggered	1,1		Recovery when temp < T <sub>SD,rst</sub>
Thermal swing	Н		T <sub>sw</sub> triggered	L	$V_{CS,h}$	AUTO

<sup>(1)</sup> Need external pullup resistor during off-state

Table 2. DIAG\_EN Logic Table

DIAG_EN	IN Condition	Protections and Diagnostics			
HIGH	ON	See Table 1			
півп	OFF	See Table 1			
LOW	ON	Diagnostics disabled, protection normal CS or ST is high Impedance			
LOW	OFF	Diagnostics disabled, no protections CS or ST is high impedance			



#### 7.3.4.1 Short-to-GND and Overload Detection

In the on state, the short-to-GND fault is reported as the low status output or  $V_{CS,h}$  on CS, when a current limit is triggered. The lower one of the internal and external set values is applied for the actual current limit. It is in autorecovery when the fault condition is cleared. If not cleared, thermal shutdown triggers to protect the power FET.

#### 7.3.4.2 Open-Load Detection

In the on state for version A, if the current flowing through the output is less than I<sub>ol,on</sub>, the device recognizes an open-load fault. For version B, faults are diagnosed by reading the voltage on the CS pin and judged by the user. A benefit of high-accuracy current sense down to a verylow current range, this device can achieve a very low open-load detection threshold, which correspondingly expands the normal operation region. TI suggests 10 mA as the upper limit for the open-load detection threshold and 25 mA as the lower limit for the normal operation current. In Figure 35, the recommended open-load detection region is shown as the dark-shaded region and the light-shaded region is for normal operation. As a guideline, do not overlap these two regions.

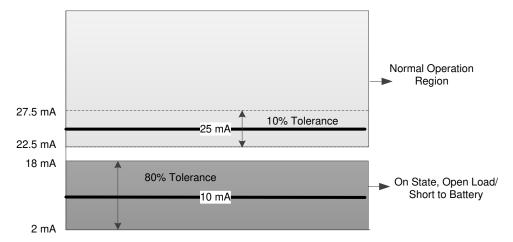


Figure 35. On-State Open-Load Detection and Normal-Operation Diagram

In the off state, if a load is connected, the output voltage is pulled to 0 V. In the case of an open load, the output voltage is close to the supply voltage,  $V_S - V_{OUT} < V_{ol,off}$ . For version A, the ST pin goes low to indicate the fault to the MCU. For version B, the CS pin is pulled up to  $V_{CS,h}$ . There is always a leakage current  $I_{ol,off}$  present on the output, due to the internal logic control path or external humidity, corrosion, and so forth. Thus, TI recommends an external pullup resistor to offset the leakage current. This pullup current should be less than the output load current to avoid false detection in the normal operation mode. To reduce the standby current, TI recommends always to use a switch in series with? the pullup resistor. TI recommends  $R_{ou} \le 15 \text{ k}\Omega$ .

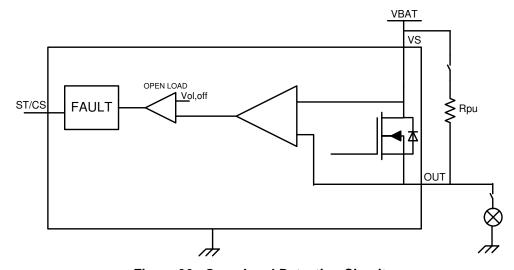


Figure 36. Open-Load Detection Circuit



#### 7.3.4.3 Short-to-Battery Detection

Short-to-battery detection has the same detection mechanism and behavior as open-load detection, both in the on-state and off-state. See the fault truth table, Table 1, for more details. In the on-state, the reverse current flows through the FET instead of the body diode, leading to less power dissipation. Thus, the worst case for off-state is when reverse current occurs. In the off-state, if  $V_{OUT} - V_{VS} < V_F$ , short to battery can be detected. ( $V_F$  is the body diode forward voltage and typically 0.7 V.) However, the reverse current does not occur. If  $V_{OUT} - V_{VS} > V_F$ , short to battery can be detected, and the reverse current should be lower than  $I_{rev2}$  to ensure the survival of the device. TI recommends switching on the input for lower power dissipation or the reverse block circuitry for the supply. See *Reverse Current Protection* for more external protection circuitry information.

### 7.3.4.4 Reverse-Polarity Detection

Reverse-polarity detection has the same detection mechanism and behavior as open-load detection, both in the on-state and off-state. See the fault truth table, Table 1, for more details. In the on-state, the reverse current flows through the FET instead of the body diode, leading to less power dissipation. Thus, the worst case off-state is when reverse current occurs. In off-state, the reverse current should be lower than I<sub>rev1</sub> to ensure the survival of the device. See *Reverse Current Protection* for more external protection circuitry information.

