













LM5050-1, LM5050-1-Q1

ZHCSKM9F-MAY 2011-REVISED DECEMBER 2019

# LM5050-1、LM5050-1-Q1 高侧 OR-ing FET 控制器

### 1 特性

- 提供标准和符合 AEC-Q100 标准版本的 LM5050Q0MK-1(高达 150°C T<sub>J</sub>)和 LM5050Q1MK-1(高达 125°C T<sub>J</sub>)
- 提供功能安全
  - 提供文档以帮助创建功能安全系统设计
- 宽工作输入电压范围 V<sub>IN</sub>: 1V 至 75V (V<sub>IN</sub> < 5V 时 需要 V<sub>BIAS</sub>)
- 100V 瞬态电压
- 适用于外部 N 沟道 MOSFET 的电荷泵栅极驱动器
- 针对电流反向 50ns 快速响应
- 2A 峰值栅极关断电流
- 超小 V<sub>DS</sub> 关断电压,可缩短关断时间
- 封装: SOT-6 (薄型 SOT-23-6)

# 2 应用

冗余 (N+1) 电源的有源 OR-ing

# 3 说明

LM5050-1/-Q1 高侧 OR-ing FET 控制器与外部 MOSFET 配合工作,当与电源串联时则用作理想的二极管整流器。此 ORing 控制器可使 MOSFET 替换电源分配网络中的二极管整流器,从而降低功率损耗和压隆。

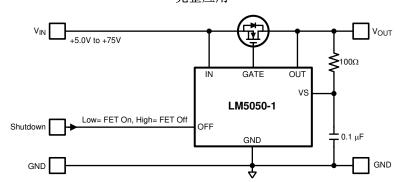
LM5050-1/-Q1 控制器为外部 N 沟道 MOSFET 和快速响应比较器提供电荷泵栅极驱动,以在电流反向流动时关断 FET。LM5050-1/-Q1 可连接 5V 至 75V 的电源,可承受高达 100V 的瞬态电压。

#### 器件信息(1)

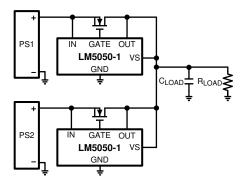
器件型号	封装	封装尺寸 (标称值)
LM5050-1	COT (C)	2.90mm × 1.60mm
LM5050-1-Q1	SOT (6)	2.90mm x 1.60mm

(1) 如需了解所有可用封装,请参阅数据表末尾的可订购产品附录。

### 完整应用



# 典型冗余电源配置



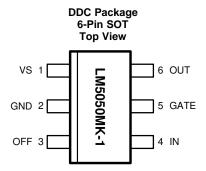


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分、器件和文档支持部分以及机械、封装和可订购信息部分.......1



# **5 Pin Configuration and Functions**



**Pin Functions** 

PIN		1/0	DESCRIPTION				
NO.	NAME	1/0	DESCRIPTION				
1	VS	1	The main supply pin for all internal biasing and an auxiliary supply for the internal gate drive charge pump. Typically connected to either $V_{OUT}$ or $V_{IN}$ ; a separate supply can also be used.				
2	GND	PWR	Ground return for the controller				
3	OFF	I	A logic high state at the OFF pin will pull the GATE pin low and turn off the external MOSFET. Note that when the MOSFET is off, current will still conduct through the FET's body diode. This pin should may be left open or connected to GND if unused.				
4	IN	I	Voltage sense connection to the external MOSFET Source pin.				
5	GATE	0	Connect to the Gate of the external MOSFET. Controls the MOSFET to emulate a low forward-voltage diode.				
6	OUT	0	Voltage sense connection to the external MOSFET Drain pin.				



# 6 Specifications

### 6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

	MIN	MAX	UNIT
IN, OUT Pins to Ground (2)	-0.3	100	V
GATE Pin to Ground <sup>(2)</sup>	-0.3	100	V
VS Pin to Ground	-0.3	100	V
OFF Pin to Ground	-0.3	7	V
Storage Temperature	-65	150	°C

(1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) The GATE pin voltage is typically 12 V above the IN pin voltage when the LM5050-1 is enabled (that is, OFF Pin is Opén or Low, and VIN > VOUT). Therefore, the absolute maximum rating for the IN pin voltage applies only when the LM5050-1 is disabled (that is, OFF Pin is logic high), or for a momentary surge to that voltage because the Absolute Maximum Rating for the GATE pin is also 100 V

### 6.2 ESD Ratings: LM5050-1

			VALUE	UNIT
.,	Electrostatio disebense	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 <sup>(1)</sup>	±2000	\ /
V <sub>(ESD)</sub>	Electrostatic discharge	Machine model (MM) <sup>(2)</sup>	±150	V

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
- (2) The MM is a 200-pF capacitor discharged through a 0-Ω resistor (that is, directly) into each pin. Applicable test standard is JESD-A115-A.

### 6.3 ESD Ratings: LM5050-1-Q1

			VALUE	UNIT
V Floring to the discharge	Electrostatic discharge	Human-body model (HBM), per AEC Q100-002 <sup>(1)</sup>	±2000	V
V <sub>(ESD)</sub>	Electrostatic discharge	Machine model (MM) <sup>(2)</sup>	±150	V

- 1) AEC Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specification.
- 2) The MM is a 200-pF capacitor discharged through a 0-Ω resistor (that is, directly) into each pin. Applicable test standard is JESD-A115-A.

### 6.4 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

		MIN	MAX	UNIT
IN, OUT, VS Pins	5	75	V	
OFF Pin		0	5.5	V
	Standard Grade	-40	125	°C
Junction Temperature (T <sub>J</sub> )	LM5050Q0MK-1	-40	150	°C
	LM5050Q1MK-1	-40	125	°C

# 6.5 Thermal Information

	THERMAL METRIC <sup>(1)</sup>	DDC (SOT)	UNIT
		6 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	180.7	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	41.3	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	28.2	°C/W
ΨЈТ	Junction-to-top characterization parameter	0.7	°C/W
ΨЈВ	Junction-to-board characterization parameter	27.8	°C/W

For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report, SPRA953.



# Thermal Information (continued)

	THERMAL METRIC <sup>(1)</sup>	DDC (SOT)	UNIT
		6 PINS	
R <sub>0</sub> JC(bot)	Junction-to-case (bottom) thermal resistance	N/A	°C/W

### 6.6 Electrical Characteristics

Typical values represent the most likely parametric norm at  $T_J$  = 25°C, and are provided for reference purposes only. Unless otherwise stated the following conditions apply:  $V_{IN}$  = 12 V,  $V_{VS}$  =  $V_{IN}$ ,  $V_{OUT}$  =  $V_{IN}$ ,  $V_{OFF}$  = 0 V,  $C_{GATE}$ = 47 nF, and  $T_J$  = 25°C.

