











CSD86360Q5D

ZHCSAE5B - SEPTEMBER 2012 - REVISED APRIL 2018

CSD86360Q5D 同步降压 NexFET™ 电源块

特性

- 半桥电源块
- 25A 电流下系统效率高达 91%
- 运行电流高达 50A
- 高频工作(高达 1.5MHz)
- 高密度 SON 5mm x 6mm 封装
- 针对 5V 栅极驱动进行了优化
- 开关损耗较低
- 超低电感封装
- 符合 RoHS 标准
- 无卤素
- 无铅引脚镀层

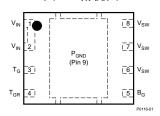
应用 2

- 同步降压转换器
 - 高频 应用
 - 高电流、低占空比应用
- 多相位同步降压转换器
- 负载点 (POL) 直流/直流转换器
- IMVP、VRM 和 VRD 应用

3 说明

CSD86360Q5D NexFET™电源块是面向同步降压 应 用 的优化设计方案,能够以 5mm x 6mm 的小巧外形 提供高电流、高效率以及高频率性能。该产品针对 5V 栅极驱动 应用进行了优化, 在与外部控制器/驱动器的 任一 5V 栅极驱动配套使用时,可提供一套灵活的解决 方案来实现高密度电源。

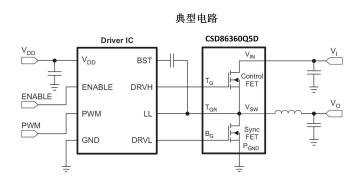
图 1. 俯视图

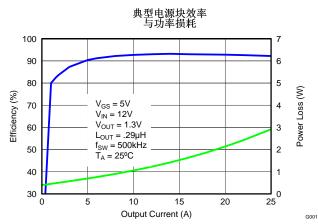


器件信息(1)

器件	介质 数量		封装	配送
CSD86360Q5D	13 英寸卷带	2500	5.00mm × 6.00mm SON 塑料封装	卷带 封装

(1) 如需了解所有可用封装,请参阅产品说明书末尾的可订购产品







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4 修订历史记录

注: 之前版本的页码可能与当前版本有所不同。

C	hanges from Revision A (May 2013) to Revision B	Page
•	Changed Recommended PCB Design Overview section to Layout section	16
•	已添加 器件和文档支持部分	
•	已更改 将机械数据部分更改为机械、封装和可订购信息 部分	19
•	更新了 Q5D 封装尺寸 部分	19
•	更新了焊盘图案建议 图	20
•	更新了模版建议 图	21

CI	nanges from Original (September 2012) to Revision A	Page
•	Changed the footnote notations in the THERMAL INFORMATION table	
•	Updated Figure 7	6
•	Updated Figure 8	6
•	Updated Figure 9	6
•	Updated Figure 10	6



5 Specifications

5.1 Absolute Maximum Ratings

 $T_A = 25$ °C (unless otherwise noted) (1)

PARAMETER	CONDITIONS	MIN	MAX	UNIT
	V _{IN} to P _{GND}		25	
	V _{SW} to P _{GND}		25	
Voltage	V _{SW} to P _{GND} (10 ns)		27	V
	T_G to T_{GR}	-8	10	
	B _G to P _{GND}	-8	10	
Pulsed current rating, I _D	M ⁽²⁾		120	Α
Power dissipation, P _D ⁽³⁾			13	W
Avalancha anaray F	Sync FET, I _D = 110 A, L = 0.1 mH		605	- mJ
Avalanche energy, E _{AS}	Control FET, I _D = 61 A, L = 0.1 mH		186	IIIJ
Operating junction, T _J		- 55	150	°C
Storage temperature, T _{STG}		- 55	150	°C

⁽¹⁾ Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the Recommended Operating Conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

5.2 Recommended Operating Conditions

 $T_A = 25$ °C (unless otherwise noted)

	PARAMETER	CONDITIONS	MIN	MAX	UNIT
V _{GS}	Gate drive voltage		4.5	8	V
V _{IN}	Input supply voltage			22	V
f_{SW}	Switching frequency	$C_{BST} = 0.1 \mu\text{F (min)}$	200	1500	kHz
	Operating current			50	А
T_{J}	Operating temperature			125	°C

5.3 Power Block Performance

 $T_{\Lambda} = 25^{\circ}C$ (unless otherwise noted)

· A —	(
	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNIT
P _{LOSS}	Power loss ⁽¹⁾	$V_{\rm IN} = 12 \ {\rm V, V_{GS}} = 5 \ {\rm V, V_{OUT}} = 1.3 \ {\rm V, I_{OUT}} = 25 \ {\rm A, f_{SW}} = 500 \ {\rm kHz, L_{OUT}} = 0.3 \ {\rm \mu H, T_{J}} = 25 {\rm ^{\circ}C}$		2.6		W
I _{QVIN}	V _{IN} quiescent current	T_G to $T_{GR} = 0$ V B_G to $P_{GND} = 0$ V		10		μΑ

Measurement made with six 10-μF (TDK C3216X5R1C106KT or equivalent) ceramic capacitors placed across V_{IN} to P_{GND} pins and using a high current 5-V driver IC.

5.4 Thermal Information

 $T_A = 25^{\circ}C$ (unless otherwise stated)

	THERMAL METRIC	MIN	TYP	MAX	UNIT
D	Junction-to-ambient thermal resistance (min Cu) ⁽¹⁾			102	°C/W
$R_{\theta JA}$	Junction-to-ambient thermal resistance (max Cu) ⁽¹⁾⁽²⁾			50	· C/VV

⁽¹⁾ $R_{\theta JC}$ is determined with the device mounted on a 1-in² (6.45-cm²), 2-oz (0.071-mm) thick Cu pad on a 1.5-in \times 1.5-in (3.81-cm \times 3.81-cm), 0.06-in (1.52-mm) thick FR4 board. $R_{\theta JC}$ is specified by design while $R_{\theta JA}$ is determined by the user's board design

⁽²⁾ Pulse duration ≤ 50 µs. Duty cycle ≤ 0.01%.

⁽³⁾ $T_{PCB} \le 95^{\circ}C$.

⁽²⁾ Device mounted on FR4 material with 1-in² (6.45-cm²) Cu.