#### 7.3.4.5 Thermal Protection Behavior

Both the absolute temperature thermal shutdown and the dynamic temperature thermal swing diagnostic and protection are built into the device to increase the maximum reliability of the power FET. Thermal swing is active when the temperature of the power FET is increasing sharply, that is  $\Delta T = T_{DMOS} - T_{Logic} > T_{sw}$ , then the output is shut down, and the ST pin goes low, or the CS pin is pulled up to  $V_{CS,h}$ . It auto-recovers and clears the fault signal until  $\Delta T = T_{DMOS} - T_{Logic} < T_{sw} - T_{hys}$ . Thermal swing function improves device reliability against repetitive fast thermal variation, as shown in Figure 37. Multiple thermal swings are triggered before thermal shutdown happens. Thermal shutdown is active when absolute temperature T >  $T_{SD}$ . When active, the output is shut down, and the ST pin goes low, or the CS pin is pulled up to  $V_{CS,h}$ . The output is auto-recovered when T <  $T_{SD} - T_{hys}$ ; the current limit is reduced to  $I_{lim,tsd}$ , or half of the programmable current limit value, to avoid repeated thermal shutdown. However, the thermal shutdown fault signal and half-current limit value are not cleared until the junction temperature decreases to less than  $T_{SD rst}$ .



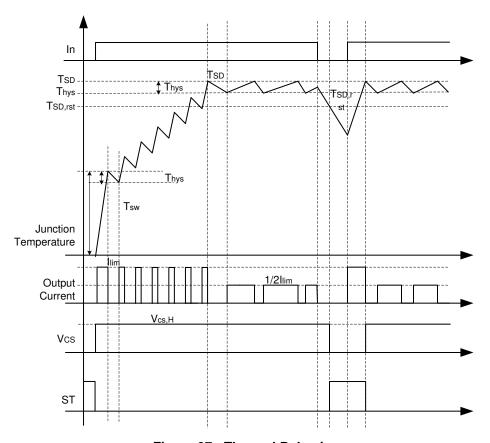


Figure 37. Thermal Behavior

## 7.3.4.6 UVLO Protection

The device monitors the supply voltage  $V_{VS}$  to prevent unpredicted behaviors in the event that the supply voltage is too low. When the supply voltage falls down to  $V_{VS,UVF}$ , the output stage is shut down automatically. When the supply rises up to  $V_{VS,UVR}$ , the device turns on.



### 7.3.4.7 Loss of GND Protection

When loss of GND occurs, output is turned off regardless of whether the input signal is high or low.

Case 1 (loss of device GND): Loss of GND protection is active when the Tab,  $I_{C\_GND}$ , and current limit GND are one trace connected to the board GND, as shown in Figure 38. Tab floating is also a choice.

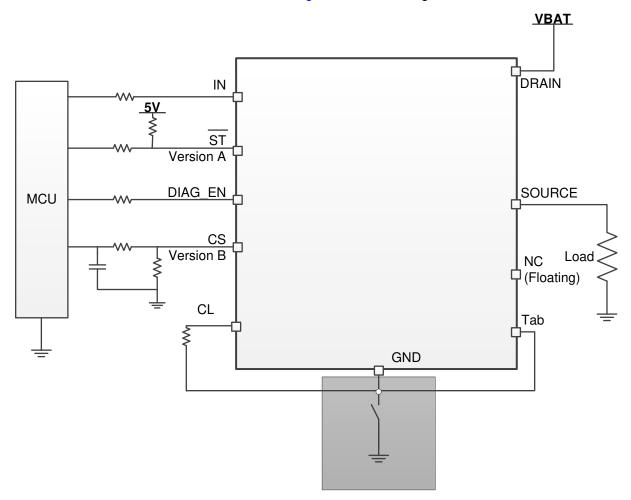


Figure 38. Loss of Device GND



Case 2 (loss of module GND): When the whole ECU module GND is lost, protections are also active. At this condition, the load GND remains connected.

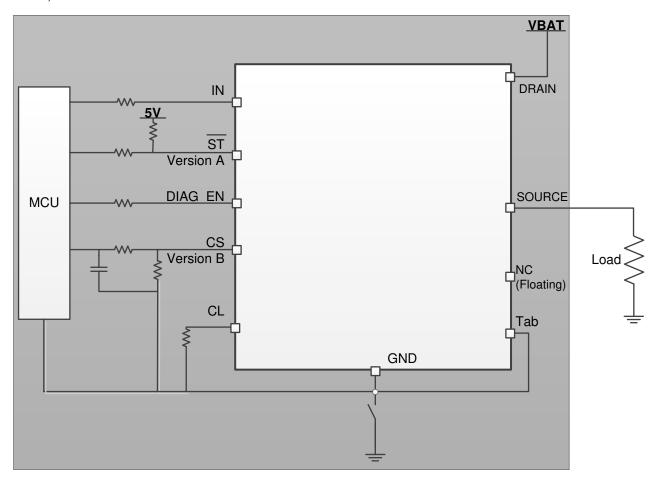


Figure 39. Loss of Module GND



## 7.3.4.8 Loss of Power Supply Protection

When loss of supply occurs, output is turned off regardless of whether the input is high or low. For a resistive or capacitive load, loss-o-supply protection is easy to achieve due to no more power. The worst case is a charged inductive load. In this case, the current is driven from all of the IOs to maintain the inductance output loop. TI recommends either the MCU serial resistor plus the GND network (diode and resistor in parallel) or external free-wheeling circuitry.