PARAMETER		TEST CONDITIONS			MIN	TYP	MAX	UNIT	
VS PIN									
V <sub>VS</sub>	Operating Supply Voltage Range	$T_{J} = -40^{\circ}\text{C to } 125^{\circ}\text{C}$			5		75	٧	
		V <sub>VS</sub> = 5 V, V <sub>IN</sub> = 5 V	T <sub>J</sub> = 25°C			75			
		$V_{OUT} = V_{IN} - 100 \text{ mV}$	$T_{J} = -40^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$				105		
L	Operating	V <sub>VS</sub> = 12 V, V <sub>IN</sub> = 12 V	$T_J = 25^{\circ}C$			100		μА	
I <sub>VS</sub>	Supply Current	$V_{OUT} = V_{IN} - 100 \text{ mV}$	$T_{J} = -40^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$				147	μΑ	
		V <sub>VS</sub> = 75 V, V <sub>IN</sub> = 75 V	$T_J = 25^{\circ}C$			130			
		$V_{OUT} = V_{IN} - 100 \text{ mV}$	$T_J = -40$ °C to 125°C				288		
IN PIN									
V <sub>IN</sub>	Operating Input Voltage Range	$T_{J} = -40^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$			5		75	٧	
		V <sub>IN</sub> = 5 V	$T_J = 25$ °C			190			
		$V_{VS} = V_{IN}$ $V_{OUT} = V_{IN} - 100 \text{ mV}$ GATE = Open	$T_{J} = -40^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$		32		305	5	
I <sub>IN</sub>	IN Pin current	$V_{IN}$ = 12 V to 75 V $V_{VS}$ = $V_{IN}$ $V_{OUT}$ = $V_{IN}$ - 100 mV GATE = Open	$T_J = 25^{\circ}C$			320		μΑ	
			$T_{J} = -40^{\circ}\text{C to } 125^{\circ}\text{C}$	LM5050MK-1, LM5050Q1MK-1	233		400		
			$T_J = -40^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$	LM5050Q0MK-1	233		475		
OUT PIN				-			*		
V <sub>OUT</sub>	Operating Output Voltage Range	$T_{J} = -40^{\circ}\text{C to } 125^{\circ}\text{C}$			5		75	V	
		V <sub>IN</sub> = 5 V to 75 V	T <sub>J</sub> = 25°C		3.				
I <sub>OUT</sub>	OUT Pin Current	$V_{VS} = V_{IN}$ $V_{OUT} = V_{IN} - 100 \text{ mV}$	$T_{J} = -40^{\circ}\text{C to } 125^{\circ}\text{C}$				8	μA	
GATE PIN			I						
		V <sub>IN</sub> = 5 V	T <sub>J</sub> = 25°C			30			
	Gate Pin Source	$V_{VS} = V_{IN}$ $V_{GATE} = V_{IN}$ $V_{OUT} = V_{IN} - 175 \text{ mV}$	$T_{J} = -40^{\circ}\text{C to } 125^{\circ}\text{C}$		12		41		
I <sub>GATE(ON)</sub>	Current	V <sub>IN</sub> = 12 V to 75 V	T <sub>J</sub> = 25°C			32		- μΑ	
		$V_{VS} = V_{IN}$ $V_{GATE} = V_{IN}$ $V_{OUT} = V_{IN} - 175 \text{ mV}$	$T_{J} = -40^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$		20		41		
		V <sub>IN</sub> = 5 V	T <sub>J</sub> = 25°C			7			
	V <sub>GATE</sub> - V <sub>IN</sub> in	$V_{VS} = V_{IN}$ $V_{OUT} = V_{IN} - 175 \text{ mV}$	$T_{J} = -40^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$		4		9	-	
$V_{GS}$	Forward Operation <sup>(1)</sup>	V <sub>IN</sub> = 12 V to 75 V	T <sub>J</sub> = 25°C			12		V	
	Operation	$V_{VS} = V_{IN}$ $V_{OUT} = V_{IN} - 175 \text{ mV}$						_	



# **Electrical Characteristics (continued)**

Typical values represent the most likely parametric norm at  $T_J = 25$ °C, and are provided for reference purposes only. Unless otherwise stated the following conditions apply:  $V_{IN} = 12 \text{ V}$ ,  $V_{VS} = V_{IN}$ ,  $V_{OUT} = V_{IN}$ ,  $V_{OFF} = 0 \text{ V}$ ,  $C_{GATE} = 47 \text{ nF}$ , and  $T_J = 25^{\circ}\text{C}$ .

RAMETER	TEST CONDITIONS			MIN	TYP	MAX	UNIT	
Gate	$C_{GATE} = 0^{(2)}$	T <sub>J</sub> = 25°C			25			
		$T_{J} = -40^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$				85		
at Forward to	$C_{GATE} = 10 \text{ nF}^{(2)}$	$T_J = 25^{\circ}C$			60		ns	
	$C_{OATE} = 47 \text{ nF}^{(2)}$	$T_J = 25^{\circ}C$			180			
See Figure 1	OGATE = 47 III	$T_J = -40$ °C to 125°C				350		
Gate Capacitance DischargeTime at OFF pin Low to High Transition See Figure 2	C <sub>GATE</sub> = 47 nF <sup>(3)</sup>	T <sub>J</sub> = 25°C			486		ns	
	V	$T_J = 25^{\circ}C$			2.8			
Gate Pin Sink Current	$V_{OUT} > V_{IN} + 100 \text{ mV}$	$T_{J} = -40^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$	LM5050MK-1, LM5050Q1MK-1	1.8			Α	
	1 = 10 ms	$T_J = -40$ °C to 125°C	LM5050Q0MK-1	1.4				
Reverse V <sub>SD</sub>		$T_J = 25^{\circ}C$			-28			
Threshold V <sub>IN</sub> < V <sub>OUT</sub>	V <sub>IN</sub> - V <sub>OUT</sub>	$T_{J} = -40^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$		-41		-16	mV	
Reverse V <sub>SD</sub> Hysteresis		T <sub>J</sub> = 25°C			10		mV	
Do sudoto d	$V_{IN} = 5 V$ $V_{VS} = V_{IN}$	T <sub>J</sub> = 25°C			19			
		$T_{J} = -40^{\circ}\text{C to } 125^{\circ}\text{C}$	LM5050MK-1, LM5050Q1MK-1	1		37		
Forward V <sub>SD</sub>	V <sub>IN</sub> - V <sub>OUT</sub>	$T_{J} = -40^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$	LM5050Q0MK-1	1		60	\/	
Threshold	eshold	$T_J = 25^{\circ}C$			22		mV	
V <sub>IN</sub> > V <sub>OUT</sub>	$V_{IN} = 12 \text{ V}$ $V_{VS} = V_{IN}$	$T_{J} = -40^{\circ}\text{C to } 125^{\circ}\text{C}$	LM5050MK-1, LM5050Q1MK-1	4.4		37		
	V <sub>IN</sub> - V <sub>OUT</sub>	$T_J = -40$ °C to 125°C	LM5050Q0MK-1	4.4		60		
OFF Input High	Vour = Vw-500 mV	$T_J = 25^{\circ}C$			1.56			
Threshold Voltage	V <sub>OFF</sub> Rising	$T_{J} = -40^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$				1.75	V	
OFF Input Low	Vout = Vin - 500 mV	$T_J = 25^{\circ}C$			1.4		V	
Threshold Voltage	V <sub>OFF</sub> Falling	$T_J = -40^{\circ}\text{C} \text{ to } 125^{\circ}\text{C}$		1.1				
OFF Threshold Voltage Hysteresis	V <sub>OFF(IH)</sub> - V <sub>OFF(IL)</sub>	T <sub>J</sub> = 25°C			155		mV	
OFF B:: 1	V 45 V	$T_J = 25^{\circ}C$			5			
OFF Pin Internal Pulldown	v <sub>OFF</sub> = 4.5 v	$T_J = -40$ °C to 125°C		3		7	μA	
i ulluowii	V <sub>OFF</sub> = 5 V	$T_J = 25^{\circ}C$			8			
	Gate Capacitance Discharge Time at Forward to Reverse Transition See Figure 1  Gate Capacitance Discharge Time at OFF pin Low to High Transition See Figure 2  Gate Pin Sink Current  Reverse V <sub>SD</sub> Threshold V <sub>IN</sub> < V <sub>OUT</sub> Reverse V <sub>SD</sub> Hysteresis  Regulated Forward V <sub>SD</sub> Threshold V <sub>IN</sub> > V <sub>OUT</sub> OFF Input High Threshold Voltage OFF Input Low Threshold Voltage OFF Pin Internal	Gate Capacitance Discharge Time at Forward to Reverse Transition See Figure 1  Gate Capacitance DischargeTime at OFF pin Low to High Transition See Figure 2  Gate Pin Sink Current  Reverse V <sub>SD</sub> Threshold V <sub>IN</sub> < V <sub>OUT</sub> Reverse V <sub>SD</sub> Hysteresis  Regulated Forward V <sub>SD</sub> Threshold V <sub>IN</sub> > V <sub>OUT</sub> Represe V <sub>SD</sub> Threshold V <sub>IN</sub> > V <sub>OUT</sub> Represe V <sub>SD</sub> Threshold V <sub>IN</sub> > V <sub>OUT</sub> Represe V <sub>SD</sub> Threshold V <sub>IN</sub> > V <sub>OUT</sub> Represe V <sub>SD</sub> Threshold V <sub>IN</sub> > V <sub>OUT</sub> Represe V <sub>SD</sub> Threshold V <sub>IN</sub> > V <sub>OUT</sub> Represe V <sub>SD</sub> Threshold V <sub>IN</sub> > V <sub>OUT</sub> Represe V <sub>SD</sub> Threshold V <sub>IN</sub> > V <sub>OUT</sub> V <sub>IN</sub> = 12 V V <sub>VS</sub> = V <sub>IN</sub> V <sub>IN</sub> - V <sub>OUT</sub> OFF Input High Threshold Voltage  OFF Input Low Threshold Voltage  OFF Threshold Voltage  OFF Threshold Voltage Hysteresis  OFF Pin Internal Pulldown  Voff = 4.5 V	$ \begin{array}{c c} \text{Gate} \\ \text{Capacitance} \\ \text{Discharge Time} \\ \text{at Forward to} \\ \text{Reverse} \\ \text{Transition} \\ \text{See Figure 1} \\ \hline \\ \text{Gate} \\ \text{Capacitance} \\ \text{DischargeTime} \\ \text{at OFF pin Low} \\ \text{to High} \\ \text{Transition} \\ \text{See Figure 2} \\ \hline \\ \text{Gate} \\ \text{Capacitance} \\ \text{DischargeTime} \\ \text{at OFF pin Low} \\ \text{to High} \\ \text{Transition} \\ \text{See Figure 2} \\ \hline \\ \text{Gate Pin Sink} \\ \text{Current} \\ \hline \\ \text{C}_{\text{GATE}} = 47 \text{ nF}^{(2)} \\ \hline \\ \text{C}_{\text{GATE}} = 47 \text{ nF}^{(2)} \\ \hline \\ \text{T}_{\text{J}} = 25^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = 25^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}\text{C to } 125^{\circ}\text{C} \\ \hline \\ \text{T}_{\text{J}} = -40^{\circ}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	