Thermal Information (continued)

 $T_A = 25$ °C (unless otherwise stated)

THERMAL METRIC		MIN	TYP	MAX	UNIT
D	Junction-to-case thermal resistance (top of package) ⁽¹⁾			20	°C/W
$R_{\theta JC}$	Junction-to-case thermal resistance (P _{GND} pin) ⁽¹⁾			2	C/VV

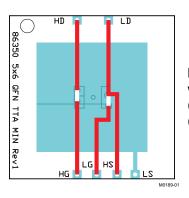
5.5 Electrical Characteristics

 $T_A = 25^{\circ}C$ (unless otherwise stated)

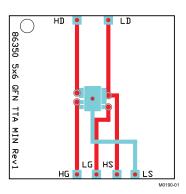
	DADAMETER	TEST CONDITIONS	Q1 C	ontrol FE	T		Q2 Synd	FET	
	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	MIN	TYP	MAX	UNIT
STATIC C	CHARACTERISTICS								
BV _{DSS}	Drain-to-source voltage	$V_{GS} = 0 \text{ V}, I_{DS} = 250 \mu\text{A}$	25			25			V
I _{DSS}	Drain-to-source leakage current	V _{GS} = 0 V, V _{DS} = 20 V			1			1	μА
I _{GSS}	Gate-to-source leakage current	V _{DS} = 0 V, V _{GS} = +10 / -8 V			100			100	nA
V _{GS(th)}	Gate-to-source threshold voltage	$V_{DS} = V_{GS}, I_{DS} = 250 \ \mu A$	1		2.1	0.75		1.15	V
Z _{DS(on)}	Drain-to-source on- impedance	$V_{IN} = 12 \text{ V}, V_{DD} = 5 \text{ V},$ $V_{OUT} = 1.3 \text{ V} I_{OUT} = 25 \text{ A},$ $f_{SW} = 500 \text{ kHz},$ $L_{OUT} = 0.3 \mu\text{H}$		3.7			0.7		mΩ
g _{fs}	Transconductance	$V_{DS} = 10 \text{ V}, I_{DS} = 20 \text{ A}$		113			169		S
DYNAMIC	CHARACTERISTICS	·							
C _{ISS}	Input capacitance ⁽¹⁾	V _{GS} = 0 V, V _{DS} = 12.5 V,		1590	2060		3910	5080	pF
Coss	Output capacitance ⁽¹⁾			840	1090		1970	2560	pF
C _{RSS}	Reverse transfer capacitance ⁽¹⁾	f = 1 MHz		42	54		53	69	pF
R_G	Series gate resistance ⁽¹⁾			1.2	2.5		1.1	2.2	Ω
Qg	Gate charge total (4.5 V) ⁽¹⁾			9.7	12.6		23	30	nC
Q_{gd}	Gate charge gate-to-drain	$V_{DS} = 12.5 \text{ V},$		2.3			3.6		nC
Q_{gs}	Gate charge gate-to-source	I _{DS} = 20 A		3.5			6.0		nC
$Q_{g(th)}$	Gate charge at Vth			1.9			3.5		nC
Q _{OSS}	Output charge	$V_{DS} = 12.5 \text{ V}, V_{GS} = 0 \text{ V}$		15.1			33		nC
t _{d(on)}	Turnon delay time			8.4			9.5		ns
t _r	Rise time	V _{DS} = 12.5 V, V _{GS} = 4.5 V,		20.4			14.8		ns
t _{d(off)}	Turnoff delay time	$I_{DS} = 20 \text{ A}, R_G = 2 \Omega$		14.5			29.3		ns
t _f	Fall time			4.3			6.6		ns
DIODE CI	HARACTERISTICS							•	
V _{SD}	Diode forward voltage	I _{DS} = 20 A, V _{GS} = 0 V		0.85	1		0.75	0.82	V
Q _{rr}	Reverse recovery charge	$V_{dd} = 12 \text{ V}, I_F = 20 \text{ A},$		27			50		nC
t _{rr}	Reverse recovery time	di/dt = 300 A/μs		22			34		ns

⁽¹⁾ Specified by design.





Max $R_{\theta JA} = 50^{\circ}\text{C/W}$ when mounted on 1 in² (6.45 cm²) of 2-oz (0.071-mm) thick Cu.

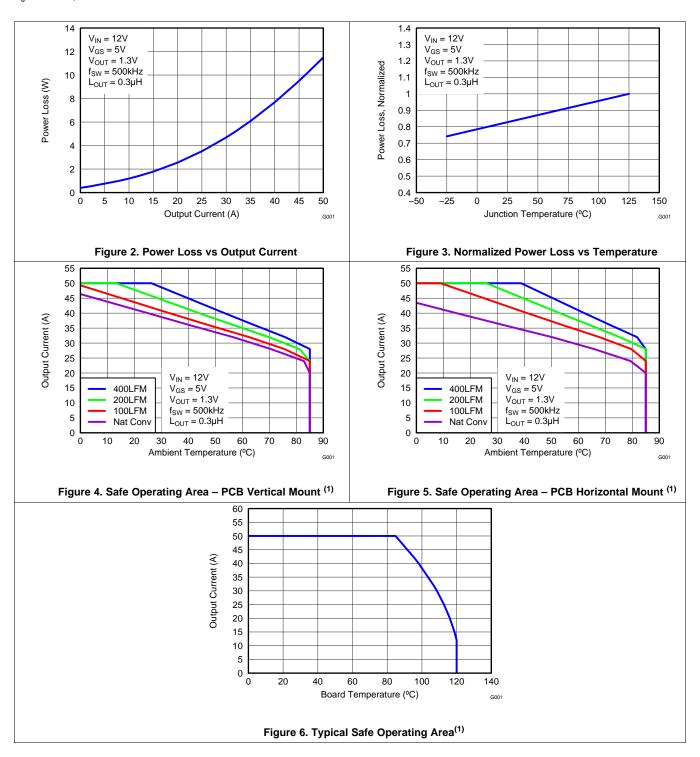


Max $R_{\theta JA} = 102^{\circ} C/W$ when mounted on minimum pad area of 2-oz (0.071-mm) thick Cu.



5.6 Typical Power Block Device Characteristics

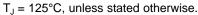
 $T_J = 125$ °C, unless stated otherwise.