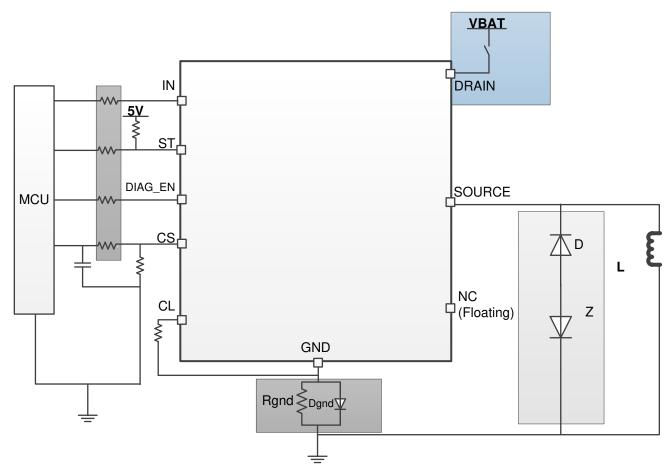


Figure 40. Loss of Battery



### 7.3.4.9 Reverse Current Protection

**Method 1:** Block diode connected with  $V_S$ . Both the device and load are protected when in reverse polarity.

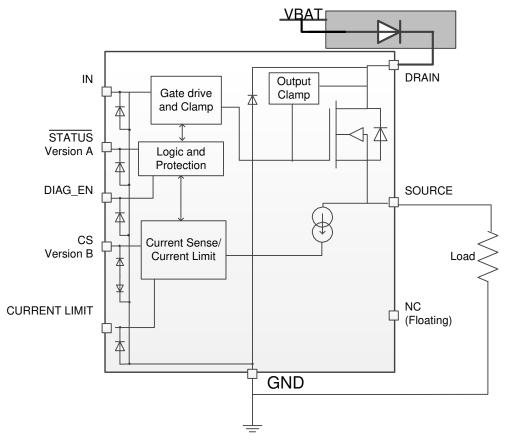


Figure 41. Reverse Protection With Block Diode



**Method 2 (GND network protection):** Only the high-side device is protected under this connection. The load reverse loop is limited by the load itself. Note when reverse polarity happens, the continuous reverse current through the power FET should be less than  $I_{rev}$ . Of the three types of ground pin networks, TI strongly recommends type 3 (the resistor and diode in parallel). No matter what types of connection are between the device GND and the board GND, if a GND voltage shift happens, ensure the following proper connections for the normal operation:

- Leave the NC pin floating or connect to the device GND. TI recommends to leave floating.
- Connect the current limit programmable resistor to the device GND.

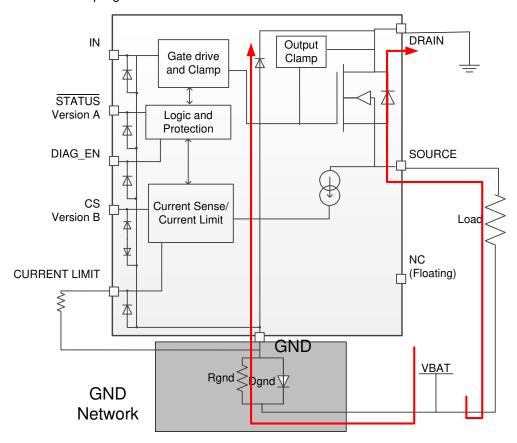


Figure 42. Reverse Protection With GND Network

• **Type 1 (resistor):** The higher resistor value contributes to a better current limit effect when the reverse battery or negative ISO pulses. However, it leads to higher GND shift during normal operation mode. Also, consider the resistor's power dissipation.

$$R_{GND} \le \frac{V_{GNDshift}}{I_{nom}}$$

$$R_{GND} \ge \frac{\left(-V_{CC}\right)}{\left(-I_{GND}\right)}$$
(9)

where

- V<sub>GNDshift</sub> is the maximum value for the GND shift, determined by the HSD and microcontroller. TI suggests a value ≤ 0.6 V.
- I<sub>nom</sub> is the nominal operating current.
- -V<sub>CC</sub> is the maximum reverse voltage seen on the battery line.

If multiple high-side power switches are used, the resistor can be shared among devices.

Type 2 (diode): A diode is needed to block the reverse voltage, which also brings a ground shift (≈ 600 mV).



However, an inductive load is not acceptable to avoid an abnormal status when switching off.

Type 3 (resistor and diode in parallel (recommended)): A peak negative spike may occur when the
inductive load is switching off, which may damage the HSD or the diode. So, TI recommends a resistor in
parallel with the diode when driving an inductive load. The recommended selection are 1-kΩ resistor in
parallel with an I<sub>F</sub> > 100-mA diode. If multiple high-side switches are used, the resistor and diode can be
shared among devices.

#### 7.3.4.10 Protection for MCU I/Os

In many conditions, such as the negative ISO pulse, or the loss of battery with an inductive load, a negative potential on the device GND pin may damage the MCU I/O pins [more likely, the internal circuitry connected to the pins]. Therefore, the serial resistors between MCU and HSD are required.

Also, for proper protection against loss of GND, TI recommends 4.7 k $\Omega$  when using 3.3-V MCU I/Os; 10 k $\Omega$  is for 5-V applications.