Time from  $V_{IN}$ - $V_{OUT}$  voltage transition from 200 mV to -500 mV until GATE pin voltage falls to  $V_{IN}$  + 1 V. See Figure 1. Time from  $V_{OFF}$  voltage transition from 0 V to 5 V until GATE pin voltage falls to  $V_{IN}$  + 1 V. See Figure 2



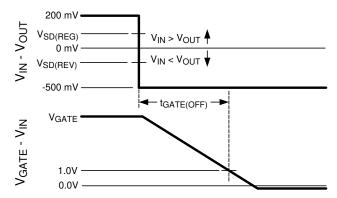


Figure 1. Gate OFF Timing for Forward to Reverse Transition

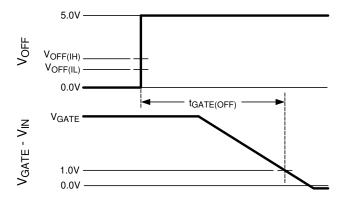
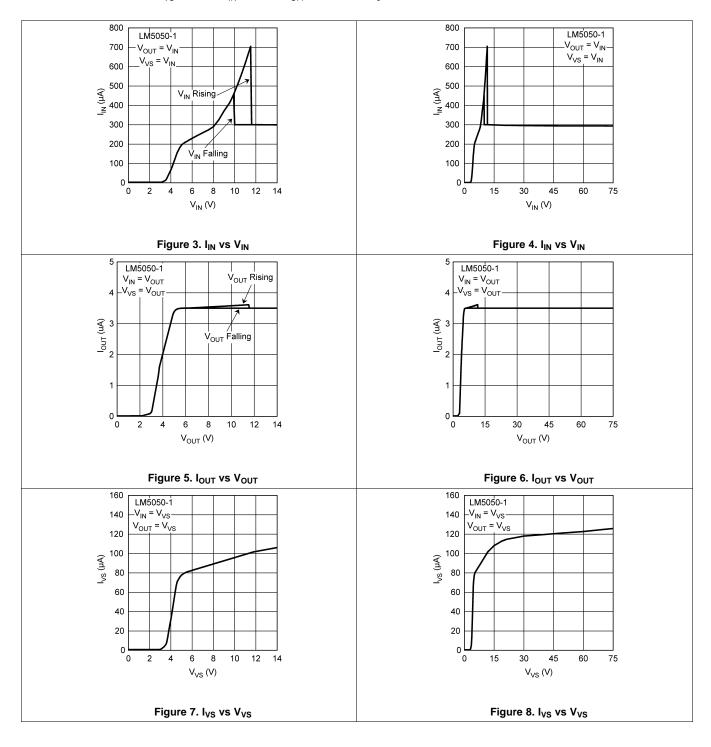


Figure 2. Gate OFF Timing for OFF Pin Low to High Transition



# 6.7 Typical Characteristics

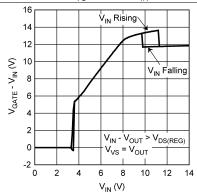
Unless otherwise stated:  $V_{VS}$  = 12 V,  $V_{IN}$  = 12 V,  $V_{OFF}$  = 0 V, and  $T_J$  = 25°C





# **Typical Characteristics (continued)**

Unless otherwise stated:  $V_{VS}$  = 12 V,  $V_{IN}$  = 12 V,  $V_{OFF}$  = 0 V, and  $T_J$  = 25°C



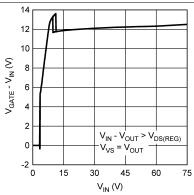
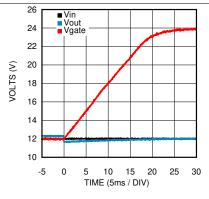


Figure 9.  $(V_{GATE} - V_{IN})$  vs  $V_{IN}$ ,  $V_{VS} = V_{OUT}$ 





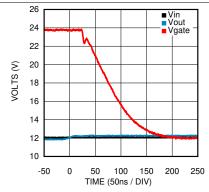
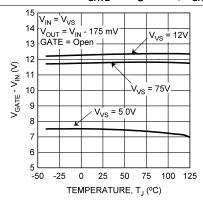