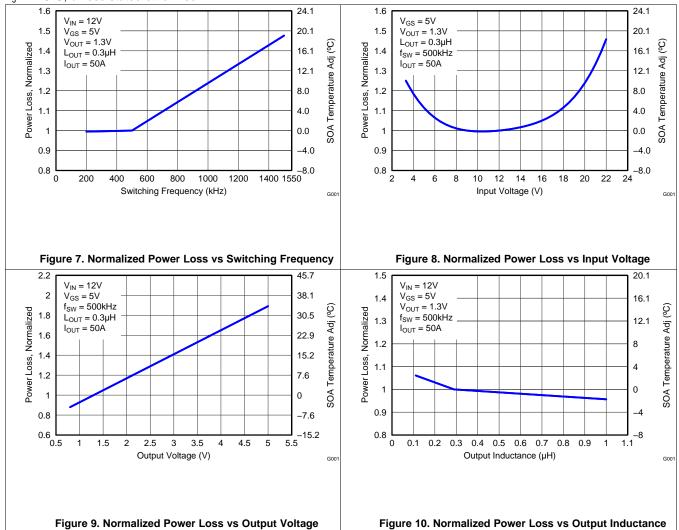


(1) The Typical Power Block System Characteristic curves are based on measurements made on a PCB design with dimensions of 4 in (W) × 3.5 in (L) × 0.062 in (H) and 6 copper layers of 1-oz copper thickness. See *Application and Implementation* section for detailed explanation.



Typical Power Block Device Characteristics (continued)

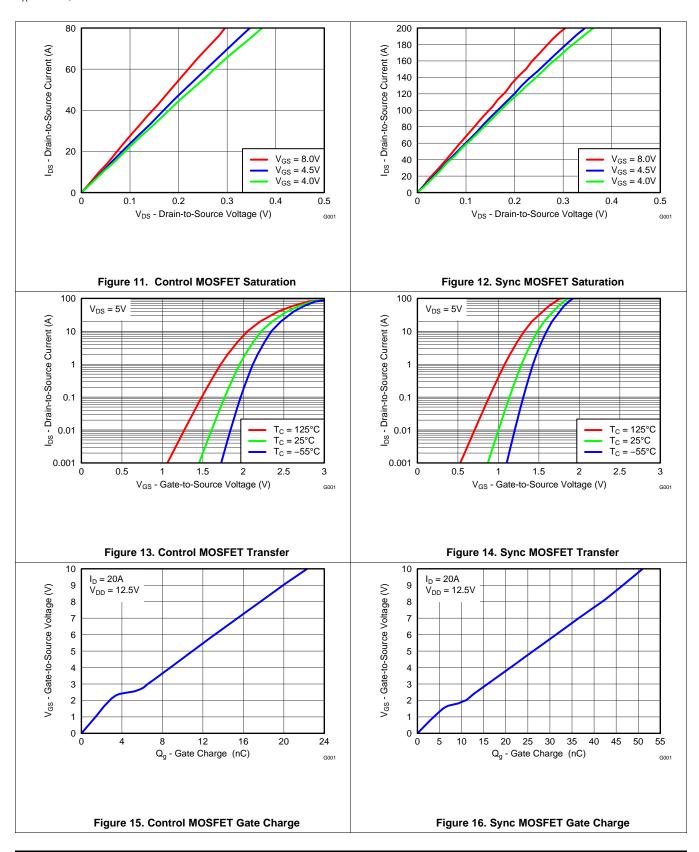






5.7 Typical Power Block MOSFET Characteristics

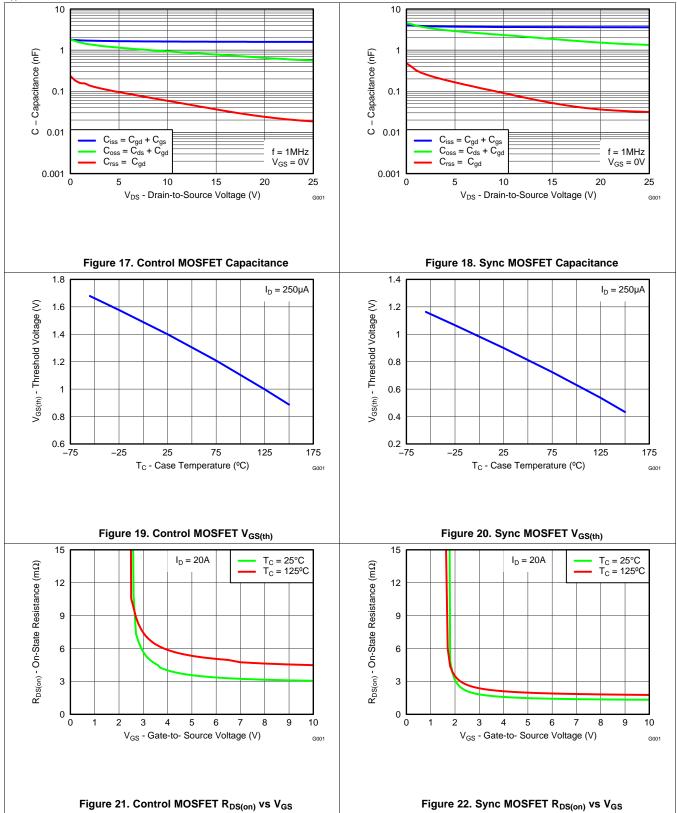
 $T_A = 25$ °C, unless stated otherwise.





Typical Power Block MOSFET Characteristics (continued)

 $T_A = 25$ °C, unless stated otherwise.



TEXAS INSTRUMENTS

Typical Power Block MOSFET Characteristics (continued)

Figure 27. Control MOSFET Unclamped Inductive Switching

 $T_A = 25$ °C, unless stated otherwise.