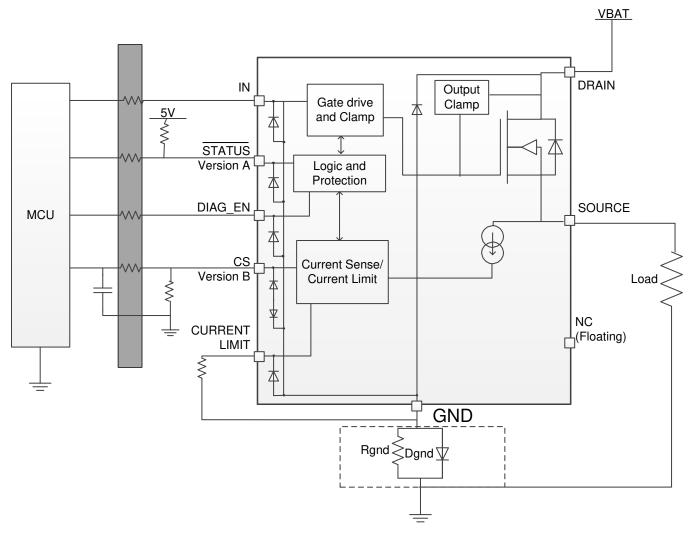


Figure 43. MCU IO Protections

## 7.3.5 Diagnostic Enable Function

The diagnostic enable pin, DIAG\_EN, offers multiplexing of the microcontroller diagnostic input for current sense or digital status, by sharing the same sense resistor and ADC line or I/O port among multiple devices.



In addition, during the output-off period, the diagnostic disable function lowers the current consumption for the standby condition. The three working modes in the device are normal mode, standby mode, and standby mode with diagnostic. If off-state power saving is required in the system, the standby current is <500 nA with DIAG\_EN low. If the off-state diagnostic is required in the system, the typical standby current is around 1 mA with DIAG\_EN high.

#### 7.4 Device Functional Modes

#### 7.4.1 Working Mode

The three working modes in the device are normal mode, standby mode, and standby mode with diagnostic. If an off-state power saving is required in the system, the standby current is less than 500 nA with DIAG\_EN low. If an off-state diagnostic is required in the system, the typical standby current is around 1 mA with DIAG\_EN high. Note that to enter standby mode requires IN low and  $t > t_{off,deg}$ .  $t_{off,deg}$  is the standby-mode deglitch time, which is used to avoid false triggering. Figure 44 shows a work-mode state-machine state diagram.

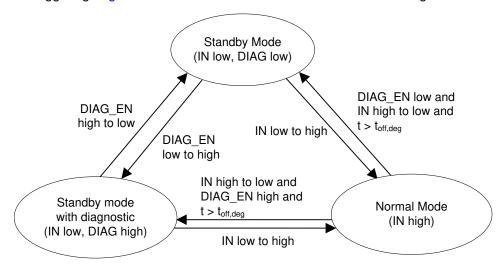


Figure 44. Work-Mode State Machine



## 8 Application and Implementation

#### **NOTE**

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

## 8.1 Application Information

The following discussion notes how to implement the device to distinguish the different fault modes and implement a ? transient-pulse immunity test.

In some applications, open load, short to battery, and short to GND must be distinguished from each other. This requires two steps.

## 8.2 Typical Application

Figure 45 shows an example of how to design the external circuitry parameters.

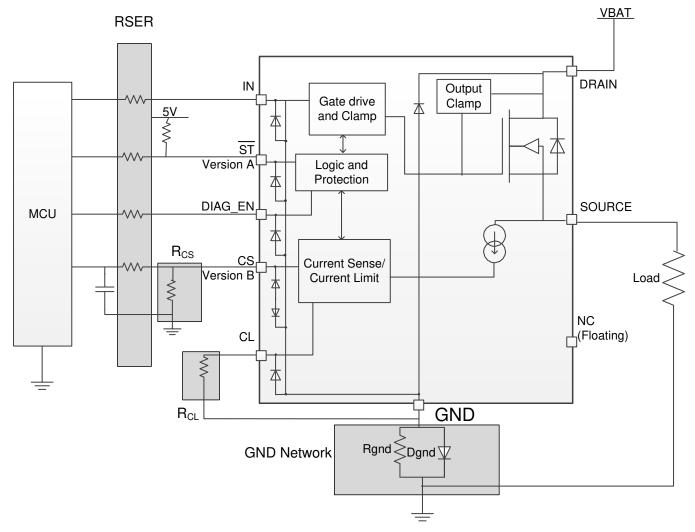


Figure 45. Typical Application Circuitry



## Typical Application (continued)

#### 8.2.1 Design Requirements

- V<sub>S</sub> range from 9 V to 16 V
- Nominal current of 2 A
- Current sense for fault monitoring
- Expected current limit value of 5 A
- Full diagnostics with 5-V MCU
- · Reverse protection with GND network

#### 8.2.2 Detailed Design Procedure

The  $R_{CS}$ ,  $V_{CS}$  linear region is from 0 to 4 V. To keep the 2-A nominal current in the 0- to 3-V range, calculate the  $R_{CS}$  as in Equation 11. To achieve better current sense accuracy, a 1% accuracy or better resistor is preferred.

$$R_{CS} = \frac{V_{CS}}{I_{CS}} = \frac{V_{CS} \times K}{I_{OUT}} = \frac{3 \times 500}{2} = 750 \ \Omega$$
 (11)

 $R_{CL}$ ,  $V_{CL,th}$  is the current-limit internal threshold, 1.233 V. To set the programmable current limit value at 5 A, calculate the  $R_{CL}$  as in Equation 12.

$$R_{CL} = \frac{V_{cl,th} \times K_{CL}}{I_{OUT}} = \frac{1.233 \times 2000}{5} = 493.2 \Omega$$
(12)

TI recommends  $R_{SFR} = 10 \text{ k}\Omega$  for 5-V MCU.