Figure 11. Forward  $C_{GATE}$  Charge Time,  $C_{GATE}$  = 47 nF

Figure 12. Reverse C<sub>GATE</sub> Discharge, C<sub>GATE</sub> = 47 nF



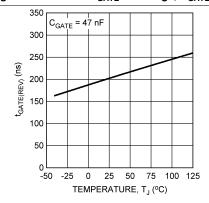


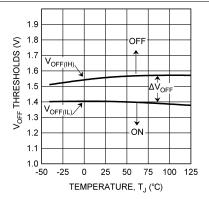
Figure 13. V<sub>GATE</sub> - V<sub>IN</sub> vs Temperature

Figure 14. t<sub>GATE(REV)</sub> vs Temperature



# **Typical Characteristics (continued)**

Unless otherwise stated:  $V_{VS}$  = 12 V,  $V_{IN}$  = 12 V,  $V_{OFF}$  = 0 V, and  $T_J$  = 25°C



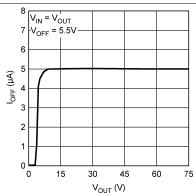
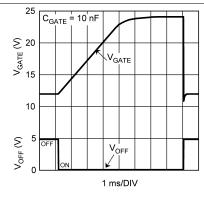


Figure 15. OFF Pin Thresholds vs Temperature





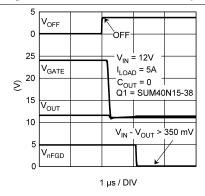
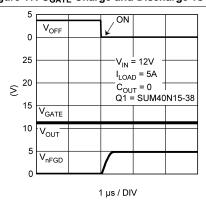


Figure 17. C<sub>GATE</sub> Charge and Discharge vs OFF Pin

Figure 18. OFF Pin, ON to OFF Transition



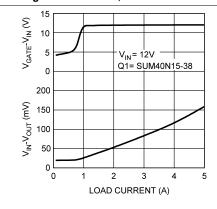


Figure 19. OFF Pin, OFF to ON Transition

Figure 20. GATE Pin vs  $(R_{DS(ON)} \times I_{DS})$ 



# 7 Detailed Description

#### 7.1 Overview

Blocking diodes are commonly placed in series with supply inputs for the purpose of ORing redundant power sources and protecting against supply reversal. The LM5050 replaces diodes in these applications with an N-MOSFET to reduce both the voltage drop and power loss associated with a passive solution. At low input voltages, the improvement in forward voltage loss is readily appreciated where headroom is tight, as shown in Figure 2. The LM5050 operates from 5 V to 75 V and it can withstand an absolute maximum of 100 V without damage. A 12-V or 15-A ideal diode application is shown in Figure 24. Several external components are included in addition to the MOSFET, Q1. Ideal diodes, like their non-ideal counterparts, exhibit a behavior known as reverse recovery. In combination with parasitic or intentionally introduced inductances, reverse recovery spikes may be generated by an ideal diode during an reverse current shutdown. D1, D2 and R1 protect against these spikes which might otherwise exceed the LM5050 100-V survival rating. COUT also plays a role in absorbing reverse recovery energy. Spikes and protection schemes are discussed in detail in the *Short Circuit Failure of an Input Supply* section.

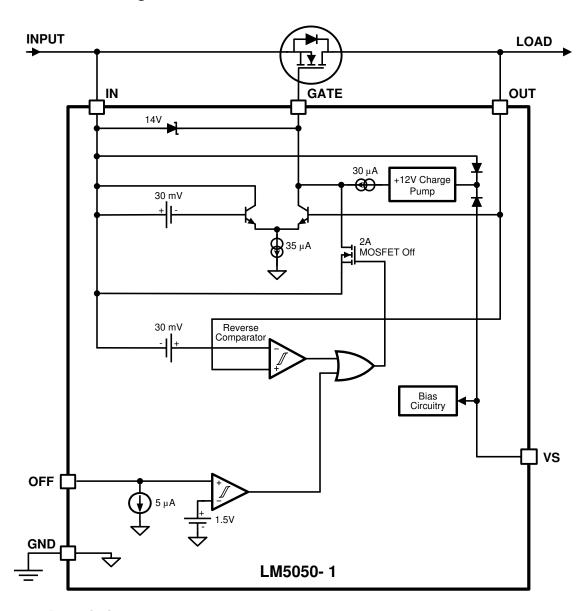
#### NOTE

The OFF pin may be used to active the GATE pull down circuit and turn off the pass MOSFET, but it does not disconnect the load from the input because Q1's body diode is still present.

If Vs is powered while IN is floating or grounded, then about 0.5mA will leak from the Vs pin into the IC and about 3mA will leak from the OUT pin into the IC. From this leakage, about 50 uA will flow out of the IN pin and the rest will flow to ground. This does not affect long term reliability of the IC, but may influence circuit design. See *Reverse Input Voltage Protection With IQ Reduction* for details on how to avoid this leakage current.



#### 7.2 Functional Block Diagram



### 7.3 Feature Description

### 7.3.1 IN, GATE, and OUT Pins

When power is initially applied, the load current will flow from source to drain through the body diode of the MOSFET. Once the voltage across the body diode exceeds  $V_{SD(REG)}$  then the LM5050-1 begins charging the MOSFET gate through a 32  $\mu$ A (typical) charge pump current source . In forward operation, the gate of the MOSFET is charged until it reaches the clamping voltage of the 12-V GATE to IN pin Zener diode internal to the LM5050-1.

The LM5050-1 is designed to regulate the MOSFET gate-to-source voltage. If the MOSFET current decreases to the point that the voltage across the MOSFET falls below the  $V_{SD(REG)}$  voltage regulation point of 22 mV (typical), the GATE pin voltage will be decreased until the voltage across the MOSFET is regulated at 22 mV. If the source-to-drain voltage is greater than the  $V_{SD(REG)}$  voltage, the gate-to-source voltage will increase and eventually reach the 12-V GATE to IN pin Zener clamp level.



### **Feature Description (continued)**

If the MOSFET current reverses, possibly due to failure of the input supply, such that the voltage across the LM5050-1 IN and OUT pins is more negative than the  $V_{SD(REV)}$  voltage of -28 mV (typical), the LM5050-1 will quickly discharge the MOSFET gate through a strong GATE to IN pin discharge transistor.

If the input supply fails abruptly, as would occur if the supply was shorted directly to ground, a reverse current will temporarily flow through the MOSFET until the gate can be fully discharged. This reverse current is sourced from the load capacitance and from the parallel connected supplies. The LM5050-1 responds to a voltage reversal condition typically within 25 ns. The actual time required to turn off the MOSFET will depend on the charge held by the gate capacitance of the MOSFET being used. A MOSFET with 47 nF of effective gate capacitance can be turned off in typically 180 ns. This fast turnoff time minimizes voltage disturbances at the output, as well as the current transients from the redundant supplies.

#### 7.3.2 VS Pin

The LM5050-1 VS pin is the main supply pin for all internal biasing and an auxiliary supply for the internal gate drive charge pump.

For typical LM5050-1 applications, where the input voltage is above 5 V, the VS pin can be connected directly to the OUT pin. In situations where the input voltage is close to, but not less than, the 5 V minimum, it may be helpful to connect the VS pin to the OUT pin through an RC Low-Pass filter to reduce the possibility of erratic behavior due to spurious voltage spikes that may appear on the OUT and IN pins. The series resistor value should be low enough to keep the VS voltage drop at a minimum. A typical series resistor value is 100  $\Omega$ . The capacitor value should be the lowest value that produces acceptable filtering of the voltage noise.