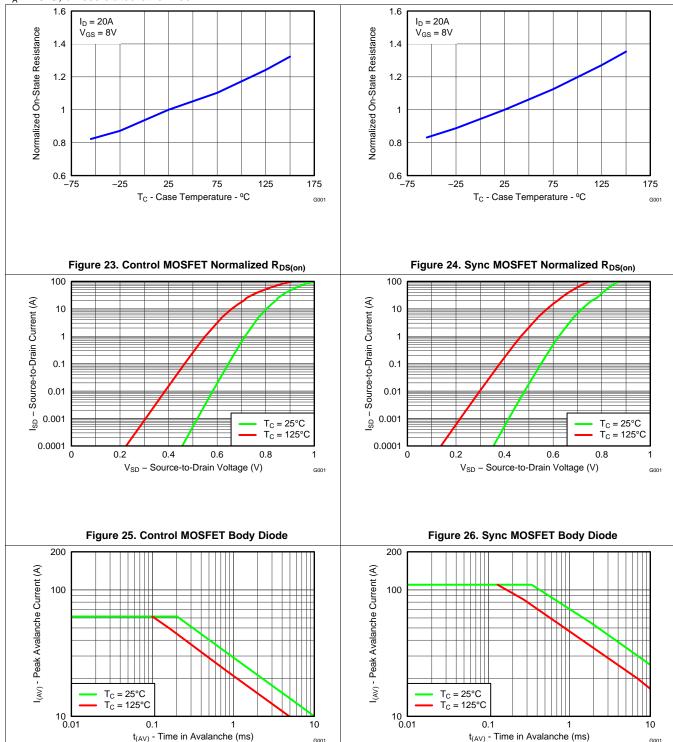


Figure 28. Sync MOSFET Unclamped Inductive Switching



6 Application and Implementation

NOTE

Information in the following Application section is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI customers are responsible for determining suitability of components selection for their designs. Customers should validate and test their design implementation to confirm system functionality.

6.1 Application Information

6.1.1 Equivalent System Performance

Many of today's high-performance computing systems require low-power consumption in an effort to reduce system operating temperatures and improve overall system efficiency. This has created a major emphasis on improving the conversion efficiency of today's synchronous buck topology. In particular, there has been an emphasis in improving the performance of the critical power semiconductor in the power stage of this application (see Figure 29). As such, optimization of the power semiconductors in these applications, needs to go beyond simply reducing R_{DS(ON)}.

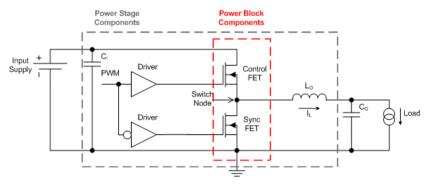


Figure 29. Equivalent System Schematic

The CSD86360Q5D is part of TI's power block product family, which is a highly optimized product for use in a synchronous buck topology requiring high current, high efficiency, and high frequency. It incorporates TI's latest generation silicon, which has been optimized for switching performance, as well as minimizing losses associated with $Q_{\rm GD}$, $Q_{\rm GS}$, and $Q_{\rm RR}$. Furthermore, TI's patented packaging technology has minimized losses by nearly eliminating parasitic elements between the control FET and sync FET connections (see Figure 30). A key challenge solved by TI's patented packaging technology is the system level impact of Common Source Inductance (CSI). CSI greatly impedes the switching characteristics of any MOSFET, which in turn increases switching losses and reduces system efficiency. As a result, the effects of CSI need to be considered during the MOSFET selection process. In addition, standard MOSFET switching loss equations used to predict system efficiency need to be modified in order to account for the effects of CSI. Further details behind the effects of CSI and modification of switching loss equations are outlined in *Power Loss Calculation With CSI Consideration for Synchronous Buck Converters* (SLPA009).



Application Information (continued)

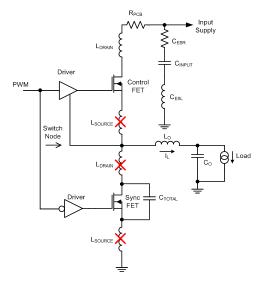
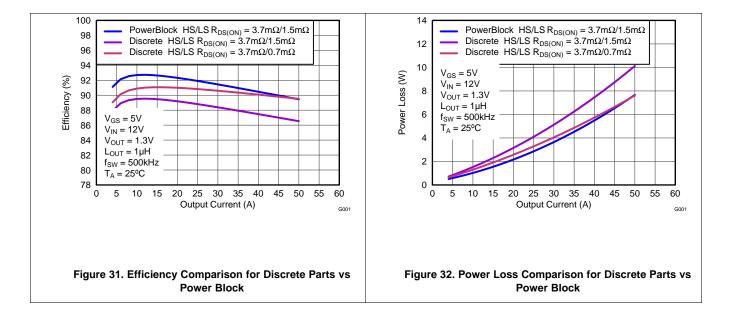


Figure 30. Elimination of Parasitic Inductances

The combination of Tl's latest generation silicon and optimized packaging technology has created a benchmarking solution that outperforms industry standard MOSFET chipsets of similar $R_{DS(ON)}$ and MOSFET chipsets with lower $R_{DS(ON)}$. Figure 31 and Figure 32 compare the efficiency and power loss performance of the CSD86360Q5D versus industry standard MOSFET chipsets commonly used in this type of application. This comparison purely focuses on the efficiency and generated loss of the power semiconductors only. The performance of CSD86360Q5D clearly highlights the importance of considering the effective AC on-impedance $(Z_{DS(ON)})$ during the MOSFET selection process of any new design. Simply normalizing to traditional MOSFET $R_{DS(ON)}$ specifications is not an indicator of the actual in-circuit performance when using Tl's power block technology.





Application Information (continued)

Table 1 below compares the traditional DC measured $R_{DS(ON)}$ of CSD86360Q5D versus its $Z_{DS(ON)}$. This comparison takes into account the improved efficiency associated with Tl's patented packaging technology. As such, when comparing Tl's power block products to individually packaged discrete MOSFETs or dual MOSFETs in a standard package, the in-circuit switching performance of the solution must be considered. In this example, individually packaged discrete MOSFETs or dual MOSFETs in a standard package would need to have DC measured $R_{DS(ON)}$ values that are equivalent to CSD86360Q5D's $Z_{DS(ON)}$ value in order to have the same efficiency performance at full load. Mid to light-load efficiency will still be lower with individually packaged discrete MOSFETs or dual MOSFETs in a standard package.

Table 1. Comparison of R_{DS(ON)} vs Z_{DS(ON)}

PARAMETER	н	ıs	LS		
PARAMETER	TYP	MAX	TYP	MAX	
Effective AC on-impedance Z _{DS(ON)} (V _{GS} = 5 V)	3.7	_	0.7	_	
DC measured R _{DS(ON)} (V _{GS} = 4.5 V)	3.7	4.5	1.5	1.9	

The CSD86360Q5D NexFET™ power block is an optimized design for synchronous buck applications using 5-V gate drive. The control FET and sync FET silicon are parametrically tuned to yield the lowest power loss and highest system efficiency. As a result, a new rating method is needed, which is tailored towards a more systemscentric environment. System-level performance curves such as power loss, Safe Operating Area (SOA), and normalized graphs allow engineers to predict the product performance in the actual application.