TI recommends a 1-k $\Omega$  resistor and 200-V, 0.2-A diode for the GND network.

### 8.2.2.1 Distinguishing of Different Fault Modes

Some applications require that open load, short to battery, and short to GND can be distinguished from each other. This requires two steps:

- 1. In the on-state, for the current-sense version device (version B), on-state open load and short to battery are recognized as an extremely-low voltage level on the current-sense pin, whereas short to GND is reported as a pulled-up voltage V<sub>CS.h</sub>. Therefore, the user can find a short to GND (see Figure 46).
- 2. If reported as an on-state open-load or short-to-battery fault in the first step, turn off the input signal. In the off-state, with an external pulldown resistor, open load and short to battery can be easily distinguished. When the output pulls down, the short to battery is still reported as an off-state fault condition, whereas the open load is ignored.

## **Typical Application (continued)**

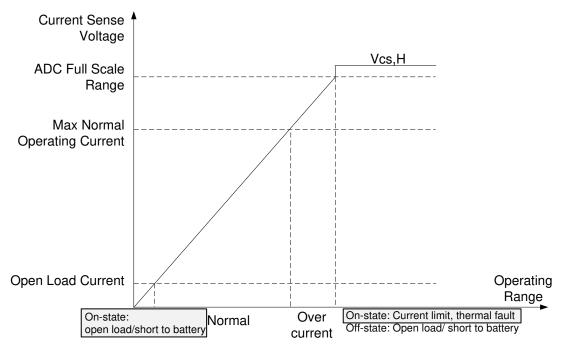


Figure 46. Step 1: Short-to-GND Detection in the On-State

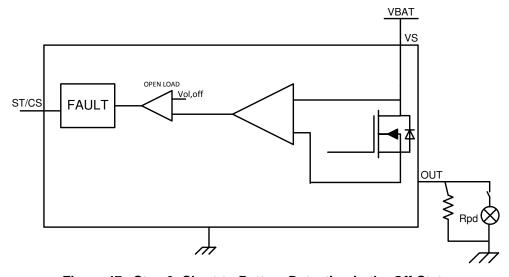


Figure 47. Step 2: Short-to-Battery Detection in the Off-State

#### 8.2.2.2 AEC Q100-012 Test Grade A Certification

Short-circuit reliability is critical for smart high-side power switch devices. The AEC-Q100-012 standard is used to determine the reliability of the devices when operating in a continuous short-circuit condition. Different grade levels are specified according to the pass cycles. This device is qualified with the highest level, Grade A, 1 million times short-to-GND certification.

Three test modes are defined in the AEC Q100-012 standard. See Table 3 for cold repetitive short-circuit test – long pulse, cold repetitive short-circuit test – short pulse, and hot repetitive short-circuit test.



## **Typical Application (continued)**

#### Table 3. Tests

Test Items	Test Condition	Test Cycles
Cold repetitive short-circuit test – short pulse	-40°C, 10-ms pulse, cool down	1M
Cold repetitive short-circuit test – long pulse	-40°C, 300-ms pulse, cool down	1M
Hot repetitive short-circuit test	25°C, continuous short	1M

Different grade levels are specified according to the pass cycles. The TPS1H100-Q1 device gets the certification of Grade A level, 1 million short-to-GND cycles, which is the highest test standard in the market.

Table 4. Grade Levels

Grade	Number of Cycles	Lots,Samples Per Lot	Number of Fails
Α	>1000000	3, 10	0
В	>300000 to 1000000	3, 10	0
С	>100000 to 300000	3, 10	0
D	>30000 to 100000	3, 10	0
E	>10000 to 30000	3, 10	0
F	>3000 to 10000	3, 10	0
G	>1000 to 3000	3, 10	0
Н	300 to 1000	3, 10	0
0	<300	3, 10	0

#### 8.2.2.3 EMC Transient Disturbances Test

Due to the severe electrical conditions in the automotive environment, immunity capacity against electrical transient disturbances is required, especially for a high-side power switch, which is connected directly to the battery. Detailed test requirements are in accordance with the ISO 7637-2:2011 and ISO 16750-2:2010 standards. The TPS1H100-Q1 device is tested and certificated by a third-party organization.

Table 5. ISO 7637-2:2011(E) in 12-V System (1)(2)(3)(4)

Test		e Severity Level Accordingly	Pulse	Minimum Number of	Burst-Cyc Repetition		Input Resistance	Function Performance	
Item	Level	Vs/V	Duration (t <sub>d</sub> )	Pulses or Test Time	MIN	MAX	(Ω)	Status Classification	
1	III	-112	2 ms	500 pulses	0.5 s	e s	10	Status II	
2a	III	55	50 µs	500 pulses	0.2 s	5 s	2	Status II	
2b	IV	10	0.2 to 2 s	10 pulses	0.5 s	5 s	0 to 0.05	Status II	
3a	IV	-220	0.1 µs	1h	90 ms	100 ms	50	Status II	
3b	IV	150	0.1 µs	1h	90 ms	100 ms	50	Status II	

- (1) Tested both under input low condition and high condition.
- (2) Considering the worst test condition, it is tested without any filter capacitors in V<sub>S</sub> and V<sub>OUT</sub>.
- (3) GND pin network is a 1-k $\Omega$  resistor in parallel with a diode BAS21-7-F.
- (4) Status II: The function does not perform as designed during the test, but returns automatically to normal operation after the test.