If Vs is powered while IN is floating or grounded, then about 0.5 mA will leak from the Vs pin into the IC and about 3mA will leak from the OUT pin into the IC. From this leakage, about 50 uA will flow out of the IN pin and the rest will flow to ground. This does not affect long term reliability of the IC, but may influence circuit design. See *Reverse Input Voltage Protection With IQ Reduction* for details on how to avoid this leakage current.

Alternately, it is possible to operate the LM5050-1 with  $V_{IN}$  value as low as 1 V if the VS pin is powered from a separate supply. This separate VS supply must be from 5 V and 75 V. See Figure 27.

#### 7.3.3 OFF Pin

The OFF pin is a logic level input pin that is used to control the gate drive to the external MOSFET. The maximum operating voltage on this pin is 5.5 V.

When the OFF pin is high, the MOSFET is turned off (independent of the sensed IN and OUT voltages). In this mode, load current will flow through the body diode of the MOSFET. The voltage difference between the IN pin and OUT pins will be approximately 700 mV if the MOSFET is operating normally through the body diode.

The OFF pin has an internal pulldown of 5 µA (typical). If the OFF function is not required the pin may be left open or connected to ground.

#### 7.4 Device Functional Modes

#### 7.4.1 ON/OFF Control Mode

The MOSFET can be turned off by asserting the OFF pin high. This mode only disables the MOSFET, but V<sub>OUT</sub> is still available through the body diode of the MOSFET.

#### 7.4.2 External Power Supply Mode

The Vs pin of the LM5050 can be operated from 5 V to 75 V as the bias input supply. In this mode  $V_{IN}$  voltage can be as low as 1 V, as shown in Figure 27.



# 8 Application and Implementation

#### NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 8.1 Application Information

Systems that require high availability often use multiple, parallel-connected redundant power supplies to improve reliability. Schottky OR-ing diodes are typically used to connect these redundant power supplies to a common point at the load. The disadvantage of using OR-ing diodes is the forward voltage drop, which reduces the available voltage and the associated power losses as load currents increase. Using an N-channel MOSFET to replace the OR-ing diode requires a small increase in the level of complexity, but reduces, or eliminates, the need for diode heat sinks or large thermal copper area in circuit board layouts for high power applications.

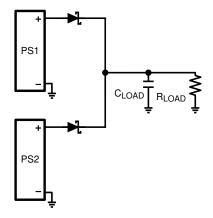


Figure 21. OR-ing with Diodes

The LM5050-1/-Q1 is a positive voltage (that is, high-side) OR-ing controller that will drive an external N-channel MOSFET to replace an OR-ing diode. The voltage across the MOSFET source and drain pins is monitored by the LM5050-1 at the IN and OUT pins, while the GATE pin drives the MOSFET to control its operation based on the monitored source-drain voltage. The resulting behavior is that of an ideal rectifier with source and drain pins of the MOSFET acting as the anode and cathode pins of a diode respectively.

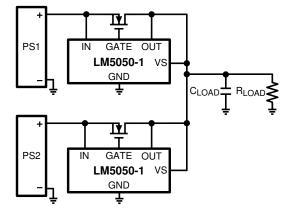


Figure 22. OR-ing With MOSFETs



### Application Information (continued)

#### 8.1.1 MOSFET Selection

The important MOSFET electrical parameters are the maximum continuous Drain current  $I_D$ , the maximum Source current (that is, body diode)  $I_S$ , the maximum drain-to-source voltage  $V_{DS(MAX)}$ , the gate-to-source threshold voltage  $V_{GS(TH)}$ , the drain-to-source reverse breakdown voltage  $V_{(BR)DSS}$ , and the drain-to-source On resistance  $R_{DS(ON)}$ .

The maximum continuous drain current,  $I_D$ , rating must exceed the maximum continuous load current. The rating for the maximum current through the body diode,  $I_S$ , is typically rated the same as, or slightly higher than the drain current, but body diode current only flows while the MOSFET gate is being charged to  $V_{GS(TH)}$ .

Gate Charge Time =  $Q_g / I_{GATE(ON)}$ 

- 1. The maximum drain-to-source voltage,  $V_{DS(MAX)}$ , must be high enough to withstand the highest differential voltage seen in the application. This would include any anticipated fault conditions.
- The drain-to-source reverse breakdown voltage, V<sub>(BR)DSS</sub>, may provide some transient protection to the OUT pin in low voltage applications by allowing conduction back to the IN pin during positive transients at the OUT pin.
- 3. The gate-to-source threshold voltage,  $V_{GS(TH)}$ , should be compatible with the LM5050-1 gate drive capabilities. Logic level MOSFETs, with  $R_{DS(ON)}$  rated at  $V_{GS(TH)}$  at 5 V, are recommended, but sub-Logic level MOSFETs having  $R_{DS(ON)}$  rated at  $V_{GS(TH)}$  at 2.5 V, can also be used.
- 4. The dominate MOSFET loss for the LM5050-1 active OR-ing controller is conduction loss due to source-to-drain current to the output load, and the  $R_{DS(ON)}$  of the MOSFET. This conduction loss could be reduced by using a MOSFET with the lowest possible  $R_{DS(ON)}$ . However, contrary to popular belief, arbitrarily selecting a MOSFET based solely on having low  $R_{DS(ON)}$  may not always give desirable results for several reasons:
  - Reverse transition detection. Higher R<sub>DS(ON)</sub> will provide increased voltage information to the LM5050-1 Reverse Comparator at a lower reverse current level. This will give an earlier MOSFET turnoff condition should the input voltage become shorted to ground. This will minimize any disturbance of the redundant bus.
  - Reverse current leakage. In cases where multiple input supplies are closely matched it may be possible
    for some small current to flow continuously through the MOSFET drain to source (that is, reverse)
    without activating the LM5050-1 Reverse Comparator. Higher R<sub>DS(ON)</sub> will reduce this reverse current
    level.
  - 3. Cost. Generally, as the R<sub>DS(ON)</sub> rating goes lower, the cost of the MOSFET goes higher.
- 5. The dominate MOSFET loss for the LM5050-1 active OR-ing controller is conduction loss due to source-to-drain current to the output load, and the  $R_{DS(ON)}$  of the MOSFET. This conduction loss could be reduced by using a MOSFET with the lowest possible  $R_{DS(ON)}$ . However, contrary to popular belief, arbitrarily selecting a MOSFET based solely on having low  $R_{DS(ON)}$  may not always give desirable results for several reasons:
  - a. Selecting a MOSFET with an R<sub>DS(ON)</sub> that is too large will result in excessive power dissipation. Additionally, the MOSFET gate will be charged to the full value that the LM5050-1 can provide as it attempts to drive the Drain to Source voltage down to the V<sub>SD(REG)</sub> of 22 mV typical. This increased Gate charge will require some finite amount of additional discharge time when the MOSFET needs to be turned off.
  - b. As a guideline, it is suggest that R<sub>DS(ON)</sub> be selected to provide at least 22 mV, and no more than 100 mV, at the nominal load current.
  - c.  $(22 \text{ mV} / I_D) \le R_{DS(ON)} \le (100 \text{ mV} / I_D)$
  - d. The thermal resistance of the MOSFET package should also be considered against the anticipated dissipation in the MOSFET to ensure that the junction temperature (T<sub>J</sub>) is reasonably well controlled, because the R<sub>DS(ON)</sub> of the MOSFET increases as the junction temperature increases.
- 6.  $P_{DISS} = I_D^2 \times (R_{DS(ON)})$
- 7. Operating with a maximum ambient temperature ( $T_{A(MAX)}$ ) of 35°C, a load current of 10 A, and an  $R_{DS(ON)}$  of 10 m $\Omega$ , and desiring to keep the junction temperature under 100°C, the maximum junction-to-ambient thermal resistance rating ( $\theta_{JA}$ ) must be:
  - a.  $R_{\theta JA} \le (T_{J(MAX)} T_{A(MAX)})/(I_D^2 \times R_{DS(ON)})$
  - b.  $R_{\theta JA} \le (100^{\circ}C 35^{\circ}C)/(10 \text{ A} \times 10 \text{ A} \times 0.01 \Omega)$