6.1.2 Power Loss Curves

MOSFET centric parameters such as $R_{DS(ON)}$ and Q_{gd} are needed to estimate the loss generated by the devices. In an effort to simplify the design process for engineers, Texas Instruments has provided measured power loss performance curves. Figure 2 plots the power loss of the CSD86360Q5D as a function of load current. This curve is measured by configuring and running the CSD86360Q5D as it would be in the final application (see Figure 33). The measured power loss is the CSD86360Q5D loss and consists of both input conversion loss and gate drive loss. Equation 1 is used to generate the power loss curve.

$$(V_{IN} \times I_{IN}) + (V_{DD} \times I_{DD}) - (V_{SW AVG} \times I_{OUT}) = Power loss$$
 (1)

The power loss curve in Figure 2 is measured at the maximum recommended junction temperatures of 125°C under isothermal test conditions.

6.1.3 Safe Operating Area (SOA) Curves

The SOA curves in the CSD86360Q5D data sheet provides guidance on the temperature boundaries within an operating system by incorporating the thermal resistance and system power loss. Figure 4 to Figure 6 outline the temperature and airflow conditions required for a given load current. The area under the curve dictates the safe operating area. All the curves are based on measurements made on a PCB design with dimensions of 4 in (W) \times 3.5 in (L) \times 0.062 in (T) and 6 copper layers of 1-oz copper thickness.

6.1.4 Normalized Curves

The normalized curves in the CSD86360Q5D data sheet provides guidance on the power loss and SOA adjustments based on their application specific needs. These curves show how the power loss and SOA boundaries will adjust for a given set of systems conditions. The primary Y-axis is the normalized change in power loss and the secondary Y-axis is the change is system temperature required in order to comply with the SOA curve. The change in power loss is a multiplier for the power loss curve and the change in temperature is subtracted from the SOA curve.



6.2 Typical Application

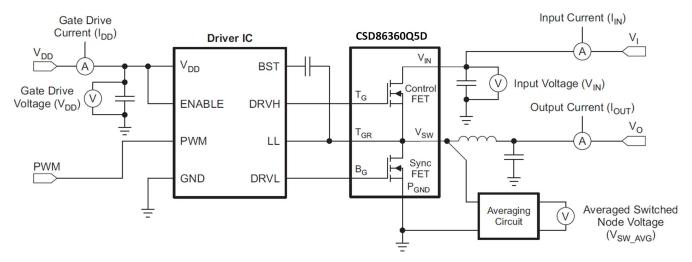


Figure 33. Typical Application



Typical Application (continued)

6.2.1 Design Example: Calculating Power Loss and SOA

The user can estimate product loss and SOA boundaries by arithmetic means (see *Operating Conditions* section). Though the power loss and SOA curves in this data sheet are taken for a specific set of test conditions, the following procedure will outline the steps the user should take to predict product performance for any set of system conditions.

6.2.1.1 Operating Conditions

- Output current = 25 A
- Input voltage = 7 V
- Output voltage = 1 V
- Switching frequency = 800 kHz
- Inductor = 0.2 μH

6.2.1.2 Calculating Power Loss

- Power loss at 25 A = 3.5 W (Figure 2)
- Normalized power loss for input voltage ≈ 1.03 (Figure 8)
- Normalized power loss for output voltage ≈ 0.90 (Figure 9)
- Normalized power loss for switching frequency ≈ 1.15 (Figure 7)
- Normalized power loss for output inductor ≈ 1.03 (Figure 10)
- Final calculated power loss = 3.5 W x 1.03 x 0.90 x 1.15 x 1.03 ≈ 3.84 W

6.2.1.3 Calculating SOA Adjustments

- SOA adjustment for input voltage ≈ 1.3°C (Figure 8)
- SOA adjustment for output voltage ≈ -2.5°C (Figure 9)
- SOA adjustment for switching frequency ≈ 6.0°C (Figure 7)
- SOA adjustment for output inductor ≈ 1.3°C (Figure 10)
- Final calculated SOA adjustment = 1.3 + (-2.5) + 6.0 + 1.3 ≈ 6.1°C

In the design example above, the estimated power loss of the CSD86360Q5D would increase to 3.84 W. In addition, the maximum allowable board and/or ambient temperature would have to decrease by 6.1°C. Figure 34 graphically shows how the SOA curve would be adjusted accordingly.

- 1. Start by drawing a horizontal line from the application current to the SOA curve.
- 2. Draw a vertical line from the SOA curve intercept down to the board/ambient temperature.
- 3. Adjust the SOA board/ambient temperature by subtracting the temperature adjustment value.

In the design example, the SOA temperature adjustment yields a reduction in allowable board/ambient temperature of 6.1°C. In the event the adjustment value is a negative number, subtracting the negative number would yield an increase in allowable board/ambient temperature.

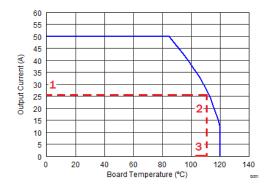


Figure 34. Power Block SOA



7 Layout

7.1 Layout Guidelines

There are two key system-level parameters that can be addressed with a proper PCB design: electrical and thermal performance. Properly optimizing the PCB layout will yield maximum performance in both areas. A brief description on how to address each parameter is provided.

7.1.1 Electrical Performance

The power block has the ability to switch voltages at rates greater than 10 kV/µs. Special care must be then taken with the PCB layout design and placement of the input capacitors, driver IC, and output inductor.