Table 6. ISO 16750-2:2010(E) Load Dump Test B in 12-V System<sup>(1)(2)(3)(4)(5)</sup>

Test Item		Severity Level ccordingly	Pulse	Minimum Number of	Burst Cyc Repetitio		Input Resistance	Function Performance Status Classification	
	Level	Vs/V	Duration (t <sub>d</sub> )	Pulses or Test Time	MIN (s)	MAX (s)	(Ω)		
Test B		45	40 to 400 ms	5 pulses	60	е	0.5 to 4	Status II	

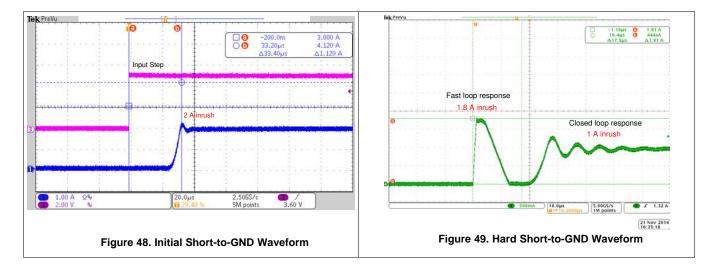
- (1) Tested both under input low condition and high condition, IDIAG EN, IN, and VS are all classified as inputs, Which one?
- (2) Considering the worst test condition, the device is tested without any filter capacitors on VS and OUT.
- 3) The GND pin network is a 1-k $\Omega$  resistor in parallel with a diode BAS21-7-F.
- 4) Status II: The function does not perform as designed during the test, but returns automatically to normal operation after the test.
- (5) Select a 45-V external suppressor.



### 8.2.3 Application Curves

Figure 48 shows a test example of initial short-circuit inrush-current limit. Test conditions:  $V_S = 13.5 \text{ V}$ , input is from low to high, load is short-to-GND or with a 470- $\mu$ F capacitive load, external current limit is 2 A. CH1 is the output current. CH3 is the input step.

Figure 49 shows a test example of a hard short-circuit inrush-current limit. Test conditions:  $V_S$ = 13.5 V, input is high, load is 5  $\mu$ H + 100 m $\Omega$ , external current limit is 1 A. A short to GND suddenly happens.





## 9 Power Supply Recommendations

The device is qualified for both automotive and industrial applications. The normal power supply connection is a 12-V automotive system or 24-V industrial system. The supply voltage should be within the range specified in the *Recommended Operating Conditions*.

## 10 Layout

## 10.1 Layout Guidelines

To prevent thermal shutdown,  $T_J$  must be less than 150°C. If the output current is very high, the power dissipation may be large. The HTSSOP package has good thermal impedance. However, the PCB layout is very important. Good PCB design can optimize heat transfer, which is absolutely essential for the long-term reliability of the device.

- Maximize the copper coverage on the PCB to increase the thermal conductivity of the board. The major heatflow path from the package to the ambient is through the copper on the PCB. Maximum copper is extremely important when there are not any heat sinks attached to the PCB on the other side of the board opposite the package.
- Add as many thermal vias as possible directly under the package ground pad to optimize the thermal conductivity of the board.
- All thermal vias should either be plated shut or plugged and capped on both sides of the board to prevent solder voids. To ensure reliability and performance, the solder coverage should be at least 85%.

### 10.2 Layout Example

#### 10.2.1 Without a GND Network

Without a GND network, tie the thermal pad directly to the board GND copper for better thermal performance.

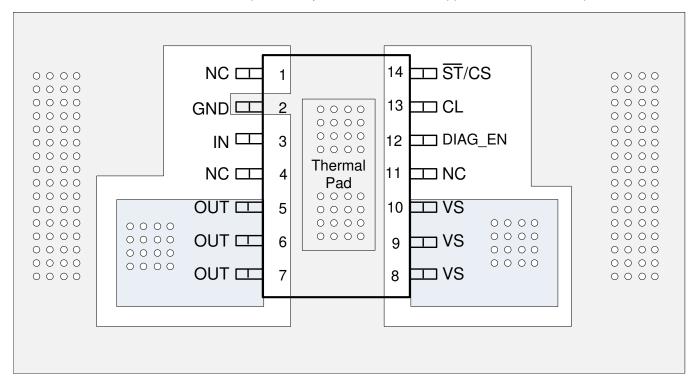


Figure 50. Layout Without a GND Network

37



## **Layout Example (continued)**

#### 10.2.2 With a GND Network

With a GND network, tie the thermal pad with a single trace through the GND network to the board GND copper.