### Application Information (continued)

c.  $R_{\theta JA} \le 65^{\circ}C/W$ 

### 8.1.2 Short Circuit Failure of an Input Supply

An abrupt  $0-\Omega$  short circuit across the input supply will cause the highest possible reverse current to flow while the internal LM5050-1 control circuitry discharges the gate of the MOSFET. During this time, the reverse current is limited only by the  $R_{DS(ON)}$  of the MOSFET, along with parasitic wiring resistances and inductances. Worst case instantaneous reverse current would be limited to:

$$I_{D(REV)} = (V_{OUT} - V_{IN}) / R_{DS(ON)}$$

$$\tag{1}$$

The internal Reverse Comparator will react, and will start the process of discharging the Gate, when the reverse current reaches:

$$I_{D(REV)} = V_{SD(REV)} / R_{DS(ON)}$$
 (2)

When the MOSFET is finally switched off, the energy stored in the parasitic wiring inductances will be transferred to the rest of the circuit. As a result, the LM5050-1 IN pin will see a negative voltage spike while the OUT pin will see a positive voltage spike. The IN pin can be protected by diode clamping the pin to GND in the negative direction. The OUT pin can be protected with a TVS protection diode, a local bypass capacitor, or both. In low voltage applications, the MOSFET drainto- source breakdown voltage rating may be adequate to protect the OUT pin (that is,  $V_{\text{IN}} + V_{\text{(BR)DSS(MAX)}} < 75 \text{ V}$ ), but most MOSFET data sheets do not ensure the maximum breakdown rating, so this method should be used with caution.

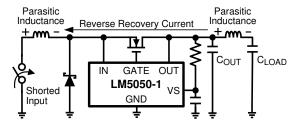


Figure 23. Reverse Recovery Current Generates Inductive Spikes at VIN and VOUT pins.

### 8.2 Typical Applications

### 8.2.1 Typical Application With Input and Output Transient Protection

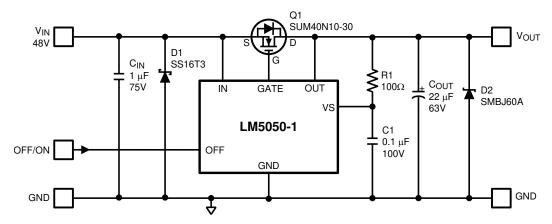


Figure 24. Typical Application With Input and Output Transient Protection Schematic



# **Typical Applications (continued)**

#### 8.2.1.1 Design Requirements

Table 1 shows the parameters for Figure 24

**Table 1. Design Parameters** 

DESIGN PARAMETER	EXAMPLE VALUE
Minimum Input Voltage, VIN <sub>MIN</sub>	6 V
Maximum Input Voltage, VIN <sub>Max</sub>	50 V
Output Current Range, IOUT	0 to 15 A
Ambient Temperature Range, T <sub>A</sub>	0°C to 50°C

### 8.2.1.2 Detailed Design Procedure

The following design procedure can be used to select component values for the LM5050-1.

#### 8.2.1.2.1 Power Supply Components (R1 C1,) Selection

The LM5050-1 VS pin is the main supply pin for all internal biasing and an auxiliary supply for the internal gate drive charge pump. The series resistor (R1) value should be low enough to keep the VS voltage drop at a minimum. A typical series resistor value is  $100 \Omega$ . The capacitor value (0.1 uF typical) should be the lowest value that produces acceptable filtering of the voltage noise.

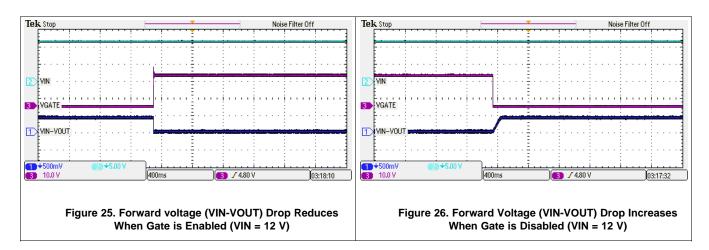
### 8.2.1.2.2 MOSFET (Q1) Selection

The MOSFET (Q1) selection procedure is explained in detail in *MOSFET Selection*. The MOSFET used in the design example is SUM40N10-30-E3.

#### 8.2.1.2.3 D1 and D2 Selection for Inductive Kick-Back Protection

Diode D1 and capacitor C1 and diode D2 and capacitor C2 in the Figure 27 serve as inductive kick-back protection to limit negative transient voltage spikes generated on the input when the input supply voltage is abruptly shorted to zero volts. As a result, the LM5050-1 IN pin will see a negative voltage spike while the OUT pin will see a positive voltage spike. The IN pin can be protected by schottky diode (D1) clamping the pin to GND in the negative direction, similarly the OUT pin should be protected with a TVS protection diode (D1), or with a local bypass capacitor, or both. D1 is selected as 1-A, 60-V Schottky Barrier Rectifier (SS16T3G) and D2 is the 60 V, TVS (SMBJ60A-13-F).

#### 8.2.1.3 Application Curves





### 8.2.2 Using a Separate VS Supply for Low Vin Operation

In some applications, it is desired to operate LM5050-1 from low supply voltage. The LM5050-1 can operate with a 1-V rail voltage, provided its VS pin is biased from 5 V to 75 V. The detail of such application is depicted in Figure 27.

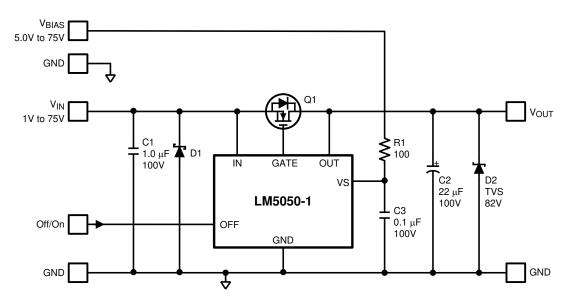


Figure 27. Using a Separate vs Supply for Low Vin Operation Schematic

### 8.2.3 ORing of Two Power Sources

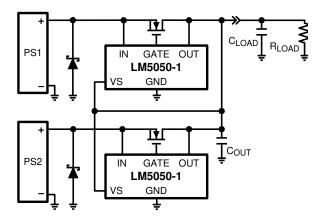


Figure 28. ORing of Two Power Sources



### 8.2.4 Reverse Input Voltage Protection With IQ Reduction

If Vs is powered while IN is floating or grounded, then about 0.5 mA will leak from the Vs pin into the IC and about 3 mA will leak from the OUT pin into the IC. From this leakage, about 50 uA will flow out of the IN pin and the rest will flow to ground. This does not affect long term reliability of the IC, but may influence circuit design.