- The placement of the input capacitors relative to the power block's VIN and PGND pins should have the highest priority during the component placement routine. It is critical to minimize these node lengths. As such, ceramic input capacitors need to be placed as close as possible to the VIN and PGND pins (see Figure 35). The example in Figure 35 uses 6 x 10-µF ceramic capacitors (TDK Part # C3216X5R1C106KT or equivalent). Notice there are ceramic capacitors on both sides of the board with an appropriate amount of vias interconnecting both layers. In terms of priority of placement next to the power block, C5, C7, C19, and C8 should follow in order.
- The driver IC should be placed relatively close to the power block gate pins. T_G and B_G should connect to the
 outputs of the driver IC. The T_{GR} pin serves as the return path of the high-side gate drive circuitry and should
 be connected to the phase pin of the IC (sometimes called LX, LL, SW, PH, etc.). The bootstrap capacitor for
 the driver IC will also connect to this pin.
- The switching node of the output inductor should be placed relatively close to the power block VSW pins. Minimizing the node length between these two components will reduce the PCB conduction losses and actually reduce the switching noise level. In the event the switch node waveform exhibits ringing that reaches undesirable levels, the use of a boost resistor or RC snubber can be an effective way to easily reduce the peak ring level. The recommended boost resistor value will range between 1 Ω to 4.7 Ω depending on the output characteristics of driver IC used in conjunction with the power block. The RC snubber values can range from 0.5 Ω to 2.2 Ω for the R and 330 pF to 2200 pF for the C. Please refer to TI App Note *Snubber Circuits: Theory, Design and Application* (SLUP100) for more details on how to properly tune the RC snubber values. The RC snubber should be placed as close as possible to the VSW node and PGND see Figure 35 (1)

7.1.2 Thermal Performance

The power block has the ability to utilize the GND planes as the primary thermal path. As such, the use of thermal vias is an effective way to pull away heat from the device and into the system board. Concerns of solder voids and manufacturability problems can be addressed by the use of three basic tactics to minimize the amount of solder attach that will wick down the via barrel:

- Intentionally space out the vias from each other to avoid a cluster of holes in a given area.
- Use the smallest drill size allowed in your design. The example in Figure 35 uses vias with a 10-mil drill hole and a 16-mil capture pad.
- Tent the opposite side of the via with solder-mask.

In the end, the number and drill size of the thermal vias should align with the end user's PCB design rules and manufacturing capabilities.

Keong W. Kam, David Pommerenke, "EMI Analysis Methods for Synchronous Buck Converter EMI Root Cause Analysis", University of Missouri – Rolla



7.2 Layout Example

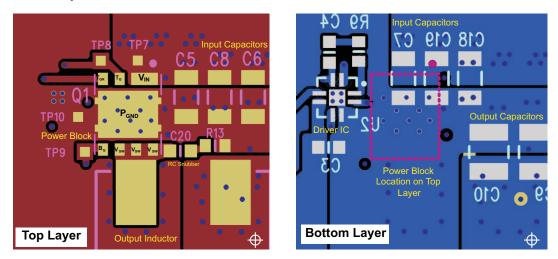


Figure 35. Recommended PCB Layout (Top Down View)



8 器件和文档支持

8.1 文档支持

8.1.1 相关文档

请参阅如下相关文档:

- 针对同步降压转换器的功率损耗计算(包含共源电感注意事项)(SLPA009)
- 阻尼器电路: 理论、设计和应用 (SLUP100)

8.2 接收文档更新通知

要接收文档更新通知,请导航至 Tl.com.cn 上的器件产品文件夹。单击右上角的通知我进行注册,即可每周接收产品信息更改摘要。有关更改的详细信息,请查看任何已修订文档中包含的修订历史记录。

8.3 社区资源

下列链接提供到 TI 社区资源的连接。链接的内容由各个分销商"按照原样"提供。这些内容并不构成 TI 技术规范,并且不一定反映 TI 的观点;请参阅 TI 的 《使用条款》。

TI E2E™ 在线社区 TI 的工程师对工程师 (E2E) 社区。此社区的创建目的在于促进工程师之间的协作。在 e2e.ti.com 中,您可以咨询问题、分享知识、拓展思路并与同行工程师一道帮助解决问题。

设计支持 TI 参考设计支持 可帮助您快速查找有帮助的 E2E 论坛、设计支持工具以及技术支持的联系信息。

8.4 商标

NexFET, E2E are trademarks of Texas Instruments. All other trademarks are the property of their respective owners.

8.5 静电放电警告



这些装置包含有限的内置 ESD 保护。 存储或装卸时,应将导线一起截短或将装置放置于导电泡棉中,以防止 MOS 门极遭受静电损伤。

8.6 术语表

SLYZ022 — TI 术语表。

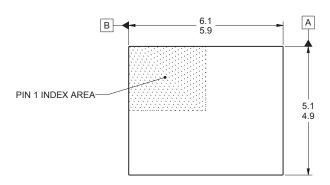
这份术语表列出并解释术语、缩写和定义。

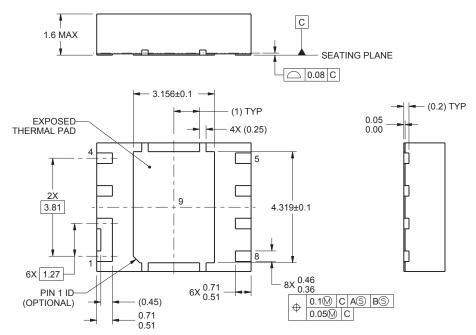


9 机械、封装和可订购信息

以下页面包含机械、封装和可订购信息。这些信息是指定器件的最新可用数据。数据如有变更,恕不另行通知,且不会对此文档进行修订。如需获取此数据表的浏览器版本,请参阅左侧的导航栏。

9.1 Q5D 封装尺寸





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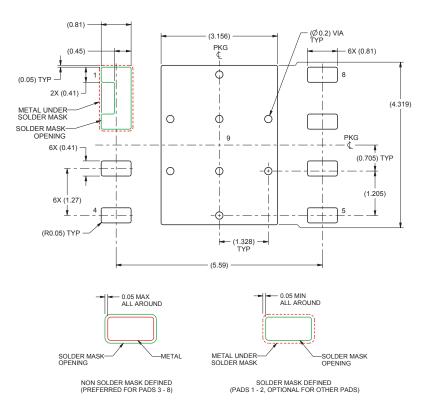
- 1. 所有线性尺寸的单位均为毫米。括号中的任何尺寸仅供参考。尺寸和公差值符合 ASME Y14.5M 标准。
- 2. 本图如有变更, 恕不另行通知。
- 3. 必须在印刷电路板上焊接封装散热焊盘,以获得良好的散热和机械性能。



Q5D 封装尺寸 (接下页)