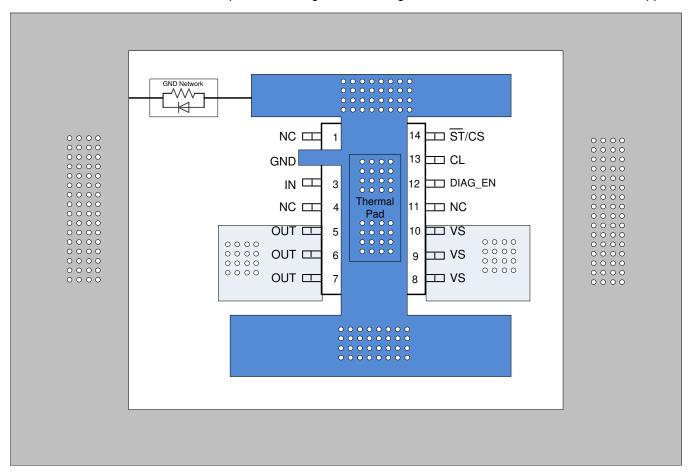


Figure 51. Layout With a GND Network

## 10.3 Thermal Considerations

This device possesses thermal shutdown (TSD) circuitry as a protection from overheating. For continuous normal operation, the junction temperature should not exceed the thermal-shutdown trip point. If the junction temperature exceeds the thermal-shutdown trip point, the output turns off. When the junction temperature falls below the thermal-shutdown trip point, the output turns on again.

Calculate the power dissipated by the device according to Equation 13.

$$P_T = I_{OUT}^2 \times R_{DSON} + V_S \times I_{nom}$$

where

After determining the power dissipated by the device, calculate the junction temperature from the ambient temperature and the device thermal impedance.

$$T_{J} = T_{A} + R_{\theta JA} \times P_{T} \tag{14}$$

(13)



## 11 器件和文档支持

### 11.1 接收文档更新通知

要接收文档更新通知,请导航至 Tl.com.cn 上的器件产品文件夹。单击右上角的通知我 进行注册,即可每周接收产品信息更改摘要。有关更改的详细信息,请查看任何已修订文档中包含的修订历史记录。

### 11.2 社区资源

TI E2E<sup>TM</sup> support forums are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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### 11.3 商标

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### 11.4 静电放电警告



这些装置包含有限的内置 ESD 保护。 存储或装卸时,应将导线一起截短或将装置放置于导电泡棉中,以防止 MOS 门极遭受静电损伤。

## 11.5 Glossary

SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.

## 12 机械、封装和可订购信息

以下页面包含机械、封装和可订购信息。这些信息是指定器件的最新可用数据。数据如有变更,恕不另行通知,且不会对此文档进行修订。如需获取此数据表的浏览器版本,请查阅左侧的导航栏。

www.ti.com 4-Aug-2025

#### PACKAGING INFORMATION

Orderable part number	Status	Material type	Package   Pins	Package qty   Carrier	RoHS	Lead finish/ Ball material	MSL rating/ Peak reflow	Op temp (°C)	Part marking (6)
						(4)	(5)		
TPS1H100AQPWPRQ1	Active	Production	HTSSOP (PWP)   14	2000   LARGE T&R	Yes	NIPDAU	Level-3-260C-168 HR	-40 to 125	1H100AQ
TPS1H100AQPWPRQ1.A	Active	Production	HTSSOP (PWP)   14	2000   LARGE T&R	Yes	NIPDAU	Level-3-260C-168 HR	-40 to 125	1H100AQ
TPS1H100BQPWPRQ1	Active	Production	HTSSOP (PWP)   14	2000   LARGE T&R	Yes	NIPDAU	Level-3-260C-168 HR	-40 to 125	1H100BQ
TPS1H100BQPWPRQ1.A	Active	Production	HTSSOP (PWP)   14	2000   LARGE T&R	Yes	NIPDAU	Level-3-260C-168 HR	-40 to 125	1H100BQ

<sup>(1)</sup> Status: For more details on status, see our product life cycle.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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<sup>(3)</sup> RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

<sup>(4)</sup> Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

<sup>(5)</sup> MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

<sup>(6)</sup> Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

# **PACKAGE MATERIALS INFORMATION**

www.ti.com 24-Apr-2024

## TAPE AND REEL INFORMATION





A0	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



#### \*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS1H100AQPWPRQ1	HTSSOP	PWP	14	2000	330.0	12.4	6.9	5.6	1.6	8.0	12.0	Q1
TPS1H100BQPWPRQ1	HTSSOP	PWP	14	2000	330.0	12.4	6.9	5.6	1.6	8.0	12.0	Q1

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## \*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS1H100AQPWPRQ1	HTSSOP	PWP	14	2000	350.0	350.0	43.0
TPS1H100BQPWPRQ1	HTSSOP	PWP	14	2000	350.0	350.0	43.0