In battery powered applications, whenever LM5050-1 functionality is not needed, the supply to the LM5050-1 can be disconnected by turning "OFF" Q2, as shown in Figure 29. This disconnects the ground path of the LM5050-1 and eliminates the current leakage from the battery.

The quiescent current of LM5050-1 can be also reduced by disconnecting the supply to VS pin, whenever LM5050-1 function is not need.

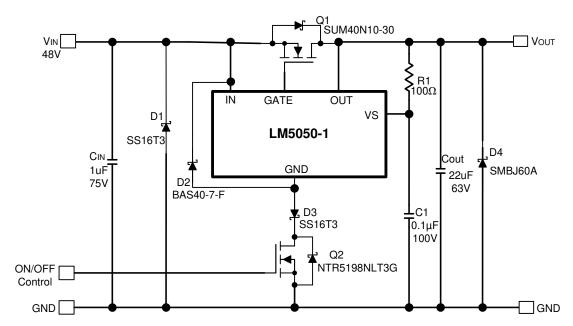


Figure 29. Reverse Input Voltage Protection With IQ Reduction Schematic

### 8.2.5 Basic Application With Input Transient Protection

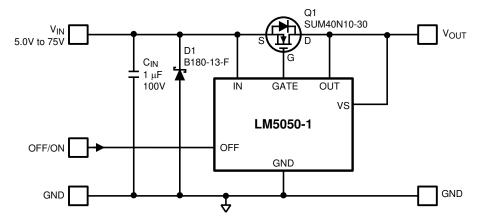


Figure 30. Basic Application With Input Transient Protection Schematic



# 8.2.6 48-V Application With Reverse Input Voltage ( $V_{IN} = -48 \text{ V}$ ) Protection

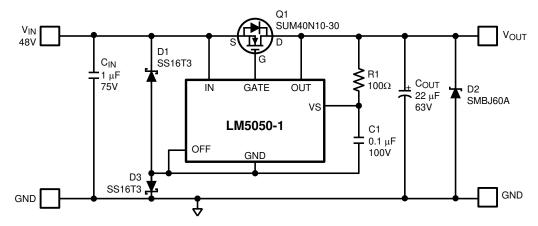
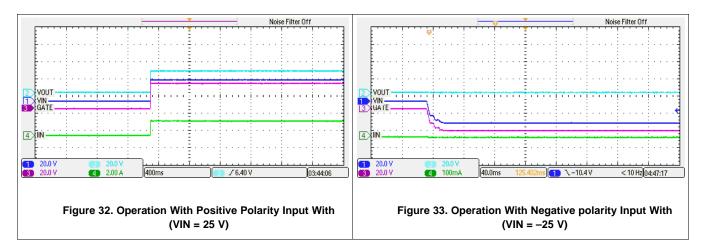


Figure 31. 48-V Application With Reverse Input Voltage ( $V_{IN} = -48 \text{ V}$ ) Protection Schematic

### 8.2.6.1 Application Curves





# 9 Power Supply Recommendations

When the LM5050-1/-Q1 shuts off the external MOSFET, transient voltages will appear on the input and output due to reverse recovery, as discussed in *Short Circuit Failure of an Input Supply*. To prevent LM5050-1 and surrounding components from damage under the conditions of a direct input short circuit, it is necessary to clamp the negative transient at IN, and OUT pins with TVS.

# 10 Layout

### 10.1 Layout Guidelines

The typical PCB layout for LM5050-1/-Q1 is shown in Figure 34. TI recommends connecting the IN, Gate and OUT pins close to the source and drain pins of the MOSFET. Keep the traces of the MOSFET drain wide and short to minimize resistive losses. Place surge suppressors (D1 and D4) components as shown in the example layout of LM5050-1 in *Layout Example*.

# 10.2 Layout Example

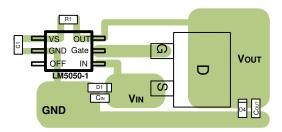


Figure 34. Typical Layout Example With D2PAK N-MOSFET



### 11 器件和文档支持

### 11.1 文档支持

#### 11.1.1 相关文档

《使用具有低电流和高噪声输入电源的 LM5050-1 实现稳定 VGS》, SLVA684

#### 11.2 相关链接

下表列出了快速访问链接。类别包括技术文档、支持与社区资源、工具和软件,以及申请样片或购买产品的快速链接。

表 2. 相关链接

器件	产品文件夹	样片与购买	技术文档	工具与软件	支持和社区
LM5050-1	单击此处	单击此处	单击此处	单击此处	单击此处
LM5050-1-Q1	单击此处	单击此处	单击此处	单击此处	单击此处

# 11.3 社区资源

TI E2E™ support forums are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

Linked content is provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's Terms of Use.

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#### 11.5 静电放电警告



这些装置包含有限的内置 ESD 保护。 存储或装卸时,应将导线一起截短或将装置放置于导电泡棉中,以防止 MOS 门极遭受静电损伤。

### 11.6 Glossary

SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.

### 12 机械、封装和可订购信息

以下页面包含机械、封装和可订购信息。这些信息是指定器件的最新可用数据。数据如有变更,恕不另行通知,且不会对此文档进行修订。如需获取此数据表的浏览器版本,请查阅左侧的导航栏。

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24-Jul-2025

### **PACKAGING INFORMATION**

Orderable part number	Status (1)	Material type	Package   Pins	Package qty   Carrier	<b>RoHS</b> (3)	Lead finish/ Ball material	MSL rating/ Peak reflow	Op temp (°C)	Part marking (6)
LM5050MK-1/NOPB	Active	Production	SOT-23- THIN (DDC)   6	1000   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	SZHB
LM5050MK-1/NOPB.A	Active	Production	SOT-23- THIN (DDC)   6	1000   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	SZHB
LM5050MK-1/NOPB.B	Active	Production	SOT-23- THIN (DDC)   6	1000   SMALL T&R	-	SN	Level-1-260C-UNLIM	-40 to 125	SZHB
LM5050MKX-1/NOPB	Active	Production	SOT-23- THIN (DDC)   6	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	SZHB
LM5050MKX-1/NOPB.A	Active	Production	SOT-23- THIN (DDC)   6	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	SZHB
LM5050MKX-1/NOPB.B	Active	Production	SOT-23- THIN (DDC)   6	3000   LARGE T&R	-	SN	Level-1-260C-UNLIM	-40 to 125	SZHB
LM5050Q0MK-1/NOPB	Active	Production	SOT-23- THIN (DDC)   6	1000   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 150	SL5B
LM5050Q0MK-1/NOPB.A	Active	Production	SOT-23- THIN (DDC)   6	1000   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 150	SL5B
LM5050Q0MKX-1/NOPB	Active	Production	SOT-23- THIN (DDC)   6	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 150	SL5B
LM5050Q0MKX-1/NOPB.A	Active	Production	SOT-23- THIN (DDC)   6	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 150	SL5B
LM5050Q1MK-1/NOPB	Active	Production	SOT-23- THIN (DDC)   6	1000   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	SP3B
LM5050Q1MK-1/NOPB.A	Active	Production	SOT-23- THIN (DDC)   6	1000   SMALL T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	SP3B
LM5050Q1MKX-1/NOPB	Active	Production	SOT-23- THIN (DDC)   6	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	SP3B
LM5050Q1MKX-1/NOPB.A	Active	Production	SOT-23- THIN (DDC)   6	3000   LARGE T&R	Yes	SN	Level-1-260C-UNLIM	-40 to 125	SP3B

<sup>(1)</sup> Status: For more details on status, see our product life cycle.