DIM	毫米		英寸			
DIIVI	最小值	最大值	最小值	最大值		
a	1.40	1.5	0.055	0.059		
b	0.360	0.460	0.014	0.018		
С	0.150	0.250	0.006	0.010		
c1	0.150	0.250	0.006	0.010		
d	1.630	1.730	0.064	0.068		
d1	0.280	0.380	0.011	0.015		
d2	0.200	0.300	0.008	0.012		
d3	0.291	0.391	0.012	0.015		
D1	4.900	5.100	0.193	0.201		
D2	4.269	4.369	0.168	0.172		
Е	4.900	5.100	0.193	0.201		
E1	5.900	6.100	0.232	0.240		
E2	3.106	3.206	0.122	0.126		
е	1.27 典型值		0.050			
f	0.396	0.496	0.016	0.020		
L	0.510	0.710	0.020	0.028		
θ	0.00	_	_	_		
K	0.812		0.032			

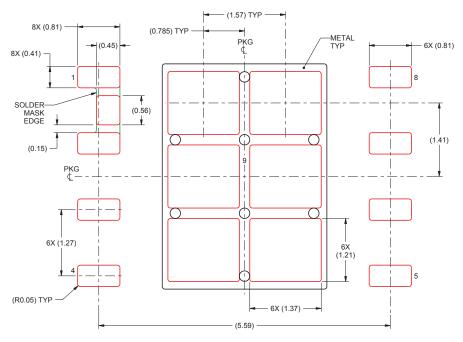
9.2 焊盘布局建议



- 1. 此封装设计用于焊接到电路板的散热焊盘上。有关更多信息,请参阅《QFN/SON PCB 连接》(SLUA271)。
- 2. 根据应用决定是否选用过孔,详情请参见器件数据表。如果实现了部分或全部过孔,则会显示建议的过孔位置。

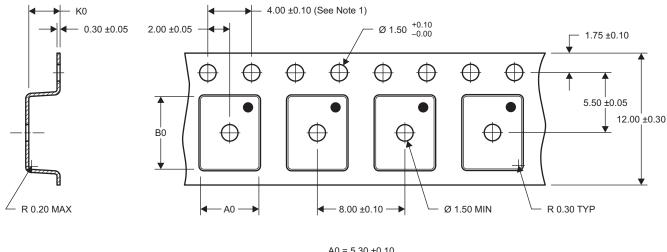


9.3 模版建议



1. 具有漏斗形壁和圆角的激光切割孔可提供更佳的锡膏脱离。IPC-7525 可能提供替代设计建议。要获得与 PCB 设计相关的建议电路布局,请参阅《通过 PCB 布局技巧来减少振铃》(SLPA005)。

9.4 Q5D 卷带信息



 $A0 = 5.30 \pm 0.10$ $B0 = 6.50 \pm 0.10$ $K0 = 1.90 \pm 0.10$

M0191-01

NOTES: 1.10 链轮孔距累积容差为 ±0.2

- 2. 每 100mm 长度的翘曲不能超过 1mm, 在 250mm 长度上不累积。
- 3. 材料: 黑色抗静电聚苯乙烯。
- 4. 全部尺寸单位为 mm,除非另外注明。
- 5. 厚度: 0.3 ± 0.05mm。
- 6. 符合 MSL1 260°C (红外和对流) PbF 回流焊要求。

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PACKAGING INFORMATION

Orderable part number	Status	Material type	Package Pins	Package qty Carrier	RoHS	Lead finish/	MSL rating/	Op temp (°C)	Part marking
	(1)	(2)			(3)	Ball material	Peak reflow		(6)
						(4)	(5)		
CSD86360Q5D	Active	Production	LSON-CLIP (DQY) 8	2500 LARGE T&R	ROHS Exempt	NIPDAU SN	Level-1-260C-UNLIM	-55 to 150	86360D
CSD86360Q5D.B	Active	Production	LSON-CLIP (DQY) 8	2500 LARGE T&R	ROHS Exempt	NIPDAU	Level-1-260C-UNLIM	-55 to 150	86360D
CSD86360Q5DG4	Active	Production	LSON-CLIP (DQY) 8	2500 LARGE T&R	ROHS Exempt	NIPDAU	Level-1-260C-UNLIM	-55 to 150	86360D
CSD86360Q5DG4.B	Active	Production	LSON-CLIP (DQY) 8	2500 LARGE T&R	ROHS Exempt	NIPDAU	Level-1-260C-UNLIM	-55 to 150	86360D

⁽¹⁾ Status: For more details on status, see our product life cycle.

Multiple part markings will be inside parentheses. Only one part marking contained in parentheses and separated by a "~" will appear on a part. If a line is indented then it is a continuation of the previous line and the two combined represent the entire part marking for that device.

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⁽²⁾ Material type: When designated, preproduction parts are prototypes/experimental devices, and are not yet approved or released for full production. Testing and final process, including without limitation quality assurance, reliability performance testing, and/or process qualification, may not yet be complete, and this item is subject to further changes or possible discontinuation. If available for ordering, purchases will be subject to an additional waiver at checkout, and are intended for early internal evaluation purposes only. These items are sold without warranties of any kind.

⁽³⁾ RoHS values: Yes, No, RoHS Exempt. See the TI RoHS Statement for additional information and value definition.

⁽⁴⁾ Lead finish/Ball material: Parts may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

⁽⁵⁾ MSL rating/Peak reflow: The moisture sensitivity level ratings and peak solder (reflow) temperatures. In the event that a part has multiple moisture sensitivity ratings, only the lowest level per JEDEC standards is shown. Refer to the shipping label for the actual reflow temperature that will be used to mount the part to the printed circuit board.

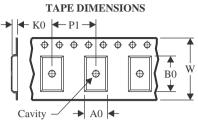
⁽⁶⁾ Part marking: There may be an additional marking, which relates to the logo, the lot trace code information, or the environmental category of the part.