4.4 x 5.0, 0.65 mm pitch

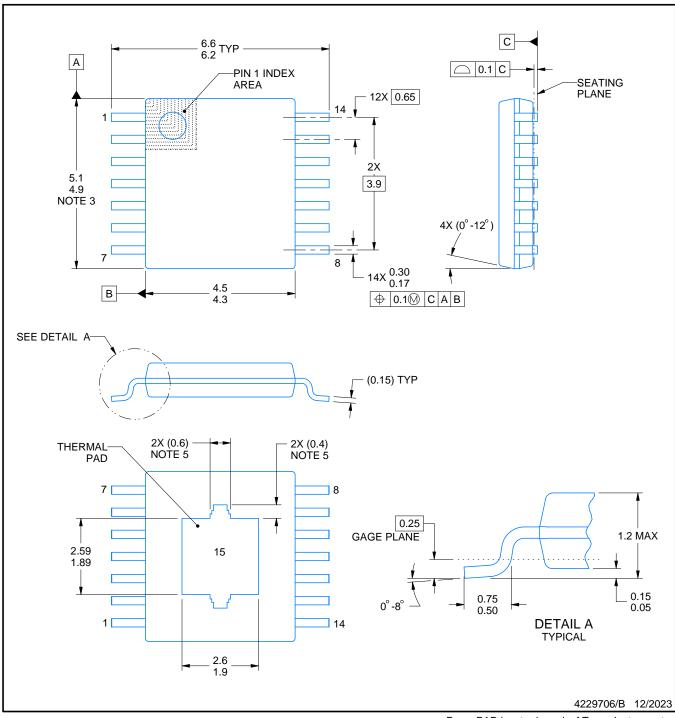
PLASTIC SMALL OUTLINE

This image is a representation of the package family, actual package may vary. Refer to the product data sheet for package details.



# PowerPAD<sup>™</sup> TSSOP - 1.2 mm max height

SMALL OUTLINE PACKAGE



### NOTES:

PowerPAD is a trademark of Texas Instruments.

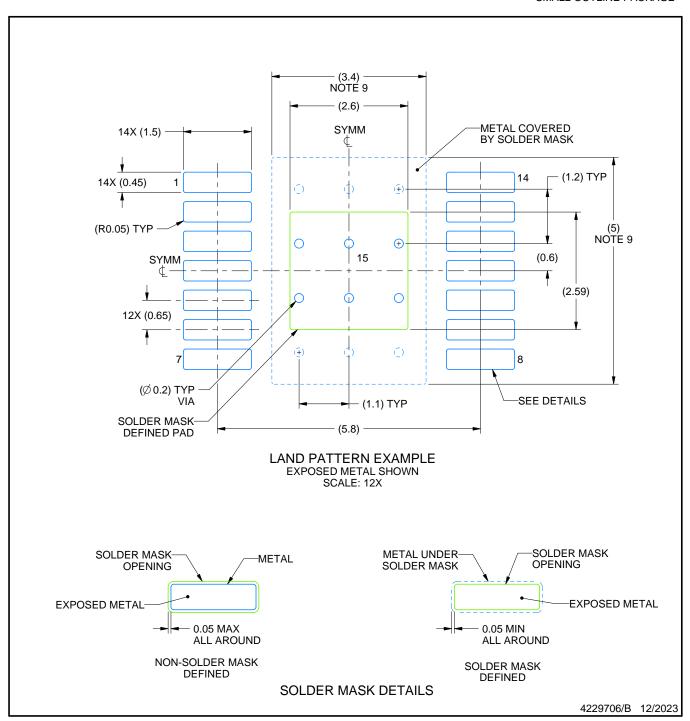
- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.

  2. This drawing is subject to change without notice.

  3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not
- exceed 0.15 mm per side.
  4. Reference JEDEC registration MO-153.
- 5. Features may differ or may not be present.



SMALL OUTLINE PACKAGE

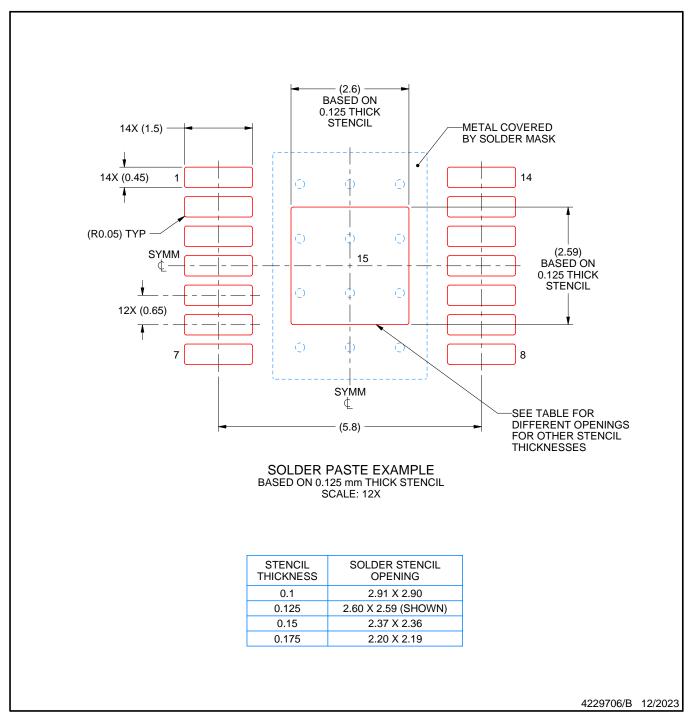


NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- 8. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature numbers SLMA002 (www.ti.com/lit/slma002) and SLMA004 (www.ti.com/lit/slma004).
- 9. Size of metal pad may vary due to creepage requirement.
- 10. Vias are optional depending on application, refer to device data sheet. It is recommended that vias under paste be filled, plugged or tented.



SMALL OUTLINE PACKAGE



NOTES: (continued)

- 11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 12. Board assembly site may have different recommendations for stencil design.



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