<sup>(2)</sup> Material type: When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

# PACKAGE OPTION ADDENDUM

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- (3) RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.
- (4) Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.
- (5) MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.
- (6) Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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#### OTHER QUALIFIED VERSIONS OF LM5050-1, LM5050-1-Q1:

Catalog: LM5050-1

Automotive : LM5050-1-Q1

NOTE: Qualified Version Definitions:

- Catalog TI's standard catalog product
- Automotive Q100 devices qualified for high-reliability automotive applications targeting zero defects



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### TAPE AND REEL INFORMATION





	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



#### \*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LM5050MK-1/NOPB	SOT-23- THIN	DDC	6	1000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
LM5050MKX-1/NOPB	SOT-23- THIN	DDC	6	3000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
LM5050Q0MK-1/NOPB	SOT-23- THIN	DDC	6	1000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
LM5050Q0MKX-1/NOPB	SOT-23- THIN	DDC	6	3000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
LM5050Q1MK-1/NOPB	SOT-23- THIN	DDC	6	1000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3
LM5050Q1MKX-1/NOPB	SOT-23- THIN	DDC	6	3000	178.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3



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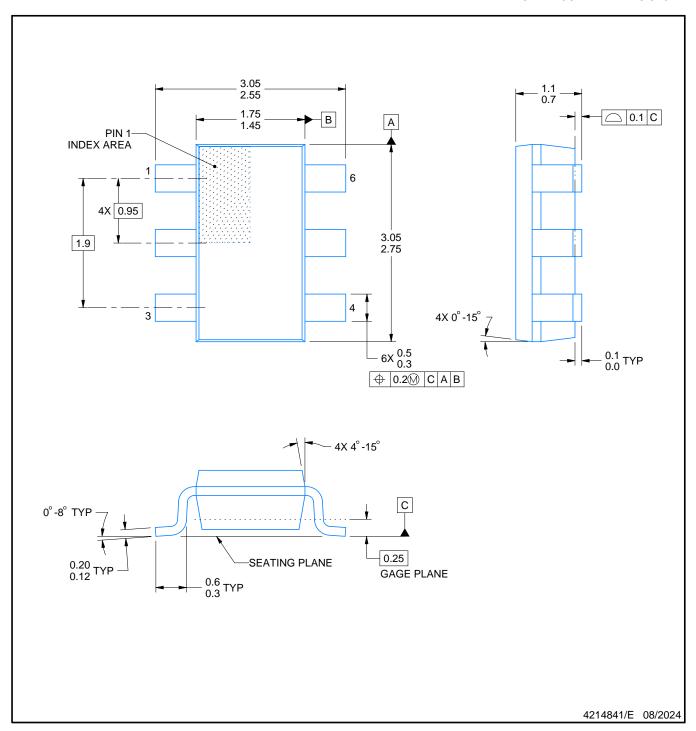


### \*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LM5050MK-1/NOPB	SOT-23-THIN	DDC	6	1000	208.0	191.0	35.0
LM5050MKX-1/NOPB	SOT-23-THIN	DDC	6	3000	208.0	191.0	35.0
LM5050Q0MK-1/NOPB	SOT-23-THIN	DDC	6	1000	208.0	191.0	35.0
LM5050Q0MKX-1/NOPB	SOT-23-THIN	DDC	6	3000	208.0	191.0	35.0
LM5050Q1MK-1/NOPB	SOT-23-THIN	DDC	6	1000	208.0	191.0	35.0
LM5050Q1MKX-1/NOPB	SOT-23-THIN	DDC	6	3000	208.0	191.0	35.0



SMALL OUTLINE TRANSISTOR

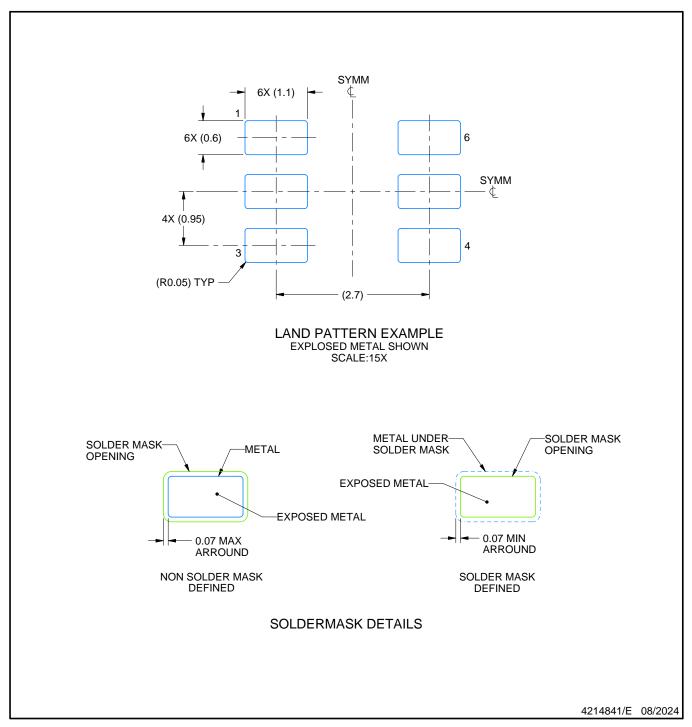


### NOTES:

- All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
   This drawing is subject to change without notice.
   Reference JEDEC MO-193.



SMALL OUTLINE TRANSISTOR

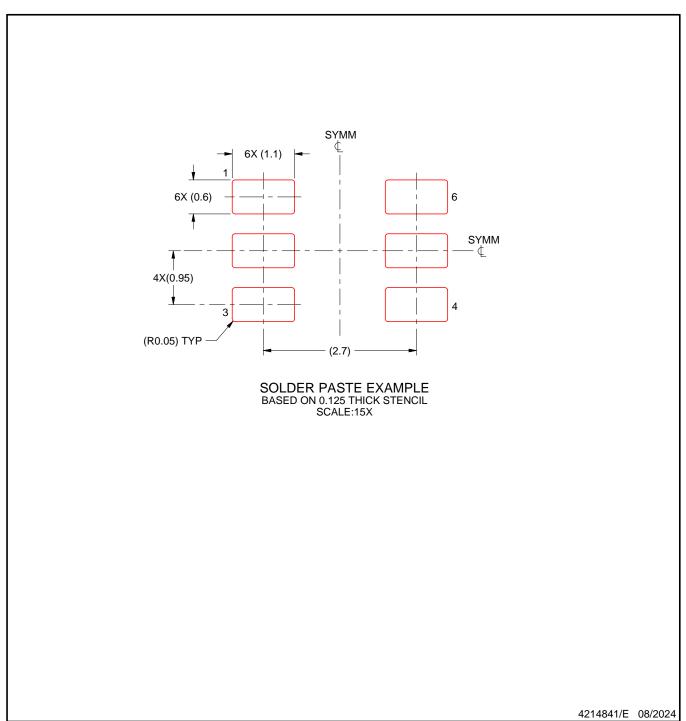


NOTES: (continued)

- 4. Publication IPC-7351 may have alternate designs.
- 5. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SMALL OUTLINE TRANSISTOR



NOTES: (continued)

- 6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

  7. Board assembly site may have different recommendations for stencil design.



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