PACKAGE MATERIALS INFORMATION

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TAPE AND REEL INFORMATION





A0	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

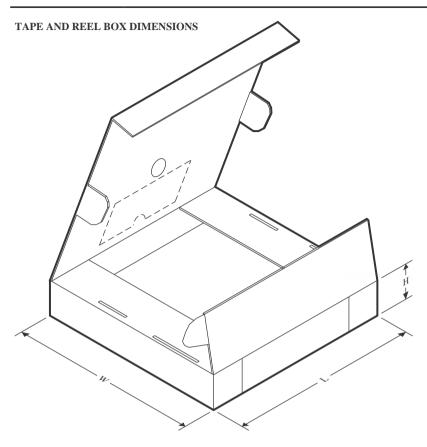


*All dimensions are nominal

Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	` ,	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
CSD86360Q5D	LSON- CLIP	DQY	8	2500	330.0	12.4	5.3	6.3	1.8	8.0	12.0	Q2
CSD86360Q5DG4	LSON- CLIP	DQY	8	2500	330.0	12.4	5.3	6.3	1.8	8.0	12.0	Q2

PACKAGE MATERIALS INFORMATION

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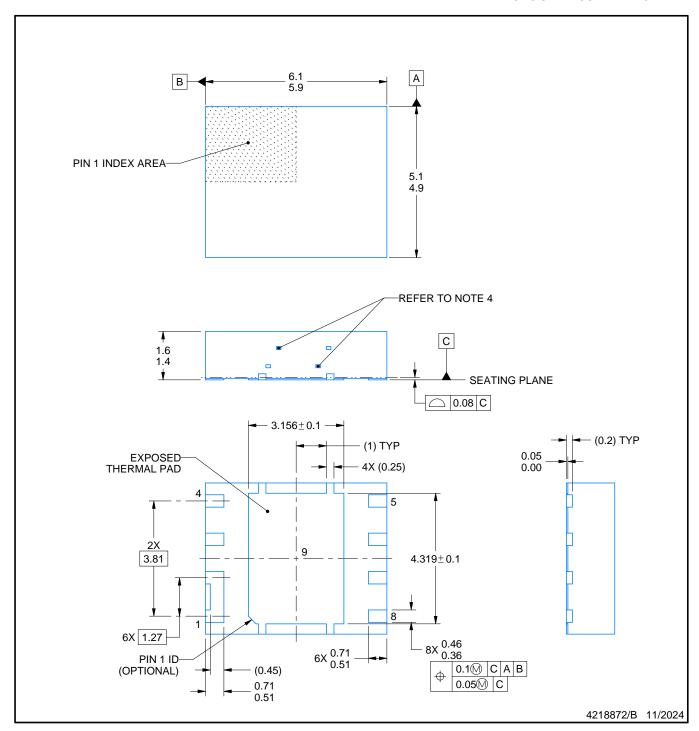


*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
CSD86360Q5D	LSON-CLIP	DQY	8	2500	346.0	346.0	33.0
CSD86360Q5DG4	LSON-CLIP	DQY	8	2500	346.0	346.0	33.0



PLASTIC SMALL OUTLINE - NO LEAD



NOTES:

- 1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.

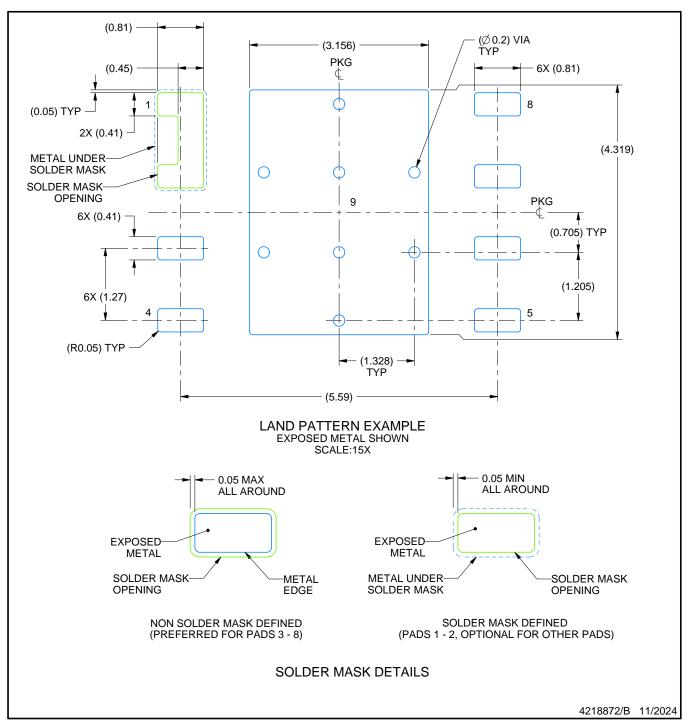
 2. This drawing is subject to change without notice.

 3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.

- 4. Exposed metals on side wall may vary or not visible



PLASTIC SMALL OUTLINE - NO LEAD

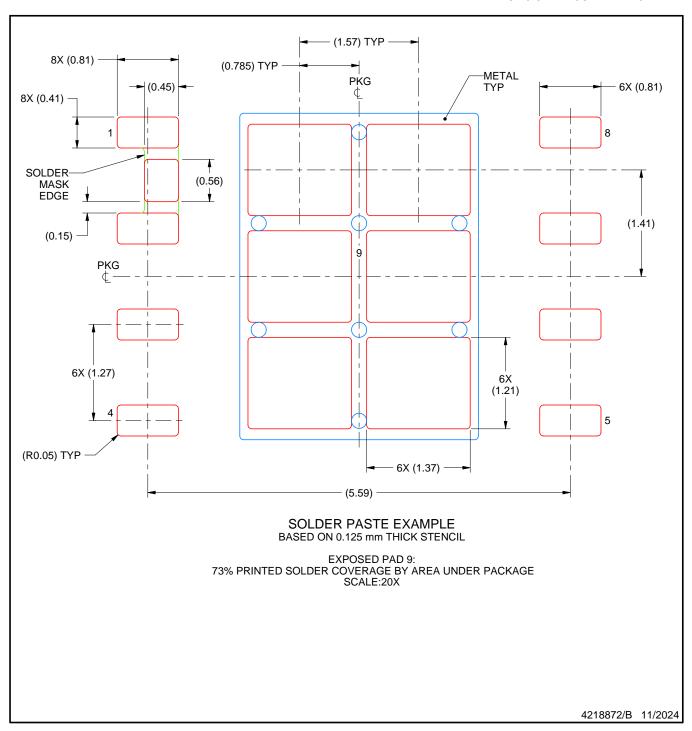


NOTES: (continued)

- 5. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).
- 6. Vias are optional depending on application, refer to device data sheet. If some or all are implemented, recommended via locations are shown.



PLASTIC SMALL OUTLINE - NO LEAD



NOTES: (continued)

7. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.



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